

**SEMI-WORKS MANUFACTURING PROCESS
EMISSIONS TEST REPORT
TEST DATES: 10-11 JANUARY 2019**

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FAYETTEVILLE, NORTH CAROLINA**

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1. INTRODUCTION

1.1 FACILITY AND BACKGROUND INFORMATION

The Chemours Fayetteville Works (Chemours) is located in Bladen County, North Carolina, approximately 10 miles south of the city of Fayetteville. The Chemours operating areas on the site include the Fluoromonomers, IXM and Polymers Processing Aid (PPA) manufacturing areas, Wastewater Treatment, and Powerhouse.

Chemours contracted Weston Solutions, Inc. (Weston) to perform HFPO Dimer Acid Fluoride, captured as HFPO Dimer Acid, emission testing on the Semi-Works stack. Testing was performed on 10-11 January 2019 and generally followed the “Emission Test Protocol” reviewed and approved by the North Carolina Department of Environmental Quality (NCDEQ). This report provides the results from the emission test program.

1.2 TEST OBJECTIVES

The specific objectives for this test program were as follows:

- Measure the emissions concentrations and mass emissions rates of HFPO Dimer Acid Fluoride from the Semi-Works stack.
- Monitor and record process data in conjunction with the test program.
- Provide representative emissions data.

1.3 TEST PROGRAM OVERVIEW

During the emissions test program, the concentrations and mass emissions rates of HFPO Dimer Acid Fluoride was measured on the Semi-Works stack.

Table 1-1 provides a summary of the test location and the parameters that were measured along with the sampling/analytical procedures that were followed.

Section 2 provides a summary of test results. A description of the processes is provided in Section 3. Section 4 provides a description of the test location. The sampling and analytical procedures are provided in Section 5. Detailed test results and discussion are provided in Section 6.

Appendix B includes the summary reports for the laboratory analytical results. The full laboratory data packages are provided in electronic format and on CD with each hard copy.

**Table 1-1
Sampling Plan for Semi-Works Stack**

Sampling Point & Location	Semi-Works Stack				
Number of Tests:	2				
Parameters To Be Tested:	HFPO Dimer Acid Fluoride (HFPO-DAF)	Volumetric Flow Rate and Gas Velocity	Carbon Dioxide	Oxygen	Water Content
Sampling or Monitoring Method	EPA M-0010	EPA M1, M2, M3A, and M4 in conjunction with M-0010 tests	EPA M3A		EPA M4 in conjunction with M-0010 tests
Sample Extraction/ Analysis Method(s):	LC/MS/MS	NA ⁶	NA		NA
Sample Size	> 1m ³	NA	NA	NA	NA
Total Number of Samples Collected ¹	2	2	2	2	2
Reagent Blanks (Solvents, Resins) ¹	1 set	0	0	0	0
Field Blank Trains ¹	1 per source	0	0	0	0
Proof Blanks ¹	1 per train	0	0	0	0
Trip Blanks ^{1,2}	1 set	0	0	0	
Lab Blanks	1 per fraction ³	0	0	0	0
Laboratory or Batch Control Spike Samples (LCS)	1 per fraction ³	0	0	0	0
Laboratory or Batch Control Spike Sample Duplicate (LCSD)	1 per fraction ³	0	0	0	0
Media Blanks	1 set ⁴	0	0	0	0
Isotope Dilution Internal Standard Spikes	Each sample	0	0	0	0
Total No. of Samples	6 ⁵	2	2	2	2

Key:

¹ Sample collected in field.

² Trip blanks include one XAD-2 resin module and one methanol sample per sample shipment.

³ Lab blank and LCS/LCSD includes one set per analytical fraction (front half, back half and condensate).

⁴ One set of media blank archived at laboratory at media preparation.

⁵ Actual number of samples collected in field.

⁶ Not applicable.

2. SUMMARY OF TEST RESULTS

A total of two tests were performed on the Semi-Works Stack. Table 2-1 provides a summary of the HFPO Dimer Acid emission test results. Detailed test results summaries are provided in Section 6.

It is important to note that emphasis is being placed on the characterization of the emissions based on the stack test results. Research conducted in developing the protocol for stack testing HFPO Dimer Acid Fluoride, HFPO Dimer Acid Ammonium Salt and HFPO Dimer Acid realized that the resulting testing, including collection of the air samples and extraction of the various fraction of the sampling train, would result in all three compounds being expressed as simply the HFPO Dimer Acid. However, it should be understood that the total HFPO Dimer Acid results provided on Table 2-1 and in this report include a percentage of each of the three compounds.

Table 2-1
Summary of HFPO Dimer Acid Test Results

Source	Run No.	Emission Rates	
		lb/hr	g/sec
Semi-Works	1	1.00E-03	1.26E-04
	2	6.19E-04	7.79E-05
	Average	8.10E-04	1.02E-04

3. PROCESS DESCRIPTIONS

The Semi-Works area is included in the scope of this test program.

3.1 SEMI-WORKS AREA

Semi-Works is generally a Research and Development facility. However, there are two products made in this unit on a periodic basis: Dimer Peroxide and a high Equivalent Weight (EW) polymer. The Dimer Peroxide is then used in the IXM Polymers manufacturing area and the high EW polymer is used in the IXM Products area to make a specific membrane product.

The following process streams vent to the Semi-Works building stack:

- Continuous Polymerization Process – when making high EW polymer
- Batch Polymerization – when making the Dimer Peroxide

3.2 PROCESS OPERATIONS AND PARAMETERS

Source	Operation/Product	Batch or Continuous
Semi-Works	Dimer Peroxide	Batch

There are no parameters to monitor from Semi-Works, as there is no control device associated with this stack.

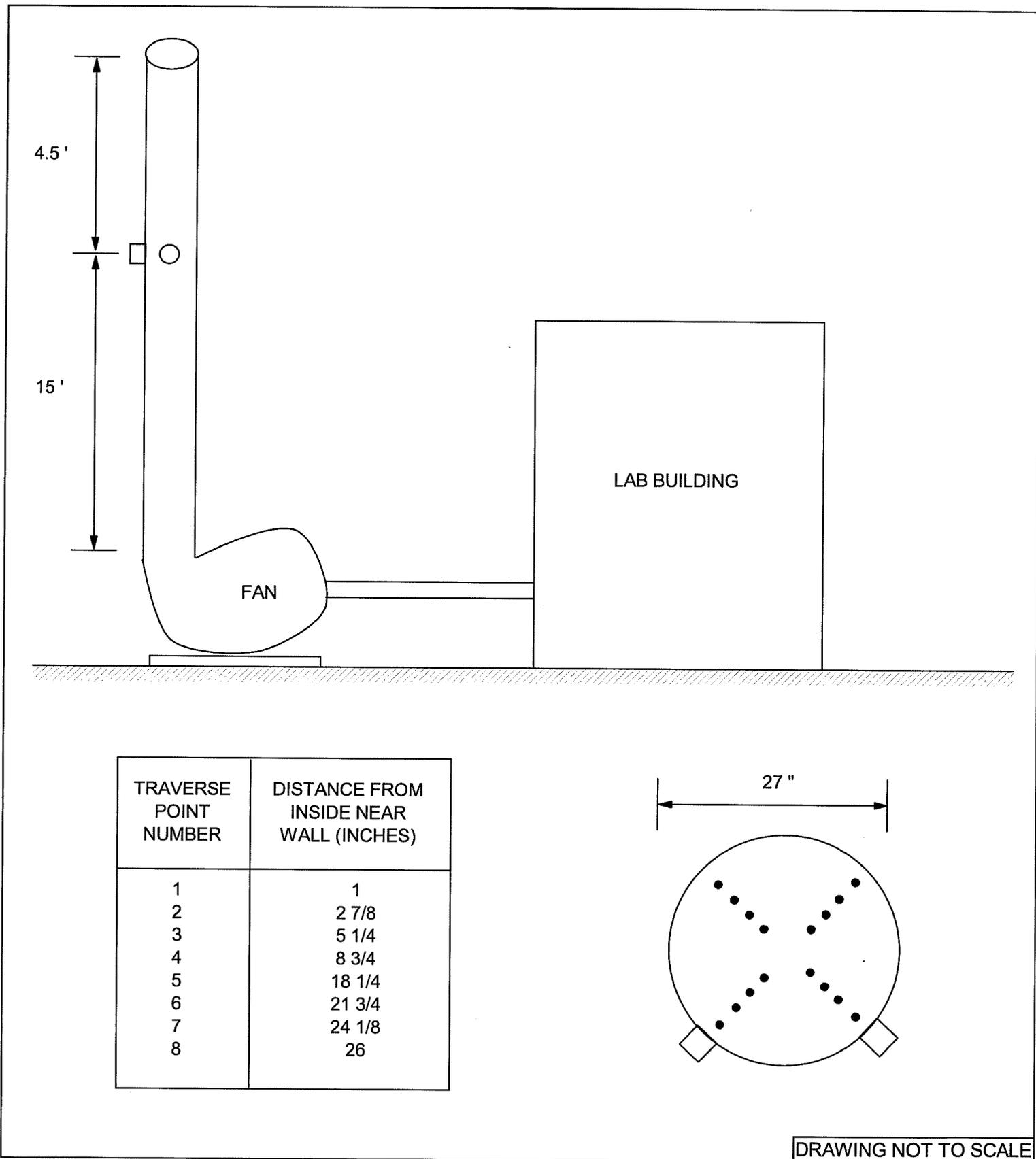
4. DESCRIPTION OF TEST LOCATIONS

4.1 SEMI-WORKS STACK

The Semi-Works stack is a circular steel stack outside the laboratory building. The ID fan is located at ground level. The stack ID is 27 inches. Two sample ports, 90° apart are installed 4.5 feet down from the top of the stack and 15 feet up from the ID fan discharge. Per EPA Method 1, sixteen traverse points, eight per port, were used for sampling.

Figure 4-1 provides a schematic of the test port and traverse point locations.

Note: All measurements at the test location were confirmed prior to sampling.



**FIGURE 4-1
SEMI-WORKS STACK
TEST PORT AND TRAVERSE POINT LOCATION**

5. SAMPLING AND ANALYTICAL METHODS

5.1 STACK GAS SAMPLING PROCEDURES

The purpose of this section is to describe the stack gas emissions sampling train and to provide details of the stack sampling and analytical procedures utilized during the emissions test program.

5.1.1 Pre-Test Determinations

Preliminary test data was obtained at the test location. Stack geometry measurements were measured and recorded, and traverse point distances verified. A preliminary velocity traverse was performed utilizing a calibrated S-type pitot tube and an inclined manometer to determine velocity profiles. Flue gas temperatures were observed with a calibrated direct readout panel meter equipped with a chromel-alumel thermocouple. Preliminary water vapor content was estimated by wet bulb/dry bulb temperature measurements.

A check for the presence or absence of cyclonic flow was previously conducted at the test location. The cyclonic flow check was negative ($< 20^\circ$) verifying that the source was acceptable for testing.

Preliminary test data was used for nozzle sizing and sampling rate determinations for isokinetic sampling procedures.

Calibration of probe nozzles, pitot tubes, metering systems, and temperature measurement devices was performed as specified in Section 5 of EPA Method 5 test procedures.

5.2 STACK PARAMETERS

5.2.1 EPA Method 0010

The sampling train utilized to perform the HFPO Dimer Acid sampling was an EPA Method 0010 train (see Figure 5-1). The Method 0010 consisted of a borosilicate nozzle that attached directly to a heated borosilicate probe. In order to minimize possible thermal degradation of the HFPO Dimer Acid, the probe and particulate filter were heated above stack temperature to minimize water vapor condensation before the filter. The probe was connected directly to a heated borosilicate filter holder containing a solvent extracted glass fiber filter.

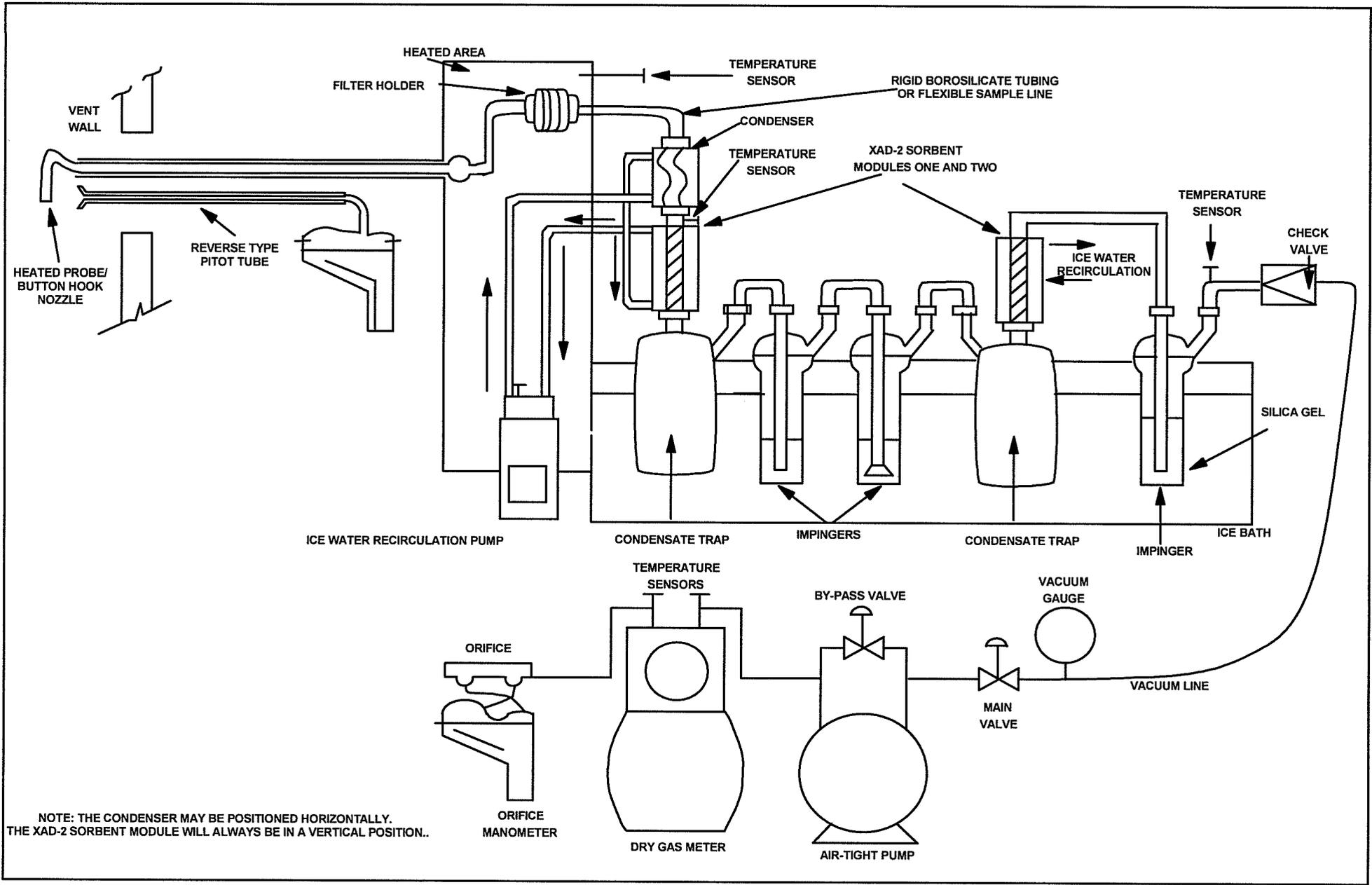


FIGURE 5-1
EPA METHOD 0010 SAMPLING TRAIN

A section of borosilicate glass or flexible polyethylene tubing connected the filter holder exit to a Graham (spiral) type ice water-cooled condenser, an ice water-jacketed sorbent module containing approximately 40 grams of XAD-2 resin. The XAD-2 resin tube was equipped with an inlet temperature sensor. The XAD-2 resin trap was followed by a condensate knockout impinger and a series of two impingers that each contained 100 milliliters of high purity distilled water. The train also included a second XAD-2 resin trap behind the impinger section to evaluate possible sampling train breakthrough. Each XAD-2 resin trap was connected to a 1-liter condensate knockout trap. The final impinger contained 300 grams of dry pre-weighed silica gel. All impingers and the condensate traps were maintained in an ice bath. Ice water was continuously circulated in the condenser and both XAD-2 modules to maintain method-required temperature. A control console with a leakless vacuum pump, a calibrated orifice, and dual inclined manometers was connected to the final impinger via an umbilical cord to complete the sample train.

HFPO Dimer Acid Fluoride (CAS No. 2062-98-8) that is present in the stack gas is expected to be captured in the sampling train along with HFPO Dimer Acid (CAS No. 13252-13-6). HFPO Dimer Acid Fluoride undergoes hydrolysis instantaneously in water in the sampling train and during the sample recovery step and will be converted to HFPO Dimer Acid such that the amount of HFPO Dimer Acid emissions represents a combination of both HFPO Dimer Acid Fluoride and HFPO Dimer Acid.

During sampling, gas stream velocities were measured by attaching a calibrated S-type pitot tube into the gas stream adjacent to the sampling nozzle. The velocity pressure differential was observed immediately after positioning the nozzle at each traverse point, and the sampling rate adjusted to maintain isokineticity at $100\% \pm 10$. Flue gas temperature was monitored at each point with a calibrated panel meter and thermocouple. Isokinetic test data was recorded at each traverse point during all test periods, as appropriate. Leak checks were performed on the sampling apparatus according to reference method instructions, prior to and following each run, component change (if required), or during midpoint port changes.

5.2.2 EPA Method 0010 Sample Recovery

At the conclusion of each test, the sampling train was dismantled, the openings sealed, and the components transported to the field laboratory trailer for recovery.

A consistent procedure was employed for sample recovery:

1. The two XAD-2 covered (to minimize light degradation) sorbent modules (1 and 2) were sealed and labeled.
2. The glass fiber filter(s) were removed from the holder with tweezers and placed in a polyethylene container along with any loose particulate and filter fragments.
3. The particulate adhering to the internal surfaces of the nozzle, probe and front half of the filter holder were rinsed with a solution of methanol and ammonium hydroxide into a polyethylene container while brushing a minimum of three times until no visible particulate remained. Particulate adhering to the brush was rinsed with methanol/ammonium hydroxide into the same container. The container was sealed.
4. The volume of liquid collected in the first condensate trap was measured, the value recorded, and the contents poured into a polyethylene container.
5. All train components between the filter exit and the first condensate trap were rinsed with methanol/ammonium hydroxide. The solvent rinse was placed in a separate polyethylene container and sealed.
6. The volume of liquid in impingers one and two, and the second condensate trap, were measured, the values recorded, and the sample was placed in the same container as Step 4 above, then sealed.
7. The two impingers, condensate trap, and connectors were rinsed with methanol/ammonium hydroxide. The solvent sample was placed in a separate polyethylene container and sealed.
8. The silica gel in the final impinger was weighed and the weight gain value recorded.
9. Site (reagent) blank samples of the methanol/ammonium hydroxide, XAD resin, filter and distilled water were retained for analysis.

Each container was labeled to clearly identify its contents. The height of the fluid level was marked on the container of each liquid sample to provide a reference point for a leakage check during transport. All samples were maintained cool.

During the test campaign, an M-0010 blank train was set up near the test location, leak checked and recovered along with the sample train. Following sample recovery, all samples were transported to TestAmerica Laboratories, Inc. (TestAmerica) for sample extraction and analysis.

See Figure 5-2 for a schematic of the M-0010 sample recovery process.

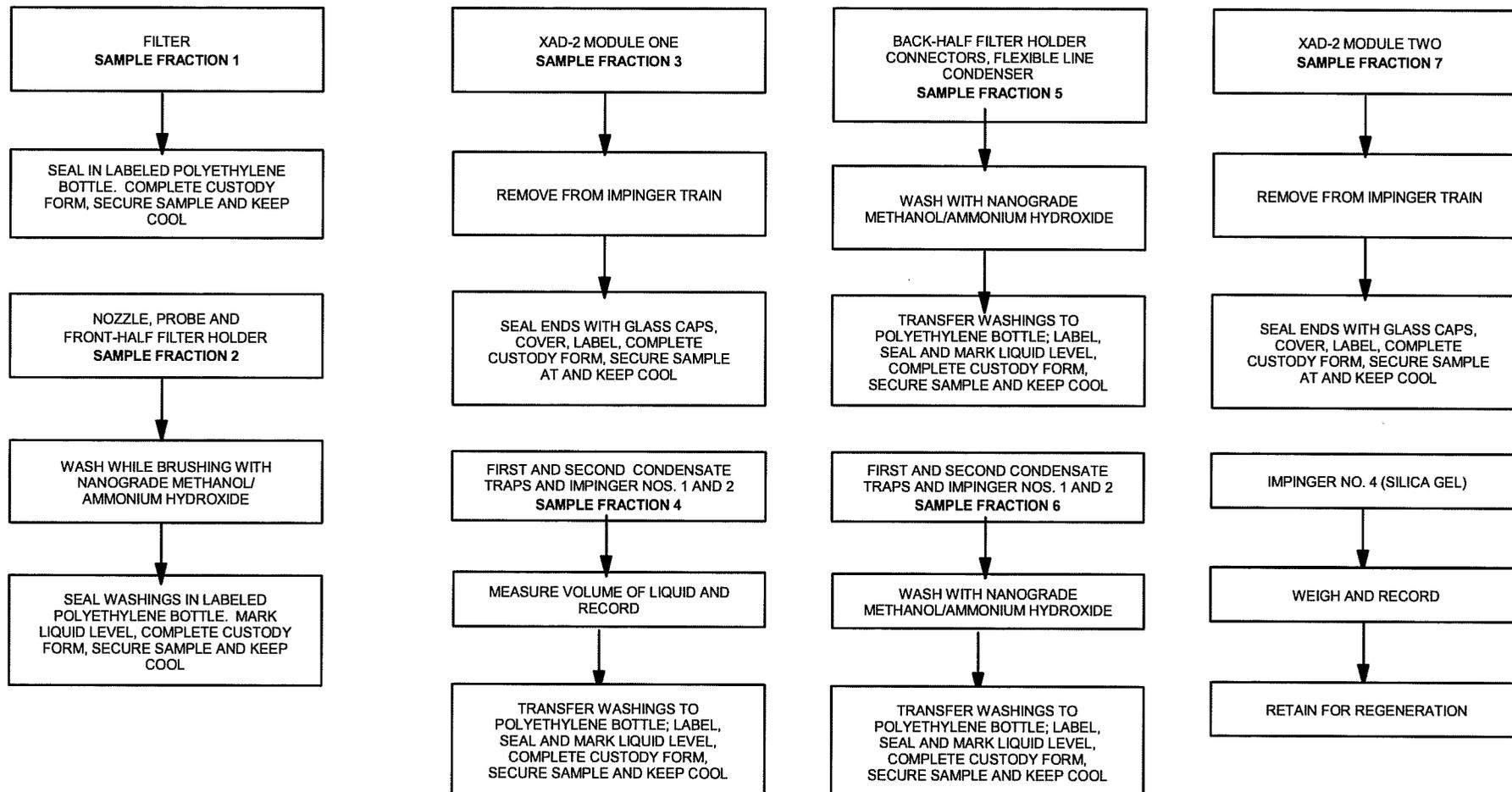


FIGURE 5-2
HFPO DIMER ACID SAMPLE RECOVERY PROCEDURES FOR METHOD 0010

5.2.3 EPA Method 0010 – Sample Analysis

The Method 0010 sampling trains resulted in four separate analytical fractions for HFPO Dimer Acid analysis according to SW-846 Method 3542:

- Front-Half Composite—comprised of the particulate filter, and the probe, nozzle, and front-half of the filter holder solvent rinses;
- Back-Half Composite—comprised of the first XAD-2 resin material and the back-half of the filter holder with connecting glassware solvent rinses;
- Condensate Composite—comprised of the aqueous condensates and the contents of impingers one and two with solvent rinses;
- Breakthrough XAD-2 Resin Tube—comprised of the resin tube behind the series of impingers.

The second XAD-2 resin material was analyzed separately to evaluate any possible sampling train HFPO-DA breakthrough.

The front-half and back-half composites and the second XAD-2 resin material were placed in polypropylene wide-mouth bottles and tumbled with methanol containing 5% NH₄OH for 18 hours. Portions of the extracts were processed analytically for the HFPO dimer acid by liquid chromatography and dual mass spectroscopy (HPLC/MS/MS). The condensate composite was concentrated onto a solid phase extraction (SPE) cartridge followed by desorption from the cartridge using methanol. Portions of those extracts were also processed analytically by HPLC/MS/MS.

Samples were spiked with isotope dilution internal standard (IDA) at the commencement of their preparation to provide accurate assessments of the analytical recoveries. Final data was corrected for IDA standard recoveries.

TestAmerica developed detailed procedures for the sample extraction and analysis for HFPO Dimer Acid. These procedures were incorporated into the test.

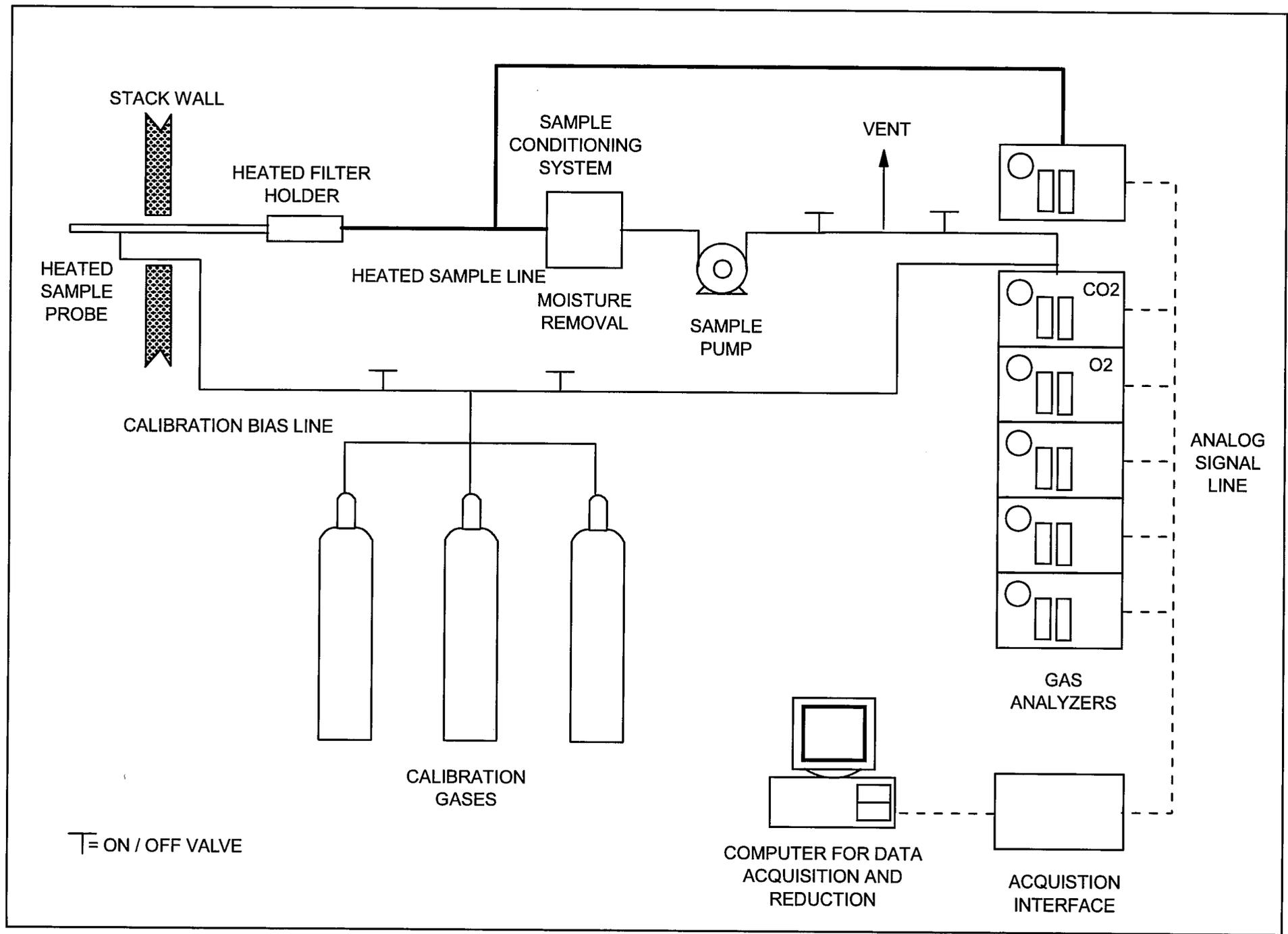
5.3 GAS COMPOSITION

The Weston mobile laboratory equipped with instrumental analyzers was used to measure carbon dioxide (CO₂) and oxygen (O₂) concentrations. A diagram of the Weston sampling system is presented in Figure 5-3.

Each analyzer was set up and calibrated internally by introduction of calibration gas standards directly to the analyzer from a calibration manifold. The calibration manifold is designed with an atmospheric vent to release excess calibration gas and maintains the calibration at ambient pressure. The direct calibration sequence consisted of alternate injections of zero and mid-range gases with appropriate adjustments until the desired responses were obtained. The high-range standards were then introduced in sequence without further adjustment.

The sample line integrity was verified by performing a bias test before and after each test period. The sampling system bias test consisted of introducing the zero gas and one up-range calibration standard in excess to the valve at the probe end when the system was sampling normally. The excess calibration gas flowed out through the probe to maintain ambient sampling system pressure. Calibration gas supply was regulated to maintain constant sampling rate and pressure. Instrument bias check response was compared to internal calibration responses to ensure sample line integrity and to calculate a bias correction factor after each run using the ratio of the measured concentration of the bias gas certified by the calibration gas supplier.

The oxygen and carbon dioxide content of each stack gas was measured according to EPA Method 3A procedures which incorporate the latest updates of EPA Method 7E. A Servomex Model 4900 analyzer (or equivalent) was used to measure oxygen content. A Servomex Model 4900 analyzer (or equivalent) was used to measure carbon dioxide content of the stack gas. Both analyzers were calibrated with EPA Protocol gases prior to the start of the test program and performance was verified by sample bias checks before and after each test run.



**FIGURE 5-3
WESTON SAMPLING SYSTEM**

6. DETAILED TEST RESULTS AND DISCUSSION

Preliminary testing and the associated analytical results required significant sample dilution to bring the HFPO Dimer Acid concentration within instrument calibration, therefore, sample times and sample volumes were reduced for the formal test program. This was approved by the North Carolina Department of Environmental Quality (NCDEQ).

Each test was 96 minutes in duration. A total of two tests were performed on the Semi-Works Stack.

Table 6-1 provides detailed test data and test results for the Semi-Works stack.

The Method 3A sampling on all sources indicated that the O₂ and CO₂ concentrations were at ambient air levels (20.9% O₂, 0% CO₂), therefore, 20.9% O₂ and 0% CO₂ values were used in all calculations.

TABLE 6-1
CHEMOURS - FAYETTEVILLE, NC
SUMMARY OF HFPO DIMER ACID TEST DATA AND TEST RESULTS

Test Data

	1	2
Run number		
Location	Semi-Works	Semi-Works
Date	1/10/2019	1/11/2019
Time period	1310-1458	0851-1049

SAMPLING DATA:

Sampling duration, min.	96.0	96.0
Nozzle diameter, in.	0.235	0.235
Cross sectional nozzle area, sq.ft.	0.000301	0.000301
Barometric pressure, in. Hg	29.93	30.24
Avg. orifice press. diff., in H ₂ O	1.37	1.34
Avg. dry gas meter temp., deg F	60.5	52.9
Avg. abs. dry gas meter temp., deg. R	521	513
Total liquid collected by train, ml	36.8	25.8
Std. vol. of H ₂ O vapor coll., cu.ft.	1.7	1.2
Dry gas meter calibration factor	0.9915	0.9915
Sample vol. at meter cond., dcf	61.011	58.493
Sample vol. at std. cond., dscf ⁽¹⁾	61.563	60.510
Percent of isokinetic sampling	104.4	100.9

GAS STREAM COMPOSITION DATA:

CO ₂ , % by volume, dry basis	0.0	0.0
O ₂ , % by volume, dry basis	20.9	20.9
N ₂ , % by volume, dry basis	79.1	79.1
Molecular wt. of dry gas, lb/lb mole	28.84	28.84
H ₂ O vapor in gas stream, prop. by vol.	0.027	0.020
Mole fraction of dry gas	0.973	0.980
Molecular wt. of wet gas, lb/lb mole	28.54	28.62

GAS STREAM VELOCITY AND VOLUMETRIC FLOW DATA:

Static pressure, in. H ₂ O	-0.21	-0.22
Absolute pressure, in. Hg	29.91	30.22
Avg. temperature, deg. F	61	54
Avg. absolute temperature, deg.R	521	514
Pitot tube coefficient	0.84	0.84
Total number of traverse points	16	16
Avg. gas stream velocity, ft./sec.	34.5	34.0
Stack/duct cross sectional area, sq.ft.	3.98	3.98
Avg. gas stream volumetric flow, wacf/min.	8229	8117
Avg. gas stream volumetric flow, dscf/min.	8108	8252

⁽¹⁾ Standard conditions = 68 deg. F. (20 deg. C.) and 29.92 in Hg (760 mm Hg)

**TABLE 6-1(cont.)
CHEMOURS - FAYETTEVILLE, NC
SUMMARY OF HFPO DIMER ACID TEST DATA AND TEST RESULTS**

TEST DATA

	1	2
Run number	Semi-Works	Semi-Works
Location	Semi-Works	Semi-Works
Date	1/10/2019	1/11/2019
Time period	1310-1458	0851-1049

LABORATORY REPORT DATA, ug.

HFPO Dimer Acid	57.6084	34.2887
-----------------	---------	---------

EMISSION RESULTS, ug/dscm.

HFPO Dimer Acid	33.0	20.0
-----------------	------	------

EMISSION RESULTS, lb/dscf.

HFPO Dimer Acid	2.06E-09	1.25E-09
-----------------	----------	----------

EMISSION RESULTS, lb/hr.

HFPO Dimer Acid	1.00E-03	6.19E-04
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EMISSION RESULTS, g/sec.

HFPO Dimer Acid	1.26E-04	7.79E-05
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APPENDIX A
RAW AND REDUCED TEST DATA

**CHEMOURS - FAYETTEVILLE, NC
INPUTS FOR HFPO DIMER ACID CALCULATIONS**

Test Data

Run number	1	2
Location	Semi-Works	Semi-Works
Date	1/10/2019	1/11/2019
Time period	1310-1458	0851-1049
Operator	JM	JM

Inputs For Calcs.

Sq. rt. delta P	0.61496	0.61461
Delta H	1.3744	1.3428
Stack temp. (deg.F)	60.9	54.1
Meter temp. (deg.F)	60.5	52.9
Sample volume (act.)	61.011	58.493
Barometric press. (in.Hg)	29.93	30.24
Volume H ₂ O imp. (ml)	20.4	11.0
Weight change sil. gel (g)	16.4	14.8
% CO ₂	0.0	0.0
% O ₂	20.9	20.9
% N ₂	79.1	79.1
Area of stack (sq.ft.)	3.976	3.976
Sample time (min.)	96.0	96.0
Static pressure (in.H ₂ O)	-0.21	-0.22
Nozzle dia. (in.)	0.235	0.235
Meter box cal.	0.9915	0.9915
Cp of pitot tube	0.84	0.84
Traverse points	16	16

Sample and Velocity Traverse Point Data Sheet - Method 1

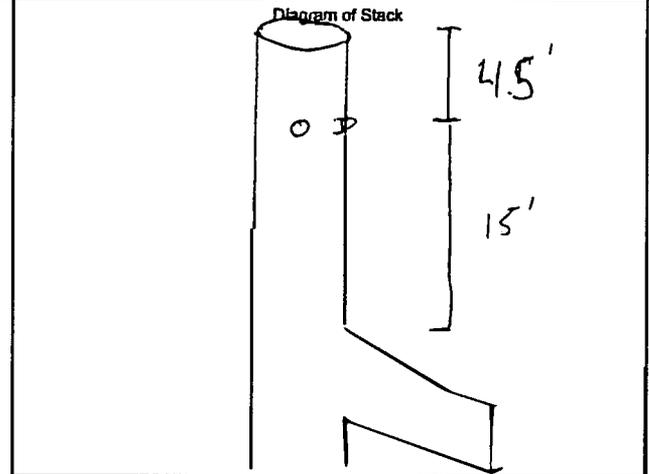
Client Chemours
 Location/Plant Fayetteville
 Source SEMI WORKS

Operator SR
 Date 3/22/18
 W.O. Number _____

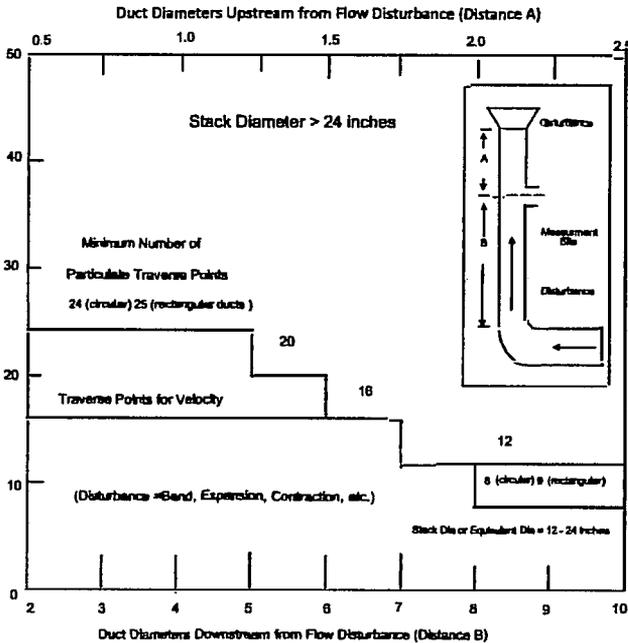
Duct Type	<input type="checkbox"/> Circular	<input type="checkbox"/> Rectangular Duct	Indicate appropriate type
Traverse Type	<input type="checkbox"/> Particulate Traverse	<input type="checkbox"/> Velocity Traverse	<input type="checkbox"/> CEM Traverse

Distance from far wall to outside of port (in.) = C	45
Port Depth (in.) = D	18
Depth of Duct, diameter (in.) = C-D	27
Area of Duct (ft ²)	3.98
Total Traverse Points	16
Total Traverse Points per Port	8
Port Diameter (in.) —(Flange-Threaded-Hole)	
Monorail Length	
Rectangular Ducts Only	
Width of Duct, rectangular duct only (in.)	
Total Ports (rectangular duct only)	
Equivalent Diameter = (2*L*W)/(L+W)	

Flow Disturbances	
Upstream - A (ft)	4.5
Downstream - B (ft)	15
Upstream - A (duct diameters)	2
Downstream - B (duct diameters)	6.5



Traverse Point Locations			
Traverse Point	% of Duct	Distance from Inside Duct Wall (in)	Distance from Outside of Port (in)
1	3.2	1	19
2	10.5	2 7/8	20 7/8
3	19.4	5 1/4	23 1/4
4	32.3	8 3/4	26 3/4
5	47.7	13 1/4	31 1/4
6	60.6	21 3/4	39 3/4
7	89.5	24 1/8	42 1/8
8	96.8	26	44
9			
10			
11			
12			



CEM 3 Point (Long Measurement Line) Stratification Point Locations			
1	0.167		
2	0.50		
3	0.833		

Note: If stack dia < 12 inch use EPA Method 1A (Sample port upstream of pitot port)
 Note: If stack dia > 24" then adjust traverse point to 1 inch from wall
 If stack dia < 24" then adjust traverse point to 0.5 inch from wall

Traverse Point Location Percent of Stack -Circular													
		Number of Traverse Points											
		1	2	3	4	5	6	7	8	9	10	11	12
Circular	1	14.6											
	2	85.4	25										
	3		75	29.6									
	4			93.3	70.4								
	5				85.4	67.7							
	6					95.6	80.6						
	7						89.5	77.4					
	8							96.8	85.4				
	9								91.8	82.3			
	10									97.4	88.2		
	11										93.3		
	12											97.9	

Traverse Point Location Percent of Stack -Rectangular													
		Number of Traverse Points											
		1	2	3	4	5	6	7	8	9	10	11	12
Rectangular	1	25.0	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2	
	2	75.0	50.0	37.5	30.0	25.0	21.4	18.8	16.7	15.0	13.6	12.5	
	3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8	
	4			87.5	70.0	58.3	50.0	43.8	38.9	35.0	31.8	29.2	
	5				90.0	75.0	64.3	56.3	50.0	45.0	40.9	37.5	
	6					91.7	78.6	68.8	61.1	55.0	50.0	45.8	
	7						92.9	81.3	72.2	65.0	59.1	54.2	
	8							93.8	83.3	75.0	68.2	62.5	
	9								94.4	85.0	77.3	70.8	
	10									95.0	86.4	79.2	
	11										95.5	87.5	
	12											95.8	

7 ft monorail for split train



ISOKINETIC FIELD DATA SHEET

Method 0010 HFPO Dimer Acid

Client: Chemours
 W.O.#: 15418.002.009.0001
 Project ID: Chemours
 Mode/Source ID: Semi Division: water
 Smp. Loc. ID: STK
 Run No. ID: 1
 Test Method ID: M 0010 HFPO Dimer Acid
 Date ID: 9JAN2019
 Source/Location: Semi Division: Stack
 Sample Date: 01/10/19
 Baro. Press (in Hg): 29.93
 Operator: MILLS

Stack Conditions	
Assumed	Actual
1.5	20.4
	16.4
0	0.0
20.9	20.9
65	
65	
-0.2	-0.2

Meter Box ID: INC21
 Meter Box Y: 0.995
 Meter Box Del H: 2.0889
 Probe ID / Length: 5
 Probe Material: Boro
 Pitot / Thermocouple ID: P704
 Pitot Coefficient: 0.84
 Nozzle ID:
 Avg Nozzle Dia (in): 0.235
 Area of Stack (ft²): 3.976
 Sample Time: 96
 Total Traverse Pts: 16

K Factor <u>3.58</u>		
Initial	Mid-Point	Final
0.008	0.010	0.002
15	11	8
yes / no	yes / no	yes / no
yes / no	yes / no	yes / no
Pre-Test Set		Post-Test Set
48		43
50		45
Pass / Fail		Pass / Fail
yes / no		yes / no

Leak Checks
 Sample Train (ft³): 5
 Leak Check @ (in Hg): NA
 Pitot good: NA
 Orsat good: NA
 Temp Check
 Meter Box Temp: 48
 Reference Temp: 50
 Pass/Fail (+/- 2°): Pass / Fail
 Temp Change Response: yes / no

TRAVERSE POINT NO.	SAMPLE TIME (min)	CLOCK TIME (plant time)	VELOCITY PRESSURE Delta P (in H2O)	ORIFICE PRESSURE Delta H (in H2O)	DRY GAS METER READING (ft ³)	STACK TEMP (°F)	DGM INLET TEMP (°F)	DGM OUTLET TEMP (°F)	PROBE TEMP (°F)	FILTER BOX TEMP (F)	IMPINGER EXIT TEMP (°F)	SAMPLE TRAIN VAC (in Hg)	COMMENTS
X1	0	17:10			436.682								
1	3		0.46	1.65	438.9	62	39	62	99	105	42	5	
1	6		0.46	1.65	440.8	63	37	62	99	108	41	5	
2	9		0.46	1.65	442.9	62	37	62	99	106	41	5	
2	12		0.46	1.65	445.1	63	37	62	100	107	42	5	
3	15		0.44	1.57	447.4	62	38	62	98	104	42	5	
3	18		0.44	1.57	449.3	61	39	60	99	107	42	5	
4	21		0.44	1.57	451.1	59	40	62	97	106	43	5	
4	24		0.43	1.54	453.3	61	41	62	98	108	42	5	
5	27		0.40	1.43	455.2	61	41	64	98	104	41	4.5	29.653
5	30		0.40	1.43	457.2	62	41	64	98	104	41	4.5	
6	33		0.33	1.18	459.0	62	42	64	98	109	43	4	
6	36		0.32	1.14	460.6	61	42	64	100	104	41	4	
7	39		0.22	0.79	462.2	60	42	64	99	103	42	3	
7	42		0.23	0.82	463.7	59	41	64	100	111	43	3	
8	45		0.20	0.72	465.2	57	42	63	100	106	43	3	
8	48	13:50	0.18	0.64	466.335	57	41	63	99	105	44	3	

Avg Sqrt Delta P	Avg Delta H	Total Volume	Avg Ts	Avg Tm	Min/Max	Min/Max	Max Temp	Max Vac	Max Temp
	Avg Sqrt Del H	Comments:							



amad

ISOKINETIC FIELD DATA SHEET

Method 0010 HFPO Dimer Acid

Client Chemours Operator Mills
 Source Semiworks Division Division Run No. 1
 Sample Loc. Stack Date 01/10/19

K Factor 3.58

TRAVERSE POINT NO.	SAMPLE TIME (min)	CLOCK TIME (plant time)	VELOCITY PRESSURE Delta P (in H2O)	ORIFICE PRESSURE Delta H (in H2O)	DRY GAS METER READING (ft ³)	STACK TEMP (°F)	DGM INLET TEMP (°F)	DGM OUTLET TEMP (°F)	PROBE TEMP (°F)	FILTER BOX TEMP (F)	IMPING EXIT TEMP (°F)	SAMPLE TRAIN VAC (in Hg)	COMMENTS
	0	1410			466.430								
1	3		0.48	1.72	469.0	62	43	61	99	101	44	5	
1	6		0.49	1.75	471.1	62	40	61	98	109	46	5	
2	9		0.47	1.68	473.2	62	41	61	99	102	43	5	
2	12		0.46	1.65	475.2	63	40	62	99	104	41	5	
3	15		0.45	1.61	477.1	63	40	61	100	104	42	5	
3	18		0.45	1.61	479.5	63	42	60	100	107	40	5	
4	21		0.43	1.54	481.6	63	41	59	99	107	41	5	
4	24		0.43	1.54	483.6	63	42	58	99	107	41	5	31.358
5	27		0.41	1.47	485.5	62	41	58	99	108	41	4.5	
5	30		0.40	1.43	487.4	62	41	58	99	106	42	4.5	
6	33		0.38	1.36	489.2	61	41	57	99	107	42	4	
6	36		0.38	1.36	491.0	61	41	57	99	107	41	4	
7	39	0.33	0.25	1.18	493.0	59	41	56	99	107	41	4	
7	42		0.32	1.14	494.7	57	41	55	99	110	41	4	
8	45		0.27	0.97	496.1	57	41	55	99	104	41	3.5	
8	48	1458	0.27	0.97	497.788	57	40	52.1	98	107	41	3.5	

Avg Sqrt Delta P 0.61495 ✓
 Avg Delta H 1.37438 ✓
 Total Volume 61.011 ✓
 Avg Ts 60.9 ✓
 Max Avg Tm 43.60 / 60.5 ✓
 Min/Max 98 / 100
 Min/Max 102 / 111
 Max Temp 46
 Max Vac 5
 Max Temp

Comments:
 Avg ΔP = 0.38406 ✓



X-
MR.

amd

ISOKINETIC FIELD DATA SHEET

Method 0010 HFPO Dimer Acid

Client: Chemours
 W.O.#: 15418.002.009.0001
 Project ID: Chemours % Moisture
 Mode/Source ID: Semi Division Waste Impinger Vol (ml)
 Samp. Loc. ID: STK Silica gel (g)
 Run No. ID: 2 CO2, % by Vol
 Test Method ID: M 0010 HFPO Dimer Acid O2, % by Vol
 Date ID: 9JAN2019 Temperature (°F)
 Source/Location: Semi Division Stack Meter Temp (°F)
 Sample Date: 1/11/19 ✓ Static Press (in H₂O)
 Baro. Press (in Hg): 30.24 ✓
 Operator: MILLS Ambient Temp (°F)

Stack Conditions

Assumed	Actual
<u>2</u>	<u>11</u>
<u>0</u>	<u>0.0</u>
<u>20.9</u>	<u>19.9</u>
<u>55</u>	
<u>50</u>	
<u>-0.2</u>	<u>-0.22</u>

Meter Box ID: WC21
 Meter Box Y: 0.9915 ✓
 Meter Box Del H: 2.0089
 Probe ID / Length: Boro
 Probe Material: P704
 Pitot / Thermocouple ID: 0.84
 Pitot Coefficient: 0.235 ✓
 Nozzle ID: 3.976 ✓
 Avg Nozzle Dia (in): 96 ✓
 Area of Stack (ft²): 16 ✓
 Sample Time:
 Total Traverse Pts:

K Factor 3.5

Initial	Mid-Point	Final
<u>0.012</u>	<u>0.014</u>	<u>0.006</u>
<u>15</u>	<u>12</u>	<u>8</u>
<u>yes / no</u>	<u>yes / no</u>	<u>yes / no</u>
<u>yes / no</u>	<u>yes / no</u>	<u>yes / no</u>

Leak Checks
 Sample Train (ft³):
 Leak Check @ (in Hg):
 Pitot good: NA
 Orsat good: NA

Pre-Test Set	Post-Test Set
<u>32</u>	<u>41</u>
<u>32</u>	<u>42</u>
<u>Pass / Fail</u>	<u>Pass / Fail</u>
<u>yes / no</u>	<u>yes / no</u>

Temp Check
 Meter Box Temp:
 Reference Temp:
 Pass/Fail (+/- 2°):
 Temp Change Response:

TRAVERSE POINT NO.	SAMPLE TIME (min)	CLOCK TIME (plant time)	VELOCITY PRESSURE Delta P (in H ₂ O)	ORIFICE PRESSURE Delta H (in H ₂ O)	DRY GAS METER READING (ft ³)	STACK TEMP (°F)	XAD INLET TEMP (°F)	DGM OUTLET TEMP (°F)	PROBE TEMP (°F)	FILTER BOX TEMP (F)	IMPING EXIT TEMP (°F)	SAMPLE TRAIN VAC (in Hg)	COMMENTS
	<u>0</u>	<u>0851</u>			<u>498.302</u>								
<u>1</u>	<u>3</u>		<u>0.47</u>	<u>1.68</u>	<u>502.7</u>	<u>52</u>	<u>34</u>	<u>45</u>	<u>98</u>	<u>103</u>	<u>31</u>	<u>4</u>	
<u>1</u>	<u>6</u>		<u>0.48</u>	<u>1.72</u>	<u>502.4</u>	<u>53</u>	<u>33</u>	<u>44</u>	<u>99</u>	<u>104</u>	<u>32</u>	<u>4</u>	
<u>2</u>	<u>9</u>		<u>0.48</u>	<u>1.72</u>	<u>504.5</u>	<u>53</u>	<u>36</u>	<u>45</u>	<u>98</u>	<u>102</u>	<u>34</u>	<u>4</u>	
<u>2</u>	<u>12</u>		<u>0.48</u>	<u>1.72</u>	<u>506.4</u>	<u>54</u>	<u>38</u>	<u>45</u>	<u>98</u>	<u>104</u>	<u>34</u>	<u>4</u>	
<u>3</u>	<u>15</u>		<u>0.47</u>	<u>1.68</u>	<u>508.5</u>	<u>51</u>	<u>36</u>	<u>46</u>	<u>98</u>	<u>104</u>	<u>35</u>	<u>4</u>	
<u>3</u>	<u>18</u>		<u>0.46</u>	<u>1.61</u>	<u>510.4</u>	<u>54</u>	<u>37</u>	<u>45</u>	<u>98</u>	<u>104</u>	<u>35</u>	<u>4</u>	
<u>4</u>	<u>21</u>		<u>0.44</u>	<u>1.54</u>	<u>512.4</u>	<u>54</u>	<u>40</u>	<u>45</u>	<u>98</u>	<u>105</u>	<u>35</u>	<u>4</u>	
<u>4</u>	<u>24</u>		<u>0.42</u>	<u>1.47</u>	<u>514.2</u>	<u>54</u>	<u>41</u>	<u>44</u>	<u>99</u>	<u>104</u>	<u>35</u>	<u>3.5</u>	
<u>5</u>	<u>27</u>		<u>0.40</u>	<u>1.40</u>	<u>516.1</u>	<u>54</u>	<u>39</u>	<u>45</u>	<u>99</u>	<u>107</u>	<u>36</u>	<u>3.5</u>	
<u>5</u>	<u>30</u>		<u>0.39</u>	<u>1.37</u>	<u>518.1</u>	<u>53</u>	<u>37</u>	<u>44</u>	<u>99</u>	<u>105</u>	<u>35</u>	<u>3.5</u>	
<u>6</u>	<u>33</u>		<u>0.34</u>	<u>1.19</u>	<u>519.7</u>	<u>53</u>	<u>35</u>	<u>44</u>	<u>98</u>	<u>106</u>	<u>34</u>	<u>3</u>	
<u>6</u>	<u>36</u>		<u>0.34</u>	<u>1.19</u>	<u>521.5</u>	<u>54</u>	<u>35</u>	<u>45</u>	<u>97</u>	<u>102</u>	<u>34</u>	<u>3</u>	
<u>7</u>	<u>39</u>		<u>0.30</u>	<u>1.05</u>	<u>523.2</u>	<u>53</u>	<u>34</u>	<u>46</u>	<u>97</u>	<u>101</u>	<u>34</u>	<u>3</u>	
<u>7</u>	<u>42</u>		<u>0.31</u>	<u>1.08</u>	<u>524.7</u>	<u>52</u>	<u>34</u>	<u>47</u>	<u>97</u>	<u>104</u>	<u>34</u>	<u>3</u>	
<u>8</u>	<u>45</u>		<u>0.29</u>	<u>1.01</u>	<u>526.4</u>	<u>52</u>	<u>34</u>	<u>48</u>	<u>97</u>	<u>103</u>	<u>34</u>	<u>3</u>	<u>29.516</u>
<u>8</u>	<u>48</u>	<u>0949</u>	<u>0.29</u>	<u>1.01</u>	<u>527.818</u>	<u>52</u>	<u>31</u>	<u>48</u>	<u>98</u>	<u>102</u>	<u>34</u>	<u>3</u>	
			Avg Sqrt Delta P	Avg Delta H	Total Volume	Avg Ts	Avg Tm		Min/Max	Min/Max	Max Temp	Max Vac	Max Temp
			Avg Sqrt Del H		Comments:								



ama

ISOKINETIC FIELD DATA SHEET

Method 0010 HFPO Dimer Acid

Client Chemours Operator Mills
 Source Semi Works Division Run No. 2
 Sample Loc. Stack Date 01/11/19

K Factor 3.5

TRAVERSE POINT NO.	SAMPLE TIME (min)	CLOCK TIME (plant time)	VELOCITY PRESSURE Delta P (in H2O)	ORIFICE PRESSURE Delta H (in H2O)	DRY GAS METER READING (ft ³)	STACK TEMP (°F)	XAD ECM INLET TEMP (°F)	DGM OUTLET TEMP (°F)	PROBE TEMP (°F)	FILTER BOX TEMP (F)	IMPING EXIT TEMP (°F)	SAMPLE TRAIN VAC (In Hg)	COMMENTS
	0	1001			528.186								
1	3		0.417	1.64	530.2	53	37	57	97	108	35	4.0	
1	6		0.48	1.68	532.3	55	38	56	97	101	35	4.0	
2	9		0.46	1.61	534.2	55	38	56	98	102	35	4.0	
2	12		0.46	1.61	536.3	56	36	57	97	100	36	4.0	
3	15		0.42	1.47	538.2	56	40	58	98	102	37	4.0	
3	18		0.43	1.50	540.2	56	41	60	98	103	38	4.0	
4	21		0.41	1.43	542.0	56	42	60	97	103	37	3.5	
4	24		0.41	1.43	544.2	56	44	61	97	104	37	3.5	
5	27		0.37	1.30	545.8	56	43	61	97	101	37	3	
5	30		0.36	1.26	547.8	56	44	62	97	104	37	3	
6	33		0.29	1.01	549.4	55	41	61	97	100	36	2.5	
6	36		0.29	1.01	551.3	54	42	62	97	102	36	2.5	
7	39		0.27	0.95	552.6	54	44	63	97	102	38	2.5	
7	42		0.27	0.95	554.2	54	46	63	97	102	39	2.5	
8	45		0.24	0.81	555.8	55	46	65	98	102	41	2	
8	48	1049	0.24 ✓	0.84 ✓	557.163	54 ✓	45	66 ✓	97	103	40	2	28.977

Avg Sqrt Delta P 0.61461 ✓
 Avg Delta H 1.3420 ✓
 Total Volume 58,493 ✓
 Avg Ts 54.12 ✓
 Avg Tm 52.94 ✓
 Min/Max 97/98
 Min/Max 100/108
 Max Temp 41
 Max Vac 4
 Max Temp

Avg = 0.38218 ✓
 Avg Sqrt Del H 1.15179 ✓

Comments:



amd

Semi Workes (SW)
SAMPLE RECOVERY FIELD DATA

Method 0010 HFPO Dimer Acid *SW*

Client Chemours W.O. # 15418.002.009.0001
 Location/Plant Fayetteville, NC Source & Location Division Stack

Run No. 1 *SW* Sample Date 1/10/19 Recovery Date 1/10/19
 Sample I.D. Chemours - Division - STK - 1 - M 0010 HFPO Dimer Ac Analyst JM/JM Filter Number NA

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents	DO			DO		XAD 1	XAD 2		5.6	
Final	2	111	103	2		289.2	282.4		316.4	
Initial	0	100	100	0		287.2	282.0		300	
Gain	2	11	3	2		2.0	4	20.4	16.4	

Impinger Color all clear Labeled?
 Silica Gel Condition blue 90% Sealed?

Run No. 2 Sample Date 1/11/19 Recovery Date 4/1/19
 Sample I.D. Chemours - Division - STK - 2 - M 0010 HFPO Dimer Ac Analyst JM/JM Filter Number NA

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents									5.8	
Final	1	100	109	1					314.8	
Initial	0	100	100	0					300	
Gain	1	0	9	1				1.8	14.8	25.8

Impinger Color clear Labeled?
 Silica Gel Condition good Sealed?

Run No. 3 Sample Date _____ Recovery Date _____
 Sample I.D. Chemours - Division - STK - 3 - M 0010 HFPO Dimer Ac Analyst _____ Filter Number _____

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents										
Final										
Initial										
Gain										

Impinger Color _____ Labeled? _____
 Silica Gel Condition _____ Sealed? _____

Check COC for Sample IDs of Media Blanks

Cal measured
 Balance Cal 1/10/19 500 499.6 Jho
 Balance Cal 1/11/19 500. 499.8 ew



Semi Woods (SW)
SAMPLE RECOVERY FIELD DATA

Method 0010 HFPO Dimer Acid

SW

Client Chemours W.O. # 15418.002.009.0001
 Location/Plant Fayetteville, NC Source & Location Division Stack

Run No. 1 *SW* Sample Date 1/10/19 Recovery Date 1/10/19
 Sample I.D. Chemours - Division - STK - BT - M 0010 HFPO Dimer Analyst JDO/JM Filter Number NA

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents										
Final	0	100	100	0						
Initial	0	100	100	0						
Gain	0	0	0	0						

Impinger Color all clear Labeled?
 Silica Gel Condition SW 100% Sealed?

Run No. _____ Sample Date _____ Recovery Date _____
 Sample I.D. _____ Analyst _____ Filter Number _____

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents										
Final										
Initial										
Gain										

Impinger Color _____ Labeled? _____
 Silica Gel Condition _____ Sealed? _____

Run No. _____ Sample Date _____ Recovery Date _____
 Sample I.D. _____ Analyst _____ Filter Number _____

	Impinger							Imp.Total	8	Total
	1	2	3	4	5	6	7			
Contents										
Final										
Initial										
Gain										

Impinger Color _____ Labeled? _____
 Silica Gel Condition _____ Sealed? _____

Check COC for Sample IDs of Media Blanks



METHODS AND ANALYZERS

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

File: C:\DATA\Chemours\011019 Semi Works.cem
Program Version: 2.1, built 19 May 2017 **File Version:** 2.02
Computer: WSWCAIRSERVICES **Trailer:** 27
Analog Input Device: Keithley KUSB-3108

Channel 1

Analyte	O₂
Method	EPA 3A, Using Bias
Analyzer Make, Model & Serial No.	Servomex 4900
Full-Scale Output, mv	10000
Analyzer Range, %	25.0
Span Concentration, %	21.0

Channel 2

Analyte	CO₂
Method	EPA 3A, Using Bias
Analyzer Make, Model & Serial No.	Servomex 4900
Full-Scale Output, mv	10000
Analyzer Range, %	20.0
Span Concentration, %	16.6

CALIBRATION DATA

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

Start Time: 12:02

O₂

Method: EPA 3A

Calibration Type: Linear Zero and High Span

Calibration Standards

%	Cylinder ID
12.0	CC18055
21.0	SG9169108

Calibration Results

Zero	5 mv
Span, 21.0 %	8014 mv

Curve Coefficients

Slope	Intercept
381.4	5

CO₂

Method: EPA 3A

Calibration Type: Linear Zero and High Span

Calibration Standards

%	Cylinder ID
8.9	CC18055
16.6	SG9169108

Calibration Results

Zero	1 mv
Span, 16.6 %	8279 mv

Curve Coefficients

Slope	Intercept
499.3	1

CALIBRATION ERROR DATA

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Calibration 1

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

Start Time: 12:02

O₂

Method: EPA 3A
Span Conc. 21.0 %

Slope 381.4 Intercept 5.0

Standard	Response	Result	Difference	Error	Status
%	mv	%	%	%	
Zero	5	0.0	0.0	0.0	Pass
12.0	4565	12.0	0.0	0.0	Pass
21.0	8014	21.0	0.0	0.0	Pass

CO₂

Method: EPA 3A
Span Conc. 16.6 %

Slope 499.3 Intercept 1.0

Standard	Response	Result	Difference	Error	Status
%	mv	%	%	%	
Zero	1	0.0	0.0	0.0	Pass
8.9	4286	8.6	-0.3	-1.8	Pass
16.6	8279	16.6	0.0	0.0	Pass

BIAS
Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

Calibration 1

Start Time: 12:10

O₂
Method: EPA 3A
Span Conc. 21.0 %

Bias Results						
Standard	Cal.	Response	Bias	Difference	Error	Status
Gas	%	mv	%	%	%	
Zero	0.0	19	0.0	0.0	0.0	Pass
Span	12.0	4575	12.0	0.0	0.0	Pass

CO₂
Method: EPA 3A
Span Conc. 16.6 %

Bias Results						
Standard	Cal.	Response	Bias	Difference	Error	Status
Gas	%	mv	%	%	%	
Zero	0.0	20	0.0	0.0	0.0	Pass
Span	8.6	4258	8.5	-0.1	-0.6	Pass

RUN DATA

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

Calibration 1

Time	O ₂ %	CO ₂ %
13:11	20.7	0.1
13:12	20.8	0.0
13:13	20.8	0.0
13:14	20.8	0.0
13:15	20.8	0.0
13:16	20.8	0.0
13:17	20.8	0.0
13:18	20.8	0.0
13:19	20.8	0.0
13:20	20.8	0.0
13:21	20.8	0.0
13:22	20.8	0.0
13:23	20.8	0.0
13:24	20.8	0.0
13:25	20.8	0.0
13:26	20.8	0.0
13:27	20.8	0.0
13:28	20.8	0.0
13:29	20.8	0.0
13:30	20.8	0.0
13:31	20.8	0.0
13:32	20.8	0.0
13:33	20.8	0.0
13:34	20.8	0.0
13:35	20.8	0.0
13:36	20.8	0.0
13:37	20.8	0.0
13:38	20.8	0.0
13:39	20.8	0.0
13:40	20.8	0.0
13:41	20.8	0.0
13:42	20.8	0.0
13:43	20.8	0.0
13:44	20.8	0.0
13:45	20.8	0.0
13:46	20.8	0.0
13:47	20.8	0.0
13:48	20.8	0.0
13:49	20.8	0.0
13:50	20.8	0.0
13:51	20.8	0.0

RUN DATA

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

Calibration 1

Time	O ₂ %	CO ₂ %
13:52	20.8	0.0
13:53	20.8	0.0
13:54	20.8	0.0
13:55	20.8	0.0
13:56	20.8	0.0
13:57	20.8	0.0
13:58	20.8	0.0
13:59	20.8	0.0
14:00	20.8	0.0
14:01	20.8	0.0
14:02	20.8	0.0
14:03	20.8	0.0
14:04	20.8	0.0
14:05	20.8	0.0
14:06	20.7	0.0
14:07	20.7	0.0
14:08	20.7	0.0
14:09	20.7	0.0
14:10	20.7	0.0
14:11	20.7	0.0
14:12	20.7	0.0
14:13	20.8	0.0
14:14	20.8	0.0
14:15	20.8	0.0
14:16	20.8	0.0
14:17	20.8	0.0
14:18	20.8	0.0
14:19	20.8	0.0
14:20	20.8	0.0
14:21	20.8	0.0
14:22	20.8	0.0
14:23	20.8	0.0
14:24	20.8	0.0
14:25	20.8	0.0
14:26	20.8	0.0
14:27	20.8	0.0
14:28	20.8	0.0
14:29	20.8	0.0
14:30	20.8	0.0
14:31	20.8	0.0
14:32	20.8	0.0

RUN DATA

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

Calibration 1

Time	O ₂ %	CO ₂ %
14:33	20.8	0.0
14:34	20.8	0.0
14:35	20.8	0.0
14:36	20.8	0.0
14:37	20.8	0.0
14:38	20.8	0.0
14:39	20.8	0.0
14:40	20.8	0.0
14:41	20.8	0.0
14:42	20.8	0.0
14:43	20.8	0.0
14:44	20.8	0.0
14:45	20.8	0.0
14:46	20.8	0.0
14:47	20.8	0.0
14:48	20.8	0.0
14:49	20.8	0.0
14:50	20.8	0.0
14:51	20.8	0.0
14:52	20.8	0.0
14:53	20.8	0.0
14:54	20.8	0.0
14:55	20.8	0.0
14:56	20.8	0.0
14:57	20.8	0.0
14:58	20.8	0.0
Avg	20.8	0.0

RUN SUMMARY

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Calibration 1

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

Method	O₂	CO₂
Conc. Units	EPA 3A	EPA 3A
	%	%

Time: 13:10 to 14:58

Run Averages

20.8 0.0

Pre-run Bias at 12:10

Zero Bias	0.0	0.0
Span Bias	12.0	8.5
Span Gas	12.0	8.9

Post-run Bias at 14:59

Zero Bias	0.0	0.0
Span Bias	11.9	8.5
Span Gas	12.0	8.9

Run averages corrected for the average of the pre-run and post-run bias

20.9 0.0

BIAS AND CALIBRATION DRIFT

Number 2

Client: **Chemours**
Location: **CHEMOURS**
Source: **Semi Works**

Project Number: **15418.002.009**
Operator: **CW**
Date: **10 Jan 2019**

Calibration 1

Start Time: 14:59

O₂
Method: EPA 3A
Span Conc. 21.0 %

Bias Results						
Standard	Cal.	Response	Bias	Difference	Error	Status
Gas	%	mv	%	%	%	
Zero	0.0	1	0.0	0.0	0.0	Pass
Span	12.0	4525	11.9	-0.1	-0.5	Pass

Calibration Drift						
Standard	Initial*	Final	Difference	Drift	Status	
Gas	%	mv	%	%		
Zero	0.0	1	0.0	0.0	Pass	
Span	12.0	4525	11.9	-0.1	Pass	

*Bias No. 1

CO₂
Method: EPA 3A
Span Conc. 16.6 %

Bias Results						
Standard	Cal.	Response	Bias	Difference	Error	Status
Gas	%	mv	%	%	%	
Zero	0.0	22	0.0	0.0	0.0	Pass
Span	8.6	4226	8.5	-0.1	-0.6	Pass

Calibration Drift						
Standard	Initial*	Final	Difference	Drift	Status	
Gas	%	mv	%	%		
Zero	0.0	22	0.0	0.0	Pass	
Span	8.5	4226	8.5	0.0	Pass	

*Bias No. 1

METHODS AND ANALYZERS

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

File: C:\DATA\Chemours\011119 Semi Works.cem
Program Version: 2.1, built 19 May 2017 **File Version:** 2.02
Computer: WSWCAIRSERVICES **Trailer:** 27
Analog Input Device: Keithley KUSB-3108

Channel 1

Analyte	O₂
Method	EPA 3A, Using Bias
Analyzer Make, Model & Serial No.	Servomex 4900
Full-Scale Output, mv	10000
Analyzer Range, %	25.0
Span Concentration, %	21.0

Channel 2

Analyte	CO₂
Method	EPA 3A, Using Bias
Analyzer Make, Model & Serial No.	Servomex 4900
Full-Scale Output, mv	10000
Analyzer Range, %	20.0
Span Concentration, %	16.6

CALIBRATION DATA

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

Start Time: 07:10

O₂

Method: EPA 3A

Calibration Type: Linear Zero and High Span

Calibration Standards

%	Cylinder ID
12.0	CC18055
21.0	SG9169108

Calibration Results

Zero	5 mv
Span, 21.0 %	7987 mv

Curve Coefficients

Slope	Intercept
380.1	5

CO₂

Method: EPA 3A

Calibration Type: Linear Zero and High Span

Calibration Standards

%	Cylinder ID
8.9	CC18055
16.6	SG9169108

Calibration Results

Zero	1 mv
Span, 16.6 %	8285 mv

Curve Coefficients

Slope	Intercept
499.6	1

CALIBRATION ERROR DATA

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

Calibration 1

Start Time: 07:10

O₂

Method: EPA 3A

Span Conc. 21.0 %

Slope 380.1 Intercept 5.0

Standard	Response	Result	Difference	Error	Status
%	mv	%	%	%	
Zero	5	0.0	0.0	0.0	Pass
12.0	4558	12.0	0.0	0.0	Pass
21.0	7987	21.0	0.0	0.0	Pass

CO₂

Method: EPA 3A

Span Conc. 16.6 %

Slope 499.6 Intercept 1.0

Standard	Response	Result	Difference	Error	Status
%	mv	%	%	%	
Zero	1	0.0	0.0	0.0	Pass
8.9	4299	8.6	-0.3	-1.8	Pass
16.6	8285	16.6	0.0	0.0	Pass

BIAS

Number 1

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

Calibration 1

Start Time: 07:17

O₂

Method: EPA 3A
Span Conc. 21.0 %

Bias Results

Standard	Cal.	Response	Bias	Difference	Error	Status
Gas	%	mv	%	%	%	
Zero	0.0	29	0.1	0.1	0.5	Pass
Span	12.0	4573	12.0	0.0	0.0	Pass

CO₂

Method: EPA 3A
Span Conc. 16.6 %

Bias Results

Standard	Cal.	Response	Bias	Difference	Error	Status
Gas	%	mv	%	%	%	
Zero	0.0	16	0.0	0.0	0.0	Pass
Span	8.6	4277	8.6	0.0	0.0	Pass

RUN DATA

Number 2

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

Calibration 1

Time	O ₂ %	CO ₂ %
08:52	20.9	0.0
08:53	20.9	0.0
08:54	21.0	0.0
08:55	21.0	0.0
08:56	21.0	0.0
08:57	21.0	0.0
08:58	21.0	0.0
08:59	21.0	0.0
09:00	21.0	0.0
09:01	21.0	0.0
09:02	21.0	0.0
09:03	21.0	0.0
09:04	21.0	0.0
09:05	21.0	0.0
09:06	21.0	0.0
09:07	21.0	0.0
09:08	21.0	0.0
09:09	21.0	0.0
09:10	21.0	0.0
09:11	21.0	0.0
09:12	21.0	0.0
09:13	21.0	0.0
09:14	21.0	0.0
09:15	21.0	0.0
09:16	21.0	0.0
09:17	21.0	0.0
09:18	21.0	0.0
09:19	21.0	0.0
09:20	21.0	0.0
09:21	21.0	0.0
09:22	21.0	0.0
09:23	21.0	0.0
09:24	21.0	0.0
09:25	21.0	0.0
09:26	21.0	0.0
09:27	21.0	0.0
09:28	21.0	0.0
09:29	21.0	0.0
09:30	21.0	0.0
09:31	21.0	0.0
09:32	21.0	0.0

RUN DATA

Number 2

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

Calibration 1

Time	O ₂ %	CO ₂ %
09:33	21.0	0.0
09:34	21.0	0.0
09:35	21.0	0.0
09:36	21.0	0.0
09:37	21.0	0.0
09:38	21.0	0.0
09:39	21.0	0.0
09:40	21.0	0.0
09:41	21.0	0.0
09:42	21.0	0.0
09:43	21.0	0.0
09:44	21.0	0.0
09:45	21.0	0.0
09:46	21.0	0.0
09:47	21.0	0.0
09:48	21.0	0.0
09:49	21.0	0.0
09:50	21.0	0.0
09:51	21.0	0.0
09:52	21.0	0.0
09:53	21.0	0.0
09:54	21.0	0.0
09:55	21.0	0.0
09:56	21.0	0.0
09:57	21.0	0.0
09:58	21.0	0.0
09:59	21.0	0.0
10:02	21.0	0.0
10:03	21.0	0.0
10:04	21.0	0.0
10:05	21.0	0.0
10:06	21.0	0.0
10:07	21.0	0.0
10:08	21.0	0.0
10:09	21.0	0.0
10:10	21.0	0.0
10:11	21.0	0.0
10:12	21.0	0.0
10:13	21.0	0.0
10:14	21.0	0.0
10:15	21.0	0.0

RUN DATA

Number 2

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

Calibration 1

Time	O ₂ %	CO ₂ %
10:16	21.0	0.0
10:17	21.0	0.0
10:18	21.0	0.0
10:19	21.0	0.0
10:20	21.0	0.0
10:21	21.0	0.0
10:22	21.0	0.0
10:23	21.0	0.0
10:24	21.0	0.0
10:25	21.0	0.0
10:26	21.0	0.0
10:27	21.0	0.0
10:28	21.0	0.0
10:29	21.0	0.0
10:30	21.0	0.0
10:31	21.0	0.0
10:32	21.0	0.0
10:33	21.0	0.0
10:34	21.0	0.0
10:35	21.0	0.0
10:36	21.0	0.0
10:37	21.0	0.0
10:38	21.0	0.0
10:39	21.0	0.0
10:40	21.0	0.0
10:41	21.0	0.0
10:42	21.0	0.0
10:43	21.0	0.0
10:44	21.0	0.0
10:45	21.0	0.0
10:46	21.0	0.0
10:47	21.0	0.0
10:48	21.0	0.0
10:49	21.0	0.0
Avg	21.0	0.0

RUN SUMMARY

Number 2

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

Calibration 1

Method	O ₂	CO ₂
Conc. Units	EPA 3A	EPA 3A
	%	%

Time: 08:51 to 10:49

Run Averages

21.0 0.0

Pre-run Bias at 07:17

Zero Bias	0.1	0.0
Span Bias	12.0	8.6
Span Gas	12.0	8.9

Post-run Bias at 10:55

Zero Bias	0.1	0.2
Span Bias	12.0	8.6
Span Gas	12.0	8.9

Run averages corrected for the average of the pre-run and post-run bias

21.1 0.0

BIAS AND CALIBRATION DRIFT

Number 2

Client: **Chemours**
Location: **CHEMOURS**
Source:

Project Number: **15418.002.009**
Operator:
Date: **11 Jan 2019**

Calibration 1

Start Time: 10:55

O₂
Method: EPA 3A
Span Conc. 21.0 %

Bias Results						
Standard	Cal.	Response	Bias	Difference	Error	Status
Gas	%	mv	%	%	%	
Zero	0.0	46	0.1	0.1	0.5	Pass
Span	12.0	4583	12.0	0.0	0.0	Pass

Calibration Drift						
Standard	Initial*	Final	Difference	Drift	Status	
Gas	%	mv	%	%		
Zero	0.1	46	0.1	0.0	Pass	
Span	12.0	4583	12.0	0.0	Pass	

*Bias No. 1

CO₂
Method: EPA 3A
Span Conc. 16.6 %

Bias Results						
Standard	Cal.	Response	Bias	Difference	Error	Status
Gas	%	mv	%	%	%	
Zero	0.0	86	0.2	0.2	1.2	Pass
Span	8.6	4278	8.6	0.0	0.0	Pass

Calibration Drift						
Standard	Initial*	Final	Difference	Drift	Status	
Gas	%	mv	%	%		
Zero	0.0	86	0.2	0.2	1.2	Pass
Span	8.6	4278	8.6	0.0	0.0	Pass

*Bias No. 1

APPENDIX B
LABORATORY ANALYTICAL REPORT

Note: The analytical report is included on the attached CD.

Client Sample Results

Client: Chemours Company FC, LLC The
Project/Site: Semi Works Stack 1500 - M0010

TestAmerica Job ID: 140-13929-1

**Client Sample ID: H-2477,2478 SEMI WORKS 1500 STK R1
M0010 FH**

Lab Sample ID: 140-13929-1

Date Collected: 01/10/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	54.1		0.604	0.0652	ug/Sample		01/16/19 06:43	01/23/19 13:00	4
Surrogate	%Recovery	Qualifier	Limits						
13C3 HFPO-DA	106	D	50 - 200						
							Prepared	Analyzed	Dil Fac
							01/16/19 06:43	01/23/19 13:00	4

**Client Sample ID: H-2479,2480,2482 SEMI WORKS 1500 STK
R1 M0010 BH**

Lab Sample ID: 140-13929-2

Date Collected: 01/10/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	3.46		0.250	0.0500	ug/Sample		01/15/19 04:25	01/23/19 12:34	1
Surrogate	%Recovery	Qualifier	Limits						
13C3 HFPO-DA	68		50 - 200						
							Prepared	Analyzed	Dil Fac
							01/15/19 04:25	01/23/19 12:34	1

**Client Sample ID: H-2481 SEMI WORKS 1500 STK R1 M0010
IMP 1,2&3 CONDENSATE**

Lab Sample ID: 140-13929-3

Date Collected: 01/10/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - HFPO-DA

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.226	0.0115	ug/Sample		01/21/19 04:09	01/23/19 14:06	1
Surrogate	%Recovery	Qualifier	Limits						
13C3 HFPO-DA	94		50 - 200						
							Prepared	Analyzed	Dil Fac
							01/21/19 04:09	01/23/19 14:06	1

**Client Sample ID: H-2483 SEMI WORKS 1500 STK R1 M0010
BREAKTHROUGH XAD-2 RESIN TUBE**

Lab Sample ID: 140-13929-4

Date Collected: 01/10/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.0484	J	0.200	0.0400	ug/Sample		01/15/19 04:25	01/23/19 12:38	1
Surrogate	%Recovery	Qualifier	Limits						
13C3 HFPO-DA	89		50 - 200						
							Prepared	Analyzed	Dil Fac
							01/15/19 04:25	01/23/19 12:38	1

TestAmerica Knoxville

Client Sample Results

Client: Chemours Company FC, LLC The
Project/Site: Semi Works Stack 1500 - M0010

TestAmerica Job ID: 140-13929-1

**Client Sample ID: H-2484,2485 SEMI WORKS 1500 STK R2
M0010 FH**

Lab Sample ID: 140-13929-5

Date Collected: 01/11/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	32.1		0.302	0.0326	ug/Sample		01/16/19 06:43	01/23/19 13:04	2
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	106	D	50 - 200				01/16/19 06:43	01/23/19 13:04	2

**Client Sample ID: H-2486,2487,2489 SEMI WORKS 1500 STK
R2 M0010 BH**

Lab Sample ID: 140-13929-6

Date Collected: 01/11/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	2.09		0.275	0.0550	ug/Sample		01/15/19 04:25	01/23/19 12:41	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	87		50 - 200				01/15/19 04:25	01/23/19 12:41	1

**Client Sample ID: H-2488 SEMI WORKS 1500 STK R2 M0010
IMP 1,2&3 CONDENSATE**

Lab Sample ID: 140-13929-7

Date Collected: 01/11/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - HFPO-DA

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.0522	J	0.232	0.0118	ug/Sample		01/21/19 04:09	01/23/19 14:09	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	99		50 - 200				01/21/19 04:09	01/23/19 14:09	1

**Client Sample ID: H-2490 SEMI WORKS 1500 STK R2 M0010
BREAKTHROUGH XAD-2 RESIN TUBE**

Lab Sample ID: 140-13929-8

Date Collected: 01/11/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.0465	J	0.200	0.0400	ug/Sample		01/15/19 04:25	01/23/19 12:44	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	89		50 - 200				01/15/19 04:25	01/23/19 12:44	1

TestAmerica Knoxville

Client Sample Results

Client: Chemours Company FC, LLC The
Project/Site: Semi Works 1500 QC Samples

TestAmerica Job ID: 140-13932-1

**Client Sample ID: E-2696,2697 SEMI WORKS 1500 STK QC
M0010 FH BT**

Lab Sample ID: 140-13932-1

Date Collected: 01/10/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.0835		0.0260	0.00281	ug/Sample		01/16/19 06:43	01/23/19 13:20	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	83		50 - 200				01/16/19 06:43	01/23/19 13:20	1

**Client Sample ID: E-2698,2699,2701 SEMI WORKS 1500 STK
QC M0010 BH BT**

Lab Sample ID: 140-13932-2

Date Collected: 01/10/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.0637	J	0.200	0.0400	ug/Sample		01/15/19 04:25	01/23/19 12:08	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	83		50 - 200				01/15/19 04:25	01/23/19 12:08	1

**Client Sample ID: E-2700 SEMI WORKS 1500 STK QC M0010
IMP 1,2&3 CONDENSATE BT**

Lab Sample ID: 140-13932-3

Date Collected: 01/10/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - HFPO-DA

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.00250	0.000128	ug/Sample		01/21/19 04:09	01/23/19 14:32	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	116		50 - 200				01/21/19 04:09	01/23/19 14:32	1

**Client Sample ID: E-2702 SEMI WORKS 1500 STK QC M0010
BREAKTHROUGH XAD-2 RESIN TUBE BT**

Lab Sample ID: 140-13932-4

Date Collected: 01/10/19 00:00
Date Received: 01/13/19 07:30
Sample Container: Air Train

Matrix: Air

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.200	0.0400	ug/Sample		01/15/19 04:25	01/23/19 12:15	1
Surrogate	%Recovery	Qualifier	Limits				Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	81		50 - 200				01/15/19 04:25	01/23/19 12:15	1

TestAmerica Knoxville

Client Sample Results

Client: Chemours Company FC, LLC The
Project/Site: Semi Works 1500 QC Samples

TestAmerica Job ID: 140-13932-1

Client Sample ID: E-2703 SEMI WORKS 1500 STK QC M0010

Lab Sample ID: 140-13932-5

DI WATER RB

Date Collected: 01/10/19 00:00

Matrix: Air

Date Received: 01/13/19 07:30

Sample Container: Air Train

Method: 8321A - HFPO-DA

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.00250	0.000128	ug/Sample		01/21/19 04:09	01/23/19 14:35	1

Surrogate	%Recovery	Qualifier	Limits	Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	120		50 - 200	01/21/19 04:09	01/23/19 14:35	1

Client Sample ID: E-2704 SEMI WORKS 1500 STK QC M0010

Lab Sample ID: 140-13932-6

MEOH WITH 5% NH4OH RB

Date Collected: 01/10/19 00:00

Matrix: Air

Date Received: 01/13/19 07:30

Sample Container: Air Train

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.0250	0.00500	ug/Sample		01/15/19 04:25	01/23/19 12:18	1

Surrogate	%Recovery	Qualifier	Limits	Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	109		50 - 200	01/15/19 04:25	01/23/19 12:18	1

Client Sample ID: E-2705 SEMI WORKS 1500 STK QC M0010

Lab Sample ID: 140-13932-7

XAD-2 RESIN TUBE RB

Date Collected: 01/10/19 00:00

Matrix: Air

Date Received: 01/13/19 07:30

Sample Container: Air Train

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.200	0.0400	ug/Sample		01/15/19 04:25	01/23/19 12:21	1

Surrogate	%Recovery	Qualifier	Limits	Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	93		50 - 200	01/15/19 04:25	01/23/19 12:21	1

Client Sample ID: E-2706 SEMI WORKS 1500 STK QC M0010

Lab Sample ID: 140-13932-8

MEOH WITH 5% NH4OH TB

Date Collected: 01/10/19 00:00

Matrix: Air

Date Received: 01/13/19 07:30

Sample Container: Air Train

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.00598	J	0.0250	0.00500	ug/Sample		01/15/19 04:25	01/23/19 12:24	1

Surrogate	%Recovery	Qualifier	Limits	Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	108		50 - 200	01/15/19 04:25	01/23/19 12:24	1

TestAmerica Knoxville

Client Sample Results

Client: Chemours Company FC, LLC The
 Project/Site: Semi Works 1500 QC Samples

TestAmerica Job ID: 140-13932-1

Client Sample ID: E-2707 SEMI WORKS 1500 STK QC M0010

Lab Sample ID: 140-13932-9

XAD-2 RESIN TUBE TB

Date Collected: 01/10/19 00:00

Matrix: Air

Date Received: 01/13/19 07:30

Sample Container: Air Train

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	ND		0.200	0.0400	ug/Sample		01/15/19 04:25	01/23/19 12:28	1

Surrogate	%Recovery	Qualifier	Limits	Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	88		50 - 200	01/15/19 04:25	01/23/19 12:28	1

Client Sample ID: E-2708 SEMI WORKS 1500 STK QC M0010

Lab Sample ID: 140-13932-10

COMBINED GLASSWARE RINSES (MEOH/5%/NH4OH) PB

Date Collected: 01/10/19 00:00

Matrix: Air

Date Received: 01/13/19 07:30

Sample Container: Air Train

Method: 8321A - PFOA and PFOS

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
HFPO-DA	0.232		0.0250	0.00500	ug/Sample		01/15/19 04:25	01/23/19 12:31	1

Surrogate	%Recovery	Qualifier	Limits	Prepared	Analyzed	Dil Fac
13C3 HFPO-DA	104		50 - 200	01/15/19 04:25	01/23/19 12:31	1

APPENDIX C
SAMPLE CALCULATIONS

**SAMPLE CALCULATIONS FOR
SEMI-VOLATILE ORGANIC COMPOUNDS (METHOD 0010)**

Client: Chemours
Test Number: Run 1
Test Location: Semi-Works

Plant: Fayetteville, NC
Test Date: 1/10/2019
Test Period: 1310-1458

1. HFPO Dimer Acid concentration, lbs/dscf.

$$C_1 = \frac{W \times 2.2046 \times 10^{-9}}{Vm(std)}$$

$$C_1 = \frac{57.6 \times 2.2046 \times 10^{-9}}{61.563}$$

$$= 2.06E-09$$

Where:

W = Weight of HFPO Dimer Acid collected in sample in ug.

C₁ = HFPO Dimer Acid concentration, lbs/dscf.

2.2046x10⁻⁹ = Conversion factor from ug to lbs.

2. HFPO Dimer Acid concentration, ug/dscm.

$$C_2 = W / (Vm(std) \times 0.02832)$$

$$C_2 = 57.6 / (61.563 \times 0.02832)$$

$$= 3.30E+01$$

Where:

C₂ = HFPO Dimer Acid concentration, ug/dscm.

0.02832 = Conversion factor from cubic feet to cubic meters.

3. HFPO Dimer Acid mass emission rate, lbs/hr.

$$\text{PMR1} = C_1 \times Qs(\text{std}) \times 60 \text{ min/hr}$$

$$\text{PMR1} = 2.06\text{E-}09 \times 8108 \times 60$$

$$= 1.00\text{E-}03$$

Where:

$$\text{PMR1} = \text{HFPO Dimer Acid mass emission rate, lbs/hr.}$$

4. HFPO Dimer Acid mass emission rate, g/sec.

$$\text{PMR2} = \text{PMR1} \times 453.59 / 3600$$

$$\text{PMR2} = 1.00\text{E-}03 \times 453.59 / 3600$$

$$= 1.26\text{E-}04$$

Where:

$$\text{PMR2} = \text{HFPO Dimer Acid mass emission rate, g/sec.}$$

$$454 = \text{Conversion factor from pounds to grams.}$$

$$3600 = \text{Conversion factor from hours to seconds.}$$

**EXAMPLE CALCULATIONS FOR
VOLUMETRIC FLOW AND MOISTURE AND ISOKINETICS**

Client: Chemours
Test Number: Run 1
Test Location: Semi-Works

Facility: Fayetteville, NC
Test Date: 1/10/19
Test Period: 1310-1458

1. Volume of dry gas sampled at standard conditions (68 deg F, 29.92 in. Hg), dscf.

$$Vm(std) = \frac{17.64 \times Y \times Vm \times \left(Pb + \frac{\text{delta H}}{13.6} \right)}{(Tm + 460)}$$

$$Vm(std) = \frac{17.64 \times 0.9915 \times 61.011 \times \left(29.93 + \frac{1.374}{13.6} \right)}{60.53 + 460} = 61.563$$

Where:

$Vm(std)$ = Volume of gas sample measured by the dry gas meter, corrected to standard conditions, dscf.
 Vm = Volume of gas sample measured by the dry gas meter at meter conditions, dcf.
 Pb = Barometric Pressure, in Hg.
 $delt H$ = Average pressure drop across the orifice meter, in H₂O
 Tm = Average dry gas meter temperature, deg F.
 Y = Dry gas meter calibration factor.
 17.64 = Factor that includes ratio of standard temperature (528 deg R) to standard pressure (29.92 in. Hg), deg R/in. Hg.
 13.6 = Specific gravity of mercury.

2. Volume of water vapor in the gas sample corrected to standard conditions, scf.

$$Vw(std) = (0.04707 \times Vwc) + (0.04715 \times Wwsg)$$

$$Vw(std) = (0.04707 \times 20.4) + (0.04715 \times 16.4) = 1.73$$

Where:

$Vw(std)$ = Volume of water vapor in the gas sample corrected to standard conditions, scf.
 Vwc = Volume of liquid condensed in impingers, ml.
 $Wwsg$ = Weight of water vapor collected in silica gel, g.
 0.04707 = Factor which includes the density of water (0.002201 lb/ml), the molecular weight of water (18.0 lb/lb-mole), the ideal gas constant 21.85 (in. Hg) (ft³/lb-mole)(deg R); absolute temperature at standard conditions (528 deg R), absolute pressure at standard conditions (29.92 in. Hg), ft³/ml.
 0.04715 = Factor which includes the molecular weight of water (18.0 lb/lb-mole), the ideal gas constant 21.85 (in. Hg) (ft³/lb-mole)(deg R); absolute temperature at standard conditions (528 deg R), absolute pressure at standard conditions (29.92 in. Hg), and 453.6 g/lb, ft³/g.

3. Moisture content

$$\text{bws} = \frac{V_w(\text{std})}{V_w(\text{std}) + V_m(\text{std})}$$
$$\text{bws} = \frac{1.73}{1.73 + 61.563} = 0.027$$

Where:

bws = Proportion of water vapor, by volume, in the gas stream, dimensionless.

4. Mole fraction of dry gas.

$$\text{Md} = 1 - \text{bws}$$
$$\text{Md} = 1 - 0.027 = 0.973$$

Where:

Md = Mole fraction of dry gas, dimensionless.

5. Dry molecular weight of gas stream, lb/lb-mole.

$$\text{MWd} = (0.440 \times \% \text{CO}_2) + (0.320 \times \% \text{O}_2) + (0.280 \times (\% \text{N}_2 + \% \text{CO}))$$
$$\text{MWd} = (0.440 \times 0.0) + (0.320 \times 20.9) + (0.280 \times (79.1 + 0.00))$$
$$\text{MWd} = 28.84$$

Where:

MWd = Dry molecular weight, lb/lb-mole.
% CO₂ = Percent carbon dioxide by volume, dry basis.
% O₂ = Percent oxygen by volume, dry basis.
% N₂ = Percent nitrogen by volume, dry basis.
% CO = Percent carbon monoxide by volume, dry basis.
0.440 = Molecular weight of carbon dioxide, divided by 100.
0.320 = Molecular weight of oxygen, divided by 100.
0.280 = Molecular weight of nitrogen or carbon monoxide, divided by 100.

6. Actual molecular weight of gas stream (wet basis), lb/lb-mole.

$$\text{MWs} = (\text{MWd} \times \text{Md}) + (18 \times (1 - \text{Md}))$$
$$\text{MWs} = (28.84 \times 0.973) + (18 \times (1 - 0.973)) = 28.54$$

Where:

MWs = Molecular weight of wet gas, lb/lb-mole.
18 = Molecular weight of water, lb/lb-mole.

7. Average velocity of gas stream at actual conditions, ft/sec.

$$V_s = 85.49 \times C_p \times ((\Delta p)^{1/2})_{\text{avg}} \times \left(\frac{T_s (\text{avg})}{P_s \times MW_s} \right)^{1/2}$$

$$V_s = 85.49 \times 0.84 \times 0.61496 \times \left(\frac{521}{29.91 \times 28.54} \right)^{1/2} = 34.5$$

Where:

- V_s = Average gas stream velocity, ft/sec.
- 85.49 = Pitot tube constant, ft/sec $\times \frac{(\text{lb/lb-mole})(\text{in. Hg})^{1/2}}{(\text{deg R})(\text{in H}_2\text{O})}$
- C_p = Pitot tube coefficient, dimensionless.
- T_s = Absolute gas stream temperature, deg R = T_s , deg F + 460.
- P_s = Absolute gas stack pressure, in. Hg. = $P_b + \frac{P(\text{static})}{13.6}$
- Δp = Velocity head of stack, in. H₂O.

8. Average gas stream volumetric flow rate at actual conditions, wacf/min.

$$Q_s(\text{act}) = 60 \times V_s \times A_s$$

$$Q_s(\text{act}) = 60 \times 34.5 \times 3.98 = 8229$$

Where:

- $Q_s(\text{act})$ = Volumetric flow rate of wet stack gas at actual conditions, wacf/min.
- A_s = Cross-sectional area of stack, ft².
- 60 = Conversion factor from seconds to minutes.

9. Average gas stream dry volumetric flow rate at standard conditions, dscf/min.

$$Q_s(\text{std}) = 17.64 \times M_d \times \frac{P_s}{T_s} \times Q_s(\text{act})$$

$$Q_s(\text{std}) = 17.64 \times 0.973 \times \frac{29.91}{520.9} \times 8229$$

$$Q_s(\text{std}) = 8108$$

Where:

- $Q_s(\text{std})$ = Volumetric flow rate of dry stack gas at standard conditions, dscf/min.

10. Isokinetic variation calculated from intermediate values, percent.

$$I = \frac{17.327 \times T_s \times V_m(\text{std})}{V_s \times O \times P_s \times M_d \times (D_n)^2}$$

$$I = \frac{17.327 \times 521 \times 61.563}{34.5 \times 96 \times 29.91 \times 0.973 \times (0.235)^2} = 104.4$$

Where:

- I = Percent of isokinetic sampling.
- O = Total sampling time, minutes.
- Dn = Diameter of nozzle, inches.
- 17.327 = Factor which includes standard temperature (528 deg R), standard pressure (29.92 in. Hg), the formula for calculating area of circle $D^{2/4}$, conversion of square feet to square inches (144), conversion of seconds to minutes (60), and conversion to percent (100),
 $\frac{(\text{in. Hg})(\text{in}^2)(\text{min})}{(\text{deg R})(\text{ft}^2)(\text{sec})}$

APPENDIX D
EQUIPMENT CALIBRATION RECORDS

Long Cal and Temperature Cal Datasheet for Standard Dry Gas Meter Console

Calibrator PM

Meter Box Number 21

Ambient Temp 71
Thermocouple Simulator

Date 12-Feb-18

Wet Test Meter Number P-2952

Temp Reference Source (Accuracy +/- 1°F)

Dry Gas Meter Number 17485140

Baro Press, in Hg (Pb)	29.64
--------------------------	-------

Setting	Gas Volume		Temperatures				Time, min (O)	Calibration Results	
	Wet Test Meter	Dry gas Meter	Wet Test Meter	Dry Gas Meter				Y	ΔH
Orifice Manometer	ft ³ (Vw)	ft ³ (Vd)	°F (Tw)	Outlet, °F (Tdo)	Inlet, °F (Tdi)	Average, °F (Td)			
0.5	5.0	570.015	70.0	69.00	69.00	70.0	13.00	0.9948	1.9159
		575.035		71.00	71.00				
		5.020		70.00	70.00				
1.0	5.0	575.035	70.0	71.00	71.00	71.5	9.3	0.9910	1.9555
		580.082		72.00	72.00				
		5.047		71.50	71.50				
1.5	10.0	580.082	70.0	72.00	72.00	73.0	15.6	0.9898	2.0575
		590.205		74.00	74.00				
		10.123		73.00	73.00				
2.0	10.0	590.205	70.0	74.00	74.00	74.5	13.6	0.9945	2.0792
		600.296		75.00	75.00				
		10.091		74.50	74.50				
3.0	10.0	600.296	70.0	75.00	75.00	75.5	11.0	0.9873	2.0365
		610.454		76.00	76.00				
		10.158		75.50	75.50				
Average							0.9915	2.0089	

Vw - Gas Volume passing through the wet test meter
 Vd - Gas Volume passing through the dry gas meter
 Tw - Temp of gas in the wet test meter
 Tdi - Temp of the inlet gas of the dry gas meter
 Tdo - Temp of the outlet gas of the dry gas meter
 Td - Average temp of the gas in the dry gas meter

O - Time of calibration run
 Pb - Barometric Pressure
 ΔH - Pressure differential across orifice
 Y - Ratio of accuracy of wet test meter to dry gas meter

$$Y = \frac{Vw * Pb * (td + 460)}{Vd * \left[Pb + \frac{\Delta H}{13.6} \right] * (tw + 460)}$$

$$\Delta H = \left[\frac{0.0317 * \Delta H}{Pb * (td + 460)} \right] * \left[\frac{(tw + 460) * O}{Vw} \right]^2$$

Reference Temperature	Temperature Reading from Individual Thermocouple Input ¹						Average Temperature Reading	Temp Difference ² (%)
	Select Temperature	Channel Number						
<input type="radio"/> °C <input checked="" type="radio"/> °F	1	2	3	4	5	6		
32	32	32	32	32	32	32	32.0	0.0%
212	212	212	212	212	212	212	212.0	0.0%
932	932	932	932	932	932	932	932.0	0.0%
1832	1830	1830	1830	1830	1830	1830	1830.0	0.1%

¹ - Channel Temps must agree with +/- 5°F or 3°C

² - Acceptable Temperature Difference less than 1.5 %

$$\text{Temp Diff} = \left[\frac{(\text{Reference Temp}(\text{°F}) + 460) - (\text{Test Temp}(\text{°F}) + 460)}{\text{Reference Temp}(\text{°F}) + 460} \right]$$

Y Factor Calibration Check Calculation

METER BOX NO. 21

1/10/019 - 1/11/2019

	Run 1	Run 2
MWd = Dry molecular weight source gas, lb/lb-mole.		
0.32 = Molecular weight of oxygen, divided by 100.		
0.44 = Molecular weight of carbon dioxide, divided by 100.		
0.28 = Molecular weight of nitrogen or carbon monoxide, divided by 100.		
% CO ₂ = Percent carbon dioxide by volume, dry basis.	0.0	0.0
% O ₂ = Percent oxygen by volume, dry basis.	20.9	20.9

$$MWd = (0.32 * O_2) + (0.44 * CO_2) + (0.28 * (100 - (CO_2 + O_2)))$$

$$MWd = (0.32 * 20.9) + (0.44 * 0) + (0.28 * (100 - (0 + 20.9)))$$

$$MWd = (6.69) + (0.00) + (22.15)$$

MWd = 28.84 28.84

Tma = Source Temperature, absolute(°R)		
Tm = Average dry gas meter temperature, deg F.	60.5	52.9

$$Tma = Ts + 460$$

$$Tma = 60.53 + 460$$

Tma = 520.53 512.94

Ps = Absolute meter pressure, inches Hg.		
13.60 = Specific gravity of mercury.		
delta H = Avg pressure drop across the orifice meter during sampling, in H ₂ O	1.374	1.343
Pb = Barometric Pressure, in Hg.	29.93	30.24

$$Pm = Pb + (\text{delta H} / 13.6)$$

$$Pm = 29.93 + (1.374375 / 13.6)$$

Pm = 30.03 30.34

Yqa = dry gas meter calibration check value, dimensionless.		
0.03 = (29.92/528)(0.75) ² (in. Hg/ ^o /R) cfm ² .		
29.00 = dry molecular weight of air, lb/lb-mole.		
Vm = Volume of gas sample measured by the dry gas meter at meter conditions, dcf.	61.011	58.493
Y = Dry gas meter calibration factor (based on full calibration)	0.9915	0.9915
Delta H@ = Dry Gas meter orifice calibration coefficient, in. H ₂ O.	2.0089	2.0089
avg SQRT Delta H = Avg SQRT press. drop across the orifice meter during sampling, in. H ₂ O	1.1723	1.1588
O = Total sampling time, minutes.	96	96

$$Yqa = (O / Vm) * \text{SQRT} (0.0319 * Tma * 29) / (\text{Delta H}@ * Pm * MWd) * \text{avg SQRT Delta H}$$

$$Yqa = (96.00 / 61.01) * \text{SQRT} (0.0319 * 520.53 * 29) / (2.01 * 30.03 * 28.84) * 1.17$$

$$Yqa = 1.573 * \text{SQRT} 481.543 / 1,739.597 * 1.17$$

Yqa = 0.971 0.988

Diff = Absolute difference between Yqa and Y		
--	--	--

$$\text{Diff} = ((Y - Yqa) / Y) * 100$$

$$\text{Diff} = ((0.9915 - 0.971) / 0.9915) * 100$$

Diff = 2.07 0.35

Average Diff = 1.21

Allowable = 5.0

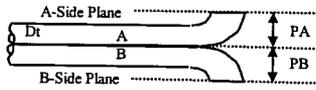
Type S Pitot Tube Inspection Data Form

Pitot Tube Identification Number: P-704

Inspection Date 5/30/18 Individual Conducting Inspection SR

If all Criteria PASS
Cp is equal to 0.84

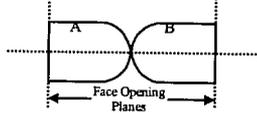
PASS/FAIL



Distance to A Plane (PA) - inches 0.46 PASS
 Distance to B Plane (PB) - inches 0.46 PASS
 Pitot OD (Dt) - inches 0.375

$1.05 D_t < P < 1.5 D_t$

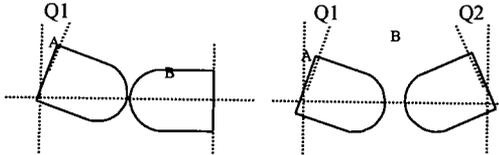
PA must Equal PB



Are Open Faces Aligned Perpendicular to the Tube Axis

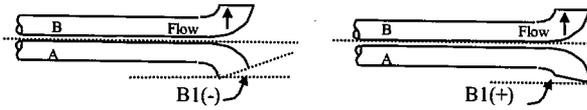
YES NO

PASS

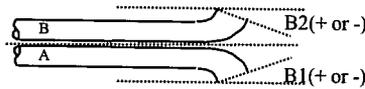


Angle of Q1 from vertical A Tube- degrees (absolute) 0 PASS
 Angle of Q2 from vertical B Tube- degrees (absolute) 0 PASS

Q1 and Q2 must be $\leq 10^\circ$

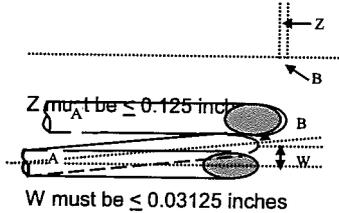


Angle of B1 from vertical A Tube- degrees (absolute) 0 PASS



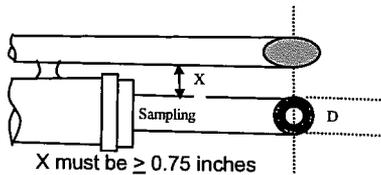
Angle of B1 from vertical B Tube- degrees (absolute) 0 PASS

B1 or B2 must be $\leq 5^\circ$



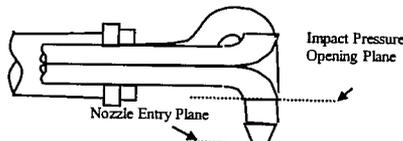
Horizontal offset between A and B Tubes (Z) - inches 0.015 PASS

Vertical offset between A and B Tubes (W) - inches 0.025 PASS



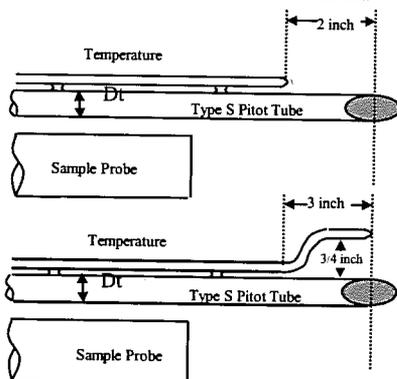
Distance between Sample Nozzle and Pitot (X) - inches 0.79 PASS

X must be ≥ 0.75 inches



Impact Pressure Opening Plane is above the Nozzle Entry Plane

YES NO
 NA



Thermocouple meets the Distance Criteria in the adjacent figure

YES NO
 NA

Thermocouple meets the Distance Criteria in the adjacent figure

YES NO
 NA

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Part Number: E03NI79E15A00E4	Reference Number: 82-401288926-1
Cylinder Number: CC18055	Cylinder Volume: 150.5 CF
Laboratory: 124 - Riverton (SAP) - NJ	Cylinder Pressure: 2015 PSIG
PGVP Number: B52018	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Sep 04, 2018

Expiration Date: Sep 04, 2026

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	9.000 %	8.864 %	G1	+/- 0.7% NIST Traceable	09/04/2018
OXYGEN	12.00 %	12.00 %	G1	+/- 0.4% NIST Traceable	09/04/2018
NITROGEN	Balance			-	

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	13060629	CC413730	13.359 % CARBON DIOXIDE/NITROGEN	+/- 0.6%	May 09, 2019

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA 510-CO2-19GYCXEG	NDIR	Aug 09, 2018
Horiba MPA 510-O2-7TWMJ041	Paramagnetic	Aug 09, 2018

Triad Data Available Upon Request



Signature on file
Approved for Release

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Part Number: E03NI62E15A0224	Reference Number: 82-401044874-1
Cylinder Number: SG9169108	Cylinder Volume: 157.2 CF
Laboratory: 124 - Riverton (SAP) - NJ	Cylinder Pressure: 2015 PSIG
PGVP Number: B52017	Valve Outlet: 590
Gas Code: CO2,O2,BALN	Certification Date: Nov 18, 2017

Expiration Date: Nov 18, 2025

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 600/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
CARBON DIOXIDE	17.00 %	16.58 %	G1	+/- 0.7% NIST Traceable	11/18/2017
OXYGEN	21.00 %	21.00 %	G1	+/- 0.5% NIST Traceable	11/18/2017
NITROGEN	Balance			-	

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	12061336	CC360792	11.002 % CARBON DIOXIDE/NITROGEN	+/- 0.6%	Jan 11, 2018
NTRM	09061415	CC273526	22.53 % OXYGEN/NITROGEN	+/- 0.4%	Mar 08, 2019

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Horiba VIA 510-CO2-19GYCXEG	NDIR	Oct 30, 2017
Horiba MPA 510-O2-7TWMJ041	Paramagnetic	Oct 27, 2017

Triad Data Available Upon Request



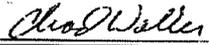
Signature on file
Approved for Release

INTERFERENCE CHECK

Date: 12/4/14-12/5/14
Analyzer Type: Servomex - O₂
Model No: 4900
Serial No: 49000-652921
Calibration Span: 21.09 %
Pollutant: 21.09% O₂ - CC418692

INTERFERENT GAS	ANALYZER RESPONSE		% OF CALIBRATION SPAN ^(a)
	INTERFERENT GAS RESPONSE (%)	INTERFERENT GAS RESPONSE, WITH BACKGROUND POLLUTANT (%)	
CO ₂ (30.17% CC199689)	0.00	-0.01	0.00
NO (445 ppm CC346681)	0.00	0.02	0.11
NO ₂ (23.78 ppm CC500749)	NA	NA	NA
N ₂ O (90.4 ppm CC352661)	0.00	0.05	0.24
CO (461.5 ppm XC006064B)	0.00	0.02	0.00
SO ₂ (451.2 ppm CC409079)	0.00	0.05	0.23
CH ₄ (453.1 ppm SG901795)	NA	NA	NA
H ₂ (552 ppm ALM048043)	0.00	0.09	0.44
HCl (45.1 ppm CC17830)	0.00	0.03	0.14
NH ₃ (9.69 ppm CC58181)	0.00	0.01	0.03
TOTAL INTERFERENCE RESPONSE			1.20
METHOD SPECIFICATION			< 2.5%

^(a) The larger of the absolute values obtained for the interferent tested with and without the pollutant present was used in summing the interferences.


 Chad Walker

INTERFERENCE CHECK

Date: 12/4/14-12/5/14

Analyzer Type: Servomex - CO₂

Model No: 4900

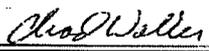
Serial No: 49000-652921

Calibration Span: 16.65%

Pollutant: 16.65% CO₂ - CC418692

INTERFERENT GAS	ANALYZER RESPONSE		% OF CALIBRATION SPAN ^(a)
	INTERFERENT GAS RESPONSE (%)	INTERFERENT GAS RESPONSE, WITH BACKGROUND POLLUTANT (%)	
CO ₂ (30.17% CC199689)	NA	NA	NA
NO (445 ppm CC346681)	0.00	0.02	0.10
NO ₂ (23.78 ppm CC500749)	0.00	0.00	0.02
N ₂ O (90.4 ppm CC352661)	0.00	0.01	0.04
CO (461.5 ppm XC006064B)	0.00	0.01	0.00
SO ₂ (451.2 ppm CC409079)	0.00	0.11	0.64
CH ₄ (453.1 ppm SG901795)	0.00	0.07	0.44
H ₂ (552 ppm ALM048043)	0.00	0.04	0.22
HCl (45.1 ppm CC17830)	0.10	0.06	0.60
NH ₃ (9.69 ppm CC58181)	0.00	0.02	0.14
TOTAL INTERFERENCE RESPONSE			2.19
METHOD SPECIFICATION			< 2.5%

^(a) The larger of the absolute values obtained for the interferent tested with and without the pollutant present was used in summing the interferences.


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Balance ID:

Date	Initials	Calibration Weight	Measured Weight ⁽¹⁾	Maintenance and Adjustments
10/30/17	MPW	500.0	499.8	
10/31/17	MPW	500.0	499.9	
9/5/18	CH	500.0	500.1	
9/13/18	ZA	500.0	500.1	
10/8/18	JDO	500	499.6	NA - SOC
10/9/18	JDO	500	499.7	NA - SOC
10/10/18	JDO	500	499.6	NA - SOC
10/11/18	JDO	500	499.7	NA - SOC
10/23/18	TB	500	499.8	NA - Chem CW
10/24/18	JDO	500	499.0	NA Chem CW
10/25/18	JDO	500	499.8	NA Chem CW
01/07/19	CH	500	499.7	NA Chemours
01/08/19	CH	500	499.7	NA Chemours
01/08/19	CH	500	499.7	NA Chemours
1/15/19	JDO	500	499.6	NA Chem
1/15/19	CW	500.0	499.8	NA Chemours

Weight must be within ± 0.5 grams of calibration weight

APPENDIX E
LIST OF PROJECT PARTICIPANTS

The following Weston employees participated in this project.

Paul Meeter	Senior Project Manager
Jeff O'Neill	Technical Manager
Steve Rathfon	Team Leader
Kyle Schweitzer	Team Member
Jack Mills	Team Member
Chad Walker	Team Member