# BEDROCK GEOLOGIC MAPS, AND FRACTURE AND FAULT DATA FOR PORTIONS OF THE COKESBURY AND NEW HILL 7.5-MINUTE QUADRANGLES, DEEP RIVER TRIASSIC BASIN, WAKE COUNTY, NORTH CAROLINA

by

Richard M. Wooten

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DIVISION OF LAND RESOURCES DEPARTMENT OF ENVIRONMENT, HEALTH AND NATURAL RESOURCES

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Richard M. Wooten

Timothy W. Clark

North Carolina Geological Survey P.O. Box 27687 Raleigh, NC 27611-7687

Timothy L. Davis<sup>1</sup>

North Carolina Geological Survey P.O. Box 27687 Raleigh, NC 27611-7687

<sup>1</sup>Now with: Exxon Production Research Company P.O. Box 2189 Houston, TX 77252-2189

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DIVISION OF LAND RESOURCES Charles H. Gardner Director and State Geologist

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# Bedrock Geologic Maps, and Fracture and Fault Data for Portions of the Cokesbury and New Hill 7.5-Minute Quadrangles, Deep River Triassic Basin, Wake County, North Carolina

by

Richard M. Wooten, Timothy W. Clark, and Timothy L. Davis

### ABSTRACT

Detailed geologic mapping (1:12 to 1:3,750 scale) and structural investigations were conducted in a well-exposed sequence of Triassic age sedimentary rocks in the New Hill and Cokesbury 7.5-minute quadrangles. The rocks studied are exposed in excavations made in the late-1970's for material to construct the auxiliary dam for the Shearon Harris nuclear power plant. These two areas, informally referred to as the north and south borrow pits, expose a heterogeneous siliciclastic sequence of conglomerate, sandstone, siltstone, and mudstone characteristic of the Deep River Triassic basin.

Geologic mapping in the study area reveals stratigraphic marker units, mapand outcrop-scale folding, and four previously unreported faults. Stratigraphic marker units can be traced along strike for up to several hundreds of feet. The main fault, informally referred to here as the south borrow pit fault (SBPF), has a generalized strike of N. 72° W. with a 30° to 70° southwest dip, and has a minimum trace length of 1,400 feet across the south borrow pit. The total displacements along the SBPF and the other faults reported here are not determinable from available data. Two dominant fracture sets occur in the study area: 1) a set striking generally parallel to the SBPF, and 2) a set striking generally north at a high angle to the SBPF.

Kinematic studies suggest two stages of displacement in the study area: 1) normal faulting, and 2) normal and dextral strike-slip faulting. The map-scale fold that characterizes the map pattern of the south borrow pit is interpreted as a hanging wall anticline related to normal faulting along the SBPF during stage 2. Two additional faults, exposed approximately 500 feet apart in the south borrow pit, strike oblique to the SBPF. A fourth fault, near the north borrow pit, strikes N. 35° E. and dips 60° S. These four newly discovered faults, along with other faults previously identified in the area, indicate this portion of the Deep River Triassic basin is a structurally complex zone of intersecting faults.

#### INTRODUCTION

This report presents geologic maps and data collected to date by North

Carolina Geological Survey (NCGS) staff during ongoing geologic investigations of the Deep River Triassic basin (fig. 1). The investigations concentrated on bedrock exposures in two borrow pits west of the Shearon Harris nuclear power plant (fig. 2) near the boundary between the Cokesbury and New Hill 7.5-minute quadrangles, Wake County, North Carolina.

The borrow pits (referred to as the north and south borrow pits) are partly within the proposed Wake/Chatham low-level radioactive waste (LLRW) disposal site and are bounded on the east by the Shearon Harris Reservoir (fig. 2). Excavated in the mid-1970's for clayey soil used to construct the auxiliary dam for the Shearon Harris nuclear power plant, the north and south borrow pits encompass approximately 0.11 and 0.08 square miles (70 and 50 acres) respectively. Although weathered and partly revegetated, the borrow pits contain abundant outcrops allowing detailed geologic mapping.

Geologic mapping (1:2,145 and 1:3,750 scale) in the study area focused on the extent of readily recognizable stratigraphic units and the delineation of major structures and structural trends (plates 1 and 2). During the course of geologic mapping three faults were identified in the south borrow pit and one fault was identified near the north borrow pit. The main fault is referred to here informally as the south borrow pit fault (SBPF) and is the primary focus of the structural analysis in this report. The other faults are informally referred to as faults A, B, and C respectively.

Larger-scale geologic mapping (1:12 to 1:300 scale ), data collection, and structural analyses were conducted at locations 1 through 7 on plate 2, and location 8 on plate 1. These detailed studies were conducted along or near these faults to determine fault kinematics and the characteristics of fractures and other faultrelated structures.

The results of this investigation contribute to two ongoing projects by the NCGS: 1) 1:100,000-scale geologic mapping in the Raleigh 30 x 60-minute quadrangle; and, 2) independent data collection and evaluation related to regulatory oversight of geologically related sections of the Safety Analysis Report for the proposed Wake/Chatham low-level radioactive waste (LLRW) disposal site prepared by Chem-Nuclear Systems, Inc. (1993). The information contained in this report is preliminary, but it is being released since it is relevant to geologic studies of the proposed Wake/Chatham LLRW site.

#### **REGIONAL OVERVIEW**

The Deep River Triassic basin is the southernmost exposed rift basin of Triassic age in eastern North America. This basin is composed of three connected basins. From north to south these are the Durham, Sanford, and Wadesboro Triassic basins (fig. 1).



Figure 1. Physiographic provinces and Triassic rift basins (shaded) of North Carolina in relationship to study area. Key: 1, 2, and 3 - Deep River basin (1 - Durham basin, 2 - Sanford basin, 3 - Wadesboro basin); 4 - Ellerbe basin; 5- Dan River basin; and 6 - Davie County basin.

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**Figure 2.** Generalized geologic map (post-Triassic units not shown) of the southern Durham basin with study area and 7.5-minute quadrangles outlined (modified after North Carolina Geological Survey, 1985). USGS 7.5-minute quadrangle names are shown in lower right corner of each quadrangle.

Rocks of the Deep River Triassic basin are included in the Chatham Group of the Newark Supergroup (Olsen, 1978; Luttrell, 1989; and Olsen and others, 1991). Campbell and Kimball (1923) subdivided the Chatham Group in the Sanford Triassic basin into the Pekin, Cumnock, and Sanford Formations, and their extent was later refined by Reinemund (1955). These formal stratigraphic names are restricted to the Sanford Triassic basin. No formal formations are recognized in the Durham basin; however, several subdivisions are made from lithofacies mapping (Bain and Harvey, 1977; Wheeler and Textoris, 1978; Gore, 1986; Hoffman and Gallagher, 1989). The Chatham Group consists of conglomerate, sandstone, siltstone, claystone, shale, coal (Sanford Basin only), and small amounts of limestone and chert (Durham Basin only) formed in lacustrine, fluvial, and alluvial fan depositional systems (e.g., Hoffman and Gallagher, 1989 and Olsen and others, 1991).

The Deep River basin is a north-northeast trending half-graben, bordered on the east by the Jonesboro fault, a west-dipping, stepped, high-angle normal fault (Bain and Brown, 1980; Olsen and others, 1991). Along the western margin, sedimentary rocks unconformably overlie Late Proterozoic and Cambrian metavolcanic and metasedimentary rocks of the Carolina slate belt (North Carolina Geological Survey, 1985). Faults also form the basin boundary locally along its western border. Sedimentary rocks in the Durham basin generally dip toward the east to a maximum thickness of approximately 6,000 to 7,000 feet (Parker, 1979).

Triassic sedimentary rocks throughout the Deep River Basin are intruded by Early Jurassic diabase dikes and sills. Locally, both Triassic and Jurassic rocks are unconformably overlain by Cretaceous deposits and fossiliferous Eocene outliers of the Atlantic Coastal Plain and Tertiary upland gravels (North Carolina Geological Survey, 1985).

The Durham and Sanford basins are separated by a narrower segment of the Deep River basin commonly referred to as the Colon cross-structure. This narrower segment contains map-scale faults, folds, and clusters of diabase dikes, and is interpreted as a basement high between the Sanford and Durham basins (Campbell and Kimball, 1923, Reinemund, 1955). Further studies are necessary to determine the extent, structural components, and evolution of the Colon cross-structure. The study area lies in the transition between the southern end of Durham basin and the northern extent of the Colon cross-structure (figs. 1 and 2).

Bain and Harvey (1977) and Bain and Brown (1980) conducted regional geologic mapping and fault investigations in the Durham Triassic basin north of the Colon cross-structure. In their model, northeast-trending faults and fracture zones are cross-faulted along north-northwest-trending faults and fracture zones to produce diamond and triangular shaped fault blocks in map view. Additional information on the geology of the Deep River Triassic basin can be found in Parker (1979), Textoris and Robbins (1988), Huber and others (1993), Hu and Textoris (1994), and Textoris and Gore (1994).

#### PREVIOUS AND ONGOING STUDIES

A detailed geologic investigation in the vicinity of the study area was conducted in the early to mid-1970's to support the site characterization and construction of the Shearon Harris nuclear power plant. The Harris fault (plate 1) was identified during excavation for the plant, and was the subject of geologic mapping (1:7,200 scale) of specifically scraped and trenched areas. This geologic information is included in an unpublished report by Ebasco Services, Inc. (1975). Arbogast (1976) studied exposures in the foundation excavations for the Shearon Harris power plant during his geologic investigation of the area.

The Harris fault is now concealed beneath the Shearon Harris nuclear power plant and the Shearon Harris Reservoir. The Harris fault strikes generally eastnortheast and dips steeply to the south. It has a known trace length of nearly 3,000 feet extending from the power plant as far west as the auxiliary dam on the Shearon Harris Reservoir (plate 1 and figure 3). A minimum age of 150 million years for the Harris fault, and evidence for both normal (down-to-the-south) and left-lateral, strike-slip displacement were reported by Ebasco Services, Inc. (1975).

Chem-Nuclear Systems, Inc. has conducted geologic investigations at the proposed Wake/Chatham LLRW site beginning in 1991 (Chem-Nuclear Systems, Inc., 1993). Two faults, informally referred to as the W8 and W82 faults, were identified during characterization of the Wake/Chatham site, and are located approximately 1,000-1,500 feet west of the study area. The confirmed segment of the W8 fault strikes north-northeast and dips towards the west; the confirmed segment of the W82 fault strikes east-northeast (subparallel to the Harris fault) and dips toward the south. Chem-Nuclear Systems, Inc. (1993) interpreted the W8 and W82 faults to be normal faults, and the Harris, W8, and W82 faults to be part of a sinistral Riedel shear system. The east-northeast strike of the W82 fault indicates it may project from its easternmost known location (approximately 1,000 feet west of the study area) into the southern part of the south borrow pit. NCGS mapping to date, however, has not located this fault in the south borrow pit.

Discussions of investigations of the W8 and W82 faults and other geologic aspects of the proposed Wake/Chatham LLRW site are contained in the Safety Analysis Report for the Wake/Chatham site (Chem-Nuclear Systems, Inc., 1993). Further information on these and possibly other faults may result from future investigations at the Wake/Chatham site.

#### METHODS

The base maps for the geologic maps of the north and the south borrow pits (plates 1 and 2) are photocopy enlargements of portions of a 1:6,000-scale (approximate) color aerial photograph. This photograph was produced by enlarging a 1:24,750-scale (approximate) photograph taken by Heart of Carolina Aerial



**Figure 3.** Data location map of the north and south borrow pits showing the distribution of bedding, fault, and fracture measurements. Data is listed in Appendix A.

Surveys, Inc. on October 28, 1989. The scale of the original aerial photograph varies slightly because of differences in the distance between the camera and the ground surface. Additional distortion of scale may have been introduced into the photocopies during the enlargement process; therefore, the scales of the resulting geologic maps shown in plate 1 (1:3,750 scale) and plate 2 (1: 2,145 scale) are also only approximate. Despite the small variations in scale, the color aerial photograph was a useful base map because: 1) outcrops could readily located in the field; 2) color differences in the unvegetated areas aided in the recognition of lithologic units; and, 3) their relatively large scale permitted detailed geologic mapping.

Geologic mapping (data collection and compilation) was conducted by standard techniques (e.g., Compton, 1962). Geologic data were collected from outcrops and shallow, hand-dug test pits. Scraping and sweeping of weathered rock outcrops was needed in many cases to expose the relevant geologic features. A leaf blower was used to remove loose material from some of the scraped outcrops. Bedding, tectonic fracture, and fault orientation data were collected from 96 stations in the borrow pits and near the auxiliary dam spillway (fig. 3) using a Brunton compass. These data are presented in tabular form in Appendices A and B. Fractures considered to be tectonic include those that: 1) have generally planar surfaces; 2) occur in sets; 3) have local or regionally consistent orientations; or, 4) have surface markings indicative of tectonic origin. Structural data were plotted on lower hemisphere, equal-area projections and rose diagrams using a computer code developed by Allmendinger (1995).

The Unified Rock Classification System (URCS), developed by Williamson (1984), was applied at the reconnaissance level to supplement standard geologic classifications with information on the basic engineering properties of the weathered rocks exposed in the borrow pits. The terminology used in the body of this report to describe the weathering state of rock conforms to the URCS. Refer to Appendix C for text and information on the engineering rock mass classification used in this study.

The 1:300-scale map (fig. 4) for locations 1 and 2 (plate 2) along the SBPF was constructed by surveying a baseline with a Brunton compass, a hand-held clinometer, and a 100-foot cloth tape. Locations of the outcrops and test pits used to construct this map were referenced to the baseline by pacing or measuring distances with a tape. The 1:240-scale map for location 4 (plate 2) shown in figure 6 was constructed using a Brunton compass, a hand-held clinometer, and a 100-foot cloth tape to locate outcrops relative to a ground reference point established for the fracture trace map shown in figure 7.

Fracture trace mapping at a scale of 1:12 was conducted over an area of approximately 500 square feet at location 4 (plate 2) using a grid separated into 1-foot-square cells. This mapping is presented as the 1:96-scale map in figure 7. Along and immediately adjacent to the SBPF, a 20-foot by 20-foot semi-permanent grid

(i.e., nails and nylon string) oriented north-to-south by a hand-held Brunton compass was used to facilitate fracture mapping. Elsewhere, a portable 4-foot by 4foot grid constructed of 5/8 inch polyvinyl-chloride pipe and nylon string was used. The portable grid was oriented using a north-to-south baseline extended from the fixed grid area. The portable grid was also used to construct the fracture trace map for figure 12. The traces of all fractures interpreted as tectonic in origin were mapped in each of the grid cells. Orientation data for each of the 300 fractures measured at this location are included in Appendix B and plotted on lower hemisphere, equal-area projections shown in figure 7.

English units of measurement are used to facilitate relating the data contained in this report with data in the Safety Analysis Report prepared by Chem-Nuclear Systems, Inc. (1993) for the proposed Wake/Chatham LLRW disposal site.

# GENERAL STRATIGRAPHY

Exposed in the north and south borrow pits is a heterogeneous, siliciclastic sequence of conglomeratic sandstone, muddy sandstone, siltstone, and mudstone (classified according to Folk 1974, 1980). Basic lithologic descriptions of the mapped rock units are included on the geologic maps (plates 1 and 2).

Geologic mapping in the borrow pits focused on the extent of readily recognizable stratigraphic markers. Conglomeratic sandstone, sandstone, and purple mudstone and siltstone were the three key marker units mapped (plates 1 and 2). In several cases, these marker units were traced for several hundreds of feet. Preliminary stratigraphic analysis of rock units in the study area indicates the thickness of individual stratigraphic units ranges from a few feet to tens of feet. Further studies are necessary to describe the sedimentary features and the stratigraphic aspects of the exposed sequence of rock in more detail.

#### STRUCTURE

#### **BEDDING ORIENTATION**

Geologic mapping of stratigraphic marker units described above resulted in defining a contrast in structural patterns between the north and south borrow pits (plates 1 and 2). Rock units in the north borrow pit generally strike northnorthwest with a gentle (approximately 8° to 25°) east-northeast dip. A small number of exposures show a localized northeast strike of rock units near a northeast-striking fault (referred to as fault C in this report) exposed along the access road to the north borrow pit (location 8, plate 1 and fig. 9). Although map data are limited, significant deflections in the orientation of stratigraphic marker units have not been observed in the north borrow pit near the Harris fault (plate 1).

Geologic mapping in the south borrow pit revealed marked variation in the

strike of rock units, which led to the discovery of the SBPF (plates 1 and 2). The change in orientation of rock units in the south borrow pit can be observed on a traverse from south to north toward the SBPF. This change in strike is discernible on aerial photographs as curved, discontinuous, light-colored bands marking completely decomposed mudstones and siltstones exposed in unvegetated parts of the south borrow pit (plates 1 and 2).

In the southernmost portion of the south borrow pit, rock units generally strike north to north-northeast and dip gently east. Approximately 450 to 600 feet (map distance) south of the SBPF, the strike of the rock units changes to the northwest and dip direction changes to the northeast. This northwest strike of rocks persists to within 35 to 50 feet of the SBPF, where locally the strike changes to the north-northeast. These changes in the orientation of rock units delineate faultrelated, map-scale anticlinal folding and outcrop-scale synclinal folding in the hanging wall of the SBPF. These folds are interpreted to be longitudinal folds subparallel to the associated fault as discussed in Schlische (1995).

Geologic mapping also indicates that immediately north of the SBPF, bedding strike changes from northeast to northwest near the drainage separating the borrow pits (plate 1 and fig. 3). This change suggests the possibility of additional faulting and fault-related folding (i.e., an east-plunging anticline) in the vegetated area between the borrow pits. The general strike of the SBPF parallels the trend of the drainage separating the north and south borrow pits suggesting a possible structural control on the drainage.

### FAULTS

#### South Borrow Pit Fault

The SBPF was identified at several exposures in the south borrow pit (locations 1, 2, 3, 4 and 7, plate 2). The generalized strike of the SBPF is N. 72° W. with dips ranging from 30°-70° S. The SBPF has a minimum trace length of approximately 1,400 feet based on known exposures and exhibits a "right-stepping" pattern across the south borrow pit with hanging wall (south side) and footwall (north side) components. The general west-northwest strike of the SBPF contrasts with the general east-northeast strike of the Harris fault.

Larger-scale geologic mapping (1:300 scale) at the westernmost exposure of the SBPF in the south borrow pit (locations 1 and 2, plate 2 and fig. 4) shows the orientation of the fault's map trace varies from N. 80° E. to N. 50° W. over a strike distance of about 200 feet. The dip of the fault plane ranges from 40° S. to vertical in this area. Figure 4 also illustrates the truncation of map units by the SBPF, and outcrop-scale synclinal folding on the hanging wall (south) side of the SBPF similar to that observed at location 4 (plate 2) and shown in figures 6 and 7.

Geologic mapping (1:24 scale) shown in figure 5 (location 2, plate 2) illustrates structures between two splays of the SBPF comprised of clayey gouge and breccia. Between these two splays, lithologic contacts and associated fractures are deformed into sigmoidal shapes resembling those expected in a Riedel shear model (inset diagram, fig. 5). Sigmoidal sandstone bodies with the same sense of asymmetry were also observed at locations 4 and 7 (plate 2).

Rocks in the SBPF exhibit fabrics characteristic of fault rock produced during brittle to semi-brittle faulting as described by Sibson (1977) and McClay (1987). These fabrics in the SBPF fault rocks include breccia, foliated breccia and clayey gouge. Random-fabric breccias with clasts up to 2.5 feet in length are derived from clastsupported rocks, whereas foliated breccias containing numerous hand specimenscale slip surfaces are more typical in matrix-supported rocks. clayey gouge ranges in color from red-brown to tan to pale gray. Breccias are typically red to red-brown. Black to dark gray oxide staining on fractures and mineral grains commonly occurs in rocks adjacent to the fault.

### Fault A

Fault A is a northeast-striking fault with a nearly vertical to steep easterly dip that crops out in the south borrow pit at location 4 (plate 2). The southern end of this fault terminates against the SBPF (fig. 6) and the northern end is covered by recent slope wash deposits. Evidence for fault A has not been identified in the north borrow pit, or elsewhere in the south borrow pit. Figure 6 shows a geologic map and cross sections of field relationships at location 4.

Fault A is characterized by partially to completely decomposed foliated breccia, random-fabric breccia and contorted beds. Foliated mudstone and siltstone breccia with local discontinuous sandstone lenses and blocks are the predominate fault zone rocks. Aligned blocks and lens-shaped bodies of sandstone and siltstone within the foliated mudstone breccia locally define intervals of compositional layering. The interval of contorted bedding and brecciated rock comprising the fault zone ranges in width from 3 to 10 feet and can be traced for approximately 110 feet along strike. Small scale folds with curved axial planes and northeast plunging fold axes occur within the fault zone. These folds are typically truncated by offsets within the fault zone (inset C, fig. 6).

Small-scale folds and contorted beds also occur along both the northwest and southeast margins of fault A. Drag folding (cross sections X-X' and Y-Y', fig. 6) indicates a component of normal displacement (down to the southeast). The strike of the foliation and compositional layering within the fault zone is generally oblique to the strike of the fault in map view. This angular relationship and the northeast-trending folds within the fault zone suggest a dextral strike-slip component of displacement, possibly associated with reactivation of fault A during movement along the SBPF. The amount of displacement along fault A has not



Figure 4. Geologic outcrop map (1:300 approx. scale) of the south borrow pit fault (SBPF) at locations 1 and 2 (plate 2). Inset A - map area for figure 5.



Figure 5. Geologic map (1:24 scale) showing internal structures between two splays of the south borrow pit fault (SBPF) exposed at location 2 (plate 2). Deformed and truncated beds occur between two fault splays defined by clay gouge, breccia, and foliated breccia. The sigmoidal shape of the lithologic contacts and associated fractures (bold lines) between the splays indicates a dextral sense of shear consistent with the Riedel shear model shown in the inset diagram (inset modified from McClay (1987)). Fault splays converge to the northwest (see figure 4).



**Figure 6.** Geologic map (1:240 scale) and cross sections showing structural relationships at location 4 (plate 2) where fault A terminates against the south borrow pit fault (SBPF). Inset A - fracture trace map area for figure 7. Inset B - detail of the fault fabric where fault A terminates against the SBPF. Inset C - schematic detail of deformation patterns within fault A.



**Figure 7.** Fracture trace map (1:96 scale) and lower hemisphere equal-area projections of the south borrow pit fault (SBPF), bedding, and fracture data from location 4 (plate 2). Map area is divided into domains I, II, III, and IV based on changes in bedding strike. Projections include: fault and bedding orientations (great circles) and fractures (poles to planes); Set A fractures (filled circles); and Set B fractures (filled squares). Data for projections are listed in Appendix B. Inset A - map area for figure 12. Inset B - lower hemisphere equal area projection of bedding and fault orientations (great circles) and synclinal fold hinge orientation (beta) from the detailed fracture trace map area.

been determined. The termination of fault A against the SBPF indicates the main displacement along fault A occurred prior to displacement along the SBPF.

## Fault B

Fault B crops out in a gully near the shore of Shearon Harris Reservoir at location 5 (plate 2) in the south borrow pit. Fault B strikes N. 20°-25°W. and dips 85°-90° W. and can be traced in outcrop about 80 feet along strike. The intersection of fault B with the SBPF is not exposed; therefore, relative age relationships between the faults could not be determined. Figure 8 shows a sketch of fault B exposed in a scraped and cleaned gully outcrop.

Fault B is marked by the contact between a completely decomposed, tan, finegrained sandstone with purple mottling in the footwall (east) side of the fault, with a sequence of partially to completely decomposed, red to red-brown, and purple mottled sandstones and mudstones in hanging wall (west) side of the fault. Foliated mudstone breccia and breccia (sandstone clasts in a mudstone matrix) characterize the fault zone and are less than 8 inches thick.

Rocks adjacent to and within the fault are intensely fractured with a fracture spacing generally less than 2 inches. Numerous high-angle fractures subparallel the strike of the fault and contain a white clayey infilling. Northwest-striking fracture sets subparallel to fault B also occur in borrow pit outcrops immediately southwest of location 5 (plate 2). Unequivocal kinematic indicators such as slip surface markings, drag folds or other folds were not observed in the vicinity of fault B. Fault B is interpreted as a normal fault (down to the southwest) given no direct evidence to the contrary, and the generally accepted extensional setting for the Deep River Triassic basin.

### Fault C

Fault C is exposed in a ditch outcrop of completely decomposed rock along the access road to the north borrow pit (location 8, plate 1). The fault zone is a 10-13 inch wide foliated breccia with gravel-sized clasts in a foliated mudstone matrix. This interval is distinguished by thin (<2 inch thick), alternating red, tan, and gray color bands. The fault has a generalized strike and dip of N. 35°E. 60°S. Figure 9 shows a schematic geologic sketch map depicting the structural features in the outcrop at location 8 (plate 1).

Several outcrop-scale folds within a red-brown mudstone with tan siltstone laminae crop out in the hanging wall (southeast) side of fault C. The fold axes of this series of small-scale anticlines and synclines generally plunge east with axial planes overturned slightly toward the north. These folds are interpreted as contractional features in the hanging wall indicating left-lateral and possibly a reverse component of displacement along fault C.



**Figure 8.** Geologic block diagram (1:12 approx. scale) showing vertical and horizontal section of fault B where it was excavated in a gully at location 5 (plate 2). The fault zone is characterized by completely decomposed, redbrown to purple-gray mudstone breccia and foliated mudstone breccia, with inclusions of red fine-grained sandstone clasts. The fault zone is bounded by 0.5-2.0 inch wide fractures with white clayey infilling.



**Figure 9.** Geologic sketch diagram (1:24 approx. scale) of structural features related to fault C in a scaped and cleaned ditch outcrop of completely decomposed rock at location 8 in the north borrow pit (plate 1). The fault zone is a 10-13 inch wide foliated breccia (foliated mudstone matrix with gravel-sized clasts) distinguished by thin (< 2 inch thick) alternating red, tan, and gray color bands. Small scale folds with east-plunging axes occur on the hanging wall (southeast side) of fault C.

Exposures of fault C could not be traced beyond the outcrop at location 8. Bedding strike ranges from northeast to northwest, and bedding dip direction changes from west to east along the access road to the spillway (to the northeast) and along the access road to the north borrow pit (to the south). These variations in the orientation of bedding suggest fault C extends from location 8 (plate 1) along strike to the northeast and southwest. It is possible fault C is related to structures in the area where the W8 fault to the west meets the Harris Fault to the north.

# FRACTURES

Fracture investigations included collection of fracture data across the borrow pits and vicinity, and a detailed study of fractures at location 4 (plate 2 and fig. 7) along the SBPF. This section of the report briefly discusses the results of these investigations.

The majority of fracture data collected across the study area provides basic information on the orientation of the dominant fracture sets observed. Investigations of fracture intensity and spacing, crosscutting and termination relationships, modes of fracture development, and relationships to local and regional structures are only briefly discussed here.

# **General Fracture Characteristics**

Both tectonic and non-tectonic fractures occur in most outcrops in the study area. Fractures attributed to tectonism typically are planar, occur in sets, and generally form systematic, rectilinear patterns in plan view (figs. 7 and 10). Fractures attributed to weathering are typically non-systematic and form curving and polygonal patterns.

Throughout the study areas fractures typically have a gray to pale green clayey infilling, or bleached zones parallel to the fracture surfaces. Black manganese oxide, and rust-colored iron oxide staining along fracture surfaces is common.

The orientation of tectonic fractures varies across both borrow areas as can be seen in plates 1 and 2, and rose diagrams and lower hemisphere equal-area projections shown in figure 11c-f. General fracture populations, however, can be discerned from the data. For example, fracture orientation data from the north borrow pit (figs. 11c and 11e) cluster around north-northwest and east-northeast strikes. The east-northeast fractures generally parallel the strike of the Harris fault. North-northwest fractures group along a similar trend as bedding azimuths (compare figs. 11a and 11c). Field observations in the north borrow pit indicate: 1) the spacing between east-northeast-striking fractures generally decreases with proximity to the Harris fault; and 2) north-northwest-striking fractures occur throughout the north borrow pit.



**Figure 10.** Photograph of fracture patterns in a completely decomposed outcrop ~100 feet south of the surface trace of the south borrow pit fault (SBPF) at location 6 (plate 2). Fractures are highlighted by a white clay infilling and bleached zones. Two fractures sets predominate: Set A oriented N.80<sup>0</sup>-85<sup>0</sup>W.  $75^{0}$ -90<sup>0</sup>S., sub-paralled to the strike of the SBPF; and Set B oriented N.10<sup>0</sup>-26<sup>0</sup>E. ~ 90<sup>0</sup>E. Termination relationships determined from this photograph for Set A and Set B fractures in 70 cases are: Set A terminates against Set B, n=32; Set B terminates against Set A, n=29; and, Sets A and B cross or relationships indeterminate, n=9. The roughly equal numbers of Set A terminations against Set B as Set B terminations against Set A suggests that here Sets A and B are coeval. The thicker zone of white clay striking NW. across the photograph marks the NE-dipping contact between a conglomeraic sandstone (css) and siltstone (si). Area shown in photograph about 9 feet by 13 feet, Brunton compass for scale.

In the south borrow pit, the orientations of fracture populations are more variable than in the north borrow pit (compare figs. 11c and 11d). Fracture populations in the south borrow pit cluster around north-northeast, northwest and west-northwest azimuths (figs. 11d and 11f). Fracture populations in the south borrow pit generally correspond to similar groupings in bedding azimuths (compare figs. 11b and 11d); however, most northeast-striking beds in the south borrow pit occur on the footwall (north) side of the SBPF. Fracture population also group around similar azimuths as the faults exposed in the south borrow pit (compare figs. 11d and 11f).

North-northeast- and particularly west-northwest-striking fractures are commonly observed in the vicinity of the SBPF. The outcrop shown in figure 10 is located about 100 feet south of the surface trace of the SBPF, and illustrates the general pattern. Here fractures are highlighted by a light gray, clayey infilling as well as bleached zones along the fracture planes. Two fracture sets predominate: 1) a set oriented N. 85° W. 75°-90° S., sub-parallel to the strike of the SBPF; and 2) a set oriented N. 10-26° E. ~90°, at a high angle to the SBPF. Field observations in the south borrow pit also indicate that fractures oriented sub-parallel to the strike of the SBPF generally increase in frequency near the fault.

#### **Fracture Trace Mapping**

This section presents the results and discussion of a detailed fracture investigation based on 1:12-scale fracture trace mapping of an exposed bedrock pavement at location 4 (plate 2) along the SBPF (figs. 6 and 7). This mapping focused on structures of the hanging wall rocks of the SBPF in an effort to understand the distribution and characteristics of fractures adjacent to the fault. Fracture trace mapping in the footwall of the SBPF is limited to that shown in figure 12. Fracture trace mapping permits evaluation of fracture orientations as well as their trace lengths, spatial distribution, interconnections, and crosscutting relationships. Fracture trace mapping is an important component in evaluating the geology and hydrology of fractured rock settings (e.g., Barton and others, 1993; La Pointe and Hudson, 1985).

The fracture trace map shown in figure 7 contains three distinct rock units; one rock unit in the footwall and two rock units in the hanging wall. The footwall rock unit is a brown to red, medium- to coarse-grained sandstone. Hanging wall rock units include a purple mudstone overlain by a fine-grained, red to brown, sandstone. Fracture trace mapping and fracture descriptions were restricted to the fine-grained sandstone unit in the hanging wall of the SBPF. The stratigraphic thickness of the fine-grained sandstone is less than 1 foot.

The strike and dip of rock units in the fracture trace map area (figs. 6 and 7) departs from the general map pattern of the southern borrow pit. In the southernmost portion of the pavement, farthest away from the SBPF, the rock units



**Figure 11.** Rose diagrams and lower hemisphere equal-area stereonet projections of structure data from the north and south borrow pits: a) bedding azimuths, north borrow pit; b) bedding azimuths, south borrow pit; c) fracture azimuths, north borrow pit; d) fracture azimuths, south borrow pit; e) fractures (poles) and fault planes (great circle), north borrow pit; f) fractures (poles) and fault planes (great circle), north borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow pit; f) fractures (poles) and fault planes (great circle), south borrow planes (great circle), south



**Figure 12.** Detailed geologic map (1:15 scale) and lower hemisphere equal area projections of structures in the footwall of the south borrow pit fault at location 4 (plate 2).

strike northwest and dip to the northeast. Near the center of the map area, rocks strike approximately north and dip gently to the east; in the northernmost portion of the pavement, near the SBPF, hanging wall rock units strike northeast and dip gently to the southeast (fig. 7). This change in bedding strike across the map defines an outcrop-scale syncline within the hanging wall of the SBPF. The beta diagram constructed from bedding data defines a fold axis of N. 83° E. 9° (inset B, fig. 7). The hanging wall portion of the fracture trace map has been divided into four domains (I, II, III, and IV) based on the change in bedding strike across the map area.

Hanging Wall Structures. Two primary fracture sets occur in the hanging wall of the SBPF at the fracture trace map location (fig. 7). These include a set striking nearly parallel to the strike of the SBPF (Set A) and a set at a high angle to the SBPF (Set B). A discussion of the fracture properties of both sets of fracture follows and is summarized in table 1.

Both fracture sets have steep dips, generally greater than 80°. Set A maintains a constant strike sub-parallel to the strike of the SBPF. The strike of Set B, however, changes across the fracture trace map area. The fracture map and corresponding equal-area stereonet projections (fig. 7) show a change in orientation of Set B from north-northwest in domains I and II to north-northeast in domains III and IV. This change to a more northeast strike of Set B, when approaching the SBPF from the south, mimics the change in strike of the bedding units previously discussed.

Individual fractures within Set A generally have a very linear surface trace, whereas Set B fractures have a more undulatory surface trace. Within the finegrained sandstone, the trace length of Set A ranges from inches to several feet. The trace length of individual fractures within Set B ranges from inches to tens of feet.

Spacing of Set A fractures is relatively consistent across most of the fracture trace map area and is approximately 8 to 12 inches. In domain I, the spacing of Set A fractures appears somewhat smaller on the order of 4 to 6 inches. The spacing of Set B is highly variable across the area, but in general is on the order of 12 to 24 inches. A green-gray, clayey infilling was observed in many fractures in the detailed study area. Field observations indicate this green-gray infilling occurs more often in Set B. Fracture surfaces of both sets commonly have a white-to-pale green surface coating or bleaching.

Fractures in the trace map area do not possess abundant surface markings or other features to aid in evaluating the mode of fracturing (i.e., modes I, II, or III; see Pollard and Aydin, 1988). Pinnate or feather structures (e.g., Hancock, 1985) indicating a shear component, were observed on several Set A fractures indicating a shearing mode. Surface markings such as plumose structures (e.g., arrest lines, hackle marks) indicative of an opening mode were rarely observed on fractures in the trace map area. A systematic and detailed analysis of individual fracture surfaces will be necessary to fully evaluate the mode(s) of fracture formation. Fracture crosscutting and fracture termination relationships in the hanging wall suggest Set A fractures, which parallel the SBPF, are generally younger than Set B fractures. This conclusion is based on several observations: 1) Set A terminates against Set B in many cases; 2) Set A fractures locally offset Set B fractures; and, 3) the strike of Set B fractures changes orientation near the SBPF similar to the stratigraphic units defining the outcrop-scale syncline at location 4. In contrast, the strike of Set A fractures maintains a constant orientation across the fracture trace map area. These facts indicate Set B fractures were deformed during folding of the outcrop-scale syncline, whereas Set A fractures were unaffected by this folding (fig. 7).

**Table 1.** Summary table of fracture properties for fracture Sets A and B in the fracture trace map area in the hanging wall of the the SBPF shown in figure 7 (location 4, plate 2).

	FRACTURE SET A	FRACTURE SET B
Strike Dip Surface Trace Trace Length Spacing Infilling Wall Bleaching Structures Terminations Offsets	WNW uniform >80° - mainly S. linear <0.5 ft to ~ 6.0 feet 4 to 12 inches clayey, green-gray white to green pinnate and feather mainly A against B A offsets B	NNWNE variable >80° - variable undulatory <0.5 ft to ~10.0 feet 12 to 24 inches clayey, green-gray (more common) white to green not observed few B against A
Mode Relative Age	opening and shearing A mainly younger than B	opening and shearing (?) some B coeval with A

**Footwall Structures.** Detailed mapping in the footwall portion of the fracture trace map area was limited to an 8 foot by 8 foot area immediately north of the SBPF at location 4 (plate 2) in a medium- to coarse-grained sandstone. The footwall structures contrast with those in the hanging wall portion of the map (figs. 7 and 12). For example, the pervasive, rectilinear hanging wall fracture Sets A and B were not observed in this portion of the footwall. Footwall structures and their orientations are shown in a 1:15-scale map (fig. 12) and the attributes of several of these features are briefly discussed below.

Fractures a, b, and c have a general northeast strike and are vertical. They have undulating surfaces, with a relatively wide, green-gray clayey infilling (up to green-gray clay. These fractures bound blocks of sandstone containing unfilled fractures of various orientations. Fractures d-i strike nearly east and are vertical. These fractures have relatively planar surfaces with 0.5 inch-wide, green-gray clayey infilling. These fractures terminate abruptly against fracture c and the feature  $\Sigma$ .

Fractures j and k strike nearly parallel (N. 70° W.) to the SBPF with a steep dip. Fracture j has a variable aperture which is partly filled with a green-gray, clayey material. Associated with j are minor fractures oriented N. 40°-50° W. Also associated with j are asymmetric, clayey bodies. Fracture k is nearly vertical with a variable aperture with a green-gray, clayey infilling. The orientation of fracture k changes from a strike nearly parallel to the SBPF to a northeast strike near feature  $\Psi$ . Feature  $\Psi$  on the map is an asymmetric-shaped block of sandstone bounded by fractures.

Feature  $\Sigma$  is a folded green-gray, clayey layer. The fold has a 90° plunge with an axial plane oriented N. 45° E. 90°. The fold is asymmetric with a sense of vergence towards the east-southeast.

Structure  $\Omega$  includes five curving fractures (labeled 1-5 on figure 12) that terminate against the SBPF. The angle between these fractures and the SBPF decreases from northwest to southeast, with fracture 1 having the largest angular difference of 64° and fracture 5 having the smallest angular difference of 28°.

#### DISCUSSION

Geologic mapping and structural analyses at locations 2, 4, 6, and 7 (plate 2) suggest at least two stages of faulting with associated folding and fracturing are represented by structures in the study area. Fault A, the northeast-striking fault terminating against the SBPF at location 4 (plate 2), represents normal faulting during stage 1. Stage 1 faulting is interpreted to be associated with longitudinal faulting and tilting of beds within the Deep River Triassic basin. Stage 2 represents a later phase of transverse faulting along the SBPF involving both normal and dextral strike-slip components of displacement that produced map-scale anticlinal folding and outcrop-scale synclinal folding in the hanging wall of the SBPF.

Table 2 shows the interpreted genetic relationships between structures, dominant fracture sets, and tectonic processes for features in the study area whose relative ages could be constrained by field data. Figure 13 shows a simplified schematic diagram for the proposed kinematic model. Faults B and C are not included in this model because their relationships to fault A and the SBPF could not be determined from the available data.

**Table 2.** Table relating structures, primary fracture sets, and tectonic processes for features in the study area whose relative ages could be interpreted from field relationships.

	STRUCTURES	PRIMARY FRACTURE SETS	TECTONIC PROCESSES
Stage 1	Fault A: NEstriking normal faulting	N. to NEstriking opening mode fractures	basin opening, longitudinal faulting, bed tilting
Stage 2A	SBPF: WNWstriking normal faulting, hanging wall anticline	Estriking opening mode fractures	transverse faulting, map-scale folding
Stage 2B	SBPF: WNWstriking dextral strike-slip faulting, hanging wall syncline	E. and Nstriking shearing mode fractures	transverse faulting, outcrop-scale folding, reactivation of fault A

# STAGE 1

We interpret the early movement along fault A to be normal displacement, longitudinal to the Deep River Triassic basin and antithetic to the Jonesboro fault (figs. 2 and 13). Although kinematic indicators for fault A are limited, features interpreted as drag folds (cross sections X-X' and Y-Y') indicate normal movement (down to the east).

Early movement along fault A predates displacement along the SBPF, which cross-cuts fault A (fig. 6). The majority of north-striking fractures throughout the study area are attributed to stage 1 processes related to extensional, longitudinal faulting and the eastward tilting of beds that predates transverse faulting along the SBPF. At location 4 (plate 2), north-striking fractures (Set B, fig. 7) generally predate east-striking fractures (Set A, fig. 8) associated with the SBPF. The general change in the orientation of north-striking fractures to a more northwest strike along a south-to-north traverse across the south borrow pit mimics the change in the orientation of the beds forming the anticline in the hanging wall of the SBPF (plate 2). This parallel change in the orientation of bedding and fractures further supports the interpretation that a north-striking fracture set predates the SBPF.

# **STAGE 2**

Stage 2 corresponds to movement along the SBPF transverse to the strike of the Deep River Triassic basin. Our structural analysis suggests displacement along the SBPF involved both normal, and dextral strike-slip components (fig. 13). Normal displacement along the SBPF resulted in the map-scale anticline in the hanging wall of the SBPF (plate 2), and the corresponding east-striking, opening mode fractures. Dextral strike-slip movement along the SBPF resulted in the outcrop-scale synclines at locations 1 and 4 on plate 2 (figs. 4, 6, and 7), and the corresponding east-striking, shearing mode fractures. The relative timing of the normal and strike-slip movement along the SBPF could not be determined conclusively from the available data. The 70° rake measured on southwest plunging slickenlines on a fault plane oriented N. 85° W. 57° S. (location 7, plate 2) indicates a phase of synchronous dip-slip and dextral strike-slip displacement on the SBPF.

#### **Stage 2 Normal Faulting**

The interpretation that the map-scale anticlinal folding is related to normal faulting is consistent with the style of extensional basins such as the Deep River Triassic basin. Concentration of deformation in the hanging wall is commonly observed along normal faults, and particularly in cases where rollover structures are formed (e.g., Davis, 1984; Hatcher, 1995).

Fractures in the hanging wall portion of the fracture trace map area (fig. 7)

# Stage 1:

- Longitudinal basin faulting (Fault A)
- Tilting of beds
- Formation of north-striking, opening-mode fractures.

![](_page_30_Picture_4.jpeg)

# Stage 2:

- Transverse basin faulting
- Initial formation of south borrow pit fault (SBPF).
- East-striking, opening mode fractures

#### Stage 2A:

- Normal faulting
- Formation of map-scale, hanging wall anticline.
- East-striking, opening mode fractures.

Stages 2A and 2B may be coeval.

#### Stage 2B:

- Continued movement along •SBPF.
- Dextral, strike-slip faulting;
- Formation of outcrop-scale, hanging wall syncline.
- East- and north-striking shearing mode fractures.

Stages 2A and 2B may be coeval.

**Figure 13.** Schematic diagram showing a possible kinematic model for the south borrow pit fault and associated structures.

also provide information about displacement along the SBPF. Field observations indicate the east-striking Set A fractures occur more commonly in the hanging wall than the footwall of the SBPF. This fact, and their orientation parallel to the SBPF, is consistent with their origin as opening mode fractures in the hanging wall of a normal fault. The concept of normal displacement along the SBPF is further supported by east-striking Set A fractures that offset north-striking Set B fractures with a normal sense of displacement observed at location 4 (plate 2).

The map pattern produced by the hanging wall anticline could also have been produced by drag folding related to reverse faulting, or sinistral strike-slip faulting along the SBPF. Aside from the geometry of the map-scale fold, no evidence for reverse faulting or sinistral strike-slip faulting was observed along the SBPF. Previous studies in the Deep River Triassic basin (e.g., Reinemund,1955) have not documented significant reverse or thrust faulting. Thrust faults were observed in trenches at the proposed Wake/Chatham LLRW site, but are generally interpreted to be very minor in significance (Chem-Nuclear Systems, Inc., 1993). A component of sinistral strike-slip displacement was reported by Ebasco Services, Inc. (1975) along the Harris fault and Chem-Nuclear Systems, Inc. (1993) presented evidence for sinistral strike-slip displacement on the W82 fault.

#### Stage 2 Strike-slip Faulting

Kinematic indicators at locations 2, 4, and 7 (plate 1) as well as the "rightstepping" outcrop pattern (see McClay, 1987) of the SBPF, indicate evidence for a component of dextral strike-slip or dextral-normal oblique faulting along the SBPF. Evidence for dextral strike-slip faulting occurs in both the hanging wall and footwall of the SBPF.

The geometry of the outcrop-scale syncline in the hanging wall of the SBPF at location 4 (plate 2) shown in figures 6 and 7 suggests it formed by drag related to dextral strike-slip faulting. This fold geometry, however, could also be explained by drag during normal faulting. The orientation of the fold hinge (N. 83° E. 9°) for this structure, however, appears to more consistent with the shortening direction expected in a dextral strike-slip system. The orientation of pinnate structures on several east-striking, Set A fractures are consistent with fracture formation during dextral strike-slip faulting. In addition, some north-striking, Set B fractures are offset in a dextral sense by Set A fractures. The change in orientation of north-striking fractures in the outcrop-scale syncline (Set B, fig. 7) is also consistent with the concept of dextral strike-slip displacement.

The asymmetry of sigmoidal-shaped sandstone bodies observed at location 2 (fig. 5) and locations 4 and 7 also suggest dextral strike-slip faulting. In addition, the geometry of fractures at location 2 are consistent with orientation of fractures expected in a dextral, Riedel shear system (inset, fig. 5). The sigmoidal shape and asymmetry of the sandstone body at location 2, however, can also be explained by a sandstone body bounded by two closely spaced, normal faults. Termination relationships between east-striking, Set A fractures and northstriking, Set B fractures observed in outcrop at location 6 (plate 2) and summarized in figure 10 indicate that at some locations the two fracture sets may have developed simultaneously during movement along the SBPF. Similarly, at location 4 (plate 2) a limited number of Set B fractures terminate against Set A fractures. Given these indications of overlapping development, some northstriking fractures may be localized shearing mode fractures developed during strikeslip movement along the SBPF (i.e.,  $R_2$  Riedel fractures).

Structural features observed in the footwall of the SBPF also suggest dextral strike-slip displacement along the SBPF (fig. 12). Fractures at location j, and structures  $\Psi$ ,  $\Omega$ ,  $\Sigma$  are particularly illustrative. The fractures at location j in figure 12 are interpreted as pinnate fractures or conjugate shear fractures and their geometry and sense of displacement are consistent with dextral shearing. Likewise, the asymmetry (S-shape) of the sigmoidal clay-filled fractures associated with structure  $\Psi$  also suggest dextral shearing. Structure  $\Psi$  is interpreted as a fault bounded block (e.g., horse block). The S-shape asymmetry of this block also supports dextral strike-slip shearing.

Structure  $\Omega$  is interpreted as a contractional strike-slip duplex similar to those described by Woodcock and Fischer (1986) and also indicates a dextral sense of displacement. The duplex comprises fractures (1-5 on fig. 12), interpreted as faults, that sole into the SBPF. The angle between each fault and the SBPF increases from fault 5 to fault 1. This change in angle is interpreted to reflect the steepening of earlier faults (e.g., 1) because of emplacement of later faults (2-5) during a forward-breaking sequence similar to that observed in foreland thrust systems.

The formation and geometry of the folded clayey layer ( $\Sigma$  on figure 12) is likely to be related to the duplex structure  $\Omega$ , similar to fault related folds developed in foreland thrust systems. The geometry of the folded clayey layer  $\Sigma$ , including its vertically plunging fold hinge, the axial surface orientation (N. 45° E. 90°), and the sense of asymmetry or vergence suggests dextral strike-slip displacement.

#### **KINEMATIC MODEL**

Based on available data and the interpretations presented above we suggest a kinematic model for the study area that includes normal faulting (fault A) during stage 1, and a combination of normal and dextral strike-slip faulting (SBPF) during stage 2. It is likely stage 2 displacement occurred during a single deformation event with components of normal, dextral, and dextral-normal oblique displacement occurring at different locations and relative times along the SBPF during this event (fig. 13). The sense of drag observed in the map- and outcrop-scale folds along the SBPF is a function of the geometry between the attitude of the stratigraphic marker units and the SBPF. This requires that stratigraphic markers were either tilted eastward prior to displacement or the entire area was tilted after faulting had

occurred. In our model, the eastward tilting of the beds is associated with stage 1 longitudinal faulting.

The total displacements along the SBPF and other faults reported here are not determinable from the available data. We interpret the relative magnitude of normal displacement along the SBPF to be greater than the magnitude of strike-slip displacement given the hanging wall anticline (inferred to be the result of normal displacement) is a map-scale feature in contrast to the smaller, outcrop-scale synclines related to strike-slip movement.

This basic kinematic model accounts for the map patterns and structural features observed at the surface in the south borrow pit. A northwest-striking normal fault (fault B) and a northeast-striking reverse(?), sinistral strike-slip fault (fault C) were identified in the study area. Further work will be required to determine any relationships of these structures to fault A and the SBPF.

## SUMMARY

Geologic mapping of Triassic-age rocks at two very well exposed areas in the New Hill and Cokesbury 7.5-minute quadrangles identified stratigraphic marker units, map and outcrop-scale folding, and four previously unreported faults. The results of this investigation are summarized as follows:

- Mappable stratigraphic marker units within a heterogeneous, siliciclastic sequence include conglomeratic sandstone, (muddy) sandstone, siltstone, and mudstone. Some stratigraphic units, even some less than six feet thick, can be traced along strike for several hundreds of feet in the map area.
- Three faults were identified in the south borrow pit (SBPF, faults A and B) and one fault (fault C) was identified in the north borrow pit. The south borrow pit fault (SBPF) strikes nearly east-west, dips south, and has a minimum trace length of 1,400 feet across the south borrow pit. Faults A, B, and C are high-angle faults that strike oblique to the SBPF. Fault A terminates against the SBPF. Further studies are needed to identify the extent and other possible structural components of these faults, and to resolve their tectonic relationships.
- A map-scale fold in the hanging wall of the SBPF is interpreted as a hanging wall anticline developed during normal displacement along the SBPF. This map-scale folding resulted in northwest-striking beds that differ from the overall north- to northeast-striking map units defined by previous work in the area. The outcrop-scale folds in the hanging wall of the SBPF are interpreted as synclinal folds developed during dextral strike-slip movement along the SBPF.

- Numerous kinematic indicators suggest components of normal and dextral strike-slip movement along the SBPF. The relative magnitude of normal displacement along the SBPF is interpreted to be greater than the magnitude of strike-slip displacement. The total displacements along the SBPF and other faults reported here are not determinable from the available data.
- Limited data and analyses indicate both normal and dextral strike-slip components of displacement along fault A. The dextral strike-slip component of displacement may be associated with reactivation of fault A during movement along the SBPF. Movement along fault B is interpreted as normal. Displacement along fault C is interpreted to have both reverse and sinistral components.
- Two dominant fracture sets are observed in the study area. One east-striking set is sub-parallel to, and genetically related to the SBPF. The other set strikes generally north, oblique to the SBPF, and is interpreted to have formed primarily prior to movement along the SBPF. Some of the fractures oblique to the SBPF appear to have formed at the same time as those fractures sub-parallel to the SBPF.
- In general, the spacing of fractures parallel to the the SBPF decreases with proximity to the fault. Adjacent to the SBPF the spacing is on the order of 4 to 12 inches.
- Kinematic studies suggest at least two stages of faulting with associated folding and fracturing are represented by structures in the study area. Stage 1 faulting (e.g., fault A) is interpreted to be associated with longitudinal normal faulting and tilting of beds within the Deep River Triassic basin. Stage 2 represents a later phase of transverse faulting along the SBPF involving both normal and dextral strike-slip components of displacement.
- The four newly discovered faults from this study, along with other faults previously identified in the area, indicate this portion of the Deep River Triassic basin is in structurally complex zone of intersecting faults.

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# APPENDICES

APPENDIX A: STRUCTURE DATA - NORTH BORROW PIT (see figure 11)

FOLD AXIS TREND & PLUNGE

TATION	NOCA	DEDDING	EDACTIDE	CDACTIDE	EDACTIDE	EDACTIDE	T ALL T	TIME IN TRIVE
NUMBER	TYPE*	ATTITUDE	ATTITUDE	ATTITUDE	ATTITUDE	ATTITUDE	ATTITUDE	OF FOLD
NB1	SS		010/90	06/080				
NB3	css/ss ee/me	310/20n	010/00	nannan	335/00			
NB4	0000		340/70 s	06/080	0000			
			352/73 n	075/85 s				
			314/77 n	018/01 8				
NB5	ss/mss	350/05 n	282/90	06/090	016/90			
		005/10 s	348/90	075/90	005/86 s			
			354/80 e	027/57 n				
NB6	CSS	030/12 s	350/90					
	88		350/90	033/90	06/220			
NB7	ms		340/90					
NB8			06/000	75/90				
NB9	SS	316/10 n	020/90	350/90				
NB10	CSS		082/90	345/90				
NB11	CSS		082/90	023/90				
NB12	CSS	010/16 s						
NB13	ms/ss	340/20 n	088/90	282/90	346/90			
NB14			025/90					
NB15	css/ms	047/25 s	340/85 n	080/72 n				
	css/mss	335/08 n	315/90	072/90	342/90			
NB16	ms		340/90					
NB17	SS		06/000					
NB18	mss		350/90					
<b>NB19</b>	mss		06/000	086/90				
NB20			015/90					
NB21	ms		335/90					
NB22	sms		06/200					
NB23		015/20 \$	070/85 \$	332/75 n	343/15 n			
			078/80 \$	346/89 n	337/ 04 n			
			082/81 n	356/85 n				
			180/84 n	332/75 n				
			0/8/80 8					
<b>NB24</b>		330/22 n	348/80 \$	06/081	8 6/ /020			
			345/72 8	00000				
		= 00/000	235/74 e	0177/00	DAR/OD			
		5 60702	a DR/RD a	nellin	00000	00000		
			330/75 0					
	0 00		06/020					
	SSS		080/90					
	SSS		000/80 \$					
	CSS	070/10 s						

\*Rock Type: css-conglomeratic sandstone, ss-sandstone, mss-muddy sandstone, si-siltstone, ms-mudstone

APPENDIX A: STRUCTURE DATA - NORTH BORROW PIT (see figure 11)

FOLD AXIS TREND & PLUNGE														080/20											
AXIAL PLANE OF FOLD																		275/70 s							
FAULT ATTITUDE														035/60 s											
FRACTURE			332/90		058/90						298/90												072/05 s		
FRACTURE	303/90 340/81 s 327/72 s 335/85 s	342/90	071/90		085/90	330/90			045/80 n		323/76 s 353/85 s		240/00	000000									322/60 n 322/60 n		
FRACTURE	059/85 n 066/89 n 078/88 s 075/90 072/83 s 082/90	317/90	345/70 s 336/69 s	068/85 n 078/90	343/90	022/90 275/90	275/85 w	300/90	020/90	06/020	027/90	06/080	30E/DO	00000									082/90 084/64 s		
FRACTURE	013/85 s 022/85 s	324/90	080/87 s 086/85 s	338/85 n 340/78 n	005/75 s	060/90	355/90	350/90	345/90	340/90	076/78 s 002/70 n	012/78 n	075/00	00000							006/000	015/90	359/51 w 355/60 n 349/60 n	11 70/700	
BEDDING	300/12 n 338/15 n	295/15 n 020/15 s 339/08 n	334/20 n 307/25 n	020/08 s 017/10 s	102002								084/32 n	051/39 n	070/33 s	068/50 n	320/35 n	066/34 s	276/80 n	064/36 \$	1 GG/00£			342/15 n	
ROCK TYPE*			SS	ett	Sim	ms/ss ss	88	SS SS	CSS	CSS			1	83 Ma	ŝ	ms	ms	ms	ms	ms	ms	mss			
STATION NUMBER	NB25		NB26 NB27	NB28		NB29 NB30	1831	NB32		<b>NB34</b>	NB35			NR36	-							/EAN	NB38	NB39	

\*Rock Type: css-conglomeratic sandstone, ss-sandstone, mss-muddy sandstone, sl-slitstone, ms-mudstone

APPENDIX A: STRUCTURE DATA - NORTH BORROW PIT (see figure 11)

FOLD AXIS TREND & PLUNGE								
AXIAL PLANE OF FOLD								
FAULT ATTITUDE								
FRACTURE ATTITUDE								
FRACTURE								
FRACTURE	350/55 e						06/080	
FRACTURE	030/80 e		358/80 w	310/75 s		335/80 s	350/80 s	
BEDDING	010/13s 065/56n 060/10n	345/16n	010/12n	u07/090	000/100	345/08n		084/32 n
ROCK TYPE*	ms ss/ms	ss/ms	ss/ms	88	mss	ss/mss	CSS	
STATION	NB40	NB41	NB42	NB43	NB44	NB45	NB46	NB47

\*Rock Type: css-conglomeratic sandstone, ss-sandstone, mss-muddy sandstone, sl-slitstone, ms-mudstone

RAKE OF SLICKENLINES		060/42S/80 030/30S/65
FAULT ATTITUDE		80/55 s 085/65 s 295/70 s 085/65 s 060/42 s 030/030 s 290/55 s
FRACTURE		
FRACTURE ATTITUDE		008/90
FRACTURE ATTITUDE	346/69 n 351/72 s 332/90	293/90 070/90 043/60 w 295/90 040/90
FRACTURE	042/90 310/90 290/90 025/90 025/90 026/45 s 313/75 n 034/80 n 308/85 s 278/90 312/90	315/90 305/90 285/90 085/65 s 295/70 s 295/70 s 350/90 315/55 s 305/85 s 305/85 s
BEDDING	310/28 n 305/20 n 017/24 s 300/18 n 310/14 n	330/18 e 018/28 s 358/29 e 042/40 s 000/12 e 027/18 s 330/18 n 330/18 n 013/13 s 354/25 n 296/30 n 013/19 s 013/19 s 012/14 s 012/14 s
ROCK TYPE*	ss/ss mss mss ss ss ss ss ss css/ms ss ss ss ss	si SS CSS SS SS SS SS SS SS SS SS SS SS SS
STATION	SB1 SB2	SB3 SB4 SB5 SB5 SB7 SB7

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APPENDIX A: STRUCTURE DATA - SOUTH BORROW PIT (see figure 11)

\*Rock Type: css-conglomeratic sandstone, ss-sandstone, mss-muddy sandstone, si-siltstone, ms-mudstone

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DE SLICKENLIN										0	0																								
FAULT										335/85	68/080																								
FRACTURE																																			
FRACTURE				033/90																								06/200	353/90	026/90	332/85 s				
FRACTURE			280/90	335/90												030/80				276/90			070/12		290/90			032/90	35/90	285/90	051/90	020/90			
ATTITUDE	012/90 270/90		008/78 n	325/90	330/90	034/90	305/90	u 8//800	353/90	325/90	2/0//0 2					295/90	010/30 0	020/90	317/90	012/90	020/90	280/90	334/90		340/90			350/90	350/90	012/90	022/90	297/90			
ATTITUDE		010/18 s	010/15 s			340/15 n		342/15 n	342/15 n	300/40 S	5 10/03 5	LI CO/DCO	U 02/267	013/19 s 300/12 n	206/30 n	010/25e						310/10 n		300/15 n		335/04 n	326/20 n		353/19 e			307/20 n	311/17 n		
TYPE*	SS	SS				sms/ms		ms	SM	mss	1	SI	SS/SI		me	2		sms		sm	ms		sms/cs/ms	ss/ms	CSS	SS		ms	SIL						
STATION	SB14	SB15		SB16	SB17	SB18		SB19		SB20	1285	2295		SB23	CBOA	SB25	SB26	SB27	SB28	SB29	SB30	SB31							SB32	SB33	SB34	SB35	SB36		

APPENDIX A: STRUCTURE DATA - SOUTH BORROW PIT (see figure 11)

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RAKE OF SLICKENLINES			150/295/72	275/57S/70 270/70S/83	
FAULT ATTITUDE			330/29 s	275/57 s 090/70 s 290/58 s 082/63 s	
FRACTURE ATTITUDE					
FRACTURE	320/90	344/68 s			
FRACTURE	281/90 320/11 s 010/90 040/90	082/90 090/90 050/90 080/90 050/90	326/80w 275/90	348/70s 005/70s 075/65n 065/90 007/55w	
FRACTURE	312/90 004/78 n 310/90 310/90	008/90 006/90 010/90 327/90 325/90 305/90	070/80 n 010/70 s	320/80 n 280/90 275/90 345/90 358/90	355/37 w
BEDDING	020/10 s 010/20 e 358/12 w	302/12 e 007/35 s 355/12 w	000/20 e 005/13 e 010/16 e	005/30s 330/10n 335/20n 335/20n 345/12e 345/12e 345/15e 345/15e 335/8e 000/14e	
ROCK TYPE*	8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 8 8 8 8 8 8	ms ss ss	ss ss ss ss/ms ss/ms ms/ss ms/ss ms/ss ms/ss ms/ss ms/ss ms/ss ms/ss	00
STATION NUMBER	SB37 SB38 SB39 SB39	SB40 SB41 SB42	SB43 SB44 SB45	SB46 SB47 SB47 SB49 SB50 SB51 SB55 SB55 SB55 SB55 SB55 SB55 SB55	CREB

\*Rock Type: css-conglomeratic sandstone, ss-sandstone, mss-muddy sandstone, sl-siltstone, ms-mudstone

# APPENDIX B: STRUCTURE DATA FOR FRACTURE TRACE MAP AT LOCATION 4 (see figure 7)

Domain I						Domain II			
<b>Bedding attitudes</b>	Fracture attitudes					<b>Bedding attitudes</b>	Fracture attitudes		
305 / 12 n	000 / 90	110/84	s	118/82	w	343/15 n	000 / 90	171/78	5
306/15 n	001/90	110/84	s	119/82	W		000 / 90	172/68	s
312/8 n	011/90	110/84	s	120/74	5		010/90	175/81	8
319/9 n	012/90	111/72	s	121/66	s		010/90	176/82	s
	014/90	111/72	s	144/60	S		012/90	178/82	s
	014/90	111/80	s	181/79	n		012/90	184/69	n
	014/90	112/68	S	181/85	n		012/90	184/74	n
	015/90	112/76	s	184/58	n		019/90	185/81	n
	018/90	112/84	S	191/68	n		021/90	189/76	n
	019/90	112/84	W	191/70	n		021/90	192/80	n
	021/90	112/85	S	192/82	n		022 / 90	199/68	n
	021/90	114/70	s	194/80	n		102/83 s	280/90	
	021/90	114/74	S	196/81	n		106/85 s	281/90	
	021/90	114/74	s	279/90			108/76 s	286/90	
	024/90	114/75	S	282/90			109/76 s	289 / 90	
	029 / 90	114/76	s	286/90			109/85 s	294 / 90	
	029 / 90	114/76	S	290/90			109/85 s	295/90	
	029 / 90	114/76	S	292 / 90			110/83 s	295/90	
	030/64 s	114/76	s	292/90			111/76 s	341/90	
	076 / 90	114/77	5	293/90			111/80 s	345/90	
	076/90	114/77	5	295/72	n		111/81 s	351/90	
	076/90	114/78	S	296/90			111/81 s	351/90	
	096/84 s	115/70	s	299/90			111/87 s	354 / 90	
	099/85 s	115/71	s	305 / 90			112/71 s	354 / 90	
	103/76 s	115/72	s	342/90			112/72 s	356 / 90	
	104/72 s	115/75	s	344 / 90			112/75 s	358 / 90	
	104/74 s	115/80	\$	346/90			112/82 s		
	105/75 s	115/80	\$	354 / 90			112/82 s		
	105/76 s	116/71	5	355 / 90			112/84 s		
	105/80 s	116/71	\$	356/65	n		112/85 s		
	105/83 s	116/77	s	356/72	n		112/85 s		
	105/85 s	116/77	\$				113/80 s		
	106/71 s	116/78	\$				114/81 s		
	106/74 s	116/80	s				114/82 s		
	106/74 s	116/80	s				114/84 s		
	106/74 s	116/80	W				114/85 s		
	106/81 s	116/80	w				115/74 s		
	106/85 s	116/81	s				115/76 s		
	109/74 s	116/84	s				115/88 s		
	109/79 s	117/82	s				116/76 s		
	109/81 s	118/70	W		*		116/76 s		
	110/72 s	118/76	W				116/81 s		
	110/76 s	118/77	s				118/79 s		
	110/76 s	118/80	w				169/71 s		
	110/78 s	118/80	W				169/84 s		

Domain III	E					Domain IV	-	
Bedding attitudes	Fracture attruces					Bedding annudes	Fracture	Innuces
005/10 s	000/90	115/80	S	196/86	n	018/12 s	025/90	
015/9 s	002/90	115/83	S	198/76	n	026/10 s	025/90	
	002/90	115/85	\$	199/70	n		029 / 90	
	006 / 90	115/85	\$	199/75	n		102/86	5
	011/90	115/86	\$	199/75	n		104 / 84	S
	012/90	116/79	S	200/81	n		106 / 75	S
	012/90	116/80	S	201/75	n		106/80	S
	012/90	116/80	5	208/75	n		106/81	S
	014/90	116/81	S	209/88	n		106/82	S
	014/90	116/85	s .	211/89	n		106/82	S
	019/90	116/86	S	242/78	n		108/86	S
	021/90	116/86	s	281/50	n		109/79	\$
	028 / 90	118/79	5	281/90			109/81	S
	029 / 90	118/81	5	286/90			109/88	5
	036 / 90	118/81	5	292 / 90			110/78	S
	098/88 s	118/81	S	292 / 90			111/76	S
	101/88 s	120/82	s	294/90			111/80	s
	102/80 s	123/80	s	294 / 90			111/85	S
	102/85 s	179/81	s	296 / 90			111/88	S
	106/76 s	180/80	w	298 / 90			112/76	S
	106/86 s	186/81	n	298 / 90			112/76	S
	109/80 s	189/80	n	299 / 90			114/74	S
	109/81 s	189/85	n	319/64	n		114/83	s
	109/81 s	190/81	n	358 / 90			120/89	S
	111/81 s	190/84	n				120/89	s
	111/88 s	191/73	n				194/81	n
	111/88 s	191/80	n				199/86	n
	112/78 s	193/85	n				201/81	n
	112/84 s	195 / 80	п				209/70	n
	115/78 s	195/83	n				209/70	n

# **APPENDIX C**

# WEATHERING AND ROCK MASS CLASSIFICATION

Excavation of the borrow pits in the mid- to late-1970's removed soil and weathered rock to estimated depths of 4 to 12 feet below the ground surface. Exposure of the previously weathered rock in the floor of the pits accelerated the normal weathering processes affecting the engineering properties of the rocks. The Unified Rock Classification System (URCS), developed by Williamson (1984), was applied at the reconnaissance level to describe the basic engineering properties of weathered rock units exposed in the borrow pits, and to supplement standard geologic classifications. The URCS rates four basic elements of the rock mass: 1) degree of weathering, 2) strength, 3) discontinuities, and 4) unit weight. A single letter abbreviation ( $\underline{A}$  through  $\underline{E}$ ) is used for each of the four properties of the rock mass. Appendix C is a condensed version of the URCS adapted from Williamson (1984). In the following brief overview, the abbreviated rating for each category is shown in parentheses immediately after qualifiers in the text.

All rocks in the borrow pits show signs of weathering; however, weathering has not progressed sufficiently to develop a soil profile. In general, the degree of weathering of the rocks ranges from the stained state ( $\underline{C}$ ), through the partly decomposed state ( $\underline{D}$ ), to the completely decomposed state ( $\underline{E}$ ). Mineral components of stained state rocks are partly or completely discolored due to oxidation alteration. Partly decomposed rocks can be remolded into gravel or larger size pieces with finger pressure. Completely decomposed rocks can be remolded to sediment without gravel or larger size fragments with finger pressure. Resistant ledges or pavements of stained state rock are invariably conglomeratic sandstone or sandstone; however, these rocks types also occur in the partly decomposed and completely decomposed states. Muddy sandstones, siltstones, and mudstones are predominately in the completely decomposed state.

As specified by the URCS, a blow from the rounded end of a 16-ounce ballpeen hammer was used to estimate rock strength. Impact reactions ranged from dent quality ( $\underline{C}$ ) to crater quality ( $\underline{D}$ ). Moldable quality ( $\underline{E}$ ) rocks are most common. According to the URCS, dent quality rocks have an estimated unconfined compressive strength of 3,000 to 8,000 pounds per square inch (psi). Crater quality rocks ranges from 3,000 to 1000 psi, and moldable quality rocks are less than 1,000 psi. Dent quality rocks invariably are conglomeratic sandstone or sandstone; however crater quality and moldable quality varieties of these rocks are common. Siltstones and mudstones are moldable quality in almost all cases.

Discontinuities may indicate directional weaknesses in the rock mass, as well its the ability to transmit water. Here, as observed in outcrop, internal planar separations in the rock mass consist mainly of fractures and bedding planes. At the

#### Appendix C Weathering and Rock Mass Classification

outcrop scale, essentially all rocks contain intersecting open planes, referred to in the URCS as three-dimensional, open planar separations ( $\underline{E}$ ). The in-filling present in some fractures and bedding plane is typically remoldable (<1000 psi) light gray to gray-green clay. Figures 7, 8, and 10 illustrate typical examples of the scale of intersecting discontinuities. The rock mass within the intersecting discontinuities varies from solid random breakage to solid preferred breakage. Solid preferred breakage typically occurs in rock units with closely spaced bedding plane partings commonly found in thinly bedded or laminated sandstones and siltstones.

Actual measurements of unit weights in of different rock units were not conducted. Estimates of unit weights in pounds per cubic foot (pcf) based on the heft of the samples indicate that in most cases the unit weight ranges from 150 pcf ( $\underline{C}$ ) to 130 pcf ( $\underline{D}$ ) for stained state, dent quality rock specimens. Completely decomposed (moldable quality) rocks are estimated to be less than 130 pcf ( $\underline{E}$ ), probably on the order of 120 to 110 pcf. These estimates are consistent with determinations of dry unit weights made for weathered Triassic-age rocks during characterization of the Wake/Chatham site. These measured values are presented in section 2.5, geotechnical characteristics, of the license application (Chem-Nuclear Systems Inc., 1993).

In summary, the relatively more resistant rocks in the borrow pits that form ledges or rock pavements are stained state, dent quality, conglomeratic sandstones and sandstones (URCS CCEC). Partly to completely decomposed units predominate, and include conglomeratic sandstone, sandstone, siltstone, and mudstone (URCS DDED to EEEE). Siltstone and mudstone are almost invariably completely decomposed, and are remoldable with finger pressure (URCS <u>EEEE</u>). In the partly to completely decomposed states these weathering products have engineering properties similar to those of soil. The weathering products of completely decomposed rocks exposed in the floors of the pits were classified in general accordance with ASTM D 2488 - 84e1 (American Society for Testing and Materials, The weathering products of completely decomposed, conglomeratic 1989). sandstone and sandstone are typically silty sand and silty sand with gravel (SM), or less commonly, silty gravel (GM). Muddy sandstone can decompose to clayey sand (SC). Siltstone and mudstone typically decompose to silt and clay mixtures, with or without sand (ML, MH, CL and CH).

# UNIFIED ROCK CLASSIFICATION SYSTEM (modified from Williamson, 1984)

DEGREE OF WEATHERING

REPRESI	REPRESENTATIVE		WEATHERED			
	Micro Fresh State State (MFS) (VFS) A B		>GRAVEL SIZE Partly Decomposed State (PDS) D		<sand size<br="">Completely Decomposed State (CDS) E</sand>	
Micro Fresh State (MFS) A						
UNIT V RELATIVE A	UNIT WEIGHT RELATIVE ABSORPTION		NON- PLASTIC	PLASTIC	NON- PLASTIC	PLASTIC

#### ESTIMATED STRENGTH

	REACTION TO IMPACT OF	1 LB. BALLPEEN HAMME	REMOLDING 1	
"Rebounds" (Elastic) (RQ) A	"Pits" (Tensional) (PQ) B	"Dents" (Compression) (DQ) C	"Craters" (Shears) (CQ) D	Moldable (Friable) (MQ) E
>15000 psi <sup>2</sup> >103 MPa	8000-15000 psi <sup>2</sup> 55-103 MPa	3000-8000 psi <sup>2</sup> 21-55 MPa	1000-3000 psi <sup>2</sup> 7-21 MPa	<1000 psi <sup>2</sup> <7 MPa
A	В	С	D	E
	21V15		-	802800

(1) Strength Estimated by Soil Mechanics Techniques
(2) Approximate Unconfined Compressive Strength

#### DISCONTINUITIES

VER	VERY LOW PERMEABILITY			MIT WATER
Solid (Random Breakage) (SRB) A	Solid (Preferred Breakage) (SPB) B	Solid (Latent Planes Of Separation) (LPS) C	Nonintersecting Open Planes (2-D) D	Intersecting Open Planes (3-D) E
			ATTITUDE	INTERLOCK

#### UNIT WEIGHT

Greater Than 160 pcf 2.55 q/cc	150-160 pcf 2.40-2.55 g/cc	140-150 pcf 2.25-2.40 g/cc	130-140 pcf 2.10-2.25 g/cc	Less Than 130 pcf 2.10 g/cc
A	В	C	D	E

#### **DESIGN NOTATION**

![](_page_49_Figure_12.jpeg)

Basic elements of the unified rock classification system

![](_page_50_Figure_0.jpeg)

![](_page_51_Figure_0.jpeg)