BISHOP PROPERTY RESTORATION PLAN
ANSON COUNTY, NORTH CAROLINA

North Carolina Ecosystem Enhancement Program
Raleigh, North Carolina

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1.0 INTRODUCTION

The North Carolina Ecosystem Enhancement Program (EEP) is currently evaluating stream and wetland restoration opportunities on the Bishop Property Restoration Site located approximately 3 miles north of the Town of Ansonville in northern Anson County, North Carolina (Figure 1). The Bishop Property consists of three parcels, owned by Mr. John Bishop, collectively encompassing approximately 900 acres of land. The proposed restoration area, including approximately 195 acres within the three parcels, has been placed under a conservation easement and will hereafter be referred to as the Site (Figure 2).

The Site is located at the confluence of the Rocky River and the Pee Dee River, immediately upstream from the approximately 8,000-acre Pee Dee National Wildlife Refuge. In the Site vicinity, the Rocky and Pee Dee River floodplains have largely been cleared of forest vegetation and are currently utilized as fertile pasture, hay fields, or agricultural fields (row crop production). The Site has potential to serve as an important wildlife corridor along two major waterways extending to the Pee Dee National Wildlife Refuge.

The Site is primarily utilized for row crop production and recreational activities (hunting and wildlife viewing). Removal of riparian vegetation, dredging/straightening of on-Site streams, annual clearing, plowing, and additions of nutrient fertilizers appear to have resulted in degraded water quality (sediment inputs and agricultural runoff into the Rocky and Pee Dee Rivers), unstable channel characteristics (stream entrenchment, erosion, and bank collapse), and decreased wetland function.

The purpose of this study is to establish stream and wetland enhancement/restoration concepts which will result in benefits to water quality and wildlife by providing stable streams and wetlands within a wildlife corridor located adjacent to two major waterways and an important wildlife refuge. This detailed restoration plan is expected to outline activities to be included in construction planning documents. The objectives of this study include the following:

- Classify the on-Site streams based on fluvial geomorphic principles.
- Identify jurisdictional wetlands and/or hydric soils within the Site boundaries.
- Identify a suitable reference forest, stream, and wetland to model Site restoration attributes.
- Develop a detailed plan of stream and wetland enhancement/restoration activities within the Site.
- Establish success criteria and a method of monitoring the Site upon completion of restoration implementation.

After implementation, restoration activities are expected to provide the following:

1. 5,663 linear feet of stream restoration
2. 1,190 linear feet of stream enhancement - level 1
3. 7,306 linear feet of stream enhancement - level 2
4. 11,250 linear feet of stream preservation
5. 5.6 acres of wetland restoration
6. 0.9 acres of wetland enhancement
7. 10.2 acres of wetland preservation

This document represents a detailed restoration plan summarizing activities proposed within the Site. The plan includes 1) descriptions of existing conditions; 2) reference stream, wetland, and forest studies; 3) restoration/enhancement plans; and 4) Site monitoring and success criteria. Upon approval of this plan by regulatory agencies, engineering construction plans will be prepared and activities implemented as outlined. Proposed restoration activities may be modified during the civil design stage due to constraints such as access issues, sediment-erosion control measures, drainage needs (floodway constraints), or other design considerations.

2.0 METHODS

Natural resource information was obtained from available sources. United States Geological Survey (USGS) 7.5-minute topographic quadrangle (Millstone Lake, NC), United States Fish and Wildlife Service (FWS) National Wetlands Inventory (NWI) mapping, Natural Resource Conservation Service (NRCS) soils mapping for Anson County (NRCS 2000), and recent Anson County aerial photography were utilized to evaluate existing landscape, stream, and soil information prior to on-Site inspection.

Reference stream geometry methods have been used to orient channel reconstruction design. Reference stream and floodplain systems were identified and measured in the field to quantify stream geometry, substrate, and hydrodynamics. Stream characteristics and detailed restoration plans were developed according to constructs outlined in Rosgen (1996), Dunne and Leopold (1978), Harrelson *et al*. (1994), Chang (1988), and State of North Carolina Interagency Stream Mitigation Guidelines (USACE *et al.* 2003). Stream pattern, dimension, and profile under stable environmental conditions were measured along reference (*i.e.* relatively undisturbed) stream reaches and applied to the degraded channel within the Site. Reconstructed stream channels and hydraulic geometry relationships have been designed to mimic stable channels identified and evaluated in the region.

Files at the North Carolina Natural Heritage Program (NHP) were evaluated for the presence of protected species. Characteristic and target natural plant community patterns were classified according to Schafale and Weakley's, *Classification of the Natural Communities of North Carolina* (1990). Plant communities were delineated and described by structure and composition.

Detailed field investigations were performed between September 2003 and May 2004 including generation of Site channel cross-sections, profiles, and plan-views; valley cross-sections; detailed soil mapping; and mapping of on-Site resources. Hydrology, vegetation, and soil attributes were analyzed to determine the status of jurisdictional areas. Jurisdictional wetlands and adjustments to hydric soil boundaries were delineated using Global Positioning System (GPS) technology. Recent (2003) aerial photography was evaluated to determine primary hydrologic features and to map relevant environmental attributes.

Information collected on-Site and in reference ecosystems was compiled in a database and incorporated with field observations to evaluate the on-Site stream under existing conditions. Subsequently, this restoration plan was developed to facilitate restoration success and to provide stream and wetland restoration to the EEP.

3.0 EXISTING CONDITIONS

3.1 Physiography, Topography, and Land Use

The Site is located in northern Anson County near the border of Stanly, Montgomery, and Richmond Counties, approximately 3 miles north of Ansonville, North Carolina. The Site falls in two USGS 14-digit Hydrologic Units (HUs).

The Site is underlain by the Carolina Slate Belt geologic formation, immediately adjacent to the Chatham Group of the Triassic Basin geologic formation, within the Piedmont physiographic province of North Carolina. The hydrophysiographic region is characterized by dissected irregular plains, some hills, linear ridges, and isolated monadnocks (Griffith 2002) (Figure 4). This region is characterized by moderate rainfall with precipitation averaging approximately 47 inches per year (NRCS 2000).

The Site is located within and adjacent to the Rocky River floodplain immediately upstream of the confluence of the Rocky River with the Pee Dee River. Slopes adjacent to the Rocky River floodplain are relatively steep and range in elevation from approximately 320 feet National Geodetic Vertical Datum (NGDV) at the upper reaches of smaller on-Site tributaries to a low of approximately 190 feet NGDV in the lower portions of the Rocky River floodplain (Figure 4).

The Site includes approximately 5,500 linear feet of frontage adjacent to the Rocky River and approximately 23,000 linear feet of channel associated with four additional streams: Camp Branch, Unnamed Tributary (UT) to Camp Branch, Dula Thoroughfare, and UT to Dula Thoroughfare (Figure 2). Camp Branch is characterized as a second-order stream extending through relatively wide, moderately sloped valley (approximately 0.0022 rise/run). Dula Thoroughfare and the UTs are characterized as first-order streams extending through relatively narrow, steeply sloped valleys (approximately 0.022 and 0.0047 rise/run). The drainage area at the Camp Branch outfall is approximately 2.9 square miles. The drainage area at the Dula Thoroughfare and UT outfall are approximately 0.36 and 0.23 square miles, respectively (Figure 4).

The watersheds for Camp Branch, Dula Thoroughfare, and the UTs are characterized predominately by agricultural land (row crops and livestock production) and forest with sparse residential development. Drainage basins for Dula Thoroughfare and the UTs are contained almost completely within property owned by Mr. Bishop or his immediate neighbor. The Camp Branch drainage basin extends upstream and encompasses several state maintained roadways, residential and agricultural structures adjacent to the roadways, and a rail line. Impervious surfaces in drainage basins upstream from the Site are expected to cover less than 5 percent of the land area.

Agricultural row crop production dominates the lower elevation floodplain terraces adjacent to the Rocky River, accounting for approximately 85 percent of the floodplain land area. Streams which cross through the floodplains are generally fringed by a disturbed stream-side assemblage; however, Dula Thoroughfare is devoid of a riparian fringe for much of its reach through the floodplain. As the streams grade upslope toward their headwaters, timber

production is the dominant land use. Forested areas are characterized by a mixture of pine and hardwood species approximately 10 to 15 years old. Recreational activities, specifically hunting, occur throughout the Site and various tree stands and food plots occur throughout the Site and adjacent properties.

Two man-made impoundments located in the UT to Camp Branch stream complex encompass approximately 2.4 acres of land. The smaller impoundment (approximately 0.1 acre) is located at the UT headwaters and the larger impoundment (approximately 2.3 acres) has been created at the outer Camp Branch floodplain edge. These impoundments appear to have been created for irrigation of crops and recreational uses.

3.2 Soils

Site soils have been mapped by the NRCS and include the Badin – Goldston complex, as well as the McQueen, Shellbluff, Tetotum, and Chewacla series (NRCS 2000) (Figure 5). A general description of each soil and its hydric/non-hydric status is included in Table 1.

Table 1 – On-Site soils mapped by NRCS

Series	Hydric Status	Family	Description
Badin Channery Silt Loam (BaB, BaC)	Non-Hydric	*Typic Hapludults*	moderately deep, well drained, moderately permeable
Badin-Goldston Complex (BgD)	Non-Hydric	*Typic Hapludults-Typic Dystrudepts*	shallow to moderately deep, well drained, moderate to moderately rapid permeability
McQueen (MrB)	Non-Hydric	*Typic Hapludults*	deep, well drained, slow permeability
Shellbluff (ShA)	Non-Hydric	*Fluventic Dystrudepts*	very deep, well drained, moderate permeability
Tetotum (ToA)	Non-Hydric	*Aquic Hapludults*	very deep, moderately well drained, moderate permeability
Chewacla (ChA)	Non-Hydric; may contain hydric inclusions	*Fluventic Dystrudepts*	very deep, somewhat poorly drained, moderate permeability

Badin Channery Silt Loam BaB, BaC:
This series is typically found on Piedmont uplands with moderate to steep slopes (2 to 8 percent or 8 to 15 percent). The soil solum is moderately deep and well drained with moderate permeability. Depth to seasonal high water table is greater than 6.0 feet, and depth to bedrock is 20 to 40 inches to soft bedrock and over 40 inches to hard bedrock. Badin Channery Silt Loam typically occurs on upland side slopes adjacent to area streams and tributaries.

Badin-Goldston Complex BgD:
This series shares many characteristics with the Badin Channery Silt Loam described above; however, the addition of Goldston in the complex produces additional ranges for some values. These soils are also found in the Piedmont on slopes of 15 to 25 percent. Depths can range from shallow to moderately deep, and permeability can be moderate to moderately rapid, though typically well drained. Depth to the seasonal high water table is greater than 6.0 feet,

and depth to bedrock varies from 10 to 20 inches and 20 to 40 inches to soft bedrock. Depth to hard bedrock is between 10 to 20 inches and greater than 40 inches. Badin-Goldston Complex occurs at the base of steep slopes adjacent to Dula Thoroughfare.

Chewacla ChA:
These frequently flooded soils can be found in floodplains of the Piedmont, Upper Coastal Plains, and Sandhills. Soils are very deep and somewhat poorly drained with moderate permeability. During the months of November through April the seasonal high water table can be at a depth of 0.5 to 1.5 feet. Depth to bedrock is more than 60 inches. Chewacla soils occur in low elevation depressions within the Rocky River floodplain.

McQueen MrB:
This series, found in the Piedmont, Upper Coastal Plain, and Sandhills along major streams and rivers, is very deep and well drained. Permeability is slow, and the seasonal high water table through the months of January through March is at a depth of 4 to 6 feet. Depth to bedrock is greater than 60 inches. McQueen soils occur in floodplains adjacent to the Rocky River and Camp Branch.

Shellbluff (ShA):
This soil series is also found in floodplains of the Piedmont, Upper Coastal Plain, and Sandhills landscapes. Shellbluff soils are typically very deep and well drained with moderate permeability. Slopes are quite flat, ranging between 0 and 2 percent. From December to March the seasonal high water table can vary between 3 and 5 feet, and depth to bedrock is more than 60 inches. Shellbluff soils occur in crowned agricultural fields within the Rocky River floodplain.

Tetotum (ToA):
These soils are located on low stream terraces in the Piedmont, Upper Coastal Plain, and Sandhills landscapes. Tetotum soils are classified as very deep and moderately well drained with moderate permeability. These soils are found in low slope areas with slopes ranging from 0 to 3 percent. Seasonal high water tables in the months of December to April are between 1.5 and 2.5 feet. Bedrock can be found at depths greater than 60 inches. Tetotum soils occur in low elevation depressions downstream from a man-made pond in the UT to Camp Branch and in the floodplain to Dula Thoroughfare.

3.3 Jurisdictional Wetlands

Jurisdictional areas are defined using the criteria set forth in the U.S. Army Corps of Engineers (USACE) Wetlands Delineation Manual (DOA 1987). Wetlands are defined by the presence of three criteria: hydrophytic vegetation, hydric soils, and evidence of wetland hydrology during the growing season (DOA 1987). Open water systems and wetlands receive similar treatment and consideration with respect to Section 404 review. Site jurisdictional areas include surface water in bank-to-bank streams, vegetated wetlands, and open water ponds.

Site jurisdictional areas were delineated and located using GPS technology between August 27 and Oct 2, 2003 (Figure 6). The delineation was reviewed and approved by the USACE (Steve Lund regional field office representative) on January 13, 2004. Based on the jurisdictional boundary mapping, approximately 15.4 acres of jurisdictional wetlands and 28,518 linear feet of

jurisdictional streams, including 5,500 linear feet of Rocky River frontage, were delineated within the Site.

Two distinct jurisdictional wetlands types occur within the Site boundaries: 1) groundwater seep depressions and 2) shallow surface water conveyances.

Groundwater Seep Depressions

Groundwater seep depressions occur at the upper headwaters of small tributaries and at the outer floodplain edge. These wetlands are formed by surface expression of groundwater over dense, low permeability clays or other impervious sub-surface horizons. On-Site groundwater seep depressions are underlain by loamy to clayey soils which are gleyed in color with frequent mottling, potentially indicating a fluctuating water table. Vegetation in these areas is frequently disturbed by land clearing in support of agriculture or timber harvest and consists of dense thickets of shrub and herbaceous species such as blackberry (*Rubus* sp.), black willow (*Salix nigra*), climbing hempweed (*Mikania scandens*), and tearthumb (*Polygonum sagittatum*).

Shallow Surface Water Conveyances

Shallow surface water conveyances occur in portions of the Rocky River floodplain where streams have been dredged, straightened, and altered from their original flow path. The reach of Dula Thoroughfare across the Rocky River floodplain is characterized by exceedingly low slopes resulting in ponding and sloughing of ditch banks, thereby creating a shallow, wide depression that remains inundated throughout most of the year. Although the area is inundated for extended periods, soils remain brightly colored (approximately 10YR 4/4 to 10 YR 4/6) which is characteristic of Triassic Basin area wetlands. Vegetation in these areas is characterized by row crop production and herbaceous species such as knotweed (*Polygonum* spp.), cat tail (*Typha latifolia*), rushes (*Juncus* spp.), and sedges (*Carex* spp.).

3.4 Hydrology

3.4.1 Surface Water

The primary hydrologic feature at the Site is the Rocky River. The Rocky River is approximately 240 feet in width and 25 feet in depth at the Site boundary. Hydro-electric facilities on the Pee Dee River, located immediately upstream from the confluence of the Rocky River and Pee Dee River, have periodic releases resulting in back-flow conditions in the Rocky River, often leading to fluctuations in the normal hydrologic flow regime. Back-flow conditions affect on-Site surface water flow patterns at the confluence of Site streams with the Rocky River.

Smaller area tributaries initiate as groundwater driven, depressional seepages on slopes adjacent to the Rocky River floodplain. Tributaries descend as first-order streams down moderate to steeply sloped, narrow valleys. As the tributaries coalesce, they form larger second and third order streams. Once the streams enter the Rocky River floodplain, they are generally impacted by agricultural practices, vegetation clearing, and channel dredging/straightening. Upon convergence with the Rocky River, the channels tend to incise to depths consistent with the dominant hydrologic feature, the Rocky River.

Discharge within the Site appears to be dominated by a combination of upstream basin catchments, groundwater flow, and precipitation. Based on regional curves (Harman *et al.* 1999) and infield measurements of channel bankfull cross-sectional area, bankfull discharges for on-Site streams include the following:

Stream Name	Drainage Area (square miles)	Bankfull Discharge (cubic feet per second)
Camp Branch	2.9	192
Dula Thoroughfare	0.4	46
UT to Dula Thoroughfare	0.2	28

Current research indicates bankfull discharge would be expected to occur approximately every 1.3 to 1.5 years (Rosgen 1996).

3.4.2 Groundwater

Groundwater seepage results from upland terrestrial catchments, subsurface lateral groundwater flow, and expression of the groundwater table in jurisdictional wetland pockets or area stream margins. Groundwater seepage is related to the size and characteristics of the catchment basin, while subsurface lateral flow is related to the porosity/conductivity of drainage basin soils. The drainage basin upstream of the Site is characterized largely by mature forest and open pasture with little impervious surface. With the exception of roads and roadside ditches, precipitation is expected to penetrate area soils and enter the groundwater table to be discharged into area wetlands and streams.

Several groundwater seepages areas were identified within the Site. Groundwater seepage areas were delineated as jurisdictional wetlands and are depicted in Figure 6. Groundwater seepage areas are located at two distinct landscape positions: 1) at the upper extend of area tributaries, or 2) at the outer floodplain edge, adjacent to steep valley slopes. Both seepage types occur in depressions induced by soil saturation and function for surface water storage, pollutant removal, wildlife habitat, and nutrient cycling (Marble 1992).

3.5 Stream Characterization

Stream geometry and substrate data have been evaluated to orient stream restoration based on a classification utilizing fluvial geomorphic principles (Rosgen 1996). This classification stratifies streams into comparable groups based on pattern, dimension, profile, and substrate characteristics. Primary components of the classification include degree of entrenchment, width/depth ratio, sinuosity, channel slope, and stream substrate composition. Each stream type is modified by a number from 1 through 6 (example: E6) denoting a stream type which indicates a substrate dominated by 1) bedrock, 2) boulders, 3) cobble, 4) gravel, 5) sand, or 6) silt/clay.

On-Site streams were measured and characterized as E-type (narrow and deep), C-type (wide and shallow), and G-type (gully) channels. The location of each stream type is depicted in Figure 7. Figures 8 through 8I and Table 2A and 2B (Appendix B) depict morphological characteristics of existing on-Site channels. Individual cross-section data and other morphological information are included in Appendix C.

Camp Branch - Reach 1 (E-Type): Upstream of Headcut

Location: Extends from the upstream northern property boundary to a channel headcut which is migrating upstream due to disturbances associated with on-Site land management practices (Figure 8).

Dimension (Figure 8A)
Bankfull Channel Cross Sectional Area - 38.7 feet^2
Existing Channel Cross Sectional Area - 38.7 to 52.8 feet^2 (slightly enlarged)
Bank Height Ratio -1.1 to 1.3 (slight to moderate erosion hazard)
Width/Depth Ratio - 8 -12

Notes: Dimension values for this reach appear suitable for E-type streams in the vicinity.

Pattern
Sinuosity - 1.18

Notes: Pattern values for this reach appear suitable for E-type streams in the vicinity.

Profile (Figure 8B)
Valley Slope - 0.0047 rise/run
Water Surface Slope - 0.0029 rise/run
Pool Slope - 0 to 0.0013 rise/run
Riffle Slope - 0.0008 to 0.0167 rise/run

Notes: The upper range of riffle slopes are higher than expected, possibly due to headcut migration into the lower portions of the reach.

Substrate:
D50 - 7 millimeters (fine gravel)

Camp Branch – Reach 2 (E-Type): Headcut to Ford

Location: Extends downstream from the headcut to an active ford, utilized to access fields north of Camp Branch (Figure 8).

Dimension (Figure 8A)
Bankfull Channel Cross Sectional Area - 38.7 feet^2
Existing Channel Cross Sectional Area - 51 to 62 feet^2 (nearly twice bankfull cross sectional area)
Bank Height Ratio - 1.5 (moderate to high erosion hazard)

Width/Depth Ratio – 8.7
Notes: This reach of Camp Branch is oversized and moderately entrenched.

Pattern
Sinuosity - 1.18

Notes: Pattern values for this reach appear suitable for E-type streams in the vicinity.

Profile (Figure 8B)
Valley Slope - 0.0047 rise/run
Water Surface Slope - 0.0029 rise/run
Pool Slope - 0 to 0.007 rise/run
Riffle Slope - 0.0042 to 0.0144 rise/run

Notes: The steeper facet slopes may result from headcuts and other knick points in the channel bottom.

Substrate:
D50 - 5 millimeters (fine gravel)

Camp Branch – Reach 3 (G-Type): Downstream of Ford

Location: Extends from the ford to a portion of Camp Branch that begins to downcut to the Rocky River (Figure 8).

Dimension (Figure 8C)
Bankfull Channel Cross Sectional Area - 42 feet^2
Existing Channel Cross Sectional Area - 104 to 124 feet^2 (nearly three times the bankfull cross-sectional area)
Bank Height Ratio - 2.2 to 2.4 (high to excessive erosion hazard)
Width/Depth Ratio – 6 to 9

Notes: This reach of Camp Branch is oversized and highly entrenched.

Pattern
Sinuosity - 1.05

Notes: Straightening of the channel has resulted in a loss of pattern variables such as pool-to-pool spacing, meander length, and radius of curvature. Pattern values for this reach are outside the modal concept for stable, E-type streams in the region.

Profile (Figure 8D)
Valley Slope - 0.0047 rise/run
Water Surface Slope - 0.0041 rise/run
Pool Slope - 0.0000 to 0.0020 rise/run
Riffle Slope - 0.0011 to 0.0614 rise/run

Notes: Riffle slope to average water surface slope ratios vary between 0.27 and 15 indicating over-steepened riffle slopes. Similarly, pool slope to average water surface slope varies from 0 to 1.6 indicating over-steepened pool slopes. Over-steepened facet slopes result from dredging and straightening of Camp Branch and impacts from land use activities through the reach.

Substrate:
D50 – 13.8 millimeters (medium gravel)

Notes: Silt and clay particles make up 14 percent of the bed material, possibly indicating bimodal sediment transport from eroding channel banks.

Dula Thoroughfare (E-Type): Upstream Reach

Location: Extends downstream from a piped road crossing to the Rocky River floodplain (Figure 8).

Dimension (Figure 8E)
Bankfull Channel Cross Sectional Area - 5.1 feet^2
Existing Channel Cross Sectional Area - 5.1 to 5.5 feet^2 (slightly enlarged)
Bank Height Ratio - 1.0 to 1.1 (low erosion hazard)
Width/Depth Ratio – 6.1 to 8.0

Notes: Dimension values for this reach appear suitable for E-type streams in the vicinity.

Pattern
Sinuosity - 1.05

Notes: Although sinuosity values are low for stable E-type streams in the area, the valley is relatively steep and narrow, resulting in relatively straight channel development.

Profile (Figure 8F)
Valley Slope - 0.0239 rise/run
Water Surface Slope - 0.0228 rise/run
Pool Slope - 0 to 0.0161 rise/run
Riffle Slope - 0.0036 to 0.096 rise/run

Notes: Pool slopes and riffle slopes are relatively steep; however, the ratio of these facet slopes to average water surface slope (average riffle 1.6 and average pool 0.13) indicate stable profile values throughout this reach.

Substrate:
D50 – less than 1 millimeter (silt and clay)

Dula Thoroughfare (C-type): Downstream Reach

Location: Contained within the Rocky River floodplain and extends from alluvial fan deposits associated with the upstream reach to the property boundary (Figure 8).

Dimension (Figure 8G)
Bankfull Channel Cross Sectional Area - 5.7 to 8.4 feet^2
Existing Channel Cross Sectional Area - 5.7 to 19.7 feet^2 (slightly enlarged to highly oversized)

Bank Height Ratio - 1.0 to 2.0 (low to excessive erosion hazard)
Width/Depth Ratio – 23 to 40

Notes: The large variation in these values results from channel dredging and straightening, impounding of the reach for duck habitat, and low slope of the channel as it migrates through an unnatural channel across the Rocky River floodplain. Dimensional values appear to reside outside the modal concept for stable streams in the area.

Pattern
Sinuosity - 1.01

Notes: Dredging and straightening of the channel resulted in no measurable channel features (riffles and pools).

Profile (Figure 8H)
Valley Slope - 0.0019 rise/run
Water Surface Slope - 0.0019 rise/run

Notes: Pool slopes and riffle slopes were not measurable due to dredging and straightening activities and slackwater conditions through the reach; however, these values are not expected to be within the acceptable range for stable streams in the area.

Substrate:
D50 – less than 1 millimeter (silt and clay)

UT to Dula Thoroughfare (G-type): Upstream Reach

Location: Extends through an eroded section of channel for approximately 195 linear feet at the upper reaches of the stream (Figure 8).

Dimension (Figure 8I)
Bankfull Channel Cross Sectional Area – 4.8 feet^2
Existing Channel Cross Sectional Area – 12.8 feet^2 (more than 2.5 times bankfull cross sectional area)
Bank Height Ratio - 1.9 (excessive erosion hazard)
Width/Depth Ratio – 2.8

Notes: This reach of UT to Dula Thoroughfare is oversized and highly entrenched.

Pattern
Sinuosity - 1.09

Notes: Although sinuosity values are low for stable E-type streams in the area, the valley is relatively steep and narrow, resulting in relatively straight channel development.

Profile
Valley Slope – Not Measured

Water Surface Slope – Mot Measured

Notes: Pool slopes and riffle slopes are appear relatively steep due to headcut formation within the reach.

Substrate:
D50 – Not Measured

UT to Dula Thoroughfare (E-type): Downstream Reach

Location: Extends from the entrenched, upstream reach to a forded crossing of Dula Thoroughfare (Figure 8).

Dimension (Figure 8I)
Bankfull Channel Cross Sectional Area – 4.4 to 5.1 feet^2
Existing Channel Cross Sectional Area – 6.9 (slightly enlarged)
Bank Height Ratio - 1.5 to 2.3 (high to excessive erosion hazard)
Width/Depth Ratio – 6

Notes: This reach of UT to Dula Thoroughfare is slightly oversized and highly entrenched. Spoil castings on stream banks and within the adjacent floodplain occur through much of the reach.

Pattern
Sinuosity - 1.17

Notes: Shoot cutoffs and channel realignment is prevalent through this reach.

Profile
Valley Slope – Not Measured
Water Surface Slope – Mot Measured

Notes: Pool slopes and riffle slopes appear relatively steep due to headcut formation within the reach.

Substrate:
D50 – Not Measured

3.6 Plant Communities

The Site is characterized by broad expanses of agricultural fields, along with mesic mixed pine/hardwood forest, upland slope forest, bottomland hardwood forest, and game species food plots. Site forests do not exhibit climax conditions due to past timber practices. Primary agricultural crops include corn, cotton, and soy beans, with interspersed patches of sorghum and clover for game species. Invasive species identified in agricultural fields during fallow times or prior to planting of crops consists primarily of morning glory (*Convolvulus arvensis*), clover (*Trifolium campestre*), cocklebur (*Xanthium strumarium*), and sicklepod (*Cassia obtusifolia*).

Mesic mixed pine/hardwood forest occurs adjacent to undisturbed streams descending from slopes adjacent to the Rocky River floodplain. The community occurs as narrow bands adjacent to smaller tributaries such as UT to Camp Branch, the upper reaches of Dula Thoroughfare, and the UT to Dula Thoroughfare. Species present include loblolly pine (*Pinus taeda*), red maple (*Acer rubrum*), American sycamore (*Platanus occidentalis*), green ash (*Fraxinus pennsylvanica*), and hackberry (*Celtis laevigata*). Vines present within this community include poison ivy (*Toxicodendron radicans*), greenbriar (*Smilax rotundifolia*), and muscadine (*Vitus rotundifolia*).

Upland slope forest occurs on steep, dry slopes adjacent to floodplains and includes species such as white oak (*Quercus alba*), water oak (*Quercus nigra)*, Virginia pine (*Pinus virginiana*), and various hickories (*Carya* spp.). Understory species include red maple, winged sumac (*Rhus copallinum*), and dogwood (*Cornus florida*) while vines present include poison ivy and muscadine.

Bottomland hardwood forest is located in moist, frequently flooded flats adjacent to the Rocky River and Camp Branch. This community is characterized by species such as American sycamore, black willow, green ash, American elm (*Ulmus americana*), tulip poplar (*Liriodendron tulipifera*), and sugarberry (*Celtis laevigata*). The shrub component of this community includes Chinese privet (*Ligustrum sinense*), Japanese honeysuckle (*Lonicera japonica*), red maple, sweetgum, and muscadine.

3.7 Protected Species

3.7.1 Federally Protected Species

Species with the Federal classification of Endangered (E), Threatened (T), or officially Proposed (P) for such listing are protected under the Endangered Species Act (ESA) of 1973, as amended (16 U.S.C. 1531 *et seq.*). The term “Endangered species” is defined as “any species which is in danger of extinction throughout all or a significant portion of its range”, and the term “Threatened species” is defined as “any species which is likely to become an Endangered species within the foreseeable future throughout all or a significant portion of its range” (16 U.S.C. 1532).

The following Federally protected species are listed for Anson County (5 February 2003 FWS list):

Common Name	Scientific Name	Status
Bald eagle	*Haliaeetus leucocephalus*	T
Red-cockaded woodpecker	*Picoides borealis*	E
Carolina heelsplitter	*Lasmigona decorata*	E
Schweinitz’s sunflower	*Heilanthus schweinitizii*	E

Bald Eagle

The bald eagle is a large raptor with a wingspan greater than 6 feet. Adult bald eagles are dark brown with a white head and tail. Immature eagles are brown with whitish mottling on the tail, belly, and wing linings. Bald eagles typically feed on fish but may also take birds and small mammals. In the Carolinas, nesting season extends from December through May (Potter *et al*. 1980). Bald eagles typically nest in tall, living trees in a conspicuous location near open water. Eagles forage over large bodies of water and utilize adjacent trees for perching (Hamel 1992). Disturbance activities within a primary zone extending 750 to 1500 feet from a nest tree are considered to result in unacceptable conditions for eagles (USFWS 1987). The FWS recommends avoiding disturbance activities, including construction and tree-cutting, within this primary zone. Within a secondary zone, extending from the primary zone boundary out to a distance of 1.0 mile from a nest tree, construction and land-clearing activities should be restricted to the non-nesting period. The FWS also recommends avoiding alteration of natural shorelines where bald eagles forage, and avoiding significant land-clearing activities within 1500 feet of known roosting sites.

The Site is located near open water systems which may be suitable for bald eagle feeding habitat. However, on-Site perching and nesting trees are limited to a disturbed, narrow fringe (approximately 25 to 50 feet in width) adjacent to the Rocky River. NHP records show the nearest elemental occurrence of bald eagle approximately 3.1 miles north of the Site, immediately south of Lake Tillery's Norwood Dam. NHP records and a lack of perching and nesting habitat indicate that, this project is not expected to adversely effect known populations of Bald Eagle.

BIOLOGICAL CONCLUSION **NO EFFECT**

Red-Cockaded Woodpecker

This small woodpecker (7 to 8.5 inches in length) has a black head, prominent white cheek patches, and a black-and-white barred back. Males often have red markings (cockades) behind the eye, but the cockades may be absent or difficult to see (Potter *et al*. 1980). Primary nest sites for red-cockaded woodpeckers include open pine stands greater than 60 years of age with little or no mid-story development. Foraging habitat is comprised of open pine or pine/mixed hardwood stands 30 years of age or older (Henry 1989). Nest cavities are constructed in the heartwood of living pines, generally older than 70 years, which have been infected with red-heart disease. Nest cavity trees tend to occur in clusters, which are referred to as colonies (USFWS 1985). The woodpecker drills holes into the bark around the cavity entrance, resulting in a shiny, resinous buildup around the entrance that allows for easy detection of active nest trees. Ideal nesting and foraging sites for this woodpecker include pine flatwoods or pine-dominated savannas which have been maintained by frequent natural or prescribed fires. Development of a thick understory may result in abandonment of cavity trees.

Field investigations indicate no suitable nesting or foraging habitat (pine stands greater than 30 years of age) within, or adjacent to, the Site. Based on NHP records, observations conducted during field investigations, and existing conditions of the Site, this project is not expected to adversely effect known populations of red-cockaded woodpecker.

BIOLOGICAL CONCLUSION **NO EFFECT**

Carolina Heelsplitter

The Carolina heelsplitter has an ovate, trapezoid shaped, unsculptured shell which grows to a maximum of approximately 4.5 inches length, by 2.7 inches height, and 1.5 inches in width (USFWS 1996). The shell varies in color from a greenish brown to dark brown on the outer surface and is often pearly to whitish blue, grading to orange on the inside surface. The dorsal margin is straight and may end in a slight wing, and the umbo is flattened. Beak sculpture is depressed and double looped, extending slightly past the hinge line. Lateral teeth are generally, thin and pseudo-cardinal teeth are lamellar and parallel to the dorsal margin (TSCFTM 1990).

Historically, this species was reported in the Abbeville district of South Carolina and Mecklenburg County in North Carolina (Clarke 1985). The Abbeville district is bordered on the south by the Savannah River and on the north by the Saluda River. Presently the species range is limited to only six small streams and one small river. The heelsplitter is usually found in mud, muddy sand, or muddy gravel substrates along stable, well-shaded stream banks (Keferl and Shelly 1988). Currently, the heelsplitter is found in only two small remnant populations in North Carolina: 1) a tributary (Goose Creek) to the Rocky River located in Union County and 2) in a tributary (Waxhaw Creek) to the Catawba River located in Union County (USFWS 2003).

NHP records indicate that this species has not been documented within 2.0 miles of the Site. However, the Site is located within the Rocky River drainage basin, and portions of Site streams are characterized by stable, vegetated stream banks; therefore, detailed surveys for presence of this species were necessary prior to initiation of Site implementation.

The Catena Group, Inc was retained to complete a field survey for the Carolina heelsplitter in the waters of Camp Branch, UT to Camp Branch, Dula Thoroughfare, UT to Dula Thoroughfare, and Rocky River. It was found that the streams surveyed were generally not suitable as freshwater mussel habitat, and no Carolina Heelsplitter mussels were found in the survey. There is a slight possibility that mussel populations exist downstream of the project site on the Rocky River, but it is unlikely that these populations include the Carolina Heelsplitter. For this reason, the Catena Group anticipates the stream mitigation within the Bishop tract to be **"Not Likely To Adversely Effect"** the Carolina Heelsplitter (Freshwater Mussel Survey, Appendix E).

BIOLOGICAL CONCLUSION **NOT LIKELY TO ADVERSELY EFFECT**

Schweinitz's Sunflower

Schweinitz's sunflower is an erect, unbranched, rhizomatous, perennial herb that grows to approximately 6 feet in height. The stem may be purple and is usually pubescent; however, the stems are sometimes nearly smooth. Leaves are sessile, opposite on the lower stem but alternate above and are lanceolate in shape, averaging 5 to 10 times as long as wide. The leaves are rather thick and stiff, with a few small serrations. The upper leaf surface is rough and

the lower surface is usually pubescent with soft white hairs. Schweinitz's sunflower blooms from September to frost. Flower heads are yellow and approximately 0.6 inches in diameter. The current range of this species is within 60 miles of Charlotte, North Carolina, occurring on upland interstream flats or gentle slopes. The plants usually occur in soils that are thin or clay in texture. The species needs open areas protected from shade or excessive competition, reminiscent of Piedmont prairies. Disturbances such as fire maintenance or regular mowing help sustain preferred habitat (USFWS 1994).

NHP records indicate that this species has not been documented within 2.0 miles of the Site. Schweinitz's sunflower needs open areas protected from shade or excessive competition, reminiscent of Piedmont prairies. Roadside edges have been maintained as an open herbaceous community and appear to be suitable habitat for Schweinitz's sunflower. Agricultural field edges may provide additional habitat, providing that they are not intensively maintained and that competition from agricultural weeds is not excessive. Detailed surveys for this species were conducted on September 21 and 22, 2004, using systematic transects along all possible habitat areas. No specimens of Schweinitz's sunflower were found. Based on NHP records, field surveys, and professional judgment, this project will not affect Schweinitz's sunflower.

BIOLOGICAL CONCLUSION **NO EFFECT**

3.7.2 State Protected Species

Plant and animal species which are on the North Carolina State list as Endangered (E), Threatened (T), Special Concern (SC), Candidate (C), Significantly Rare (SR), or Proposed (P) (Amoroso 2002) receive limited protection under the North Carolina Endangered Species Act (G.S. 113-331 *et seq.*) and the North Carolina Plant Protection Act of 1979 (G.S. 106-202 *et seq.*). A records search of NHP files indicates one element occurrence within 2.0 miles of the Site. The thin-pod white wild indigo (*Baptisia albescens*) is not federally listed; however, it is listed in North Carolina as SR-P* (-P = species at the periphery of its range in North Carolina, * = historic record, not seen since 1979). Restoration activities are not expected to adversely affect this species.

4.0 REFERENCE STUDIES

4.1 Reference Channel

A fundamental concept of stream classification entails the development and application of regional reference curves to stream reconstruction and enhancement. Regional reference curves can be utilized to predict bankfull stream geometry, discharge, and other parameters in altered systems. Development of regional reference curves for North Carolina was initiated in 1995. The curves characterize a broad range of streams within the Piedmont physiographic province. Small watersheds or deviations in valley slope, land use, or geologic substrate may not be accurately described by the curves; therefore, verification of individual watersheds may be necessary. On-Site and off-site reference reaches have been utilized in conjunction with regional curves for detailed planning and characterization of this restoration project.

In order to develop proposed geometric parameters for on-Site, degraded channels, three nearby streams were measured for reference. The primary reference reaches for larger, lower slope on-Site channels are located 1) within Camp Branch at the upper on-Site reaches of the channel and 2) approximately 35 miles northwest of the Site on an unnamed tributary to Crane Creek. These reference streams are characterized by E-type channels.

The primary reference reach for smaller, higher slope on-Site channels is located approximately 34 miles west of the Site on an unnamed tributary to Reedy Creek. This reference stream is characterized as an E-type channel.

Table 3 (Appendix B) includes a summary of dimension, profile, and pattern data for the reference reaches used to establish reconstruction parameters. Channel cross-sections were measured at systematic locations and stream profiles were developed via laser level and GPS. Stream substrates were quantified through systematic pebble counts along the reference reach. Individual cross-section data and other morphological information are included in Appendix D.

Initially, reference streams were visited and classified by stream type (Rosgen 1996). This classification stratifies streams into comparable groups based on geometric characteristics. Reference reaches identified in the vicinity were characterized primarily as E-type (highly sinuous) channels with sand or gravel substrate. E-type streams are slightly entrenched, highly sinuous (>1.5) channels which exhibit high meander width ratios (belt width/bankfull width). In North Carolina, E-type streams occur in narrow to wide valleys with well-developed alluvial floodplains (Valley Type VIII). These streams exhibit a sequence of riffles and pools associated with a sinuous flow pattern.

<u>Dimension</u>

Camp Branch - Reach 1 (E-Type): Upstream of Headcut (Figure 8)

Bankfull Channel Cross Sectional Area – 38.7 feet^2

Existing Channel Cross Sectional Area – 38.7 to 44.1 feet^2 (slightly enlarged)

Bank Height Ratio – 1.0 to 1.3 (slight erosion hazard)

Width/Depth Ratio – 8 to 12

UT to Crane Creek

Bankfull Channel Cross Sectional Area – 20.5 feet^2
Existing Channel Cross Sectional Area – 23.5 to 30.7 feet^2 (slightly enlarged)
Bank Height Ratio – 1.1 to 1.2 (low erosion hazard)
Width/Depth Ratio – 5 to 6

UT to Reedy Creek

Bankfull Channel Cross Sectional Area – 15.5 feet^2
Existing Channel Cross Sectional Area – 14.2 to 20.6 feet^2 (slightly enlarged)
Bank Height Ratio - 1.0 to 1.2 (low erosion hazard)
Width/Depth Ratio – 6 to 8

Pattern

Camp Branch - Reach 1 (E-Type): Upstream of Headcut (Figure 8)

Sinuosity - 1.18

UT to Crane Creek

Sinuosity - 1.8

UT to Reedy Creek

Sinuosity - 1.55

Profile

Camp Branch - Reach 1 (E-Type): Upstream of Headcut (Figure 8)

Valley Slope – 0.0047 rise/run
Water Surface Slope – 0.0029 rise/run
Riffle Slope – 0.0008 to 0.0167 rise/run
Pool Slope – 0 to 0.0013 rise/run

UT to Crane Creek

Valley Slope – 0.0025 rise/run
Water Surface Slope – 0.0014 rise/run
Riffle Slope – 0.0006 to 0.0033 rise/run
Pool Slope – 0 to 0.0006 rise/run

UT to Reedy Creek

Valley Slope – 0.0172 rise/run
Water Surface Slope – 0.0111 rise/run
Riffle Slope – 0.0105 to 0.0221 rise/run
Pool Slope – 0.0016 to 0.0182 rise/run

Substrate:

Camp Branch - Reach 1 (E-Type): Upstream of Headcut (Figure 8)

D50 – 7.2 millimeters

UT to Crane Creek

D50 – 1.9 millimeters

UT to Reedy Creek

D50 – 0.05 millimeters

4.2 Reference Forest Ecosystem

According to Mitigation Site Classification (MiST) guidelines (EPA 1990), Reference Forest Ecosystems (RFEs) must be established for restoration sites. RFEs are forested areas on which to model restoration efforts of the restoration site in relation to soils, hydrology, and vegetation. RFEs should be ecologically stable climax communities and should represent believed historical (pre-disturbance) conditions of the restoration site. Quantitative data describing plant community composition and structure are collected at the RFEs and subsequently applied as reference data for design of the restoration site planting scheme.

There were two RFE areas chosen to guide plant community restoration within the on-Site floodplain, channel banks, and adjacent floodplain slopes. The RFEs are both found within the Southern Outer Piedmont Ecoregion, one west and one northwest of the Site. Both RFEs support plant community, landform, and hydrological characteristics that restoration efforts will attempt to emulate. Circular, 0.1-acre plots were randomly established within the selected RFEs. Data collected within each plot include 1) tree, shrub, and herb species composition; 2) number of stems for each tree and shrub species; and 3) diameter at breast height (DBH) for each tree and shrub species. Field data (Table 4A and 4B [Appendix B]) indicate importance values (IV) of dominant tree species calculated based on relative density, dominance, and frequency of tree species composition (Smith 1980). Hydrology, surface topography, and habitat features were also evaluated.

The northwestern RFE is located in the floodplain of the UT to Crane Creek in Rowan County, North Carolina. Three 0.1-acre plots were established which best characterize expected steady-state forest composition. Forest vegetation was dominated by swamp chestnut oak (*Quercus michauxii*) (IV=0.17), green ash (IV=0.13), American elm (IV=0.10), and shagbark hickory (*Carya ovata*) (IV=0.09) (Table 4A [Appendix B]). Portions of the canopy were also dominated by willow oak (*Quercus phellos*), boxelder (*Acer negundo*), tulip poplar, black tupelo (*Nyssa sylvatica*), and red maple.

The western RFE is located in the floodplain of Reedy Creek in Mecklenburg County, North Carolina. Within the RFE, vegetative sampling at four 0.1-acre plots indicate that forest tree vegetation was dominated by tulip poplar (IV=0.12), American elm (IV=0.10), northern red oak (*Quercus rubra*) (IV=0.08), and black walnut (*Juglans nigra*) (IV=0.07) (Table 4B [Appendix B]). Other, less dominant tree species within the sample plots were green ash, boxelder, and American sycamore.

5.0 STREAM POWER AND SHEAR STRESS STUDIES

5.1 Discharge

Discharge estimates for the Site utilize an assumed definition of "bankfull" and the return interval associated with the bankfull discharge. For this study, the bankfull channel is defined as the channel dimensions designed to support the "channel forming" or "dominant" discharge (Gordon *et al.* 1992). Research indicates that a stable stream channel may support a return interval for bankfull discharge, or channel-forming discharge, between 1 to 2 years (Gordon *et. al.* 1992, Dunne and Leopold 1978). The methods of Rosgen (1996) indicate calibration of bankfull dimensions based on a potential bankfull return interval between 1.3 and 1.5 years for rural conditions.

Discharge within the Site appears to be dominated by a combination of upstream basin catchment, groundwater flow, and precipitation. Based on regional curves (Harman *et al.* 1999), the bankfull discharge for a 2.9 square mile watershed is expected to average approximately 192 cubic feet per second. Current research estimates a bankfull discharge of 192 cubic feet per second would be expected to occur approximately every 1.3 to 1.5 years (Rosgen 1996).

5.2 Stream Power, Shear Stress, and Stability Threshold

5.2.1 Stream Power

Stability of a stream refers to its ability to adjust itself to in-flowing water and sediment load. One form of instability occurs when a stream is unable to transport its sediment load, leading to aggradation, or deposition of sediment onto the stream bed. Conversely, when the ability of the stream to transport sediment exceeds the availability of sediments entering a reach, and/or stability thresholds for materials forming the channel boundary are exceeded, erosion or degradation occurs.

Stream power is the measure of a stream's capacity to move sediment over time. Stream power can be used to evaluate the longitudinal profile, channel pattern, bed form, and sediment transport of streams. Stream power may be measured over a stream reach (total stream power) or per unit of channel bed area. The total stream power equation is defined as:

$$\Omega = \rho g Q s$$

where Ω = total stream power (ft-lb/s-ft), ρ = density of water (lb/ft^3), g = gravitational acceleration (ft/s^2), Q = discharge (ft^3/sec), and s = energy slope (ft/ft). The specific weight of water (γ = 62.4 lb/ft^3) is equal to the product of water density and gravitational acceleration, ρg. A general evaluation of power for a particular reach can be calculated using bankfull discharge and water surface slope for the reach. As slopes become steeper and/or velocities increase, stream power increases and more energy is available for re-working channel materials. Straightening and clearing channels increases slope and velocity and thus stream power. Alterations to the stream channel may conversely decrease stream power. In particular, over-widening of a channel will dissipate energy of flow over a larger area. This process will

decrease stream power, allowing sediment to fall out of the water column, possibly leading to aggradation of the streambed.

The relationship between a channel and its floodplain is also important in determining stream power. Streams that remain within their banks at high flows tend to have higher stream power and relatively coarser bed materials. In comparison, streams that flood over their banks onto adjacent floodplains have lower stream power, transport finer sediments, and are more stable. Stream power assessments can be useful in evaluating sediment discharge within a stream and the deposition or erosion of sediments from the streambed.

5.2.2 Shear Stress

Shear stress, expressed as force per unit area, is a measure of the frictional force that flowing water exerts on a streambed. Shear stress and sediment entrainment are affected by sediment supply (size and amount), energy distribution within the channel, and frictional resistance of the streambed and bank on water within the channel. These variables ultimately determine the ability of a stream to efficiently transport bedload and suspended sediment.

For flow that is steady and uniform, the average boundary shear stress exerted by water on the bed is defined as follows:

$$\tau = \gamma R s$$

where τ = shear stress (lb/ft^2), γ = specific weight of water, R = hydraulic radius (ft), and s = the energy slope (ft/ft). Shear stress calculated in this way is a spatial average and does not necessarily provide a good estimate of bed shear at any particular point. Adjustments to account for local variability and instantaneous values higher than the mean value can be applied based on channel form and irregularity. For a straight channel, the maximum shear stress can be assumed from the following equation:

$$\tau_{max} = 1.5\tau$$

for sinuous channels, the maximum shear stress can be determined as a function of plan form characteristics:

$$\tau_{max} = 2.65\tau(R_c / W_{bkf})^{-0.5}$$

where R_c = radius of curvature (ft) and W_{bkf} = bankfull width (ft).

Shear stress represents a difficult variable to predict due to variability of channel slope, dimension, and pattern. Typically, as valley slope decreases channel depth and sinuosity increase to maintain adequate shear stress values for bedload transport. Channels that have higher shear stress values than required for bedload transport will scour bed and bank materials, resulting in channel degradation. Channels with lower shear stress values than needed for bedload transport will deposit sediment, resulting in channel aggradation.

The actual amount of work accomplished by a stream per unit of bed area depends on the available power divided by the resistance offered by the channel sediments, plan form, and vegetation. The stream power equation can thus be written as follows:

$$\omega = \rho g Q s = \tau v$$

where ω = stream power per unit of bed area (N/ft-sec, Joules/sec/ft^2), τ = shear stress, and v = average velocity (ft/sec). Similarly,

$$\omega = \Omega / W_{bkf}$$

where W_{bkf} = width of stream at bankfull (ft).

5.2.3 Stream Power and Shear Stress Methods and Results

Channel degradation or aggradation occurs when hydraulic forces exceed, or do not approach, the resisting forces in the channel. The amount of degradation or aggradation is a function of relative magnitude of these forces over time. The interaction of flow within the boundary of open channels is only imperfectly understood. Adequate analytical expressions describing this interaction have yet to be developed for conditions in natural channels. Thus, means of characterizing these processes rely heavily upon empirical formulas.

Traditional approaches for characterizing stability can be placed in one of two categories: 1) maximum permissible velocity and 2) tractive force, or stream power and shear stress. The former is advantageous in that velocity can be measured directly. Shear stress and stream power cannot be measured directly and must be computed from various flow parameters. However, stream power and shear stress are generally better measures of fluid force on the channel boundary than velocity.

Using these equations, stream power and shear stress were estimated for

1) Camp Branch Reach 1 and 2: Upstream of Headcut to Ford,
2) Camp Branch Reach 3: Downstream of Ford,
3) Dula Thoroughfare: Upstream Reach,
4) Dula Thoroughfare: Downstream Reach,
5) Camp Branch, Reference Reach,
6) UT to Reedy Creek (reference area),
7) UT to Crane Creek (reference area), and
8) Proposed on-Site conditions.

Important input values and output results (including stream power, shear stress, and per unit shear power and shear stress) are presented in Table 5. Average stream velocity and discharge values were calculated for existing on-Site stream reaches, reference reaches, and proposed conditions.

Table 5. Stream Power (Ω) and Shear Stress (τ) Values

Stream Reach	Discharge (Q) (ft^3/sec)	Water surface Slope (s) (ft/ft)	Total Stream Power (Ω) = γ Qs	Ω/W	Hydraulic Radius (R) = A/WP	Shear Stress (τ) = γ Rs (lb/ft^2)	Velocity (v) (ft/sec)	τ v
Camp Branch				□				□
Reach 1 and 2 (E-type) Upstream to Ford	168	0.0029	30.40	1.66	1.72	0.31	4.34	1.35
Reach 3 (G-type) Downstream of Ford	182	0.0041	**46.56**	2.62	1.86	**0.48**	4.33	2.06
Dula Thoroughfare								
Upstream Reach	19.3	0.0228	27.46	4.58	0.65	0.93	3.78	3.52
Downstream Aggrading Reach	30	0.0019	**3.56**	0.25	0.47	**0.06**	4.29	0.24
Reference								
Camp Branch	168	0.0029	30.40	1.55	1.64	0.30	4.34	1.29
UT to Reedy Creek	44	0.0111	30.48	2.93	1.17	0.81	2.84	2.31
UT to Crane Creek	119	0.0014	10.40	1.03	1.45	0.13	5.80	0.74
Proposed Camp Branch								
Camp Branch upstream	168	0.0031	32.50	1.51	1.51	0.29	4.44	1.29
Camp Branch Middle Reach	182	0.0031	35.21	1.57	1.60	0.31	4.33	1.34
Proposed Dula (non-braided reach)								
Proposed Dula	23	0.007	10.05	1.17	0.62	0.27	3.71	1.60

As would be expected, stream power and shear stress are lowest in the aggrading reaches (Dula Thoroughfare) and low slope reference reaches. Conversely, stream power and shear stress are highest in the on-Site reaches which are currently showing signs of degradation (Camp Branch Reach 3). Stream power is the highest for the dredged and straightened, G-type reach, where slopes have been steepened, cross-sectional area is high, width-to-depth ratio is low, bank erosion is high, and the channel is highly incised.

In order to maintain sediment transport functions of a stable stream system, the non-braided reaches of proposed channels should exhibit stream power and shear stress values that neither aggrade nor degrade. Results of the analysis indicate that the non-braided proposed channel reaches are expected to maintain stream power values of approximately 10 to 35 and shear stress values of approximately 0.27 to 0.31 (similar to that of reference reaches and considerably less than that of the existing degrading reaches). Therefore, the design channel is expected to effectively transport sediment through the Site, resulting in stable channel characteristics.

6.0 RESTORATION PLAN

The primary goals of this restoration plan include 1) construction of stable, riffle-pool stream complexes; 2) construction of a backwater slough, braided stream complex, 3) creation of a natural vegetation buffer along enhanced and restored stream channels; 4) maximize the re-establishment of historic wetland function; 5) restoration of wildlife functions associated with a riparian corridor, and 6) protection of the Site in perpetuity.

The complete restoration plan is depicted in Figure 9. The proposed restoration plan is expected to provide the following:

1. 5,663 linear feet of stream restoration
2. 1,190 linear feet of stream enhancement - level 1 (restoration of dimension and profile)
3. 7,306 linear feet of stream enhancement – level 2 (remove from agriculture, remove spoil from the banks, and re-vegetate)
4. 11,250 linear feet of stream preservation
5. 10.2 acres of wetland preservation
6. 5.6 acres of wetland restoration
7. 0.9 acres of wetland enhancement

Components of this plan may be modified based on construction or access constraints.

Primary activities proposed at the Site include 1) stream enhancement/restoration, 2) wetland enhancement/restoration, 3) soil scarification, and 4) plant community restoration. A monitoring plan is outlined in Section 7 of this document.

6.1 Stream Enhancement/Restoration

This stream enhancement/restoration effort is designed to reconstruct stable, meandering streams that approximate hydrodynamics, stream geometry, and local microtopography relative to reference conditions. This effort consists of 1) stream reconstruction on new location, 2) stream reconstruction in place, and 3) ford construction. Geometric attributes for the proposed, stable channels are listed in Table 6A and 6B (Appendix B).

6.1.1 Reconstruction on New Location

Reaches proposed for reconstruction on new location are depicted on Figure 9A to 9C. Primary activities designed to reconstruct the channel on new location include 1) belt-width preparation and grading, 2) floodplain bench excavation, 3) channel excavation, 4) installation of channel plugs, and 5) backfilling of the abandoned channel.

<u>Belt-width Preparation and Grading</u>

Care will be taken to avoid the removal of existing, deeply rooted vegetation within the belt-width corridor which may provide design channel stability. Material excavated during grading will be stockpiled immediately adjacent to channel segments to be abandoned and backfilled. These segments will be backfilled after stream diversion is completed.

Spoil material may be placed to stabilize temporary access roads and to minimize compaction of the underlying floodplain. However, all spoil will be removed from floodplain surfaces upon completion of construction activities.

Floodplain Bench Excavation

The creation of a bankfull, floodplain bench is expected to 1) remove the eroding material and collapsing banks, 2) promote overbank flooding during bankfull flood events, 3) reduce the erosive potential of flood waters, and 4) increase the width of the active floodplain. Bankfull benches may be created by excavating the adjacent floodplain to bankfull elevations or filling eroded/abandoned channel areas with suitable material. After excavation, or filling of the bench, a relatively level floodplain surface is expected to be stabilized with suitable erosion control measures. Planting of the bench with native floodplain vegetation is expected to reduce erosion of bench sediments, reduce flow velocities in flood waters, filter pollutants, and provide wildlife habitat.

After excavation of the floodplain bench, the design channel and updated profile survey will be developed and the location of each meander wavelength plotted and staked along the profile. Pool locations and relative frequency configurations may be modified in the field based on local variations in the floodplain profile.

Channel Excavation

The channel will be constructed within the range of values depicted in Table 6A and 6B (Appendix B). The channel will be excavated to the approximate dimensions depicted on Figure 10. The channel should be excavated to the proposed channel depth and width. Material excavated from the proposed design channel will be stockpiled adjacent to the reach of channel to be backfilled or will be wasted on upland portions of the Bishop property, as directed by the field engineer.

Stream banks and local belt-width area of constructed channels will be immediately planted with shrub and herbaceous vegetation. Particular attention will be directed toward providing vegetative cover and root growth along the outer bends of each stream meander. Live willow stake revetments will be constructed as conceptually depicted in Figure 11. Available root mats or biodegradable, erosion-control matting may be embedded into the break-in-slope to promote more rapid development of an overhanging bank. Willow stakes will be purchased and/or collected on-Site and inserted through the root/erosion mat into the underlying soil.

Channel Plugs

Impermeable plugs will be installed along abandoned channel segments at locations depicted on Figure 9A to 9C. The plugs will consist of low-permeability materials or hardened structures designed to be of sufficient strength to withstand the erosive energy of surface flow events across the Site. Dense clays may be imported from off-site or existing material, compacted within the channel, may be suitable for plug construction. The plug will be sufficiently wide and deep to form an imbedded overlap in the existing banks and channel bed.

Channel Backfilling

After impermeable plugs are installed, the abandoned channel will be back-filled. Backfilling will be performed primarily by pushing stockpiled materials into the channel. The channel will be filled to the extent that on-Site material is available and compacted to maximize microtopographic variability, including ruts, ephemeral pools, and hummocks in the vicinity of the backfilled channel.

In-Stream Structures

Stream restoration under natural stream design techniques normally involves the use of in-stream structures for bank stabilization, grade control, and habitat improvement. Primary activities designed to achieve these objectives may include the installation of cross-vane weirs, J-hook vanes, and log vanes.

Cross-vane Weirs

The purpose of the vane is to 1) sustain bank stability, 2) direct high velocity flows during bankfull events toward the center of the channel, 3) maintain average pool depth throughout the reach, 4) preserve water surface elevations and reconnect the adjacent floodplain to flooding dynamics from the stream, and 5) modify energy distributions through increases in channel roughness and local energy slopes during peak flows.

Cross-vane weirs will be constructed as conceptually depicted in Figure 12. Cross-vane weir construction will be initiated by imbedding footer rocks into the stream bed for stability and to prevent undercutting of the structure. Header rocks will then be placed atop the footer rocks at the design elevation. Footer and header rocks create an arm that slopes from the center of the channel upward at approximately 7 to 10 degrees, tying in at the bankfull floodplain elevation. The cross-vane arms at both banks will be tied into the bank with a sill to eliminate the possibility of water diverting around the structure. Once the header and footer stones are in place, filter fabric will be buried into a trench excavated around the upstream side of the vane arms. The filter fabric is then draped over the header rocks to force water over the vane. The upstream side of the structure can then be backfilled with suitable material to the elevation of the header stones.

J-hook/log vanes

The primary purpose of the J-hook and log vanes is to direct high-velocity flows during bankfull events toward the center of the channel. J-hook vanes will be constructed using the same type and size of rock employed in the construction of cross-vane weirs (Figure 13). Log vanes will be constructed utilizing large tree trunks harvested from the Site or imported from off-site. The tree stem harvested for a log-vane arm must be long enough to be imbedded into the stream channel and extend several feet into the floodplain (Figure 14). A trench will be dug into the stream channel that is deep enough for the head of the log to be at or below the channel invert. The trench is then extended into the floodplain and the log is set into the trench such that the log arm is below the floodplain elevation. If the log is not of sufficient size to completely block stream flow (gaps occur between the log and channel bed) then a footer log or stone footers will be installed beneath the header log. Boulders will then be situated at the base of the log and at the head of the log to hold the log in place.

Similar to a cross vane, the arm of the J-hook vane and the log vane (which forms an arm) must slope from the center of the channel upward at approximately 7 to 10 degrees, tying in at the bankfull floodplain elevation. Once these vanes are in place, filter fabric is toed into a trench on the upstream side of the vane and draped over the structure to force water over the vane. The upstream side of the structure is then backfilled with suitable material.

6.1.2 Stream Reconstruction In-Place

Stream reconstruction in-place is expected in 1) areas where channel pattern has not been altered; however, the channel has incised due bed or bank erosion, or 2) areas where backwater slough conditions will persist once restoration has been completed. Reaches proposed for reconstruction in-place are depicted in Figure 9A to 9C. Primary activities designed to achieve these objectives may include 1) installation of in-stream structures, 2) creation of a floodplain bench, 3) excavation of a backwater slough/braided channel system, 4) spoil removal, 5) backfilling abandoned channels, and 6) diversion of bankfull flows to historic channels.

Installation of in-stream structures and creation of a floodplain bench has been described in detail in Section 6.1.1 (Stream Reconstruction on New Location) of this document. The design, installation, and function of in-stream structures and floodplain bench are similar for stream reconstruction in-place.

Excavation of a Backwater Slough/Braided Channel System

Backwater slough/braided channel systems will be designed to mimic reference wetland and stream conditions found within the Rocky River floodplain. Conditions include 1) convoluted interception of groundwater and flood flows, 2) average slope of upland-wetland interface and slough surface, 3) micro-topographic variation along the slough surface, and 4) soil modification and debris deposition.

Backwater slough/braided channel construction will occur within, and adjacent to, the existing Dula Thoroughfare aggrading ditch/channel (Figure 9B). Construction of the backwater slough/braided channel system will initiate at the confluence of Dula Thoroughfare and the Rocky River floodplain. The system will extend approximately 1195 feet downstream as a series of shallow, irregularly shaped depressions interspersed between shallow, braided stream channels. The depressions will range to a maximum of 1-foot below the proposed surface elevation in the center of the depression. The isolated depressions are expected to fill with organic matter and sediment, with development of braided channel occurring passively over time.

Spoil Removal

Spoil material deposited adjacent to the downstream reaches of Dula Thoroughfare and the UT to Dula Thoroughfare will be removed from channel banks and deposited in abandoned channels or wasted in upland portions of the Site/adjacent agricultural fields. Spoil removal areas are depicted in Figure 9B and 9C. Removal of spoil material is expected to facilitate overbank flooding, thereby extending floodprone areas and reducing scour potential of local flood flows.

Backfilling Abandoned Channels

Several reaches of the UT to Dula Thoroughfare are characterized by shoot cutoffs; secondary channels that have been blocked from normal flows by spoil castings; and excavated channels adjacent to an historic, abandoned channel. Backfilling of these abandoned channels with spoil material or material excavated from the floodplain will redirect stream flow through the historic, abandoned reaches of channel.

Diversion of Bankfull Flows

Bankfull discharge currently appears to be re-directed through a ditch connecting the downstream reach of Dula Thoroughfare to the Rocky River. This ditch effectively splits stormwater discharge from Dula Thoroughfare during bankfull flood events. Conversely, the ditch transmits water to Dula Thoroughfare during high volume flood flows from the Rocky River. Filling this ditch, and redirecting bankfull discharge through Dula Thoroughfare will allow for "channel forming" flows to continue natural evolutionary channel processes within on-Site and downstream reaches of Dula Thoroughfare.

6.1.3 Ford Construction

Landowner constraints will necessitate the installation of three channel fords to allow access to portions of the property isolated by the conservation easement and/or stream and wetland restoration activities. Proposed channel ford locations are depicted on Figure 9. The fords are expected to consist of shallow depressions in stream banks where vehicular crossings can be made (Figure 15). The fords will be constructed of hydraulically stable rip-rap or suitable rock and will be large enough to handle the weight of anticipated vehicular traffic. Approach grades to the ford will be at a minimum 15:1 slope and constructed of hard, scour-resistant crushed rock or other permeable material, which is free of fines. The bed elevation of the ford will equal the stream bed elevation above and below the ford to reduce the risk of headcutting.

6.2 Wetland Enhancement/Restoration

Site alterations to wetland areas and/or areas underlain by hydric soils are designed to re-establish a fully functioning wetland system which will provide surface water storage, nutrient cycling, removal of imported elements and compounds, and will create a variety and abundance of wildlife habitat. Wetland enhancement/restoration activities are expected to restore approximately 5.6 acres of jurisdictional wetland and enhance approximately 0.9 acre of jurisdictional wetland (Figure 9). The proposed conservation easement also encompasses approximately 10.2 acres of existing, relatively undisturbed jurisdictional wetland which will be preserved in-perpetuity.

Portions of the Site underlain by hydric soil have been impacted by vegetative clearing, earth movement associated with the dredging and straightening of Dula Thoroughfare and compaction by placement of spoil on the floodplain. Wetland enhancement/restoration options will focus on 1) the establishment of backwater slough/braided channel systems, 2) excavation and grading of elevated spoil and sediment embankments, and 3) reestablishing hydrophytic vegetation.

Establishment of Backwater Slough / Braided Channel Systems

The existing dredged and straightened reach of Dula Thoroughfare represents the primary on-Site wetland restoration feature. Currently, Dula Thoroughfare drains from the valley wall slopes as a channelized, E-type stream. Upon entering the Rocky River Floodplain, the channel has been dredged and straightened and is currently characterized as a shallow, wide, slackwater ditch that has been isolated from the adjacent floodplain. Measures outlined in Section 6.2.1 (Stream Reconstruction In-Place - Excavation of a Backwater Sough/Braided Channel System), including excavation of a floodplain and shallow non-linear depressions connected by braided channel systems is expected to result in approximately 5.6 acres of jurisdictional wetland restoration within the Rocky River floodplain.

It should be noted that floodplains adjacent to the dredged and straightened reach of Dula Thoroughfare are underlain by brightly colored soils (approximately 10YR 4/4 to 10YR 4/6), which are characteristic of wetlands in the area. USACE representatives conducted a field visit to the Site on January 13, 2004 (Notification of Jurisdictional Determination can be found in Appendix F), and confirmed these brightly colored soils were indicative of a hydric soil for the region.

Excavation and Grading of Elevated Spoil and Sediment Embankments

Reaches of Dula Thoroughfare and its UT have experienced both natural and unnatural sediment deposition. Spoil piles appear to have been cast adjacent to the channels during dredging and straightening of the stream or during agricultural field clearing. Major flood events may have also deposited additional sediment adjacent to stream banks from eroding banks and upstream agricultural fields. The removal of spoil material and/or filling of on-Site ditches with spoil material represent a critical element of wetland restoration.

Hydrophytic Vegetation

On-Site wetland areas have endured significant disturbance from land use activities such as land clearing, row crop agriculture, and other anthropogenic maintenance. Wetland areas will be re-vegetated with native vegetation typical of wetland communities in the region. Emphasis will focus on developing a diverse plant assemblage. Sections 6.4 (Plant Community Restoration) and 6.4.2 (Planting Plan) provide detailed information concerning community species associations. Re-vegetation of portions of the Site underlain by hydric soils is expected to represent an important wetland enhancement/restoration component.

6.3 Floodplain Soil Scarification

Microtopography and differential drainage rates within localized floodplain areas represent important components of floodplain functions. Reference forests in the region exhibit complex surface microtopography. Small concavities, swales, exposed root systems, seasonal pools, oxbows, and hummocks associated with vegetative growth and hydrological patterns are scattered throughout these systems. As discussed in the stream reconstruction section, efforts to advance the development of characteristic surface microtopography will be implemented.

In areas where soil surfaces have been compacted, ripping or scarification will be performed. After construction, the soil surface is expected to exhibit complex microtopography ranging to 1 foot vertical asymmetry across local reaches of the landscape. Subsequently, community restoration will be initiated on complex floodplain surfaces.

6.4 Plant Community Restoration

Restoration of floodplain forest and stream-side habitat allows for development and expansion of characteristic species across the landscape, in addition to reducing the presence of invasive species. Ecotonal changes between community types contribute to diversity and provide secondary benefits, such as enhanced feeding and nesting opportunities for mammals, birds, amphibians, and other wildlife.

RFE data, on-Site observations, and community descriptions from Classification of the Natural Communities of North Carolina (Schafale and Weakley 1990) were used to develop the primary plant community associations that will be promoted during community restoration activities. These community associations include 1) stream-side assemblage, 2) bottomland hardwood forest, and 3) slope forest (Figure 16). Figure 17 identifies the location, based on elevation and position relative to restored streams and wetlands, of each target community to be planted. Planting elements within each map unit are listed below.

Bottomland Hardwood Forest

1. Swamp chestnut oak (*Quercus michauxii*)
2. American elm (*Ulmus americana*)
3. Sugarberry (*Celtis laevigata*)
4. Green ash (*Fraxinus pennsylvanica*)
5. Shagbark hickory (*Carya ovata*)
6. Willow oak (*Quercus phellos*)
7. Northern red oak (*Quercus rubra*)
8. Southern red oak (*Quercus falcata*)
9. Black gum (*Nyssa sylvatica*)
10. American sycamore (*Platanus occidentalis*)

Stream-Side Assemblage

1. Black willow (*Salix nigra*)
2. Elderberry (*Sambucus canadensis*)
3. River birch (*Betula nigra*)
4. American sycamore (*Platanus occidentalis*)
5. Swamp dogwood (*Cornus stricta*)
6. Tag alder (*Alnus serrulata*)
7. Buttonbush (*Cephalanthus occidentalis*)
8. Arrow-wood viburnum (*Viburnum dentatum*)
9. Possumhaw viburnum (*Viburnum nudum*)
10. Highbush blueberry (*Vaccinium corymbosum*)

Slope Forest

1. Mockernut hickory (*Carya tomentosa*)
2. Pignut hickory (*Carya glabra*)
3. White oak (*Quercus alba*)
4. Sourwood (*Oxydendrum arboreum*)
5. American holly (*Ilex opaca*)

6. Flowering dogwood (*Cornus florida*)

Stream-side trees and shrubs include species with high value for sediment stabilization, rapid growth rate, and the ability to withstand hydraulic forces associated with bankfull flow and overbank flood events. Stream-side trees and shrubs will be planted within 15 feet of the channel throughout the meander belt-width. Shrub elements will be planted along the banks of the reconstructed stream, concentrated along outer bends.

Bottomland hardwood forest vegetation is targeted for areas located in the floodplain and backwater slough/braided channel system. Species common along slope forests will be planted on slopes adjacent to the floodplain.

The following planting plan is the blueprint for community restoration. The anticipated results stated in the Success Criteria (Section 7.8) are expected to reflect potential vegetative conditions achieved after steady-state conditions prevail over time.

6.5 Planting Plan

The purpose of a planting plan is to re-establish vegetative community patterns across the landscape. The plan consists of 1) acquisition of available plant species, 2) implementation of proposed Site preparation, and 3) planting of selected species.

Species selected for planting will be dependent upon availability of local seedling sources. Advance notification to nurseries (1 year) will facilitate availability of various non-commercial elements.

Bare-root seedlings of tree species will be planted within specified map areas at a density of approximately 680 stems per acre on 8-foot centers. Shrub species in the streamside assemblage will be planted at a density of 1360 stems per acre on 4-foot centers. Table 7 depicts the total number of stems and species distribution within each vegetation association. Planting will be performed between December 1 and March 15 to allow plants to stabilize during the dormant period and set root during the spring season. A total of 63,454 diagnostic tree and shrub seedlings may be planted during restoration.

Table 7: Planting Plan

Vegetation Association	Bottomland Hardwood Forest		Stream-side Assemblage		Slope Forest		Backwater Slough		Total
Area (acres)	51.7		4.1		27.2		6.2		
Species	number planted	% of total	number planted	% of total	number planted	% of total	number planted	% of total	Number Planted
Swamp Chestnut Oak	3516	10					633	15	4149
American Elm	3516	10							3516
Sugarberry	1758	5							1758
Green Ash	7031	20					633	15	7664
Shagbark Hickory	3516	10							3516
Willow Oak	3516	10							3516
Northern Red Oak	1758	5							1758
Southern Red Oak	1758	5							1758
Black Gum	3516	10							3516
American Sycamore	5274	15	558	10					5832
River Birch			558	10					558
Swamp Dogwood			279	5					279
Black Willow			1115	20					1115
Tag Alder			558	10			633	15	1191
Buttonbush			279	5			422	10	701
Elderberry			558	10					558
Arrow-wood Vibernum			558	10					558
Possumhaw Vibernum			558	10					558
Highbush Blueberry			558	10					558
Mockernut Hickory					3699	20			3699
Pignut Hickory					3699	20			3699
White Oak					3699	20			3699
Sourwood					3699	20			3699
American Holly					1850	10			1850
Flowering Dogwood					1850	10			1850
Overcup Oak							633	15	633
Swamp Cottonwood							633	15	633
Cherrybark Oak							633	15	633
Total	**35159**	**100**	**5579**	**100**	**18496**	**100**	**4220**	**100**	**63454**

7.0 MONITORING PLAN

Monitoring of Site restoration efforts will be performed for the first five growing seasons following site construction. If necessary, monitoring will continue through additional growing seasons. Monitoring is proposed for single-strand stream channels, as well as wetland components of hydrology and vegetation. A general Site monitoring plan is depicted in Figure 18.

Stream measurements are not proposed in the backwater slough/braided channel system due to typical characteristics of a D-type (braided) stream consisting of multiple braided channels. D-type stream systems are not conducive to measurement of pattern, dimension, and profile; therefore, the stream will be visually assessed and photographically documented annually to semi-annually and any potential problem area(s) will be identified. If a problem area is noted during the review, the area will be evaluated to determine the corrective action required to resolve the problem.

7.1 Stream Monitoring

Site stream reaches proposed to be monitored for geometric activity are conceptually depicted in Figure 18. Each stream reach will extend for a minimum of 450 feet along the restored channel. Annual fall monitoring will include development of channel cross-sections on riffles and pools, pebble counts, and a water surface profile of the channel. The data will be presented in graphic and tabular format. Data to be presented will include 1) cross-sectional area, 2) bankfull width, 3) average depth, 4) maximum depth, 5) width-to-depth ratio, 6) meander wavelength, 7) belt-width, 8) water surface slope, 9) sinuosity, and 10) stream substrate composition. The stream will subsequently be classified according to stream geometry and substrate (Rosgen 1996). Significant changes in channel morphology will be tracked and reported by comparing data in each successive monitoring year.

7.2 Stream Success Criteria

Success criteria for stream restoration will include 1) successful classification of the reach as a functioning stream system (Rosgen 1996) and 2) channel variables indicative of a stable stream system. Stream restoration success criteria will follow the constructs outlined by interagency guidance (*Stream Mitigation Guidelines* [USACE *et*. *al*. 2003]).

The channel configuration will be measured on an annual basis in order to track changes in channel geometry, profile, or substrate. These data will be utilized to determine the success in restoring stream channel stability. Specifically, the channel should exhibit the following characteristics:

1) Insignificant change in dimension from as-built measurements or the previous years monitoring measurements.
2) Minor changes in channel dimension are allowed; however, dimension changes should not represent a trend towards instability (*e.g.* increased width to depth ratio or decreased width to depth ratio with decreased entrenchment ratio).
3) Little change in longitudinal profile.
4) Pool/riffle spacing should remain fairly constant.
5) Pools should not be aggrading and riffles should not scour.

6) Pebble count should trend toward a desired bed material.

The field indicator of bankfull will be described in each monitoring year and indicated on a representative channel cross-section figure. If the stream channel is down-cutting or the channel width is enlarging due to bank erosion, additional bank or slope stabilization methods may be employed.

The stream is expected to maintain shear stress values to adequately transport sediment through the Site. Pebble counts will be conducted annually to determine D50 and D84 values within the restored stream. Pebble counts would be expected to indicate a general coarsening of materials on the riffles throughout the monitoring period.

Visual assessment of in-stream structures will be conducted to determine if failure has occurred. Failure of a structure may be indicated by collapse of the structure, undermining of the structure, abandonment of the channel around the structure, and/or stream flow beneath the structure.

7.3 Hydrology Monitoring

Groundwater monitoring gauges (one gauge within reference and four gauges on-Site) will be installed to monitor groundwater elevations after hydrological modifications are performed. Hydrological sampling will continue throughout the growing season at intervals necessary to satisfy the hydrology success criteria within each design unit (EPA 1990).

7.4 Hydrology Success Criteria

Target hydrological characteristics include saturation or inundation for at least 12.5 percent of the growing season at lower landscape positions, during average climatic conditions. Upper landscape reaches may exhibit surface saturation/inundation between 5 percent and 12.5 percent of the growing season based on groundwater gauge data. These areas are expected to support hydrophytic vegetation. If wetland parameters are marginal as indicated by vegetation and/or hydrology monitoring, a jurisdictional determination will be performed in these areas.

7.5 Vegetation Monitoring

Restoration monitoring procedures for vegetation are designed in accordance with EEP Vegetation Monitoring Requirements (draft 27 August 2004). A general discussion of the restoration monitoring program is provided. A photographic record of plant growth should be included in each annual monitoring report, in addition to the necessary data forms.

After planting has been completed in winter or early spring, an initial evaluation will be performed to verify planting methods and to determine initial species composition and density. Supplemental planting and additional Site modifications will be implemented, if necessary.

During the first year, vegetation will receive cursory, visual evaluation on a periodic basis to ascertain the degree of overtopping of planted elements by nuisance species. Subsequently, quantitative sampling of vegetation will be performed annually, between May and September, until the vegetation success criterion is achieved.

During quantitative vegetation sampling in summer of the first year, approximately seven sample plots will be randomly placed within the Site. Sample-plot distributions are expected to resemble locations depicted in Figure 18; however, best professional judgment may be necessary to establish vegetative monitoring plots upon completion of construction activities. In each sample plot, vegetation parameters to be monitored include species composition and species density. Visual observations of the percent cover of shrub and herbaceous species will also be recorded.

No quantitative sampling requirements are proposed for herb assemblages as part of the vegetation success criteria. Development of floodplain forests over several decades will dictate the success in migration and establishment of desired understory and groundcover populations. Visual estimates of the percent cover of herbaceous species and photographic evidence will be reported for information purposes.

7.8 Vegetation Success Criteria

Tables and discussion for each of the following success criteria will be provided with each report. The criteria include cover for each species in each plot, strata presence for each species in each plot and stem counts of each planted species in each plot.

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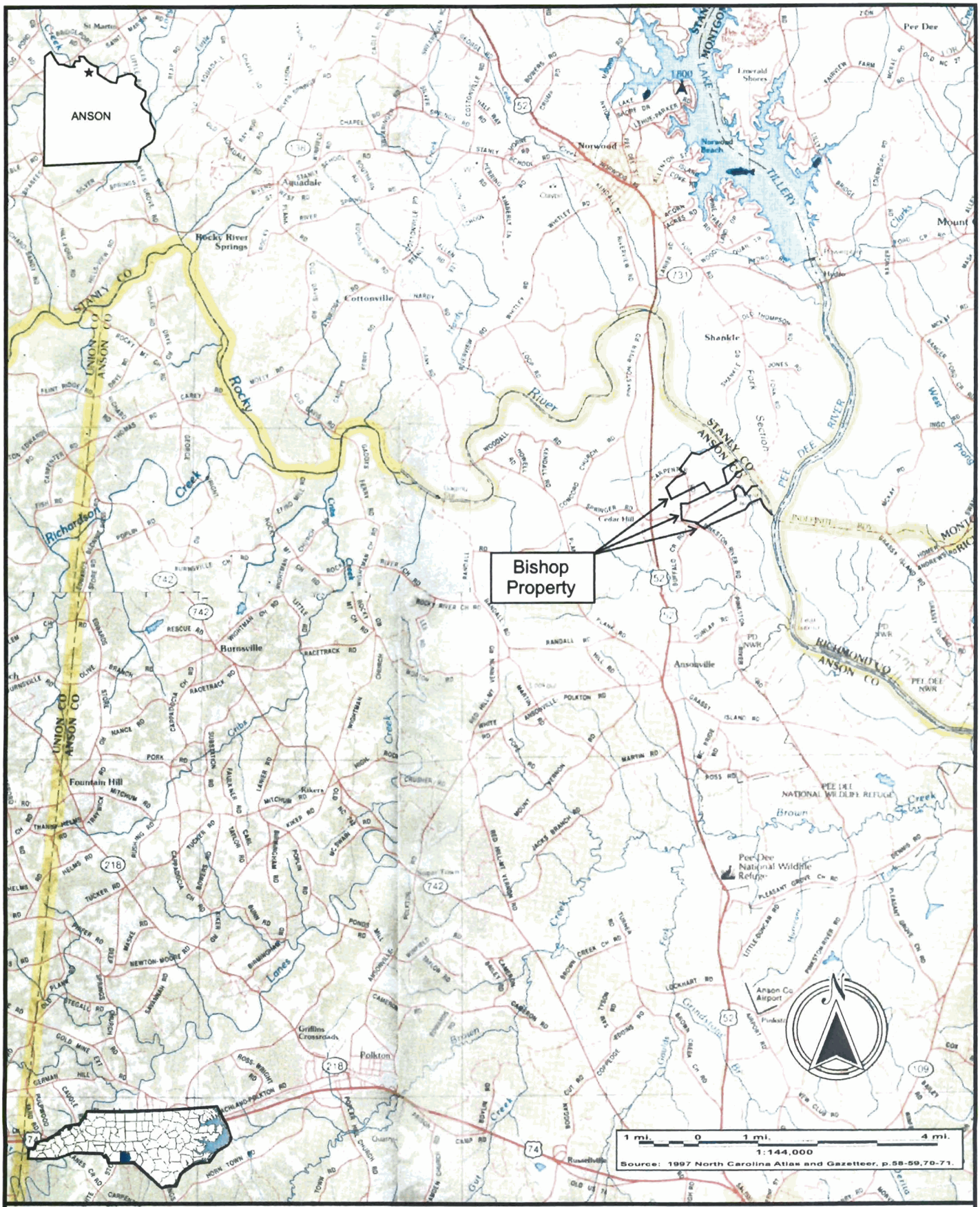
APPENDIX A

FIGURES

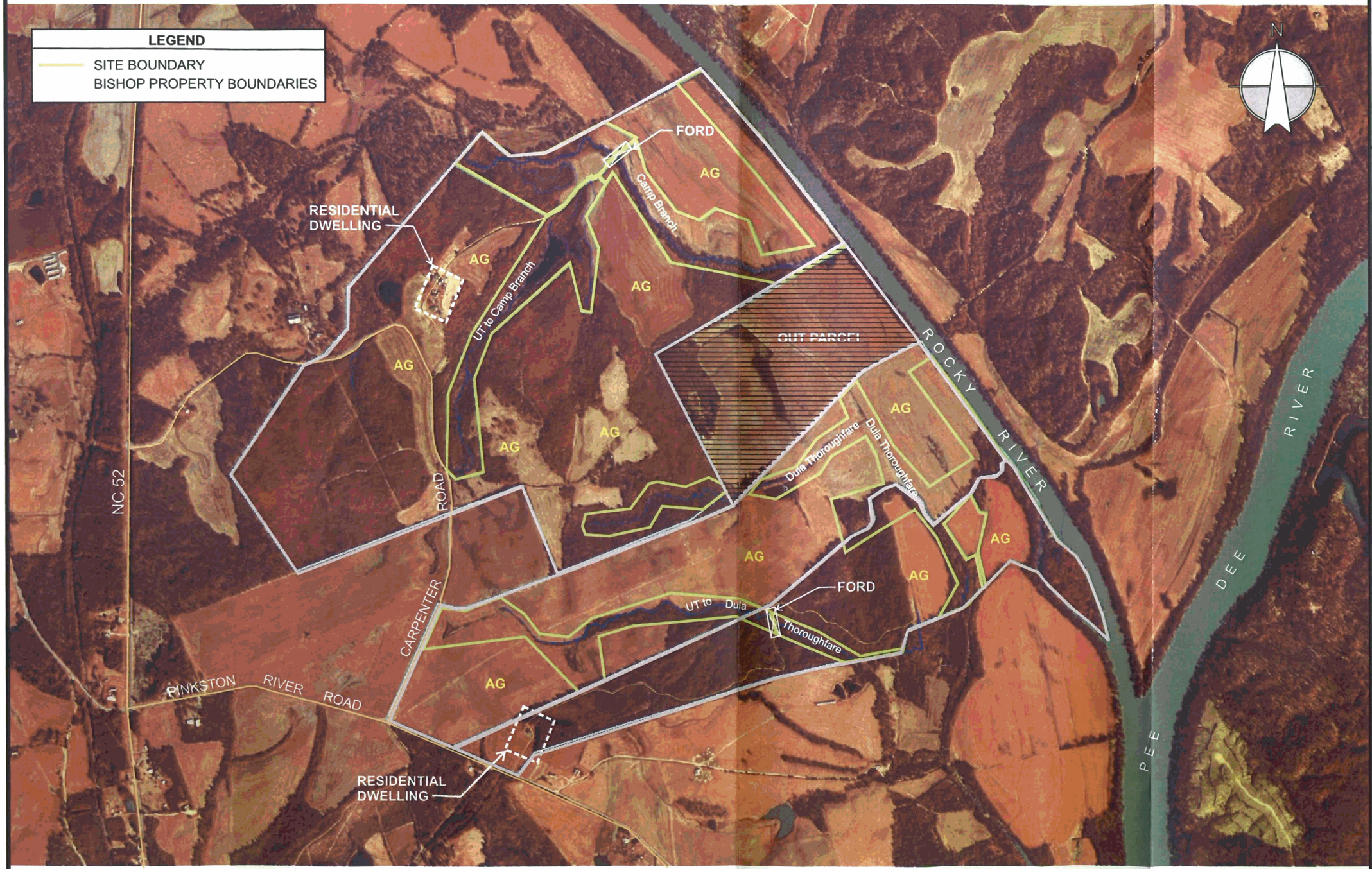


EcoScience Corporation
Raleigh, North Carolina

SITE LOCATION
Bishop Site Restoration Planning
Anson County, North Carolina

Dwn. by:	HJS
Ckd by:	WGL
Date:	SEPT 2004
Project:	02-113.34

Figure 1



EcoScience Corporation

Raleigh, North Carolina

Client:

Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

Anson County
North Carolina

Title:

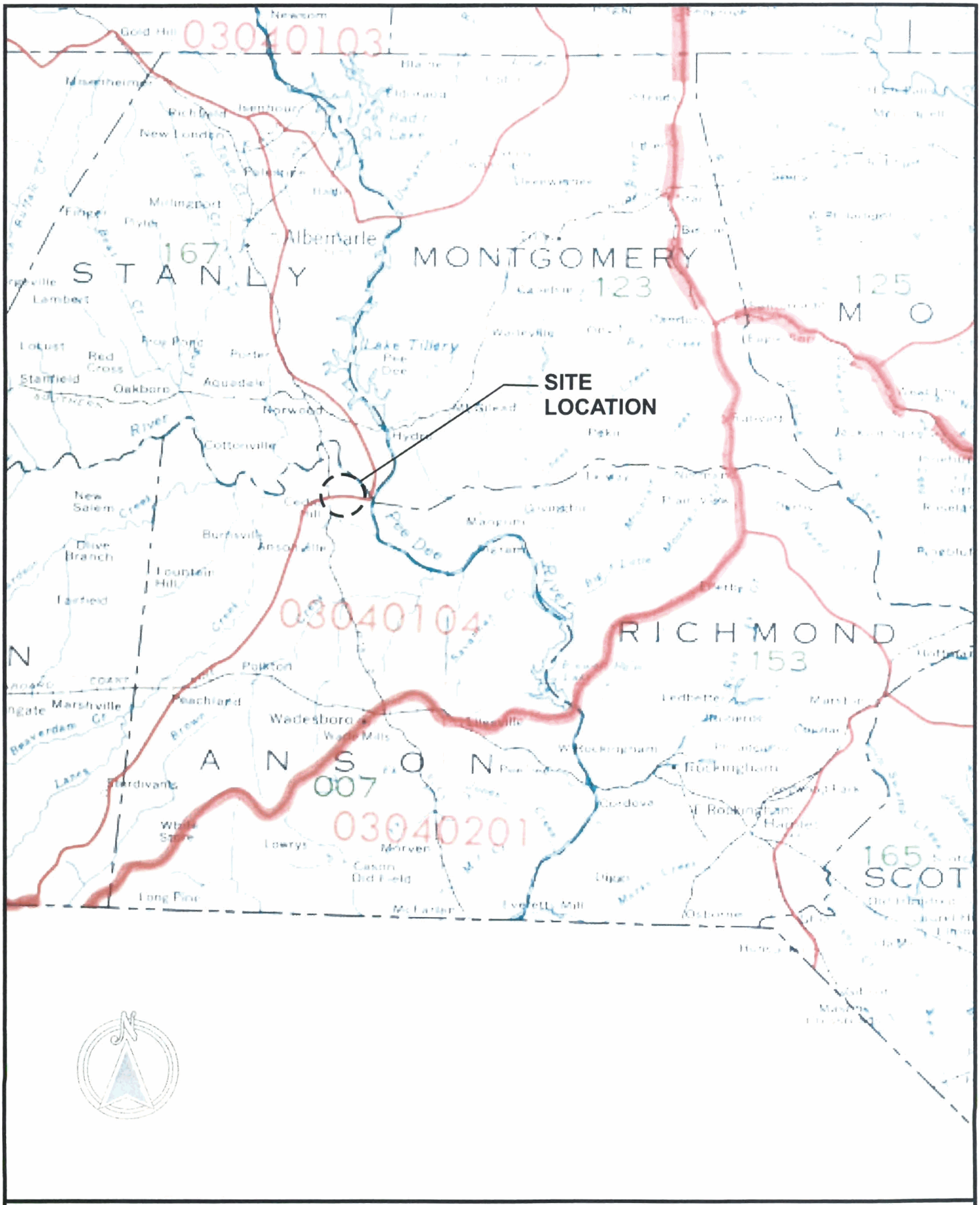
ON-SITE LAND USE

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	As Shown

ESC Project No.: 02-113.34

FIGURE

2

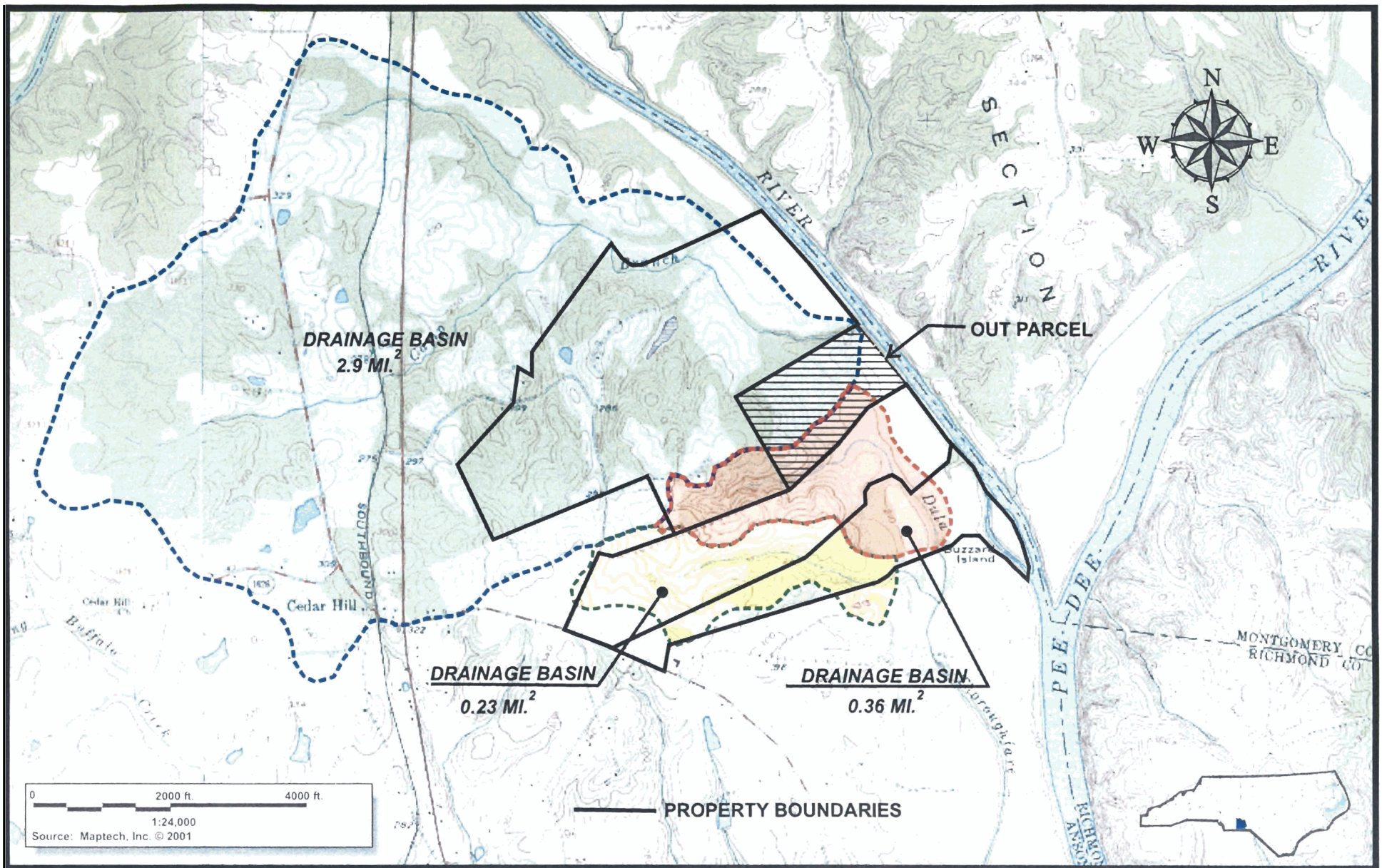


EcoScience Corporation
Raleigh, North Carolina

USGS HYDROLOGIC UNIT MAP
Bishop Site Restoration Planning
Anson County, North Carolina

Dwn. by:	MAF
Ckd by:	WGL
Date:	SEPT 2004
Project:	02-113.34

Figure 3

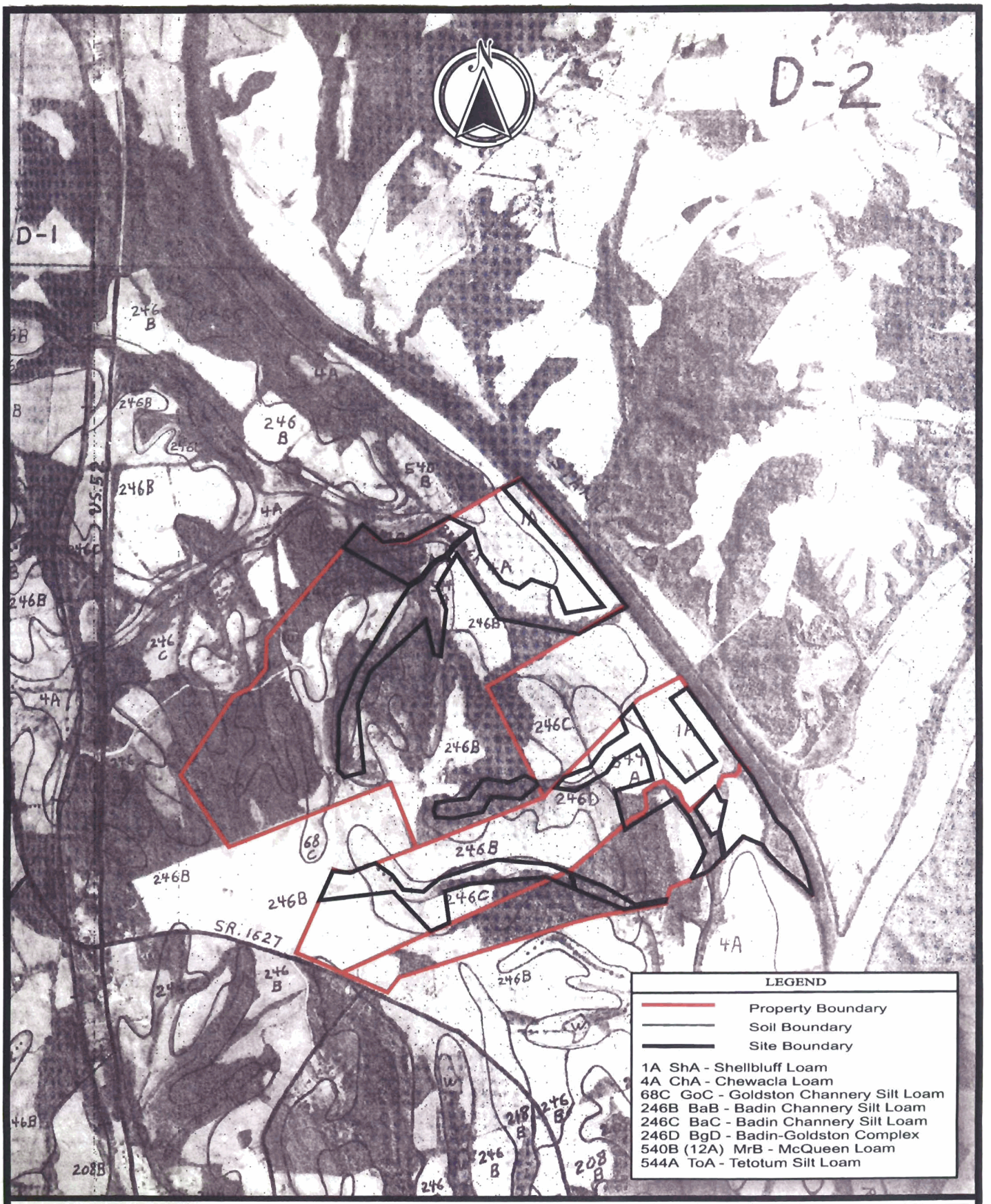


EcoScience Corporation
Raleigh, North Carolina

TOPOGRAPHY
BISHOP SITE RESTORATION PLANNING
Anson County, North Carolina

Dwn. by:	MAF
Ckd by:	WGL
Date:	SEPT 2004
Project:	02-113.34

FIGURE 4

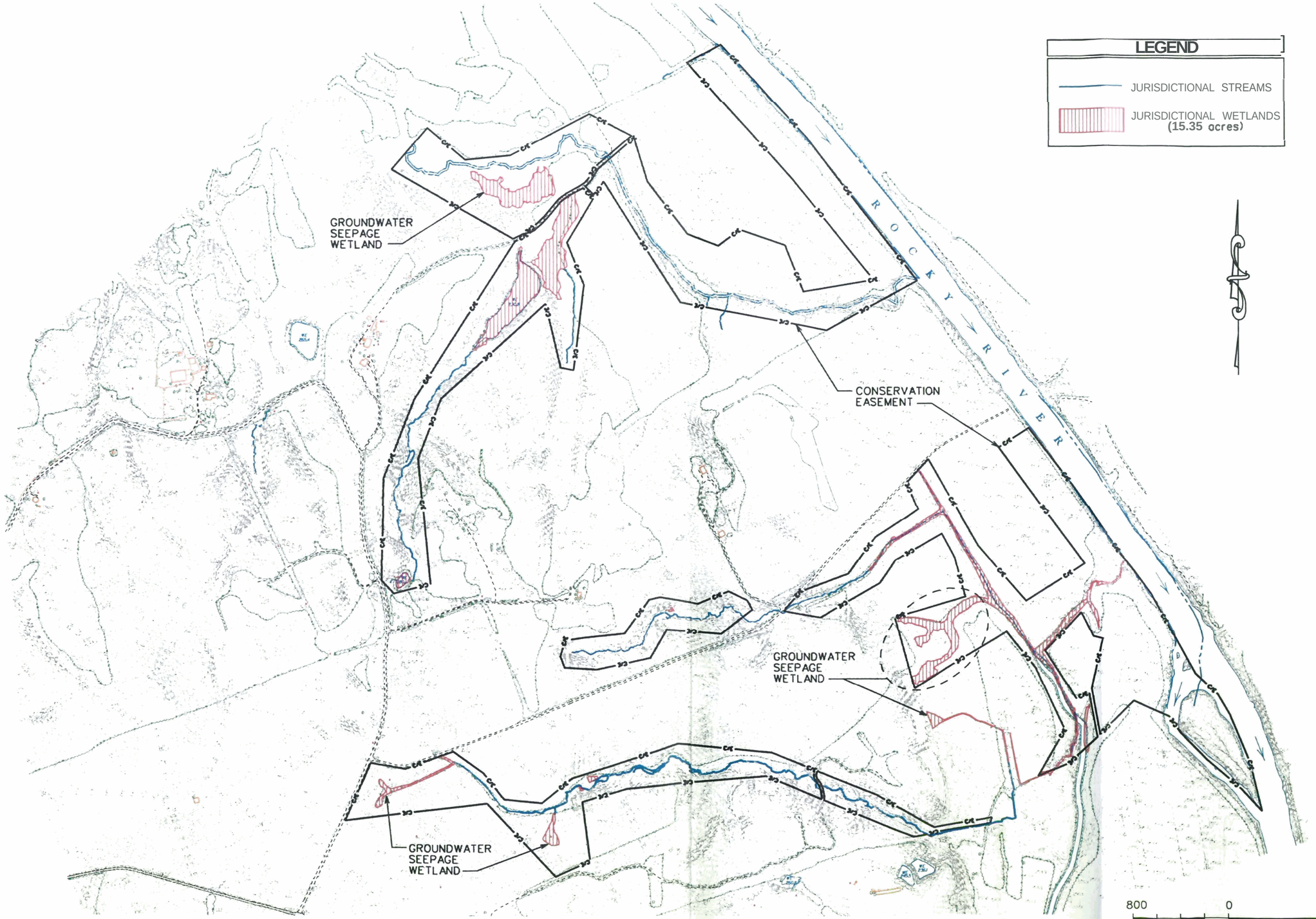


EcoScience Corporation
Raleigh, North Carolina

NRCS SOILS MAP
Bishop Site Restoration Planning
Anson County, North Carolina

Dwn. by:	MAF
Ckd by:	WGL
Date:	SEPT 2004
Project	02-113.34

Figure 5



EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

JURISDICTIONAL SYSTEMS

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=800'

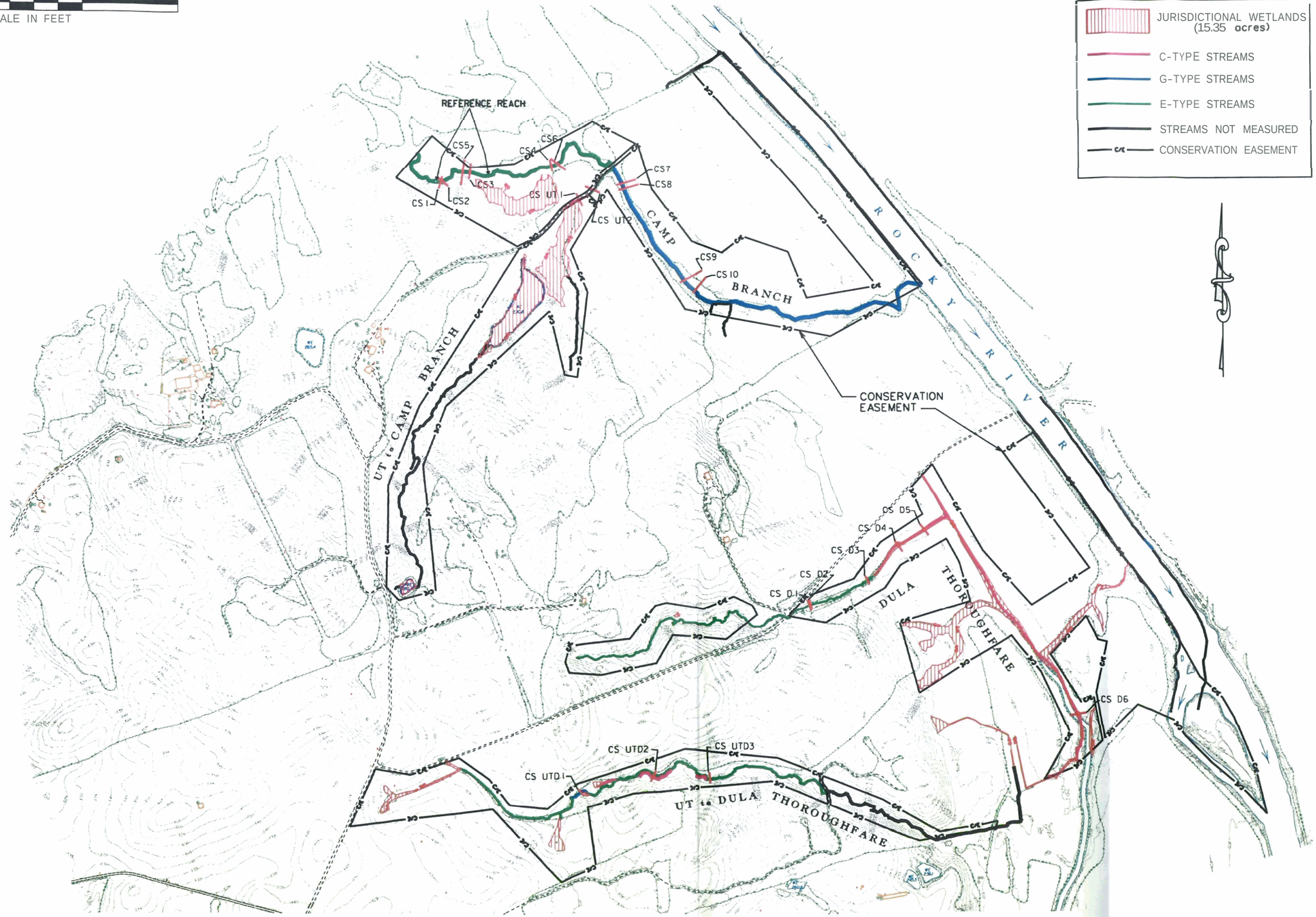
ESC Project No.: 02-113.34

FIGURE

6

800 0 800

SCALE IN FEET



LEGEND

- JURISDICTIONAL WETLANDS (15.35 acres)
- C-TYPE STREAMS
- G-TYPE STREAMS
- E-TYPE STREAMS
- STREAMS NOT MEASURED
- CE — CONSERVATION EASEMENT

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

ON-SITE STREAM TYPES

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=800'

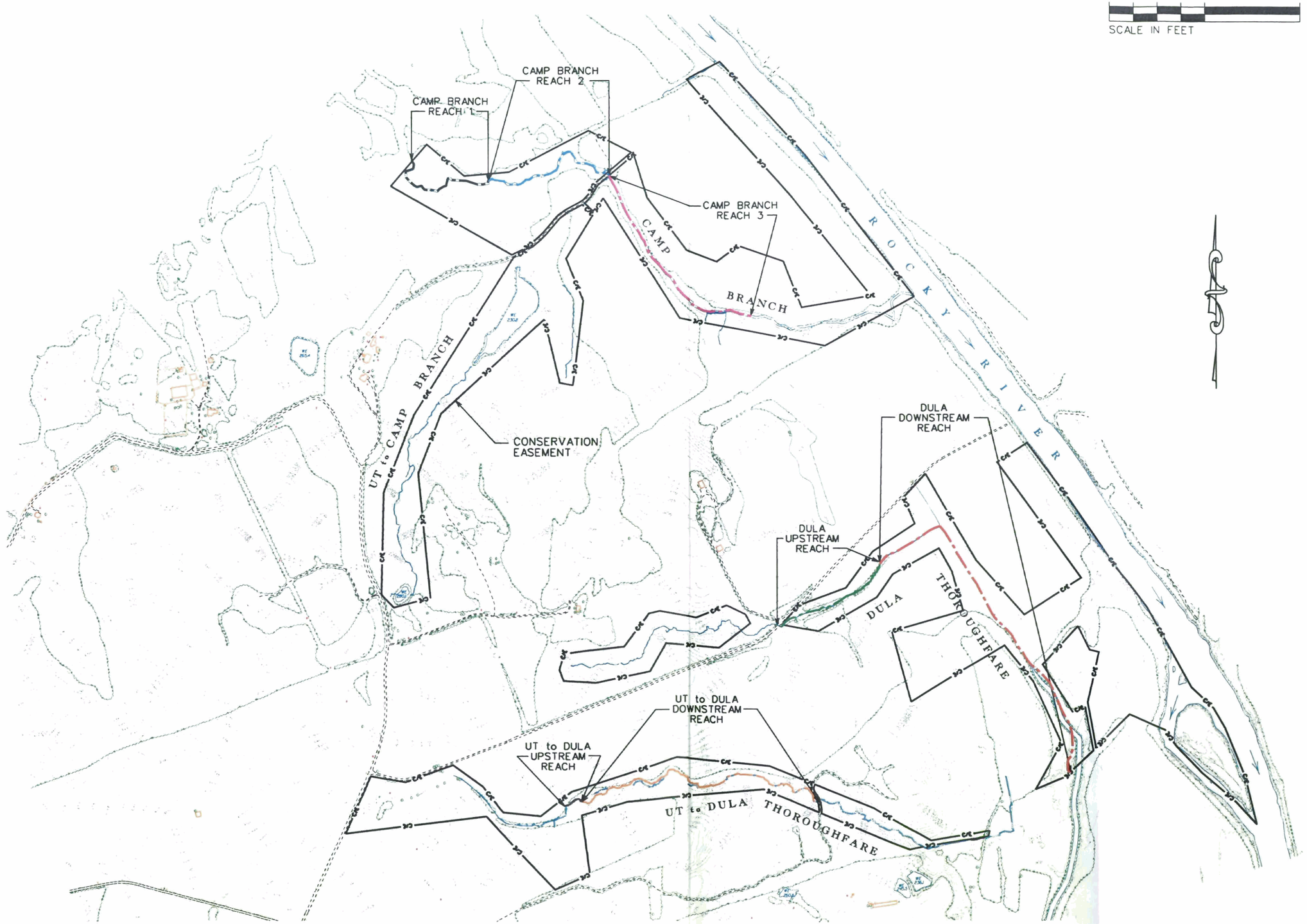
ESC Project No.: 02-113.34

FIGURE

7

800 0 800

SCALE IN FEET



EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

ON-SITE STREAM REACHES

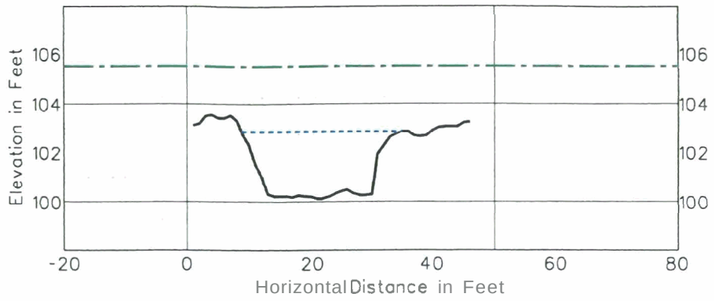
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=800'

ESC Project No.: 02-113.34

FIGURE

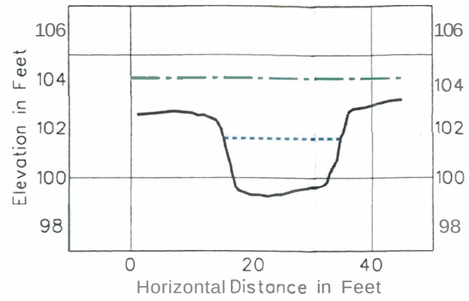
8

4+38 CROSS-SECTION 1 (Riffle)



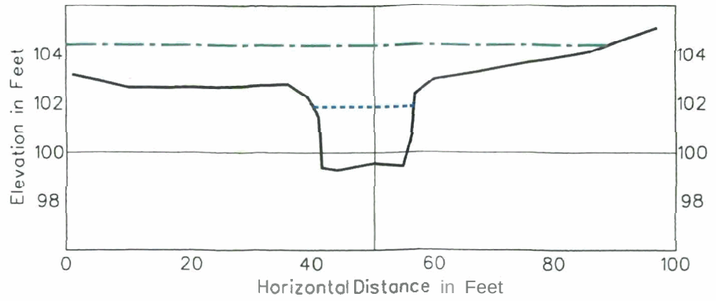
Bankfull Cross-section01 Area: 38.7 ft.sq.
Bankfull Width: 21.3'
Bankfull Maximum Depth: 2.7'
Bankfull Averoge Depth: 1.8'
Width of Flood Prone Area: 180±'

7+82 CROSS-SECTION 3 (Riffle)



Bankfull Cross-sectional Area: 38.7 ft.sq.
Bankfull Width: 19.6'
Bankfull Maximum Depth: 2.4'
Bankfull Averoge Depth: 2.0'
Width of Flood Prone Area: 75±'

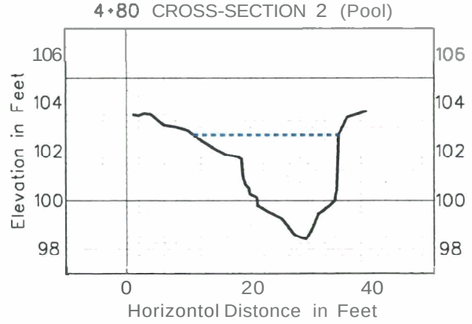
7+19 CROSS-SECTION 5 (Riffle)



Bankfull Cross-sectional Area: 36.0 ft.sq.
Bankfull Width: 16.5'
Bankfull Maximum Depth: 2.6'
Bankfull Averoge Depth: 2.2'
Width of Flood Prone Area: 110±'

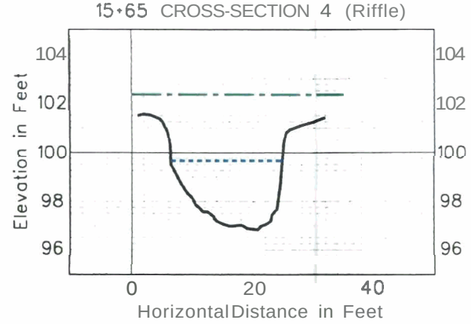
BANKFULL
EXISTING GRADE
FLOOD PRONE AREA

4+80 CROSS-SECTION 2 (Pool)



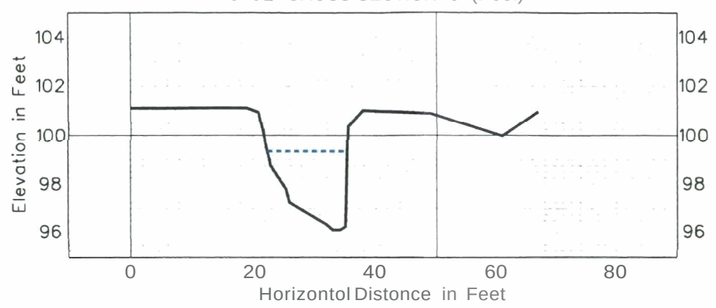
Bankfull Cross-sectional Areo: 55.8 ft.sq.
Bankfull Width: 23.6'
Bankfull Moximum Depth: 4.3'
Bankfull Averoge Depth: 2.4'

15+65 CROSS-SECTION 4 (Riffle)



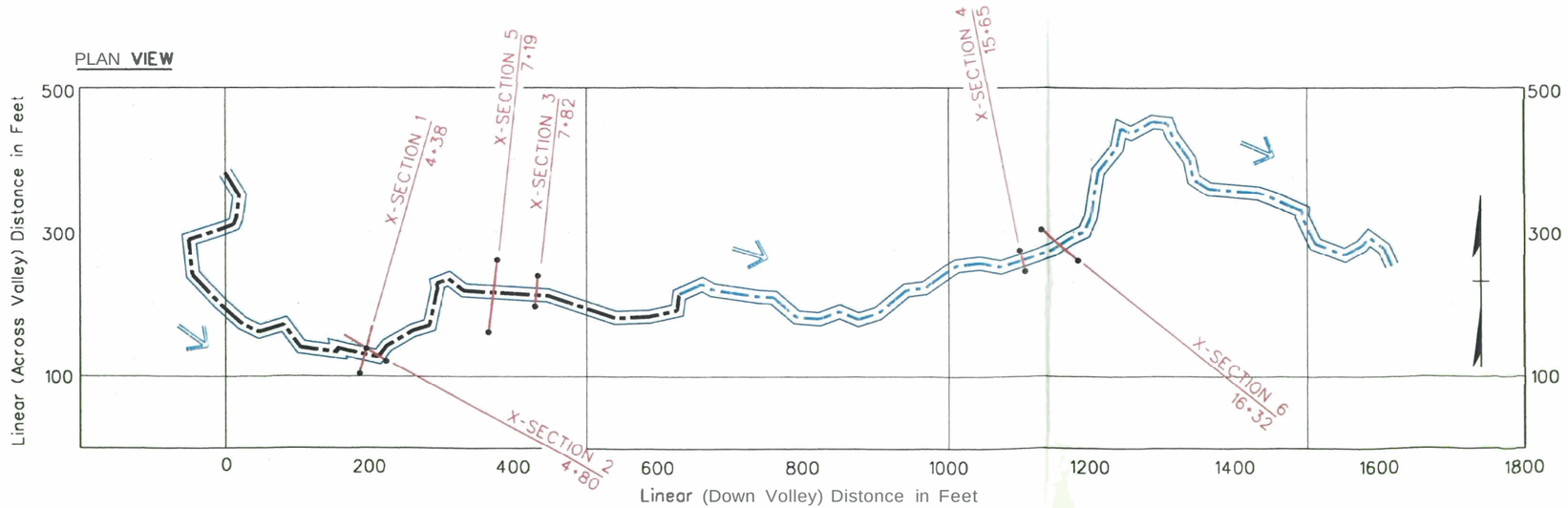
Bankfull Cross-sectional Area: 38.7 ft.sq.
Bankfull Width: 18.3'
Bankfull Moximum Depth: 2.7'
Bankfull Average Depth: 2.1'
Width of Flood Prone Area: 100±'

16+32 CROSS-SECTION 6 (Pool)



Bankfull Cross-sectional Areo: 29.2 ft.sq.
Bankfull Width: 12.9'
Bankfull Moximum Depth: 3.2'
Bankfull Averoge Depth: 2.3'

PLAN VIEW



REACH 1 (Upstream of Heodcut)
REACH 2 (Heodcut to Ford)

NOTES:

1. All Cross-sections Facing the Downstream Direction
2. Bankfull represents elevation at station point along best fit line drown through bankfull elevation points for stream profile.
3. Cross-section stationing represents opproximote field locations.

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client: Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

DIMENSION & PLAN VIEW

REACH 1 & 2 CAMP BRANCH

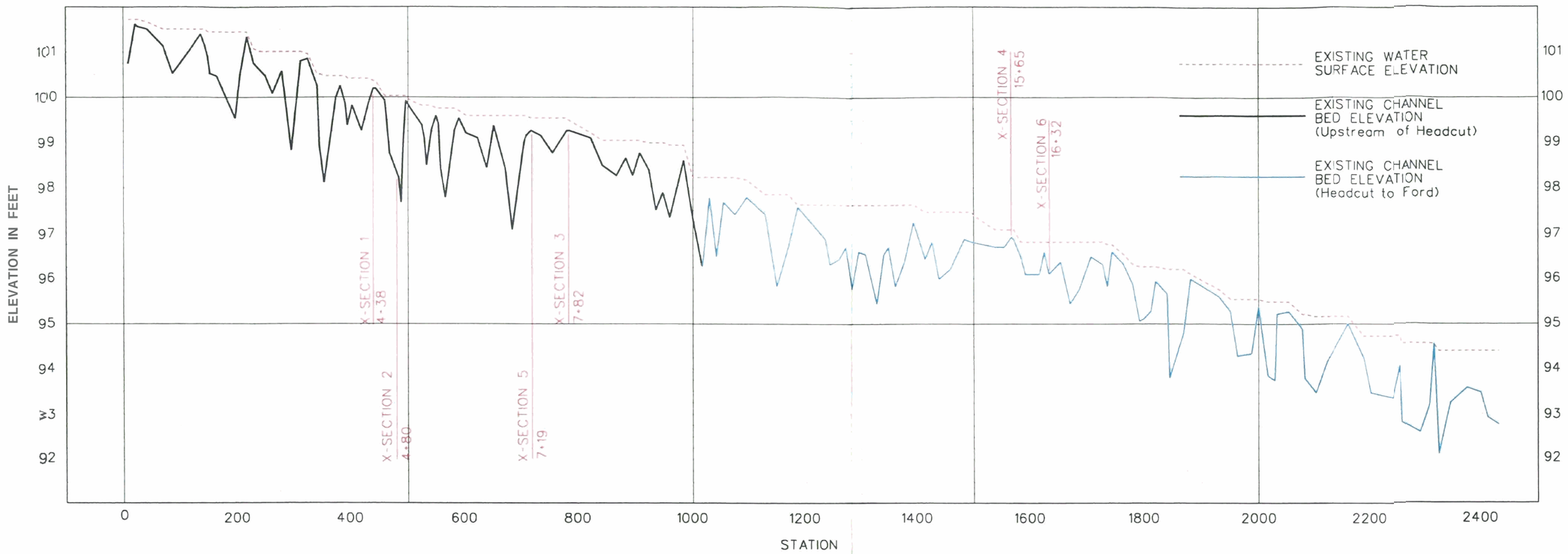
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	AS SHOWN

ESC Project No.: 02-113.34

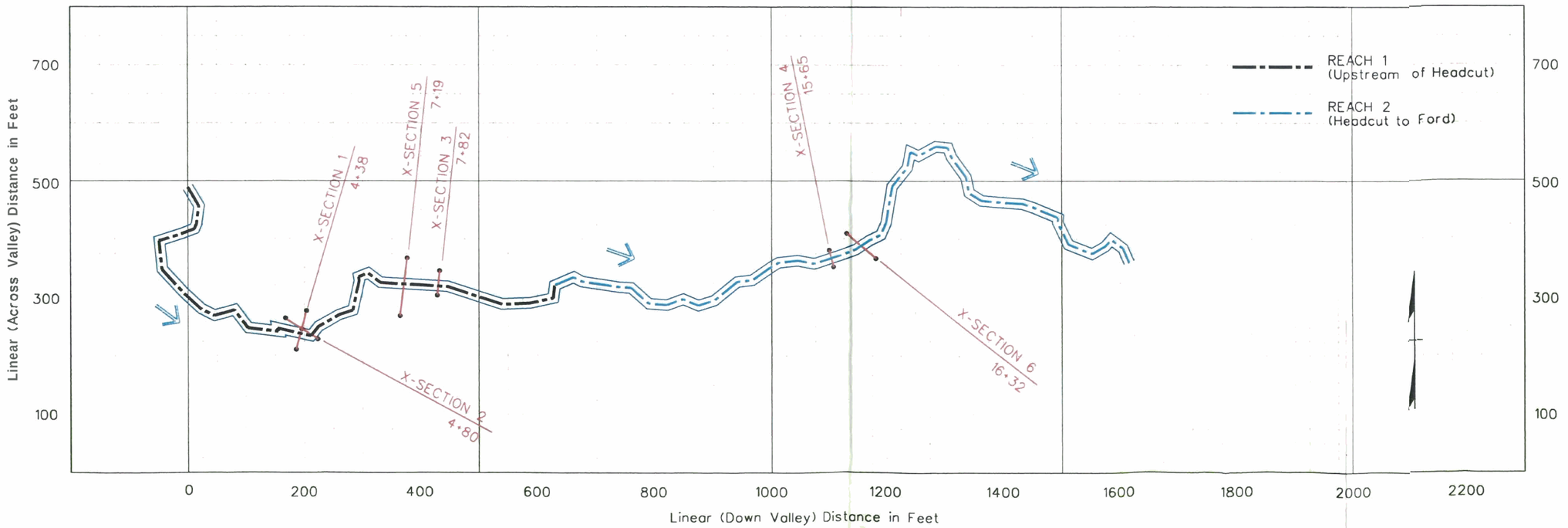
FIGURE

8A

PROFILE



PLAN VIEW



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Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

PROFILE & PLAN VIEW

REACH 1 & 2 CAMP BRANCH

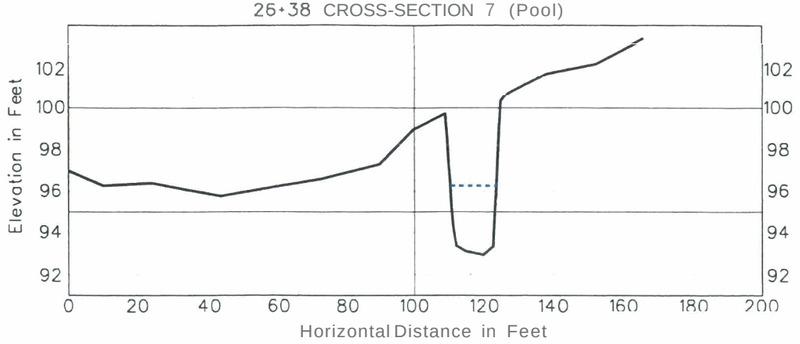
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	AS SHOWN

ESC Project No.: 02-113.34

FIGURE

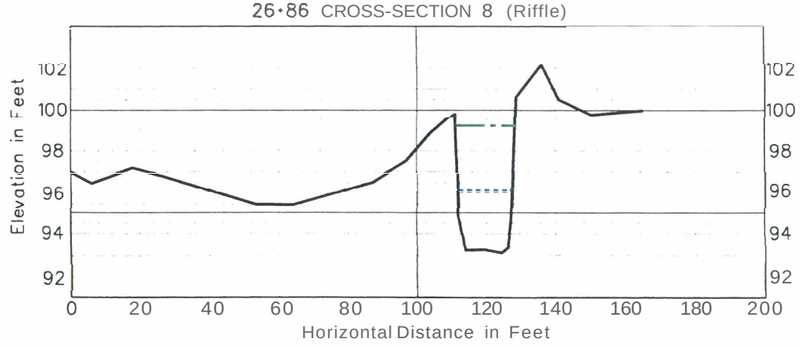
8B

26+38 CROSS-SECTION 7 (Pool)



Bankfull Cross-sectional Area: 38.4 ft.sq.
Bankfull Width: 13.4'
Bankfull Maximum Depth: 3.3'
Bankfull Average Depth: 2.9'

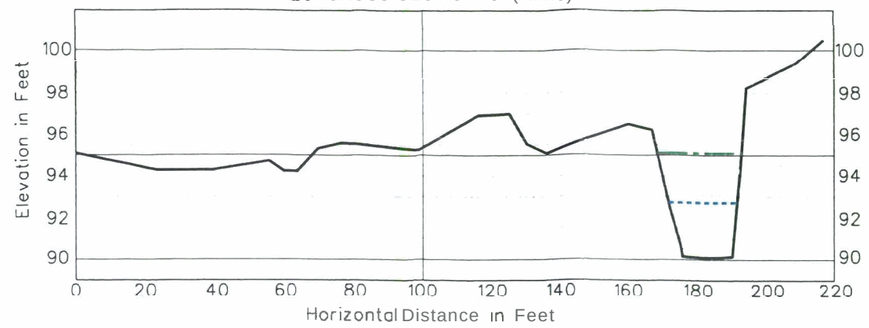
26+86 CROSS-SECTION 8 (Riffle)



Bankfull Cross-sectional Area: 42.0 ft.sq.
Bankfull Width: 16.0'
Bankfull Maximum Depth: 3.0'
Bankfull Average Depth: 2.6'
Width of Flood Prone Area: 17.2±'

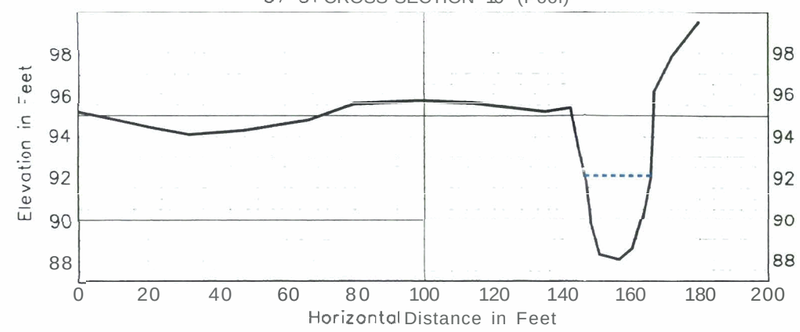
BANKFULL
EXISTING GRADE
FLOOD PRONE AREA

36+23 CROSS-SECTION 9 (Riffle)



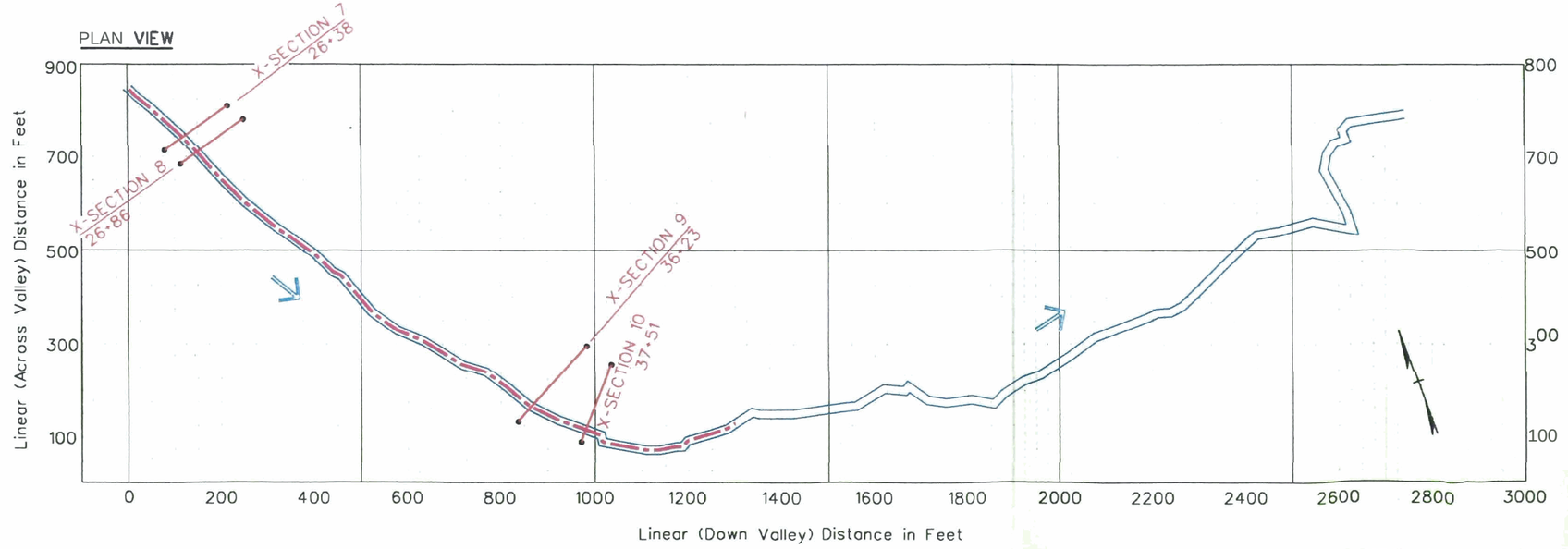
Bankfull Cross-sectlono1 Area: 42.0ft.sq.
Bankfull Width: 19.5'
Bankfull Moximum Depth 2.5'
Bankfull Average Depth: 2.2'
Width of Flood Prone Area: 24.3±'

37+51 CROSS-SECTION 10 (Pool)



Bankfull cross-sectional Area: 57.8 ft.sq.
Bankfull Width: 19.4'
Bankfull Maximum Depth: 4.1'
Bankfull Averoge Depth: 3.0'

PLAN VIEW



REACH 3
(Downstream of Ford)

NOTES:

1. All Cross-sections Facing the Downstream Direction
2. Bankfull represents elevation at station point along best fit line drawn through bankfull elevation points for stream profile.
3. Cross-section stationing represents approximate field locations.

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY.
NORTH CAROLINA

Title:

DIMENSION & PLAN VIEW

REACH 3 CAMP BRANCH

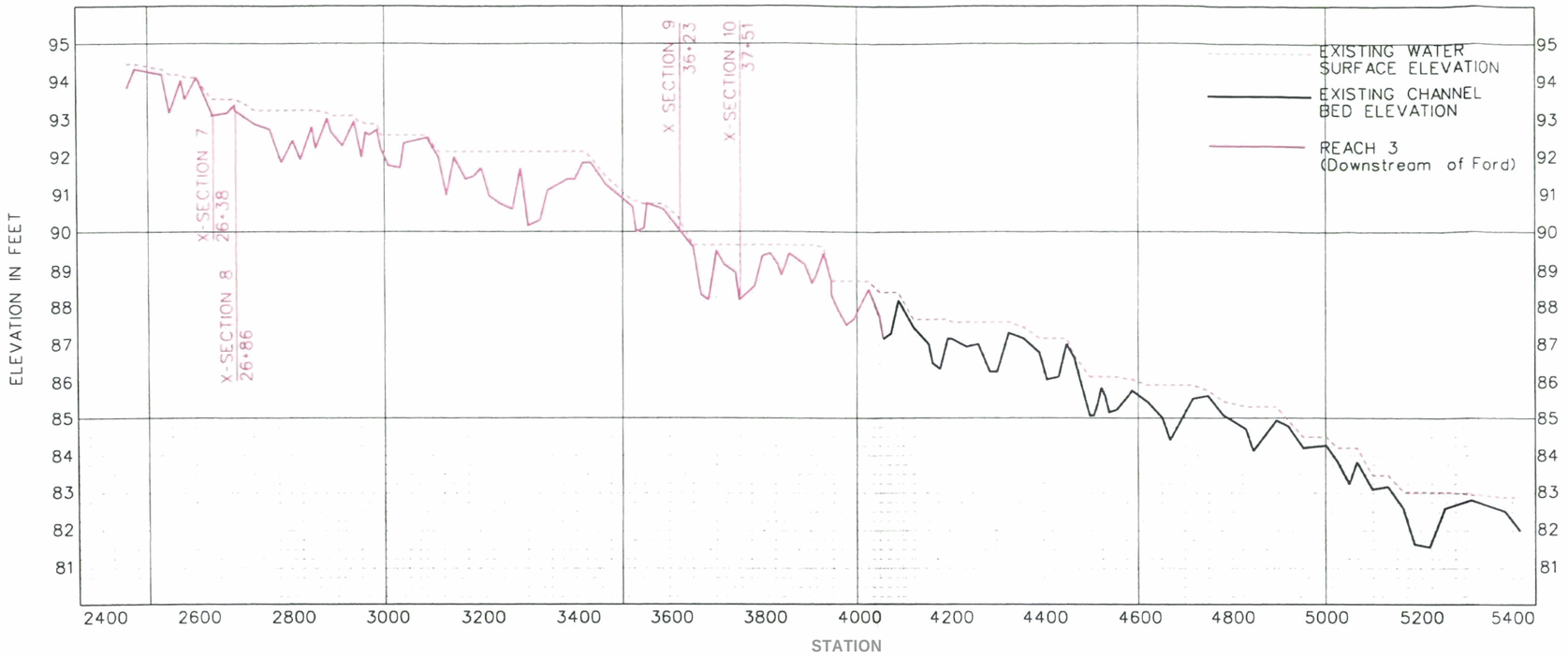
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	AS SHOWN

ESC Project No.: 02-113.34

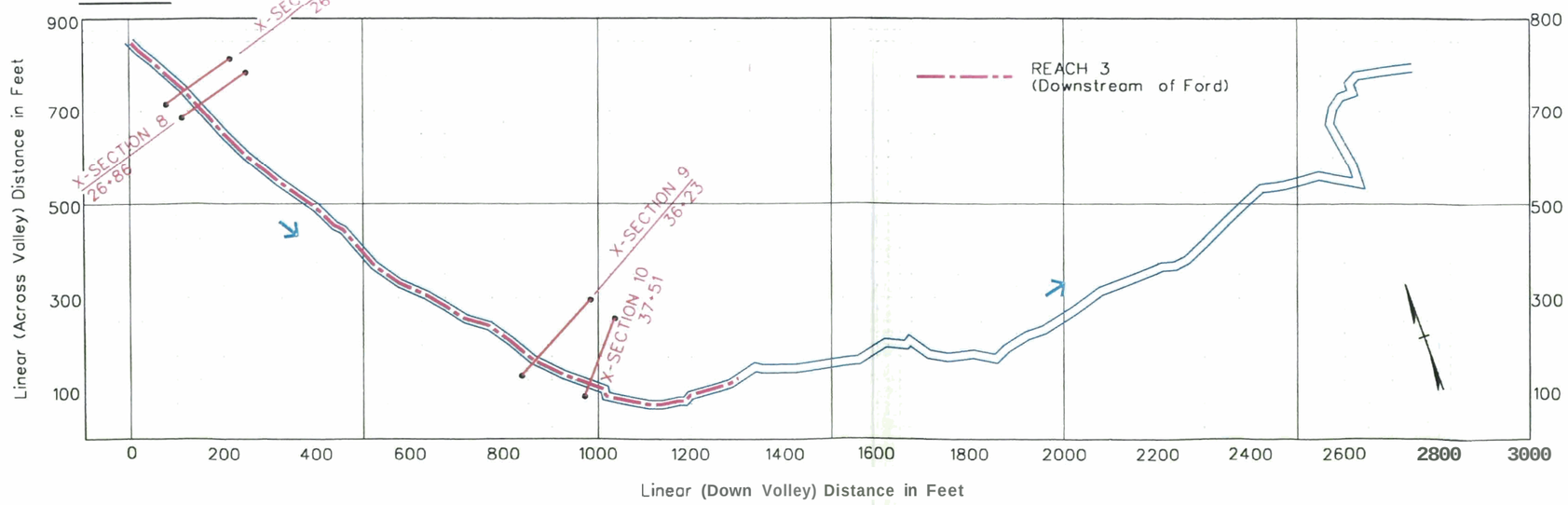
FIGURE

8C

PROFILE



PLAN VIEW



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Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY.
NORTH CAROLINA

Title:

PROFILE & PLAN VIEW

REACH 3 CAMP BRANCH

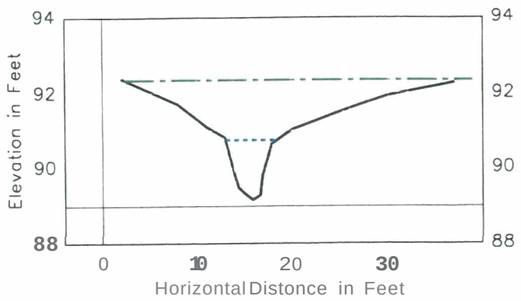
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	AS SHOWN

ESC Project No.: 02-113.34

FIGURE

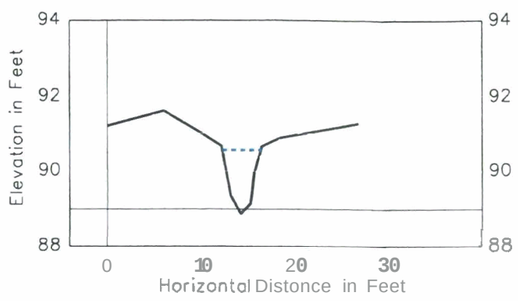
8D

2+19 CROSS-SECTION 1D (Riffle)



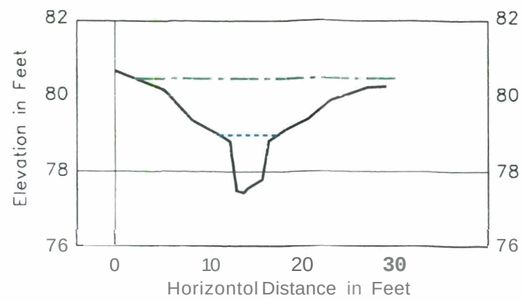
Bankfull Cross-sectional Areo: 5.1 ft.sq.
Bankfull Width: 5.5'
Bankfull Maximum Depth: 1.6'
Bankfull Averoge Depth: 0.9'
Width of Flood Prone Areo: 38±'

2+28 CROSS-SECTION 2D (Pool)



Bankfull Cross-sectional Areo: 4.3 ft.sq.
Bankfull Width: 4.1'
Bankfull Maximum Depth: 1.7'
Bankfull Averoge Depth: 1.1'

7+41 CROSS-SECTION 3D (Riffle)



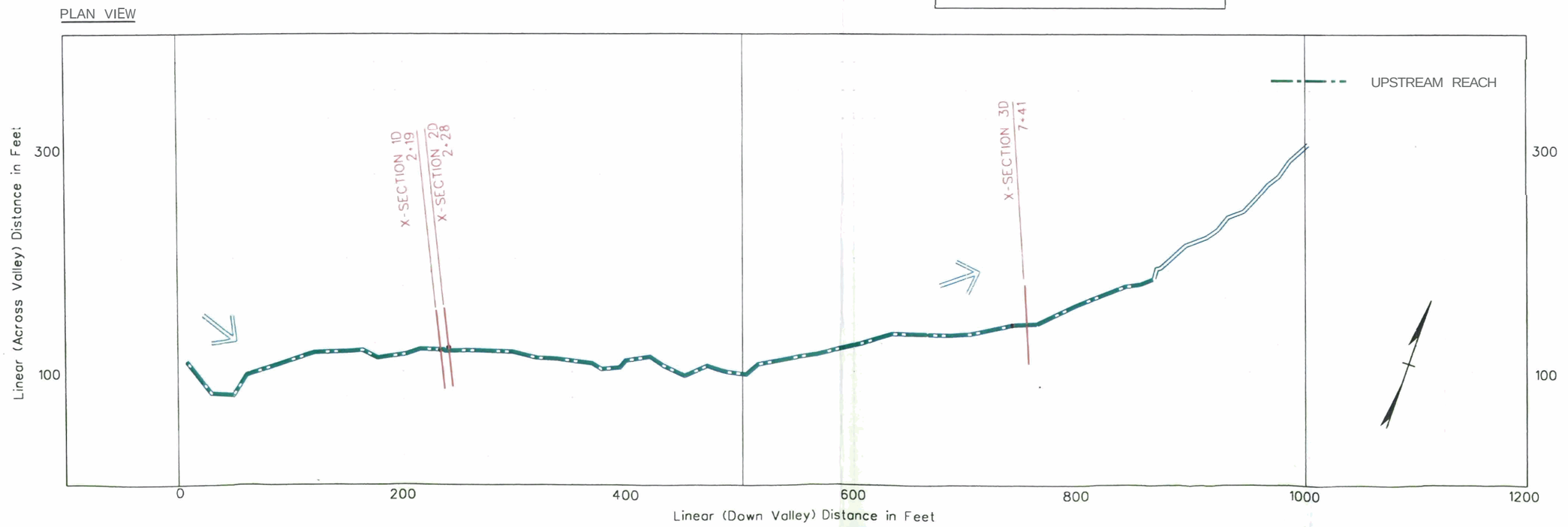
Bankfull Cross-section01Areo: 5.1 ft.sq.
Bankfull Width: 6.4'
Bankfull Maximum Depth: 1.5'
Bankfull Averoge Depth: 0.8'
Width of Flood Prone Areo: 50±'

BANKFULL
EXISTING GRADE
FLOOD PRONE AREA

NOTES:

1. All Cross-sections Focing the Downstreom Direction
2. Bankfull represents elevation at station point olong best fit line drown through bankfull elevation points for stream profile.
3. Cross-section stationing represents opproximote field locations.

PLAN VIEW



EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

DIMENSION & PLAN VIEW

UPSTREAM REACH – DULA THOROUGHFARE

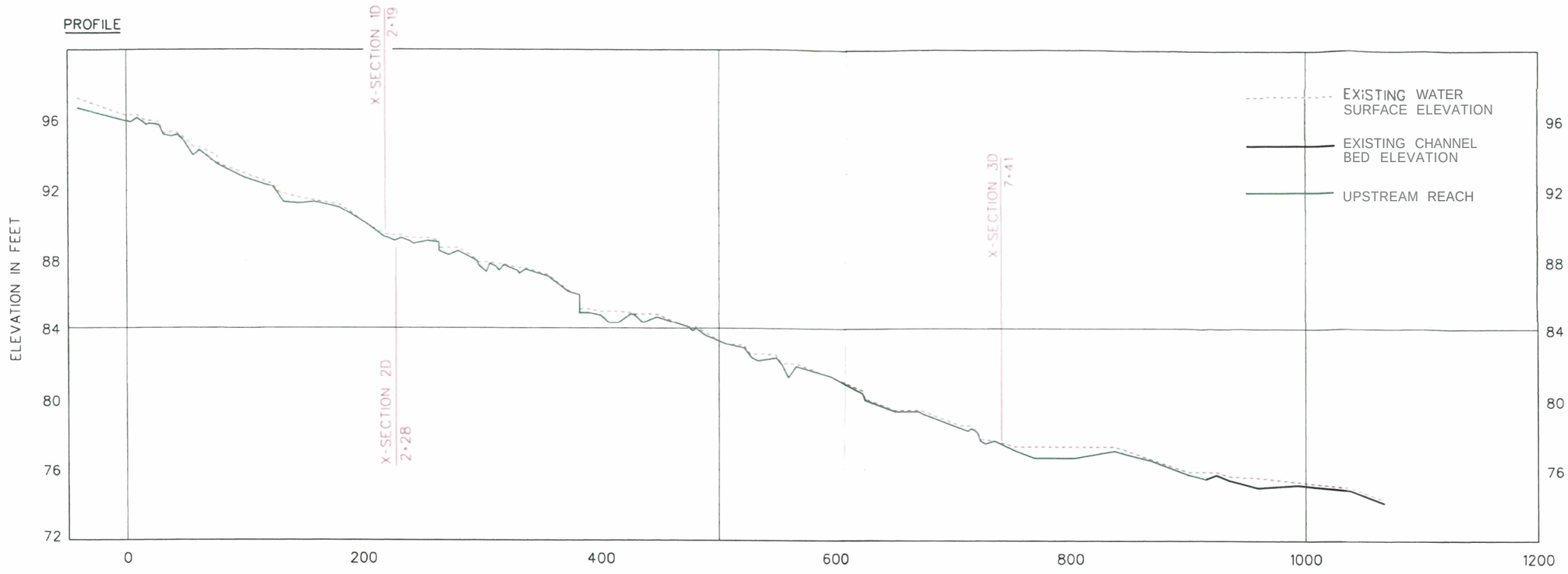
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	AS SHOWN

ESC Project No.: 02-113.34

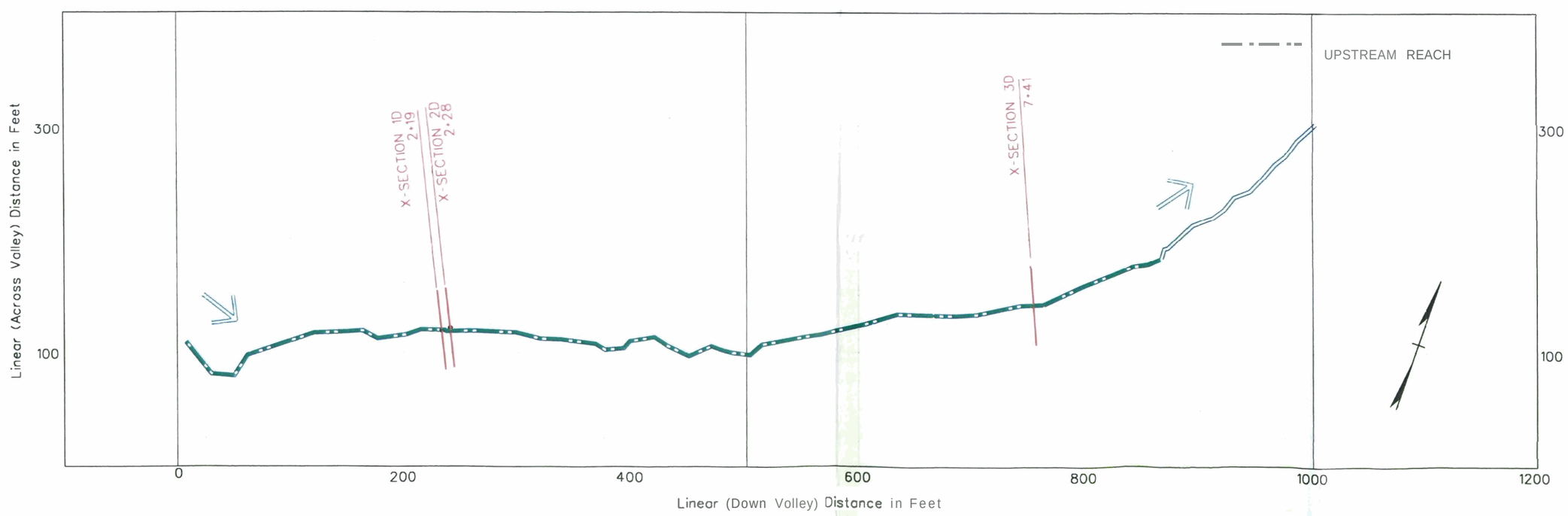
FIGURE

8E

PROFILE



PLAN VIEW



EcoScience Corporation
Raleigh, North Carolina

REVISIONS

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Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

PROFILE & PLAN VIEW

UPSTREAM REACH - DULA THOROUGHFARE

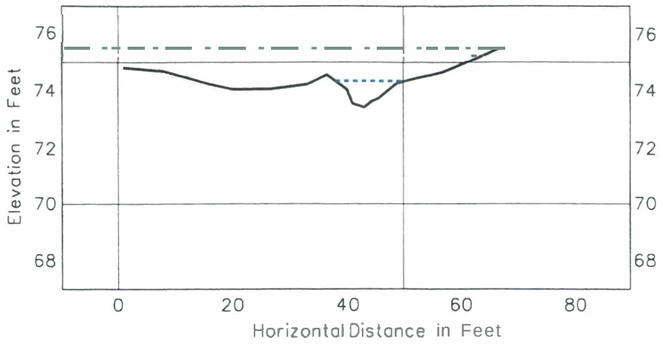
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	AS SHOWN

ESC Project No.: 02-113.34

FIGURE

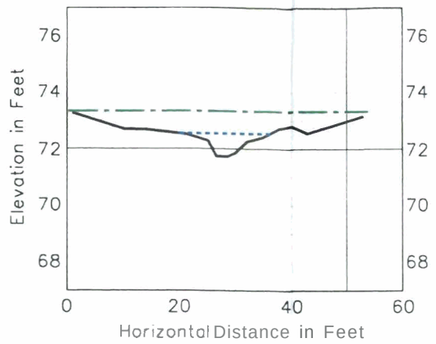
8F

11+34 CROSS-SECTION 4D (Wetland Area)



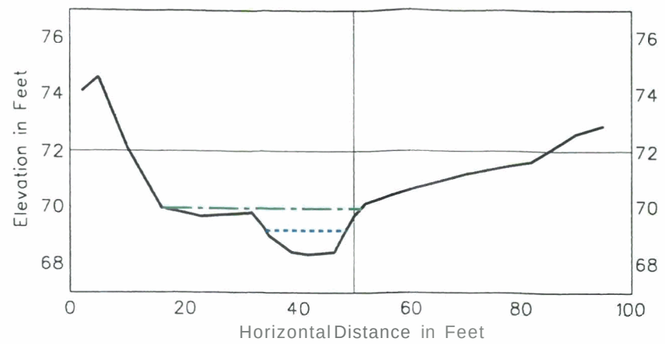
Bankfull Cross-sectional Area: 5.7 ft.sq.
Bankfull Width: 12 3'
Bankfull Maximum Depth: 0.9'
Bankfull Average Depth 0.5'
Width of Flood Prone Area: 150±'

13+88 CROSS-SECTION 5D (Wetland Area)



Bankfull Cross-sectional Area: 5.7 ft.sq.
Bankfull Width: 15.9'
Bankfull Maximum Depth: 0.8'
Bankfull Average Depth: 0.4'
Width of Flood Prone Area: 50±'

35+92 CROSS-SECTION 6D



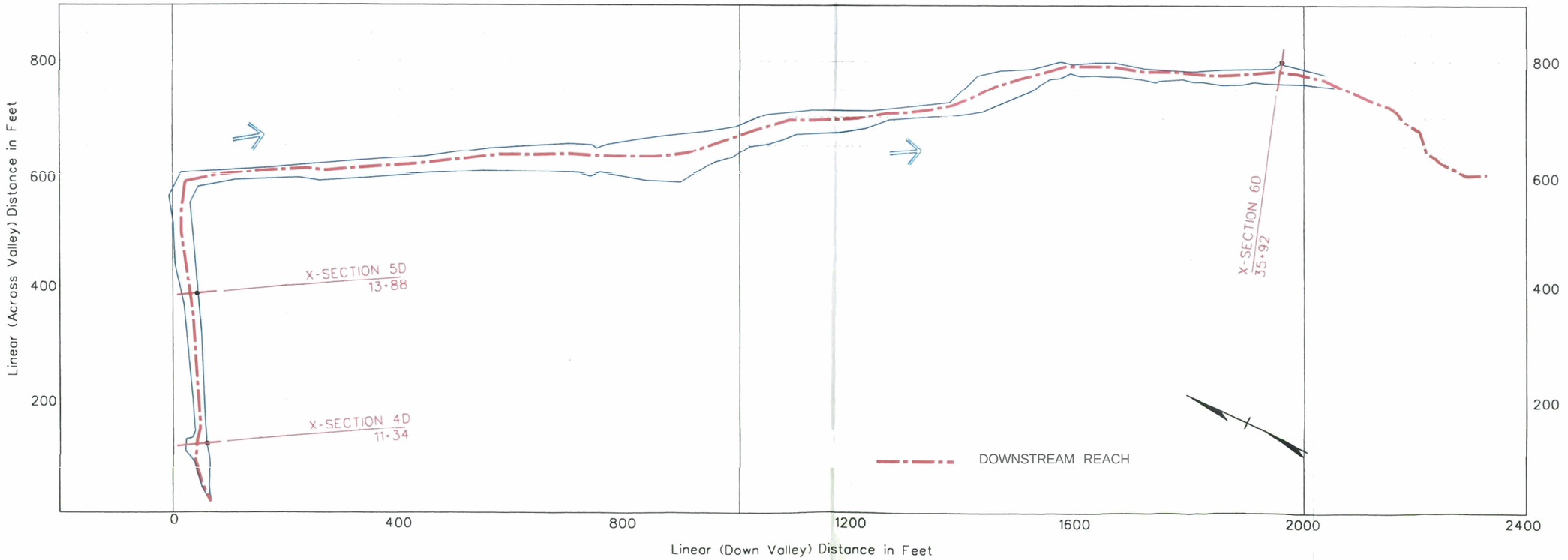
Bankfull Cross-sectional Area: 8 4 ft sq.
Bank full Width: 14.0'
Bankfull Maximum Depth: 0.8'
Bankfull Average Depth: 0.6'
Width of Flood Prone Area: 35±'

BANKFULL
EXISTING GRADE
FLOOD PRONE AREA

NOTES:

1. All Cross-sections Facing the Downstream Direction
2. Bankfullrepresents elevation at station point along best fit line drawn through bankfull elevation points for stream profile.
3. Cross-section stationing represents approximate field locations.

PLAN VIEW



EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement Program

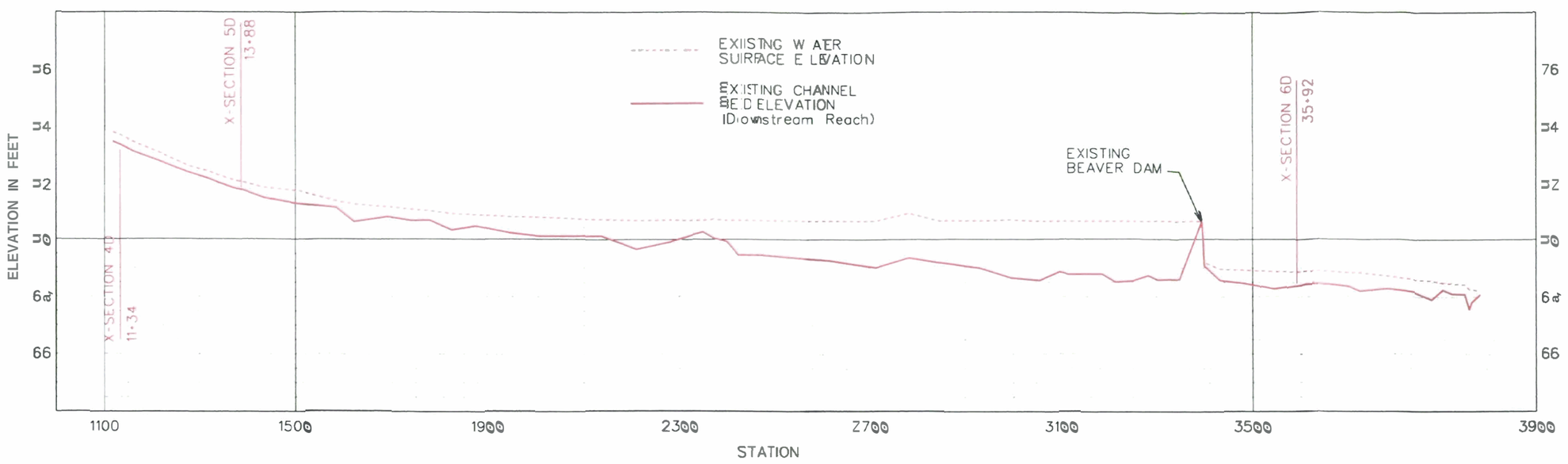
Project:
BISHOP SITE RESTORATION PLANNING
ANSON COUNTY, NORTH CAROLINA

Title:
DIMENSION & PLAN VIEW
DOWNSTREAM REACH – DULA THOROUGHFARE

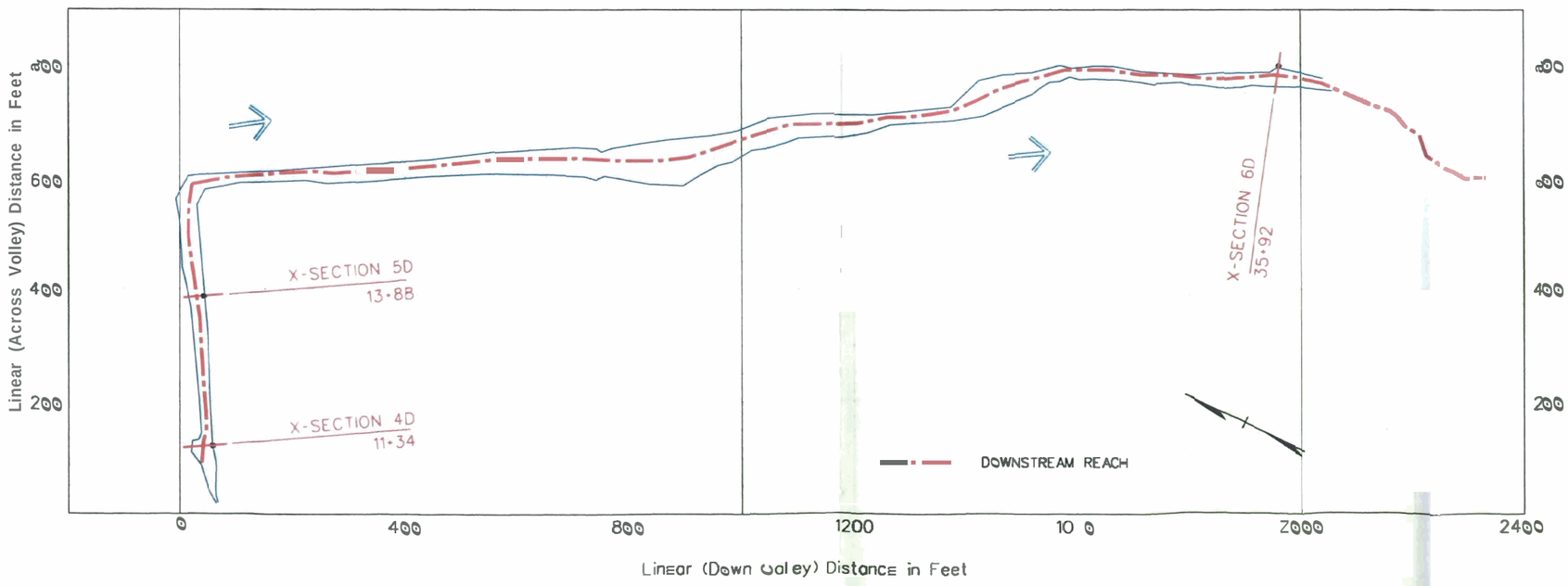
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	AS SHOWN
ESC Project No.:	
02-113.34	

FIGURE
8G

PROFILE



PLAN VIEW



EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client: Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

PROFILE & PLAN VIEW

DOWNSTREAM REACH – DULA THOROUGHFARE

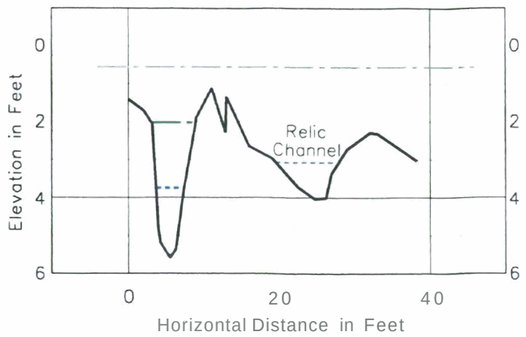
Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	AS SHOWN

ESC Project No.: 02-113.34

FIGURE

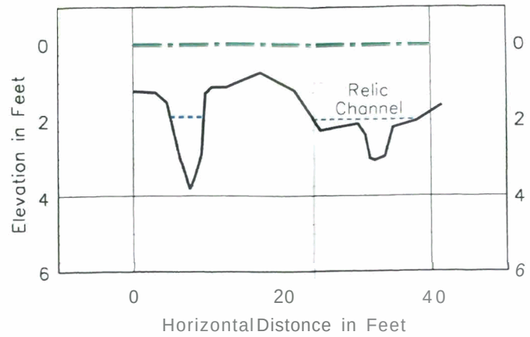
8H

CROSS-SECTION UDT1 (Riffle)



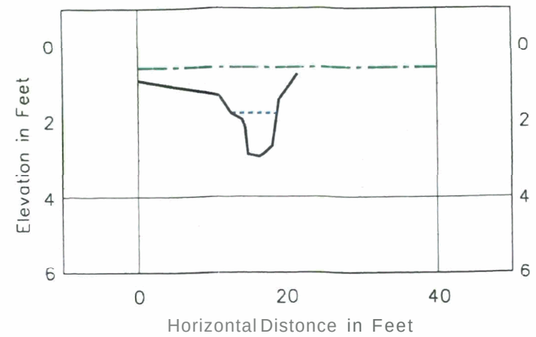
Bankfull Cross-sectional Areo: 4.8 ft.sq.
Bankfull Width: 3.7'
Bankfull Moximum Depth: 1.8'
Bankfull Average Depth: 1.3'
Width of Flood Prone Areo: 5.8'

CROSS-SECTION UDT2 (Riffle)



Bankfull Cross-sectional Areo: 5.1 ft.sq.
Bankfull Width: 4.4'
Bankfull Maximum Depth: 1.9'
Bankfull Averoge Depth: 1.2'
Width of Flood Prone Area: 40'

CROSS-SECTION UDT3 (Riffle)



Bankfull Cross-sectional Area: 4.4 ft.sq.

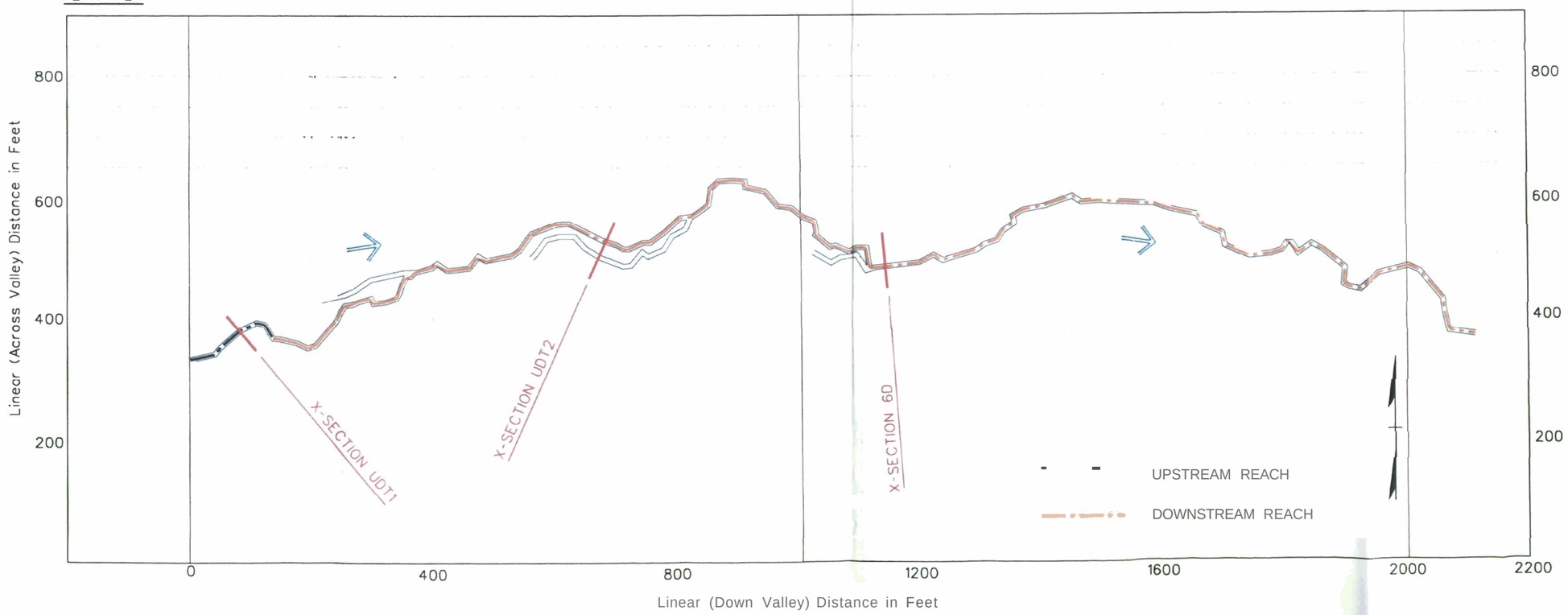
Bankfull Maximum Depth: 1.2'
Bankfull Average Depth: 0.7'
Width of Flood Prone Areo: 40'

BANKFULL
EXISTING GRADE
FLOOD PRONE AREA

NOTES:

1. All Cross-sections Facing the Downstream Direction
2. Bankfull represents elevation at station point along best fit line drown through bankfull elevation points for stream profile.
3. Cross-section stationing represents opproximote field locations.

PLAN VIEW



EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

DIMENSION & PLAN VIEW

UT to DULA THOROUGHFARE

Dwn By	Dole
MAF	SEPT 2004
Ckd By	Scale
WGL	AS SHOWN

ESC Project No
02-113.54

FIGURE

8I

800' 0 800'

SCALE IN FEET

NAD 83

CAMP BRANCH – SHEET 9A

DULA THOROUGHFARE EAST SHEET 9B

DULA THOROUGHFARE WEST – SHEET 9C

CONSERVATION EASEMENT

CONSERVATION EASEMENT

CONSERVATION EASEMENT

ROCKY RIVER

CARPENTER ROAD

PRESTON RIVER ROAD

SR 1527

TO NC 52

SR 1529

MITIGATION LEGEND

STREAM RESTORATION	4,468 ln. ft.
STREAM RESTORATION BRAIDED CHANNEL SYSTEM	1,195 ln. ft.
STREAM ENHANCEMENT (LEVEL 1)	1,190 ln. ft.
STREAM ENHANCEMENT (LEVEL 2)	7,306 ln. ft.
STREAM PRESERVATION	11,250 ln. ft.
WETLAND PRESERVATION	10.2 acres
WETLAND RESTORATION	5.6 acres
WETLAND ENHANCEMENT	0.94 acres
SPOIL REMOVAL	

EcoScience Corporation
Raleigh, North Carolina

REVISIONS	
1	CLIENT COMMENTS & FIELD INSPECTION - JDG 01-31-05

Client: Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

RESTORATION PLAN

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=800'

ESC Project No.: 02-113.34

FIGURE

9

MITIGATION LEGEND

	STREAM RESTORATION	2200 ln. ft.
	STREAM ENHANCEMENT - LEVEL 1	1190 ln. ft.
	STREAM ENHANCEMENT - LEVEL 2 (Includes Rocky River Frontage)	4395 ln. ft.
	STREAM PRESERVATION (Includes Camp Branch and UT to Camp Branch)	5200 ln. ft.
WB	WETLAND PRESERVATION	7.9 acres

LEGEND

- C/E — CONSERVATION EASEMENT
- MAJOR CONTOUR
- MINOR CONTOUR
- TREE LINE
- EXISTING ROAD
- EXISTING STREAM
- PROPOSED IN-STREAM STRUCTURE
- PROPOSED FLOODPLAIN
- PROPOSED CHANNEL BACKFILL
- PROPOSED FORD
- PROPOSED CHANNEL PLUG

LEVEL 1 STREAM ENHANCEMENT

NEW CHANNEL LOCATION

PROPOSED CHANNEL FORD

CHANNEL BACKFILL

PROPOSED FLOODPLAIN

NEW CHANNEL LOCATION

LEVEL 2 STREAM ENHANCEMENT

EXISTING CHANNEL

EXISTING POND

PROPOSED IN-STREAM STRUCTURE

PROPOSED CHANNEL PLUG

CONSERVATION EASEMENT

EXISTING TREELINE

ROCKY RIVER

C/E

WB

BM

NAD 83

300' 0 300'

SCALE IN FEET

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

RESTORATION PLAN

CAMP BRANCH

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=300'

ESC Project No.: 02-113.34

FIGURE

9A

LEGEND

- C/E — CONSERVATION EASEMENT
- MAJOR CONTOUR
- MINOR CONTOUR
- TREE LINE
- EXISTING ROAD
- EXISTING STREAM
- IN-STREAM STRUCTURE
- PROPOSED FLOODPLAIN
- CHANNEL BACKFILL
- PROPOSED FORD
- PROPOSED BRAIDED CHANNEL SYSTEM
- PROPOSED BACKWATER SLOUGH DEPRESSION
- PROPOSED CHANNEL PLUG

MITIGATION LEGEND

STREAM RESTORATION	1975 ln. ft.
STREAM RESTORATION BRAIDED CHANNEL SYSTEM	1195 ln. ft.
STREAM ENHANCEMENT - LEVEL 2 (Includes Dula Headwaters and Rocky River Frontage)	2350 ln. ft.
STREAM PRESERVATION (Includes Dula Headwaters and Rocky River Frontage)	3655 ln. ft.
WETLAND PRESERVATION	2.3 acres
WETLAND RESTORATION	5.6 acres

EXISTING ROAD

PROPOSED FLOODPLAIN

LEVEL 2 STREAM ENHANCEMENT

PROPOSED BRAIDED STREAM SYSTEM

PROPOSED BACKWATER SLOUGH DEPRESSION

LEVEL 2 STREAM ENHANCEMENT

NEW CHANNEL LOCATION

CHANNEL BACKFILL

PROPOSED CHANNEL PLUG

LEVEL 2 STREAM ENHANCEMENT

REFERENCE BACKWATER SLOUGH BRAIDED CHANNEL SYSTEM

EXISTING TREELINE

CONSERVATION EASEMENT

ROCKY RIVER

C/E

WB

300' 0 300'

SCALE IN FEET

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:

Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

RESTORATION PLAN

DULA THOROUGHFARE

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=300'

ESC Project No.: 02-113.34

FIGURE

9B

MITIGATION LEGEND

	STREAM RESTORATION	1,320 ln. ft.
	STREAM ENHANCEMENT - LEVEL 1	0 ln. ft.
	STREAM ENHANCEMENT - LEVEL 2	2310 ln. ft.
	STREAM PRESERVATION (Includes UT to Dulo Thoroughfare)	2375 ln. ft.
WB	WETLAND ENHANCEMENT	0.94 acres
	SPOIL REMOVAL	

EXISTING ROAD

EXISTING TREELINE

STREAM PRESERVATION

GRAVEL BORROW AREA

CHANNEL BACKFILL

PROPOSED CHANNEL FORD

SPOIL PILE REMOVAL

LEVEL 2 STREAM ENHANCEMENT

WETLAND ENHANCEMENT

EXISTING CHANNEL

CONSERVATION EASEMENT

WETLAND ENHANCEMENT

PROPOSED IN-STREAM STRUCTURE

STREAM RESTORATION

STREAM PRESERVATION

UT to DULA

C/E

S/C

WB

CHN

300' 0 300'

SCALE IN FEET

LEGEND

- C/E — CONSERVATION EASEMENT
- MAJOR CONTOUR
- MINOR CONTOUR
- TREE LINE
- EXISTING ROAD
- EXISTING STREAM
- IN-STREAM STRUCTURE
- PROPOSED FLOODPLAIN
- CHANNEL BACKFILL
- PROPOSED FORD
- EXISTING POWER POLE

EcoScience Corporation
Raleigh, North Carolina

REVISIONS	
1	CLIENT COMMENTS & FIELD INSPECTION - JDG 01-31-05

Client: Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

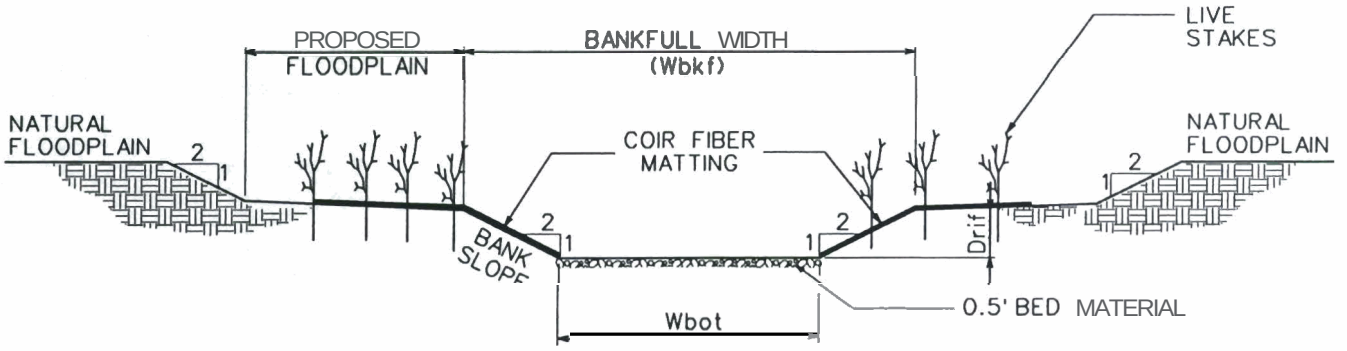
RESTORATION PLAN

UT TO DULA THOROUGHFARE

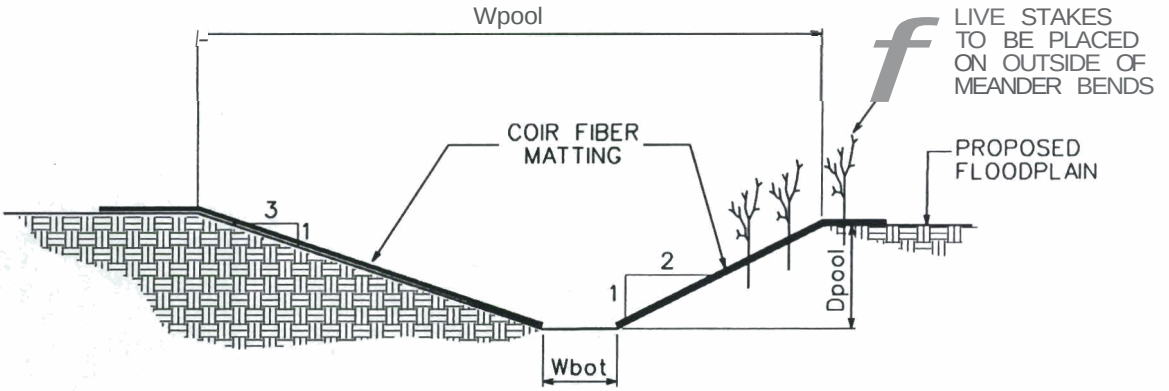
Dwn By: MAF	Date: SEPT 2004
Ckd By: WGL	Scale: 1"=300'
ESC Project No.: 02-113.34	

FIGURE

9C



TYPICAL RIFFLE CROSS-SECTION



TYPICAL POOL CROSS-SECTION

CROSS-SECTION DIMENSIONS

REACH	Wbkf (ft.)	Wbot (ft.) Riffle	Driff (ft.)	Wpool (ft.)	Wbot (ft.) Pool	Dpool (ft.)	Width/Depth Ratio
CAMP BRANCH - REACH 1 & 2	21.5	12.3	2.3	28	12	3.2	12
CAMP BRANCH - REACH 3	22.4	12.4	2.5	29.1	12.1	3.4	12
UT TO CAMP BRANCH	10.6	5	1.4	15.9	7.9	1.6	12
DULA THOROUGHFARE	8.6	4.6	1.0	12.0	6.5	1.1	12
UT TO DULA THOROUGHFARE	7.5	4.3	0.8	10.5	6	0.9	12

EcoScience Corporation
Raleigh, North Carolina

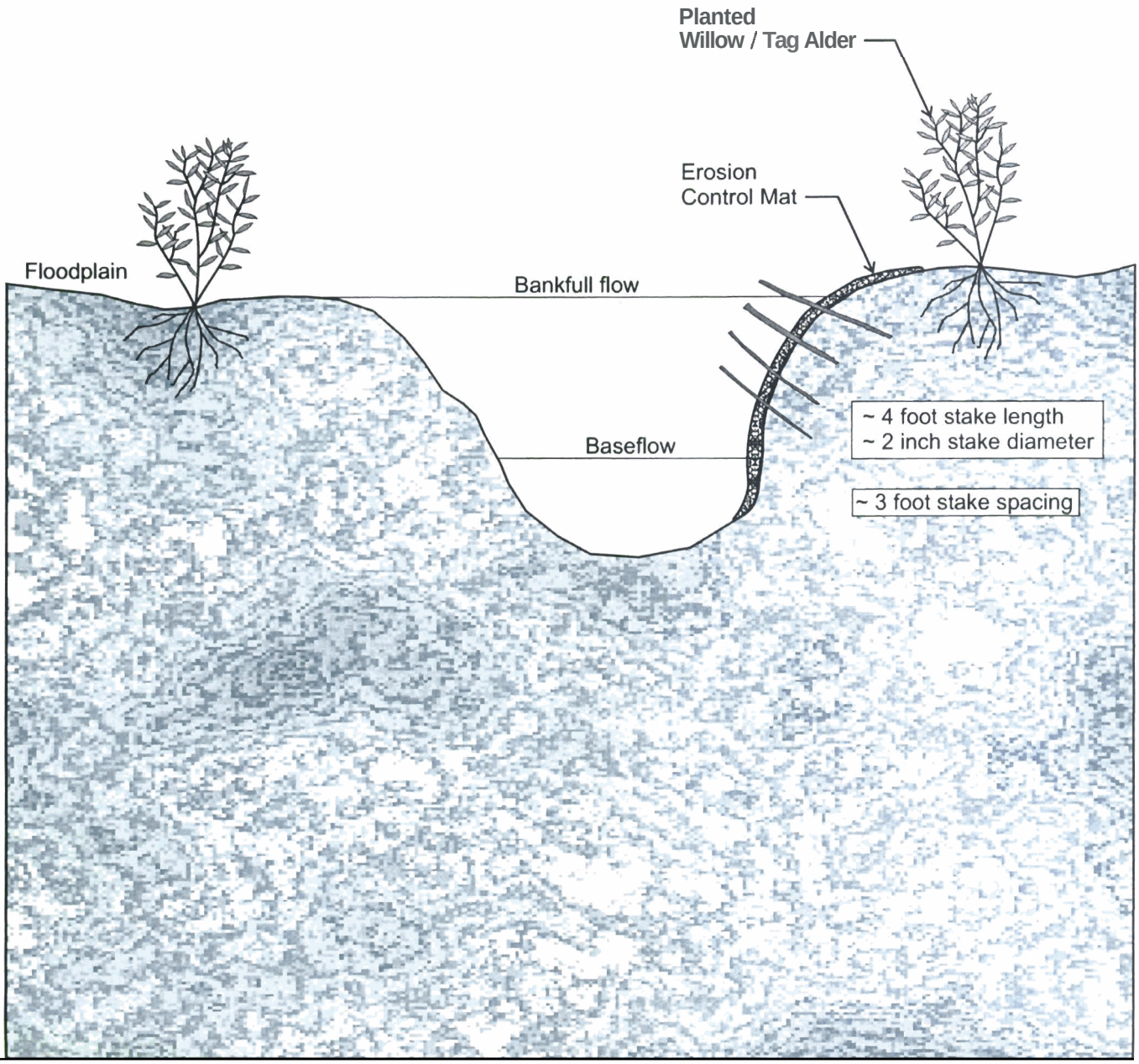
Client: Ecosystem Enhancement Program

Project:

TYPICAL CHANNEL SECTIONS
BISHOP SITE
RESTORATION PLANNING
ANSON COUNTY. NORTH CAROLINA

Dwn By: MAF | Ckd By: WGL
Date: SEPT 2004
Scale: NO SCALE
ESC Project No.: 02-113.34

FIGURE
10



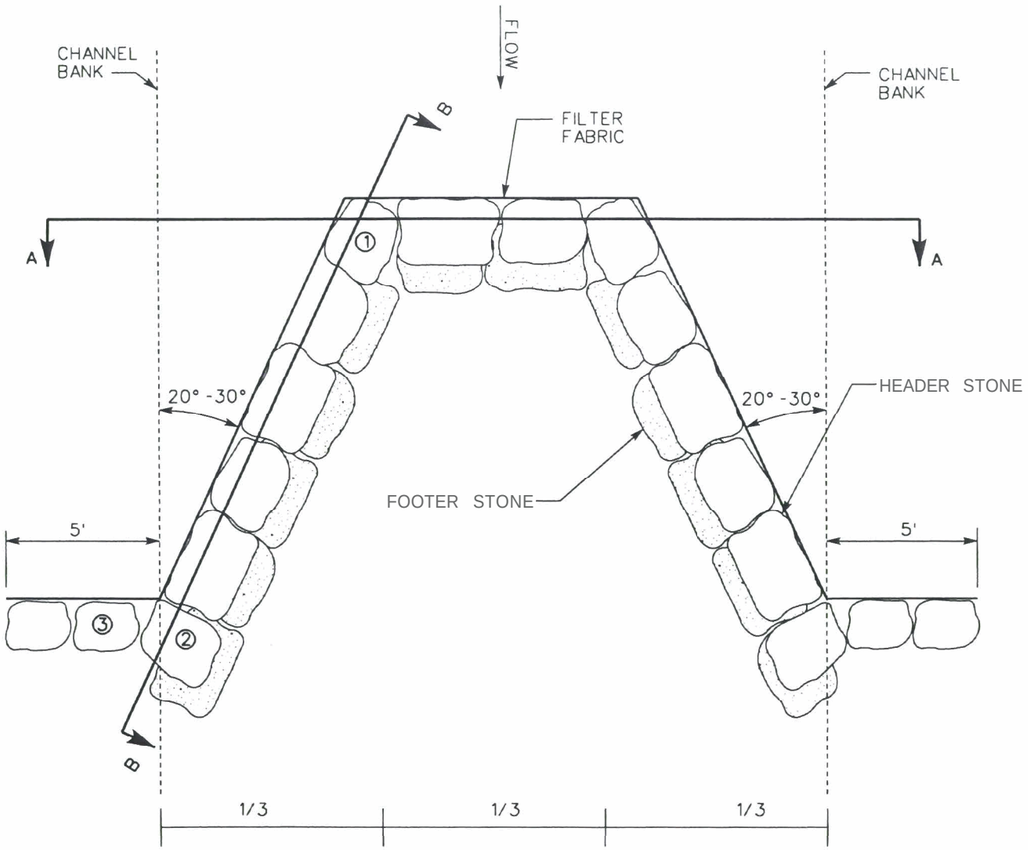
EcoScience Corporation
Raleigh, North Carolina

Live Willow Stake Embankment with Erosion Control Matting

Bishop Site Restoration Planning
Anson County, North Carolina

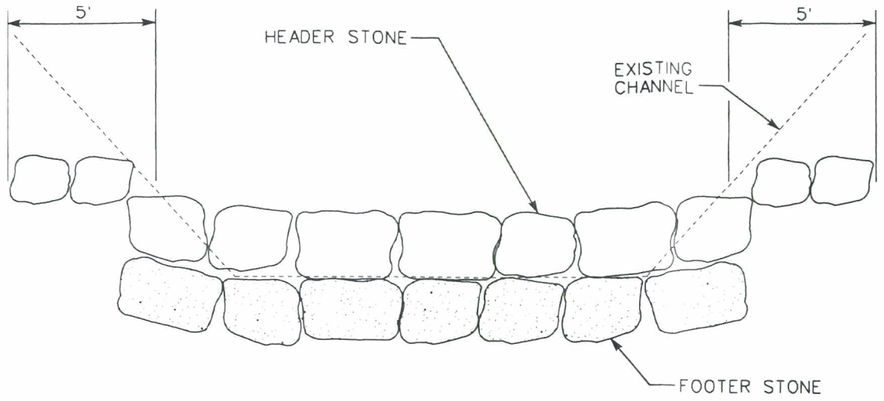
Dwn. by:	HJS
Ckd by:	WGL
	SEPT 2004
Project:	02 113 34

Figure 11

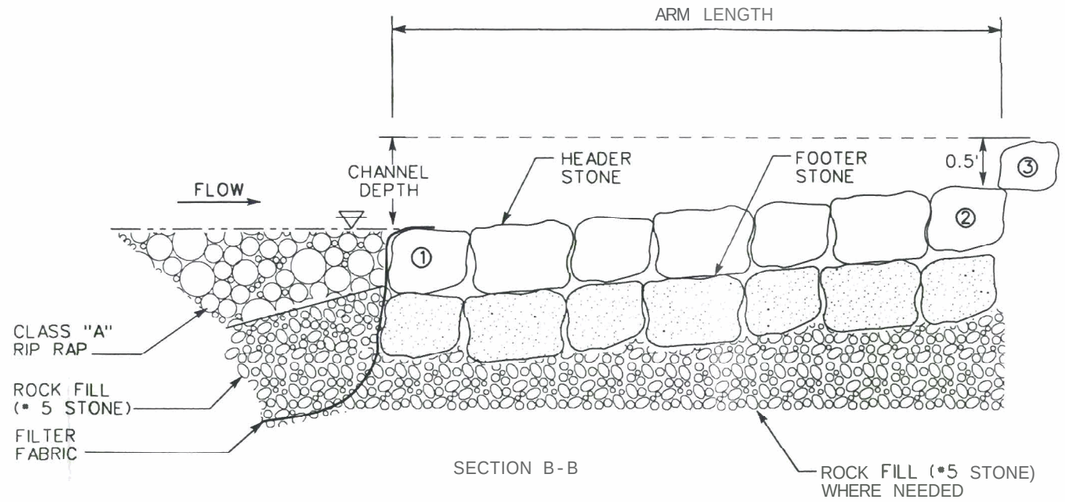


PLAN VIEW

NOTE: HEADER AND FOOTER STONES ARE LARGE, ANGULAR BOULDERS



SECTION A-A



SECTION B-B

REACH	ARM LENGTH (FT.)	CHANNEL DEPTH (FT.)
CAMP BRANCH - REACH 1& 2	18.0	2.3
CAMP BRANCH - REACH 3	20.0	2.5
UT TO CAMP BRANCH	9.0	1.4
DULA THOROUGHFARE	7.0	0.7
UT TO DULA THOROUGHFARE	8.0	0.8

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client: Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

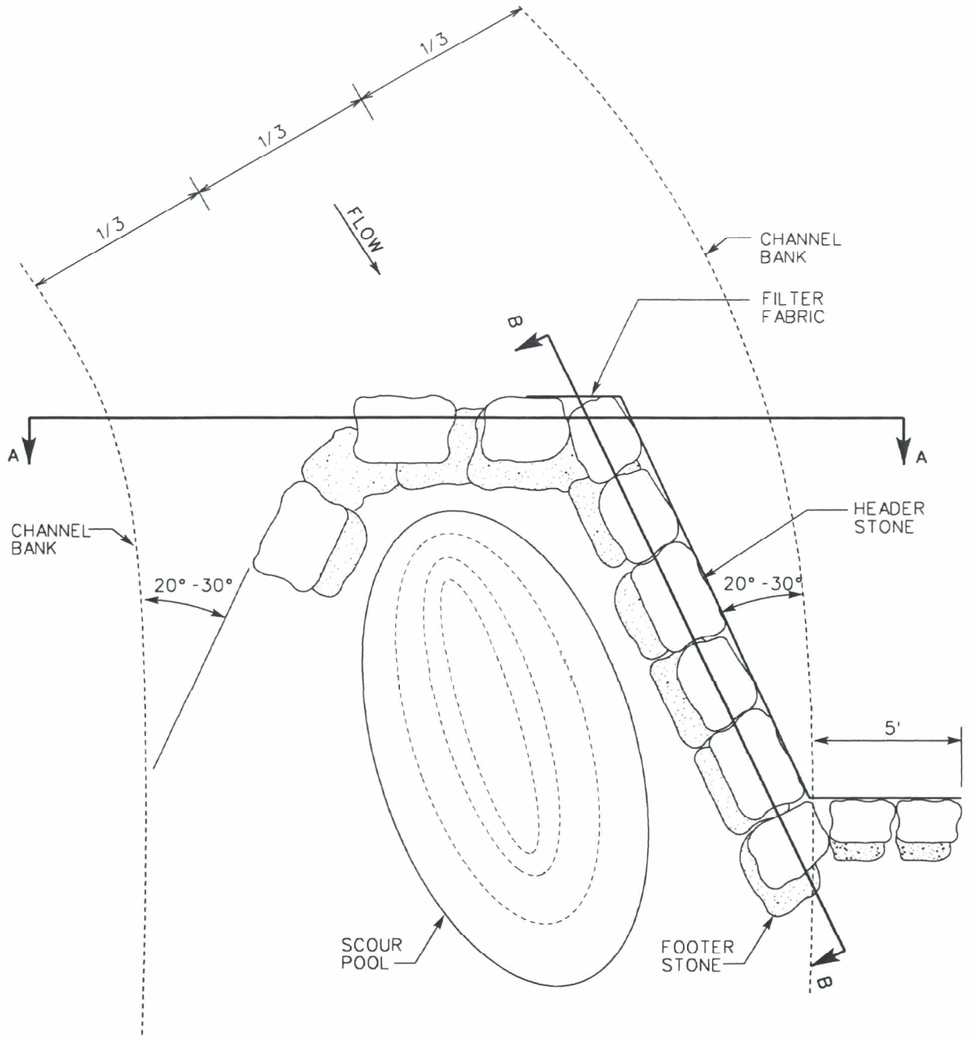
TYPICAL CROSS-VANE WEIR

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	NO SCALE

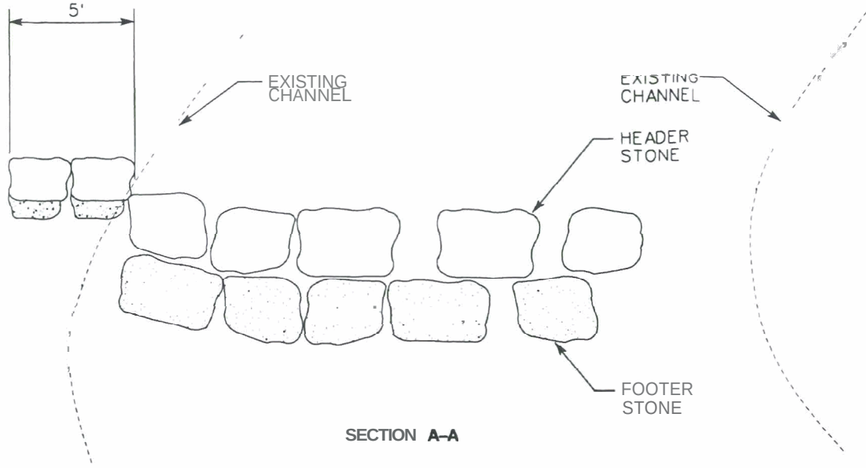
ESC Project No.: 02-113.34

FIGURE

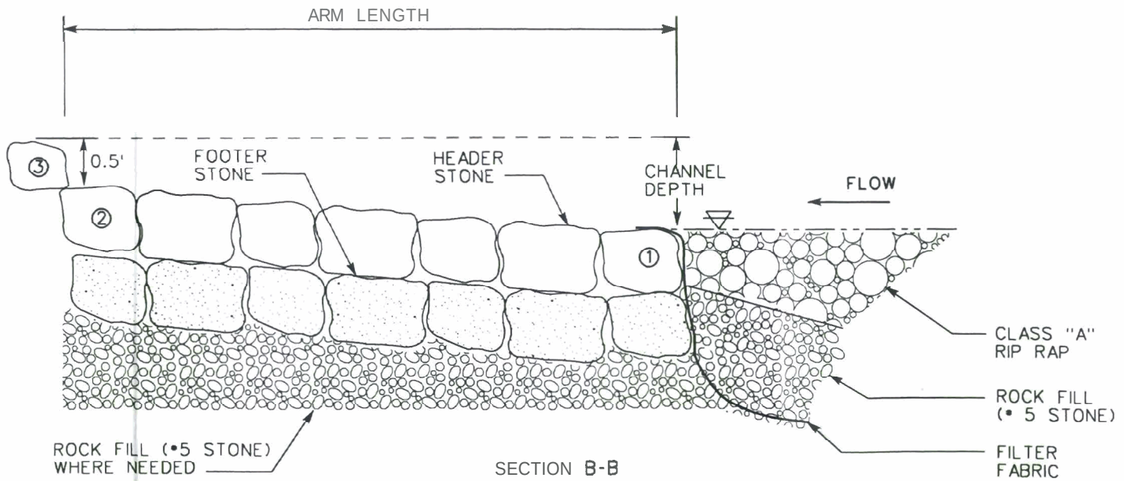
12



PLAN VIEW



SECTION A–A



SECTION B-B

REACH	ARM LENGTH (FT.)	CHANNEL DEPTH (FT.)
CAMP BRANCH - REACH 1& 2	18.0	2.3
CAMP BRANCH - REACH 3	20.0	2.5
UT TO CAMP BRANCH	9.0	1.4
DULA THOROUGHFARE	7.0	0.7
UT TO DULA THOROUGHFARE	8.0	0.8

NOTE: HEADER AND FOOTER STONES ARE LARGE, ANGULAR BOULDERS

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY.
NORTH CAROLINA

Title:

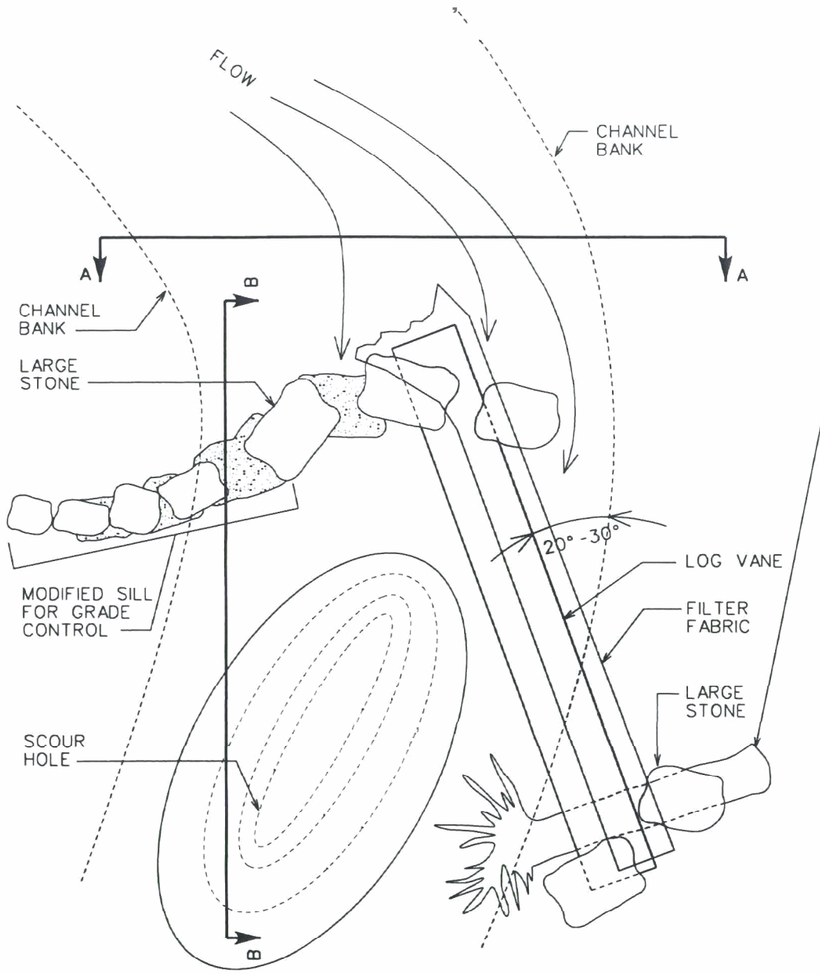
TYPICAL J-HOOK WEIR

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	NO SCALE

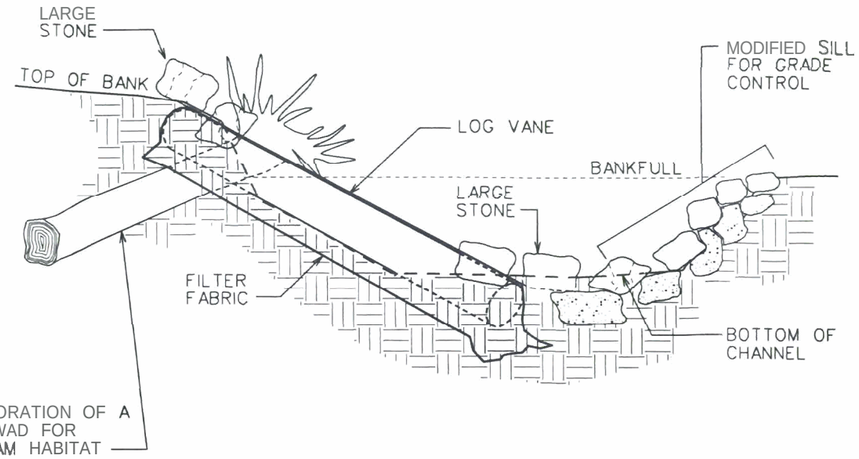
ESC Project No.: 02-113.34

FIGURE

13

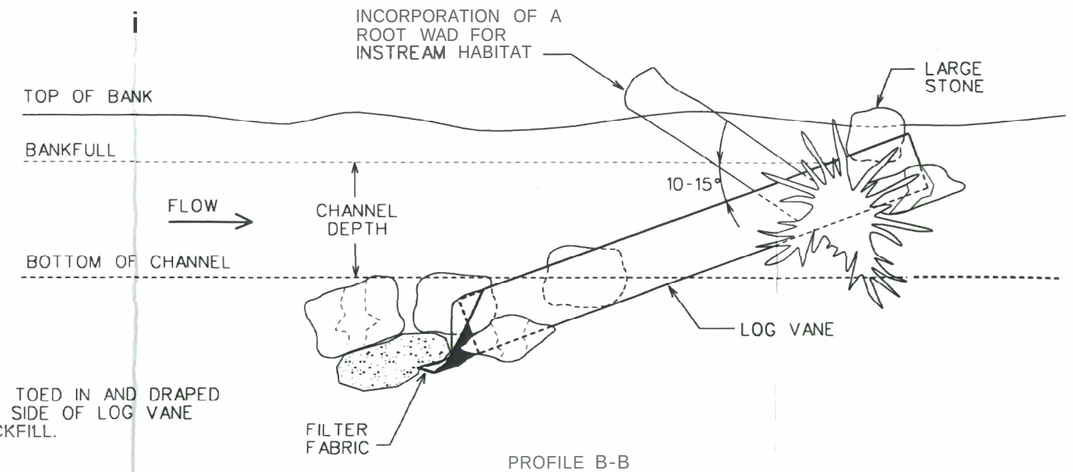


PLAN VIEW



CROSS-SECTION A-A

NOTE:
FILTER FABRIC TOED IN AND DRAPED ON UPSTREAM SIDE OF LOG VANE PRIOR TO BACKFILL.



PROFILE B-B

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

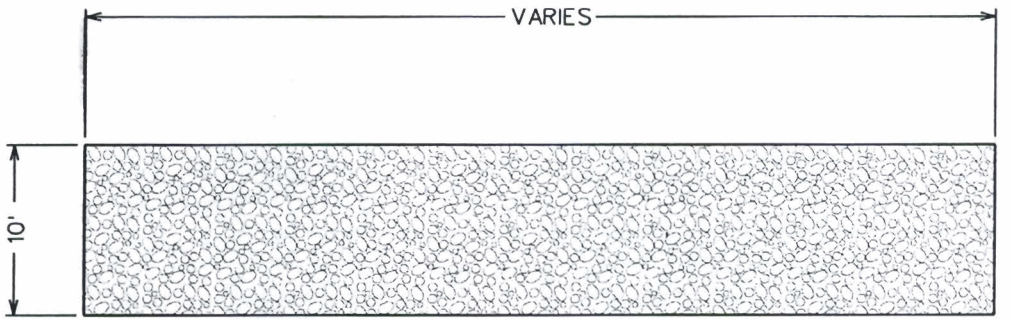
Project:
BISHOP SITE RESTORATION PLANNING
ANSON COUNTY, NORTH CAROLINA

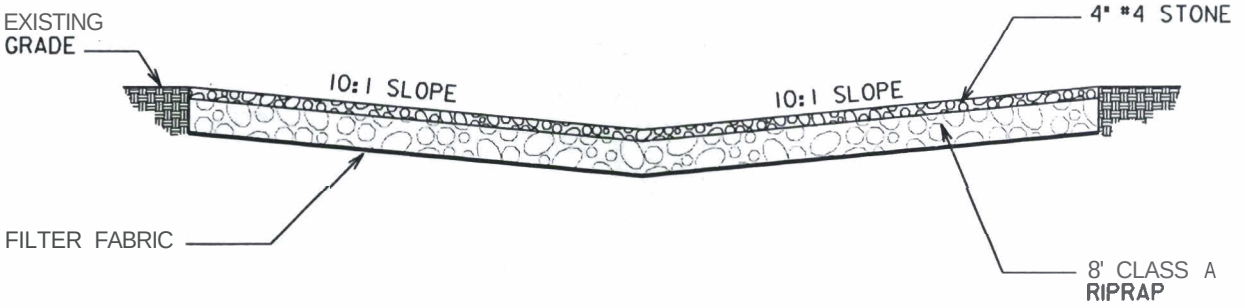
Title:
TYPICAL LOG VANE WEIR

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	NO SCALE

ESC Project No.: 02-113.34

FIGURE
14





NOTES:

1. LAY FILTER FABRIC ALONG ENTIRE LENGTH OF BED.
2. FILL WITH 8' OF 'CLASS A" RIPRAP, FOLLOWED BY 4' OF #4 STONE. BRING FINISHED GRADE UP TO LEVEL OF PROPOSED STREAM BED.

EcoScience Corporation Raleigh, North Carolina	Client: PROGRAM	Project: **PERMANENT FORD DETAIL** **Bishop Site Restoration Planning** **Anson County, North Carolina**	Dwn By: MAF Ckd WGL Date: SEPT 2004 Scale: NO SCALE ESC Project No.: 04-182	FIGURE 15

LEGEND

- —C/E— CONSERVATION EASEMENT
- MAJOR CONTOUR
- MINOR CONTOUR
- TREE LINE
- EXISTING ROAD
- EXISTING STREAM

PLANT COMMUNITIES

- STREAMSIDE ASSEMBLAGE (15' EACH SIDE OF CHANNEL) 4.1 total acres
- SLOPE FOREST 27.2 total acres
- BOTTOMLAND HARDWOOD FOREST 51.7 total acres

EXISTING TREELINE

EXISTING STREAM

EXISTING POND

WE 230.8

CONSERVATION EASEMENT

C/E

NAD 83

300' 0 300'

SCALE IN FEET

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
NCDOT Ecosystem Enhancement PROGRAM

Project:
BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:
PLANTING PLAN

CAMP BRANCH

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=300'

ESC Project No.: 02-113.34

FIGURE

16A

LEGEND

- —C/E— CONSERVATION EASEMENT
- MAJOR CONTOUR
- MINOR CONTOUR
- TREE LINE
- EXISTING ROAD
- EXISTING STREAM

PLANT COMMUNITIES

- STREAMSIDE ASSEMBLAGE (15' EACH SIDE OF CHANNEL(4.1 total acres
- SLOPE FOREST 27.2 total acres
- BOTTOMLAND HARDWOOD FOREST 51.7 total acres
- FRESHWATER MARSH/ BACKWATER SLOUGH ASSEMBLAGE 6.2 total acres

EXISTING ROAD

EXISTING TREELINE

CONSERVATION EASEMENT

C/E

NAD 83

300' 0 300'

SCALE IN FEET

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

PLANTING PLAN

DULA THOROUGHFARE EAST

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=300'

ESC Project No.: 02-113.34

FIGURE

16B

LEGEND

- C/E — CONSERVATION EASEMENT
- MAJOR CONTOUR
- MINOR CONTOUR
- TREE LINE
- EXISTING ROAD
- EXISTING STREAM
- EXISTING POWER POLE

EXISTING TREELINE

EXISTING ROAD

C/E

3/C

EXISTING CHANNEL

CONSERVATION EASEMENT

WE 260.8

300' 0 300'

SCALE IN FEET

PLANT COMMUNITIES

- SLOPE FOREST 27.2 totolocres
- BOTTOMLAND HARDWOOD FOREST 51.7 totolocres
- STREAMSIDE ASSEMBLAGE (15' EACH SIDE OF CHANNEL) 4.1 totalacres

EcoScience Corporation
Raleigh, North Carolina

REVISIONS

Client:
Ecosystem Enhancement PROGRAM

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

PLANTING PLAN

DULA THOROUGHFARE WEST

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	1"=300'

ESC Project No.: 02-113.34

FIGURE

16C

COMMUNITY ASSEMBLAGE	SLOPE FOREST	STREAMSIDE ASSEMBLAGE	BOTTOMLAND HARDWOOD FOREST
CANOPY VEGETATION	Mockernut Hickory Pignut Hickory White Oak Sourwood American Holly Flowering Dogwood	**Streamside Forest** Black Willow Elder Berry River Birch American Sycamore Swamp Dogwood **Streamside Shrub** Tag Alder Buttonbush Arrow-wood Viburnum Possumhaw Vibernum Highbush Blueberry	Swamp Chestnut Oak American Elm Sugarberry Green Ash Shagbark Hickory Willow Oak Northern Red Oak Southern Red Oak Black Gum American Sycamore
LAND FORM	Floodplain Slopes	Stream Banks and Adjacent Flood Plain	Floodplain Flats

EcoScience Corporation
Raleigh, North Carolina

Client:
Ecosystem Enhancement Program

Project:
BISHOP SITE RESTORATION PLANNING
Anson County
North Carolina

Title:
CONCEPTUAL MODEL OF TARGET COMMUNITY PATTERNS

Dwn By:	Date:
MAF	SEPT 2004
Ckd By:	Scale:
WGL	As Shown

ESC Project No.: 02-113.34

FIGURE
17

800' 0 800'

SCALE IN FEET

NAD 83

MITIGATION LEGEND

- NEW CHANNEL LOCATION
- NEW BRAIDED CHANNEL SYSTEM
- EXISTING STREAM
- WD WETLANDS
- GROUNDWATER GAUGES
- PERMANENTLY MONUMENTED CROSS-SECTIONS
- STREAM MONITORING REACH (450 ln. ft.)
- 2. VEGETATION SAMPLNG PLOTS 10m x 10m (32.8 ft. x 32.8 ft.)

CONSTRUCTION EASEMENT

ROCKY RIVER

CARPENTER ROAD

CHRISTMAN ROAD

PRESTON RIVER ROAD

SR 1829

SR 1827

TOMC 53

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11.

EcoScience Corporation

Raleigh, North Carolina

REVISIONS	
1	CLIENT COMMENTS & FIELD
	INSPECTION -JDG 01-31-05

Client: Ecosystem Enhancement Program

Project:

BISHOP SITE RESTORATION PLANNING

ANSON COUNTY, NORTH CAROLINA

Title:

MONITORING PLAN

Dwn By:	Date:
MAF	DEC 2004
Ckd By:	Scale:
JCD	1"=800'

ESC Project No.: 02-113.34

FIGURE

18

APPENDIX B

TABLES

TABLE 2A
BISHOP STREAM RESTORATION SITE
Morphological Characteristics of Existing Channels

Variables	Camp Branch Exisiting Channel			UT Camp Branch
	Reach 1: Upstream of Headcut (E)	Reach 2: Headcut to Ford (E)	Reach 3: Downstream of Ford (G)	Downstream of Pond (E/C)
1 Stream Type	E	E	G	E/G
2 Drainage Area (mi^2)	2.4	2.4	2.7	0.3
3 Bankfull Discharge (cfs)	168	168	182	37.3
Dimension Variables (Feet)				
4 Bankfull Cross Sectional Area (A_{bkf})	38.7	38.7	42	9.4
5 Bankfull Width (W_{bkf})	Mean: 19.1 Range: 16.5-21.3	Mean: 18.3 Range: NA	Mean: 17.8 Range: 16-19.5	Mean: 11 Range: 6 - 15.7
6 Bankfull Mean Depth (D_{bkf})	Mean: 2.0 Range: 1.8-2.2	Mean: 2.1 Range: NA	Mean: 2.4 Range: 2.2-2.6	Mean: 1.1 Range: 0.6 - 1.6
7 Bankfull Maximum Depth (D_{max})	Mean: 2.6 Range: 2.4-2.7	Mean: 2.7 Range: NA	Mean: 2.8 Range: 2.5-3.0	Mean: 2.1 Range: 1.4 - 2.7
8 Pool Width (W_{pool})	Mean: 23.6 Range: NA	Mean: 12.9 Range: NA	Mean: 16.4 Range: 13.4-19.4	Mean: NA Range: NA
9 Maximum Pool Depth (D_{pool})	Mean: 4.3 Range: NA	Mean: 3.2 Range: NA	Mean: 3.7 Range: 3.3-4.1	Mean: NA Range: NA
10 Width of Floodprone Area (W_{fpa})	Mean: 110 Range: 75-180	Mean: 100 Range: NA	Mean: 20.8 Range: 17.2-24.3	Mean: NA Range: NA
Dimension Ratios				
11 Entrenchment Ratio (W_{fpa}/W_{bkf})	Mean: 6.6 Range: 3.8-8.5	Mean: 5.5 Range: NA	Mean: 1.1 Range: 1.1-1.2	Mean: 11.5 Range: 6.4 - 16.6
12 Width/Depth Ratio W_{bkf}/D_{bkf})	Mean: 9.9 Range: 7.5-11.8	Mean: 8.7 Range: NA	Mean: 7.6 Range: 6.2-8.9	Mean: 15 Range: 3.75 - 26.17
13 Max. D_{riff}/D_{bkf} Ratio	Mean: 1.2 Range: 1.2-1.5	Mean: 1.3 Range: NA	Mean: 1.1 Range: 1.1-1.2	Mean: NA Range: NA
14 Low Bank Height/ Max. D_{bkf} Ratio	Mean: 1.2 Range: 1.0-1.3	Mean: 1.5 Range: NA	Mean: 2.3 Range: 2.2-2.4	Mean: 1.04 Range: 1 - 1.07
15 Pool Depth/Bankfull Mean Depth (D_{pool}/D_{bkf})	Mean: 2.2 Range: NA	Mean: 1.2 Range: NA	Mean: 1.6 Range: 1.4-1.7	Mean: NA Range: NA
16 Pool width/Bankfull Width (W_{pool}/W_{bkf})	Mean: 1.2 Range: NA	Mean: 0.7 Range: NA	Mean: 1.0 Range: 0.8-1.1	Mean: NA Range: NA
17 Pool Area/Bankfull Cross Sectional Area	Mean: 1.4 Range: NA	Mean: 0.8 Range: NA	Mean: 1.2 Range: 0.9-1.4	Mean: NA Range: NA
Pattern Variables (Feet)				
18 Pool to Pool Spacing (L_{p-p})	Mean: 74 Range: 45-145	Mean: 74 Range: 45-145	No distinctive repetitive pattern of riffles and pools due to straightening activities	No distinctive repetitive pattern of riffles and pools due to straightening activities
19 Meander Length (L_m)	Mean: 133 Range: 66-240	Mean: 133 Range: 66-240		
20 Belt Width (W_{belt})	Mean: 43 Range: 30-97	Mean: 43 Range: 30-97	Mean: 37 Range: 19-79	
21 Radius of Curvature (R_c)	Mean: 41 Range: 17-200	Mean: 41 Range: 17-200	No distinctive repetitive pattern of riffles and pools	
22 Sinuosity (Sin)	1.18	1.18	1.05	1.04
Pattern Ratios				
23 Pool to Pool Spacing/ Bankfull Width (L_{p-p}/W_{bkf})	Mean: 3.8 Range: 2.3-7.4	Mean: 4.0 Range: 2.5-7.9	No distinctive repetitive pattern of riffles and pools due to straightening activities	No distinctive repetitive pattern of riffles and pools due to straightening activities.
24 Meander Length/ Bankfull Width (L_m/W_{bkf})	Mean: 6.8 Range: 3.4-12.2	Mean: 7.3 Range: 3.6-13.1		
25 Meander Width Ratio (W_{belt}/W_{bkf})	Mean: 2.2 Range: 1.5-4.9	Mean: 2.3 Range: 1.6-5.3	Mean: 2.1 Range: 1.1-4.4	
26 Radius of Curvature/ Bankfull Width (Rc/W_{bkf})	Mean: 2.1 Range: 0.9-10.2	Mean: 2.2 Range: 0.9-10.9	No distinctive repetitive pattern of riffles and pools	
Profile Variables (Feet/Feet)				
27 Average Water Surface Slope (S_{ave})	0.0029	0.0029	0.0041	0.0212
28 Valley Slope (S_{valley})	0.0047	0.0047	0.0047	0.0220
29 Riffle Slope (S_{riffle})	Mean: 0.0070 Range: 0.0008 - 0.0167	Mean: 0.0093 Range: 0.0042 - 0.0144	Mean: 0.0127 Range: 0.0011 - 0.0614	Mean: 0.0434 Range: 0.0133 - 0.1062
30 Pool Slope (S_{pool})	Mean: 0.0004 Range: 0.0000 - 0.0013	Mean: 0.0003 Range: 0.0000 - 0.0007	Mean: 0.0005 Range: 0.0000 - 0.0020	Mean: 0.0039 Range: 0 - 0.0360
Profile Ratios				
31 Riffle Slope/ Water Surface Slope (S_{riffle}/S_{ave})	Mean: 2.4 Range: 0.28 - 5.8	Mean: 3.2 Range: 1.45 - 4.96	Mean: 3.1 Range: 0.27 - 15.0	Mean: 2.0 Range: 0.6 - 4.8
32 Pool Slope/Water Surface Slope (S_{pool}/S_{ave})	Mean: 0.06 Range: 0 - 0.18	Mean: 0.10 Range: 0 - 0.24	Mean: 0.12 Range: 0 - 0.49	Mean: 0.18 Range: 0 - 1.6
Materials (Millimeters)				
D16	0.6	N/A	N/A	N/A
D35	4.7	2.9	7.6	N/A
D50	7.2	5	13.8	N/A
D84	17	10	39	N/A
D95	30	19	60	N/A

TABLE 2B
BISHOP STREAM RESTORATION SITE
Morphological Characteristics of Existing Channels

Variables	Dulla Exisiting Channel		UT to Dulla Exisiting Channel	
	Upstream Stream Reach (E)	Downstream Reach (C)	Upstream Stream Reach (G)	Downstream Stream Reach (E)
1 Stream Type	E	C	G	E
2 Drainage Area (mi^2)	0.12	0.14-0.25	0.11	0.12-0.13
3 Bankfull Discharge (cfs)	19.3	21.5-32.7	18.1	19.3-20.4
Dimension Variables (Feet)				
4 Bankfull Cross Sectional Area (A_{bkf})	5.1	5.7-8.4	4.8	4.4-5.1
5 Bankfull Width (W_{bkf})	Mean: 6.0 Range: 5.5-6.4	Mean: 14 Range: 12.3-15.9	Mean: 3.7 Range: NA	Mean: 5.3 Range: 4.4-6.2
6 Bankfull Mean Depth (D_{bkf})	Mean: 0.9 Range: 0.8-0.9	Mean: 0.5 Range: 0.4-0.6	Mean: 1.3 Range: NA	Mean: 1.0 Range: 0.7-1.2
7 Bankfull Maximum Depth (D_{max})	Mean: 1.6 Range: 1.5-1.6	Mean: 0.8 Range: 0.8-0.9	Mean: 1.8 Range: NA	Mean: 1.6 Range: 1.2-1.9
8 Pool Width (W_{pool})	Mean: 4.1 Range: NA	No distinctive repetitive pattern of riffles and pools due to straightening activities	Mean: NA Range: NA	Mean: NA Range: NA
9 Maximum Pool Depth (D_{pool})	Mean: 1.7 Range: NA		Mean: NA Range: NA	Mean: NA Range: NA
10 Width of Floodprone Area (W_{fpa})	Mean: 44 Range: 38-50	Mean: 78 Range: 35 - 150	Mean: 5.8 Range: NA	Mean: 40 Range: NA
Dimension Ratios				
11 Entrenchment Ratio (W_{fpa}/W_{bkf})	Mean: 7.4 Range: 6.9-7.8	Mean: 5.9 Range: 2.5-12.1	Mean: 1.6 Range: NA	Mean: 7.8 Range: 6.5-9.1
12 Width/Depth Ratio W_{bkf}/D_{bkf})	Mean: 7.1 Range: 6.1-8.0	Mean: 30.1 Range: 23.3-40.0	Mean: 2.8 Range: NA	Mean: 6.3 Range: 3.6-8.9
13 Max. D_{riff}/D_{bkf} Ratio	Mean: 1.9 Range: 1.8-1.9	Mean: 1.7 Range: 1.3-2.0	Mean: 1.4 Range: NA	Mean: 1.7 Range: 1.6-1.7
14 Low Bank Height/ Max. D_{bkf} Ratio	Mean: 1.1 Range: 1.0-1.1	Mean: 1.3 Range: 1.0-2.0	Mean: 1.9 Range: NA	Mean: 1.9 Range: 1.5-2.3
15 Pool Depth/Bankfull Mean Depth (D_{pool}/D_{bkf})	Mean: 1.1 Range: NA	No distinctive repetitive pattern of riffles and pools due to straightening activities	Mean: NA Range: NA	Mean: NA Range: NA
16 Pool width/Bankfull Width (W_{pool}/W_{bkf})	Mean: 0.7 Range: NA		Mean: NA Range: NA	Mean: NA Range: NA
17 Pool Area/Bankfull Cross Sectional Area	Mean: 0.8 Range: NA		Mean: NA Range: NA	Mean: NA Range: NA
Pattern Variables (Feet)				
18 Pool to Pool Spacing (L_{p-p})	No distinctive repetitive pattern of riffles and pools due to straightening activities	No distinctive repetitive pattern of riffles and pools due to straighting activities	No distinctive repetitive pattern of riffles and pools due to straightening activities	Mean: 41 Range: 23-63
19 Meander Length (L_m)				Mean: 70 Range: 40-106
20 Belt Width (W_{belt})	Mean: 8 Range: 6-20		Mean: 21 Range: 18-22	Mean: 21 Range: 10-41
21 Radius of Curvature (R_c)	No distinctive repetitive pattern of riffles and pools		No distinctive repetitive pattern of riffles and pools	Mean: 35 Range: 13-70
22 Sinuosity (Sin)	1.05	1.01	1.09	1.17
Pattern Ratios				
23 Pool to Pool Spacing/ Bankfull Width (L_{p-p}/W_{bkf})	No distinctive repetitive pattern of riffles and pools due to straightening activities	No distinctive repetitive pattern of riffles and pools due to straightening activities	No distinctive repetitive pattern of riffles and pools due to straightening activities	Mean: 7.7 Range: 4.3-11.9
24 Meander Length/ Bankfull Width (L_m/W_{bkf})				Mean: 13.1 Range: 7.5-20
25 Meander Width Ratio (W_{belt}/W_{bkf})	Mean: 1.3 Range: 1.0-3.3		Mean: 5.7 Range: 4.9-5.9	Mean: 3.9 Range: 1.9-7.7
26 Radius of Curvature/ Bankfull Width (Rc/W_{bkf})	No distinctive repetitive pattern of riffles and pools		No distinctive repetitive pattern of riffles and pools	Mean: 6.6 Range: 2.5-13.2
Profile Variables (Feet/Feet)				
27 Average Water Surface Slope (S_{ave})	0.0228	0.0019	Not Measured	Not Measured
28 Valley Slope (S_{valley})	0.0239	0.0019	Not Measured	Not Measured
29 Riffle Slope (S_{riffle})	Mean: 0.0360 Range: 0.0036 - 0.0960	No distinctive repetitive pattern of riffles and pools due to straighting activities	Mean: N/A Range: N/A	Mean: N/A Range: N/A
30 Pool Slope (S_{pool})	Mean: 0.0031 Range: 0.0000 - 0.0161		Mean: N/A Range: N/A	Mean: N/A Range: N/A
Profile Ratios				
31 Riffle Slope/ Water Surface Slope (S_{riffle}/S_{ave})	Mean: 1.6 Range: 0.16 - 4.2	No distinctive repetitive pattern of riffles and pools due to straighting activities	Mean: N/A Range: N/A	Mean: N/A Range: N/A
32 Pool Slope/Water Surface Slope (S_{pool}/S_{ave})	Mean: 0.13 Range: 0 - 0.71		Mean: N/A Range: N/A	Mean: N/A Range: N/A
Materials (Millimeters)				
D16	N/A	N/A	Not Measured	Not Measured
D35	N/A	N/A	Not Measured	Not Measured
D50	N/A	N/A	Not Measured	Not Measured
D84	9	N/A	Not Measured	Not Measured
D95	15	N/A	Not Measured	Not Measured

TABLE 3
BISHOP STREAM RESTORATION SITE
Morphological Characteristics of Reference Channels

Variables	Reference		
	UT to Crane Creek (E4/5)	Camp Branch (E4)	UT to Reedy Creek (E5/4)
1 Stream Type	E	E	E
2 Drainage Area (mi^2)	1.5	2.4	0.4
3 Bankfull Discharge (cfs)	119	168	44
Dimension Variables (Feet)			
4 Bankfull Cross Sectional Area (A_{bkf})	20.5	38.7	15.5
5 Bankfull Width (W_{bkf})	Mean: 10.1 Range: 9.5 - 11.9	Mean: 19.6 Range: 16.5-21.3	Mean: 10.4 Range: 9.6 - 11.2
6 Bankfull Mean Depth (D_{bkf})	Mean: 2.0 Range: 1.9 - 2.1	Mean: 2.0 Range: 1.8-2.2	Mean: 1.4 Range: 1.2 - 1.6
7 Bankfull Maximum Depth (D_{max})	Mean: 2.6 Range: 2.5 - 2.9	Mean: 2.6 Range: 2.4-2.7	Mean: 2.2 Range: 1.8 - 2.2
8 Pool Width (W_{pool})	Mean: 11.1 Range: 10.5 - 11.7	Mean: 23.6 Range: NA	Mean: 14.2 Range: 13.7 - 14.7
9 Maximum Pool Depth (D_{pool})	Mean: 2.9 Range: 2.8 - 3.0	Mean: 4.3 Range: NA	Mean: 2.3 Range: 2.2 - 2.3
10 Width of Floodprone Area (W_{fpa})	Mean: 237 Range: 232 - 345	Mean: 110 Range: 75-180	Mean: 58 Range: 42 - 71
Dimension Ratios			
11 Entrenchment Ratio (W_{fpa}/W_{bkf})	Mean: 25.0 Range: 20 - 34.5	Mean: 6.6 Range: 3.8-8.5	Mean: 5.6 Range: 3.7 - 7.4
12 Width/Depth Ratio W_{bkf}/D_{bkf})	Mean: 5.1 Range: 4.5 - 5.7	Mean: 9.9 Range: 7.5-11.8	Mean: 7.8 Range: 6.4 - 8.1
13 Max. D_{riff}/D_{bkf} Ratio	Mean: 1.3 Range: 1.2 - 1.4	Mean: 1.2 Range: 1.2-1.5	Mean: 1.5 Range: 1.4 - 1.6
14 Low Bank Height/ Max. D_{bkf} Ratio	Mean: 1.2 Range: 1.1 - 1.2	Mean: 1.2 Range: 1.0-1.3	Mean: 1.0 Range: 1.0-1.2
15 Pool Depth/Bankfull Mean Depth (D_{pool}/D_{bkf})	Mean: 1.5 Range: 1.4 - 1.5	Mean: 2.2 Range: NA	Mean: 1.6 Range: NA
16 Pool width/Bankfull Width (W_{pool}/W_{bkf})	Mean: 1.1 Range: 1.0 - 1.2	Mean: 1.2 Range: NA	Mean: 1.4 Range: 1.3 - 1.4
17 Pool Area/Bankfull Cross Sectional Area	Mean: 1.0 Range: NA	Mean: 1.4 Range: NA	Mean: 1.2 Range: 1.1 - 1.2
Pattern Variables (Feet)			
18 Pool to Pool Spacing (L_{p-p})	Mean: 53 Range: 26 - 114	Mean: 74 Range: 45-145	Mean: 84 Range: 13 - 112
19 Meander Length (L_m)	Mean: 73 Range: 61 - 115	Mean: 133 Range: 66-240	Mean: 102 Range: 81 - 137
20 Belt Width (W_{belt})	Mean: 86 Range: 74 - 101	Mean: 43 Range: 30-97	Mean: 76 Range: 68 - 84
21 Radius of Curvature (R_c)	Mean: 25.3 Range: 18.6 - 30.4	Mean: 41 Range: 17-200	Mean: 27.6 Range: 17.1 - 42
22 Sinuosity (Sin)	1.8	1.18	1.55
Pattern Ratios			
23 Pool to Pool Spacing/ Bankfull Width (L_{p-p}/W_{bkf})	Mean: 5.2 Range: 2.6 - 11.3	Mean: 3.8 Range: 2.3-7.4	Mean: 8.1 Range: 1.3 - 10.8
24 Meander Length/ Bankfull Width (L_m/W_{bkf})	Mean: 7.2 Range: 6.0 - 11.4	Mean: 6.8 Range: 3.4-12.2	Mean: 9.8 Range: 7.8 - 13.2
25 Meander Width Ratio (W_{belt}/W_{bkf})	Mean: 8.5 Range: 7.4 - 10.0	Mean: 2.2 Range: 1.5-4.9	Mean: 7.3 Range: 6.5 - 8.1
26 Radius of Curvature/ Bankfull Width (Rc/W_{bkf})	Mean: 2.5 Range: 1.8 - 3.0	Mean: 2.1 Range: 0.9-10.2	Mean: 2.7 Range: 1.6 - 4.0
Profile Variables (Feet/Feet)			
27 Average Water Surface Slope (S_{ave})	0.0014	0.0029	0.0111
28 Valley Slope (S_{valley})	0.0025	0.0047	0.0172
29 Riffle Slope (S_{riffle})	Mean: 0.0019 Range: 0.0006 - 0.0033	Mean: 0.0070 Range: 0.0008 - 0.0167	Mean: 0.014 Range: 0.0105 - 0.0221
30 Pool Slope (S_{pool})	Mean: 0.0004 Range: 0.0000 - 0.0006	Mean: 0.0004 Range: 0.0000 - 0.0013	Mean: 0.0069 Range: 0.0016 - 0.0182
Profile Ratios			
31 Riffle Slope/ Water Surface Slope (S_{riffle}/S_{ave})	Mean: 1.4 Range: 0.4 - 2.4	Mean: 2.4 Range: 0.28 - 5.8	Mean: 1.3 Range: 0.9 - 2.0
32 Pool Slope/Water Surface Slope (S_{pool}/S_{ave})	Mean: 0.3 Range: 0 - 0.4	Mean: 0.06 Range: 0 - 0.18	Mean: 0.6 Range: 0.1 - 1.6
Materials (Millimeters)			
D16	N/A	0.6	0.092
D35	0.44	4.7	0.29
D50	1.9	7.2	0.5
D84	12	17	12
D95	36	30	85

TABLE 6A
BISHOP STREAM RESTORATION SITE
Morphological Characteristics of Reference and Proposed Channels

Variables	Reference		Proposed		
	UT to Crane Creek (E4/5)	Camp Branch (E)	Camp Branch (Reach 1 and 2) (C/E)	Camp Branch (Reach 3) (C/E)	UT Camp Branch (C/E)
1 Stream Type	E	E	C/E	C/E	C/E
2 Drainage Area (mi^2)	1.5	2.4	2.4	2.7	0.3
3 Bankfull Discharge (cfs)	119	168	168	182	37.3
Dimension Variables (Feet)					
4 Bankfull Cross Sectional Area (A_{bkf})	20.5	38.7	38.7	42	9.4
5 Bankfull Width (W_{bkf})	Mean: 10.1 Range: 9.5 - 11.9	Mean: 19.6 Range: 16.5-21.3	Mean: 21.5 Range: 17.6 - 24.9	Mean: 22.4 Range: 18.3 - 25.9	Mean: 10.6 Range: 8.7 - 12.3
6 Bankfull Mean Depth (D_{bkf})	Mean: 2.0 Range: 1.9 - 2.1	Mean: 2.0 Range: 1.8-2.2	Mean: 1.8 Range: 1.6 - 2.2	Mean: 1.9 Range: 1.6 - 2.3	Mean: 0.9 Range: 0.8 - 1.1
7 Bankfull Maximum Depth (D_{max})	Mean: 2.6 Range: 2.5 - 2.9	Mean: 2.6 Range: 2.4-2.7	Mean: 2.3 Range: 2.2 - 2.7	Mean: 2.5 Range: 2.3 - 2.9	Mean: 1.4 Range: 1.3 - 1.7
8 Pool Width (W_{pool})	Mean: 11.1 Range: 10.5 - 11.7	Mean: 23.6 Range: NA	Mean: 28 Range: 23.7 - 32.3	Mean: 29.1 Range: 24.6 - 33.6	Mean: 15.9 Range: 13.8 - 17.0
9 Maximum Pool Depth (D_{pool})	Mean: 2.9 Range: 2.8 - 3.0	Mean: 4.3 Range: NA	Mean: 3.2 Range: 2.5 - 4.0	Mean: 3.4 Range: 2.7 - 4.2	Mean: 1.6 Range: 1.3 - 2.0
10 Width of Floodprone Area (W_{fpa})	Mean: 237 Range: 232 - 345	Mean: 110 Range: 75-180	Mean: 110 Range: 75 - 180	Mean: 184 Range: 165 - 217	Mean: 90 Range: 30 - 110
Dimension Ratios					
11 Entrenchment Ratio (W_{fpa}/W_{bkf})	Mean: 25.0 Range: 20 - 34.5	Mean: 6.6 Range: 3.8-8.5	Mean: 5.1 Range: 4.4 - 6.3	Mean: 8.2 Range: 7.4 - 9.7	Mean: 8.3 Range: 7.3 - 10.3
12 Width/Depth Ratio W_{bkf}/D_{bkf}	Mean: 5.1 Range: 4.5 - 5.7	Mean: 9.9 Range: 7.5-11.8	Mean: 12 Range: 8 - 16	Mean: 12 Range: 8 - 16	Mean: 12 Range: 8 - 16
13 Max. D_{rift}/D_{bkf} Ratio	Mean: 1.3 Range: 1.2 - 1.4	Mean: 1.2 Range: 1.2-1.5	Mean: 1.3 Range: 1.2 - 1.5	Mean: 1.3 Range: 1.2 - 1.5	Mean: 1.5 Range: 1.4 - 1.7
14 Low Bank Height/ Max. D_{bkf} Ratio	Mean: 1.2 Range: 1.1 - 1.2	Mean: 1.2 Range: 1.0-1.3	Mean: 1.2 Range: 1.0 - 1.3	Mean: 1.2 Range: 1.0 - 1.3	Mean: 1.1 Range: 1.0 - 1.3
15 Pool Depth/Bankfull Mean Depth (D_{pool}/D_{bkf})	Mean: 1.5 Range: 1.4 - 1.5	Mean: 2.2 Range: NA	Mean: 1.8 Range: 1.4 - 2.2	Mean: 1.8 Range: 1.4 - 2.2	Mean: 1.8 Range: 1.4 - 2.2
16 Pool width/Bankfull Width (W_{pool}/W_{bkf})	Mean: 1.1 Range: 1.0 - 1.2	Mean: 1.2 Range: NA	Mean: 1.3 Range: 1.1 - 1.5	Mean: 1.3 Range: 1.1 - 1.5	Mean: 1.5 Range: 1.3 - 1.6
17 Pool Area/Bankfull Cross Sectional Area	Mean: 1.0 Range: ------	Mean: 1.4 Range: NA	Mean: 1.4 Range: 1.1 - 1.6	Mean: 1.4 Range: 1.1 - 1.6	Mean: 1.5 Range: 1.1 - 1.6
Pattern Variables (Feet)					
18 Pool to Pool Spacing (L_{p-p})	Mean: 53 Range: 26 - 114	Mean: 74 Range: 45-145	Mean: 95.8 Range: 63.9 - 213	Mean: 100 Range: 67.2 - 224	Mean: 42.4 Range: 15.9 - 95.4
19 Meander Length (L_m)	Mean: 73 Range: 61 - 115	Mean: 133 Range: 66-240	Mean: 150 Range: 128 - 256	Mean: 157 Range: 134 - 269	Mean: 63.6 Range: 25.4 - 116.6
20 Belt Width (W_{belt})	Mean: 86 Range: 74 - 101	Mean: 43 Range: 30-97	Mean: 85.2 Range: 42.6 - 213	Mean: 89.6 Range: 44.8 - 224	Mean: 42.4 Range: 21.2 - 74.2
21 Radius of Curvature (R_c)	Mean: 25.3 Range: 18.6 - 30.4	Mean: 41 Range: 17-200	Mean: 46.9 Range: 42.6 - 213	Mean: 49.3 Range: 44.8 - 224	Mean: 23.3 Range: 21.2 - 42.4
22 Sinuosity (Sin)	1.8	1.18	1.29	1.12	1.19
Pattern Ratios					
23 Pool to Pool Spacing/ Bankfull Width (L_{p-p}/W_{bkf})	Mean: 5.2 Range: 2.6 - 11.3	Mean: 3.8 Range: 2.3-7.4	Mean: 4.5 Range: 3 - 10	Mean: 4.5 Range: 3 - 10	Mean: 4.0 Range: 1.5 - 9
24 Meander Length/ Bankfull Width (L_m/W_{bkf})	Mean: 7.2 Range: 6.0 - 11.4	Mean: 6.8 Range: 3.4-12.2	Mean: 7 Range: 6 - 12	Mean: 7 Range: 6 - 12	Mean: 6 Range: 2.4 - 11
25 Meander Width Ratio (W_{belt}/W_{bkf})	Mean: 8.5 Range: 7.4 - 10.0	Mean: 2.2 Range: 1.5-4.9	Mean: 4 Range: 2 - 10	Mean: 4 Range: 2 - 10	Mean: 4 Range: 2 - 7
26 Radius of Curvature/ Bankfull Width (Rc/W_{bkf})	Mean: 2.5 Range: 1.8 - 3.0	Mean: 2.1 Range: 0.9-10.2	Mean: 2.2 Range: 2 - 10	Mean: 2.2 Range: 2 - 10	Mean: 2.2 Range: 2.0 - 4
Profile Variables (Feet/Feet)					
27 Average Water Surface Slope (S_{ave})	0.0014	0.0029	0.0031	0.0031	0.0110
28 Valley Slope (S_{valley})	0.0025	0.0047	0.0047	0.0047	0.0131
29 Riffle Slope (S_{riffle})	Mean: 0.0019 Range: 0.0006 - 0.0033	Mean: 0.0070 Range: 0.0008 - 0.0167	Mean: 0.005 Range: 0.0012 - 0.0068	Mean: 0.005 Range: 0.0012 - 0.0068	Mean: 0.017 Range: 0.0044 - 0.0242
30 Pool Slope (S_{pool})	Mean: 0.0004 Range: 0.0000 - 0.0006	Mean: 0.0004 Range: 0.0000 - 0.0013	Mean: 0.0012 Range: 0 - 0.0019	Mean: 0.0012 Range: 0 - 0.0019	Mean: 0.0044 Range: 0 - 0.0066
Profile Ratios					
31 Riffle Slope/ Water Surface Slope (S_{riffle}/S_{ave})	Mean: 1.4 Range: 0.4 - 2.4	Mean: 2.4 Range: 0.28 - 5.8	Mean: 1.6 Range: 0.4 - 2.2	Mean: 1.6 Range: 0.4 - 2.2	Mean: 1.6 Range: 0.4 - 2.2
32 Pool Slope/Water Surface Slope (S_{pool}/S_{ave})	Mean: 0.3 Range: 0 - 0.4	Mean: 0.06 Range: 0 - 0.18	Mean: 0.4 Range: 0 - 0.6	Mean: 0.4 Range: 0 - 0.6	Mean: 0.4 Range: 0 - 0.6
Materials (Millimeters)					
D16	N/A	0.6	NA	NA	NA
D35	0.44	4.7	NA	NA	NA
D50	1.9	7.2	1.5 - 16	1.5 - 16	0.125 - 2.0
D84	12	17	NA	NA	NA
D95	36	30	NA	NA	NA

TABLE 6B
BISHOP STREAM RESTORATION SITE
Morphological Characteristics of Reference and Proposed Channels

Variables	Reference	Proposed		
	UT to Reedy Creek (E5/4)	Dula Thoroughfare (E/C 5/6)	Dula Thoroughfare (D/6)	UT Dula Thoroughfare (E/C 4/5)
1 Stream Type	E	E/C	D	E/C
2 Drainage Area (mi^2)	0.4	0.16	0.18	0.11
3 Bankfull Discharge (cfs)	44	23	25	18.1
Dimension Variables (Feet)				
4 Bankfull Cross Sectional Area (A_{bkf})	15.5	6.2	6.4	4.7
5 Bankfull Width (W_{bkf})	Mean: 10.4 Range: 9.6 - 11.2	Mean: 8.6 Range: 7 - 10	Braided Channel System	Mean: 7.5 Range: 6.1 - 8.7
6 Bankfull Mean Depth (D_{bkf})	Mean: 1.4 Range: 1.2 - 1.6	Mean: 0.7 Range: 0.6 - 0.9		Mean: 0.6 Range: 0.5 - 0.8
7 Bankfull Maximum Depth (D_{max})	Mean: 2.2 Range: 1.8 - 2.2	Mean: 1.0 Range: 0.8 - 1.1		Mean: 0.8 Range: 0.7 - 1.0
8 Pool Width (W_{pool})	Mean: 14.2 Range: 13.7 - 14.7	Mean: 12.0 Range: 10.3 - 12.9		Mean: 10.5 Range: 10 - 12
9 Maximum Pool Depth (D_{pool})	Mean: 2.3 Range: 2.2 - 2.3	Mean: 1.1 Range: 1.0 - 1.2		Mean: 0.9 Range: 0.8 - 1.0
10 Width of Floodprone Area (W_{fpa})	Mean: 58 Range: 42 - 71	Mean: 61 Range: 35 - 90		Mean: 62 Range: 45 - 85
Dimension Ratios				
11 Entrenchment Ratio (W_{fpa}/W_{bkf})	Mean: 5.6 Range: 3.7 - 7.4	Mean: 7.1 Range: 4.1 - 10.5	Braided Channel System	Mean: 8.3 Range: 6 - 11.3
12 Width/Depth Ratio W_{bkf}/D_{bkf})	Mean: 7.8 Range: 6.4 - 8.1	Mean: 12 Range: 8 - 16		Mean: 12 Range: 8 - 10
13 Max. D_{riff}/D_{bkf} Ratio	Mean: 1.5 Range: 1.4 - 1.6	Mean: 1.4 Range: 1.2 - 1.6		Mean: 1.4 Range: 1.2 - 1.6
14 Low Bank Height/ Max. D_{bkf} Ratio	Mean: 1.0 Range: 1.0-1.2	Mean: 1.1 Range: 1.0 - 1.3		Mean: 1.1 Range: 1.0 - 1.3
15 Pool Depth/Bankfull Mean Depth (D_{pool}/D_{bkf})	Mean: 1.6 Range: ------	Mean: 1.5 Range: 1.4 - 1.6		Mean: 1.5 Range: 1.4 - 1.6
16 Pool width/Bankfull Width (W_{pool}/W_{bkf})	Mean: 1.4 Range: 1.3 - 1.4	Mean: 1.4 Range: 1.2 - 1.5		Mean: 1.4 Range: 1.3 - 1.6
17 Pool Area/Bankfull Cross Sectional Area	Mean: 1.2 Range: 1.1 - 1.2	Mean: 1.2 Range: 1.1 - 1.4		Mean: 1.4 Range: 1.3 - 1.6
Pattern Variables (Feet)				
18 Pool to Pool Spacing (L_{p-p})	Mean: 84 Range: 13 - 112	Mean: 43.9 Range: 22.4 - 68.8	Braided Channel System	Mean: 37.5 Range: 15 - 60
19 Meander Length (L_m)	Mean: 102 Range: 81 - 137	Mean: 68.8 Range: 51.6 - 94.6		Mean: 52.5 Range: 22.5 - 82.5
20 Belt Width (W_{belt})	Mean: 76 Range: 68 - 84	Mean: 60.2 Range: 55.9 - 86		Mean: 22.5 Range: 12.8 - 37.5
21 Radius of Curvature (R_c)	Mean: 27.6 Range: 17.1 - 42	Mean: 18.9 Range: 17.2 - 34.3		Mean: 16.5 Range: 15 - 33.8
22 Sinuosity (Sin)	1.55	1.16	1	1.17
Pattern Ratios				
23 Pool to Pool Spacing/ Bankfull Width (L_{p-p}/W_{bkf})	Mean: 8.1 Range: 1.3 - 10.8	Mean: 5.1 Range: 2.6 - 8	Braided Channel System	Mean: 5 Range: 2 - 8
24 Meander Length/ Bankfull Width (L_m/W_{bkf})	Mean: 9.8 Range: 7.8 - 13.2	Mean: 8 Range: 6 - 11		Mean: 7 Range: 3 - 11
25 Meander Width Ratio (W_{belt}/W_{bkf})	Mean: 7.3 Range: 6.5 - 8.1	Mean: 7 Range: 6.5 - 10		Mean: 3 Range: 1.7 - 5
26 Radius of Curvature/ Bankfull Width (Rc/W_{bkf})	Mean: 2.7 Range: 1.6 - 4.0	Mean: 2.2 Range: 2.0 - 4.0		Mean: 2.2 Range: 2.0 - 4.5
Profile Variables (Feet/Feet)				
27 Average Water Surface Slope (S_{ave})	0.0111	0.0070	0.0019	At Grade
28 Valley Slope (S_{valley})	0.0172	0.0044	0.0019	At Grade
29 Riffle Slope (S_{riffle})	Mean: 0.014 Range: 0.0105 - 0.0221	Mean: 0.0098 Range: 0.007 - 0.0154	Braided Channel System	Mean: NA Range: NA
30 Pool Slope (S_{pool})	Mean: 0.0069 Range: 0.0016 - 0.0182	Mean: 0.0028 Range: 0 - 0.0014		Mean: NA Range: NA
Profile Ratios				
31 Riffle Slope/ Water Surface Slope (S_{riffle}/S_{ave})	Mean: 1.3 Range: 0.9 - 2.0	Mean: 1.4 Range: 1.0 - 2.2	Braided Channel System	Mean: NA Range: NA
32 Pool Slope/Water Surface Slope (S_{pool}/S_{ave})	Mean: 0.6 Range: 0.1 - 1.6	Mean: 0.4 Range: 0 - 0.2		Mean: NA Range: NA
Materials (Millimeters)				
D16	0.092	NA	NA	NA
D35	0.29	NA	NA	NA
D50	0.5	0.125 - 2.0	0.125 - 2.0	0.25 - 4.0
D84	12	NA	NA	NA
D95	85	NA	NA	NA

Table 4A

Reference Forest Plot Summary
Bottomland Hardwood Forest (Canopy Species)
UT to Crane Creek Floodplain

Tree Species	Number of Individuals[1]	Relative Density (%)	Frequency[1] (%)	Relative Frequency (%)	Basal Area (ft^2 / acre)	Relative Basal Area (%)	Importance Value
Acer negundo	3	7.9	67	8.7	2.3	5.9	0.07
Acer rubrum	3	7.9	67	8.7	4.2	10.6	0.09
Carya ovata	5	13.2	67	8.7	2.5	6.3	0.09
Cary tomentosa	1	2.6	33	4.3	0.1	0.2	0.02
Fagus grandiflora	1	2.6	33	4.3	2.0	5.2	0.04
Fraxinus americana	1	2.6	33	4.3	1.3	3.3	0.03
Fraxinus pennsylvanica	6	15.8	100	13.0	3.5	8.8	0.13
Juniperus virginica	1	2.6	33	4.3	0.4	0.9	0.03
Liquidambar styraciflua	1	2.6	33	4.3	0.1	0.3	0.02
Liriodendron tulipifera	3	7.9	67	8.7	2.7	6.7	0.08
Nyssa sylvatica	1	2.6	33	4.3	0.1	0.2	0.02
Quercus falcata	1	2.6	33	4.3	2.9	7.3	0.05
Quercus michauxii	3	7.9	67	8.7	13.3	33.6	0.17
Quercus phellos	2	5.3	33	4.3	2.3	5.8	0.05
Ulmus americana	6	15.8	67	8.7	1.9	4.9	0.10
TOTALS	38	100	767	100	40	100	1

[1] Summary of three 0.1-acre plots

Table 4B

Reference Forest Plot Summary
Bottomland Hardwood Forest (Canopy Species)
UT to Reedy Creek Floodplain

Tree Species	Number of Individuals[1]	Relative Density (%)	Frequency[1] (%)	Relative Frequency (%)	Basal Area (ft^2 / acre)	Relative Basal Area (%)	Importance Value
Acer negundo	6	7.8	50	5.3	1.9	2.6	0.05
Acer rubrum	2	2.6	50	5.3	0.6	0.8	0.03
Carpinus caroliniana	7	9.1	50	5.3	1.2	1.7	0.05
Carya ovata	2	2.6	50	5.3	5.4	7.3	0.05
Celtis laevigata	6	7.8	50	5.3	3.1	4.2	0.06
Fagus grandiflora	2	2.6	50	5.3	6.5	8.8	0.06
Fraxinus pennsylvanica	1	1.3	25	2.6	0.4	0.5	0.01
Juglans nigra	4	5.2	75	7.9	5.2	7.0	0.07
Liquidambar styraciflua	7	9.1	75	7.9	6.6	8.9	0.09
Liriodendron tulipifera	5	6.5	75	7.9	15.9	21.5	0.12
Morus rubra	8	10.4	75	7.9	4.0	5.4	0.08
Nyssa sylvatica	3	3.9	75	7.9	3.0	4.0	0.05
Platanus occidentalis	2	2.6	25	2.6	6.5	8.8	0.05
Quercus alba	2	2.6	25	2.6	1.7	2.2	0.02
Quercus michauxii	1	1.3	25	2.6	0.5	0.7	0.02
Quercus phellos	1	1.3	25	2.6	1.6	2.2	0.02
Quercus rubra	7	9.1	50	5.3	7.2	9.8	0.08
Ulmus americana	11	14.3	100	10.5	3.0	4.0	0.10
TOTALS	77	100	950	100	74	100	1

[1] Summary of four 0.1-acre plots

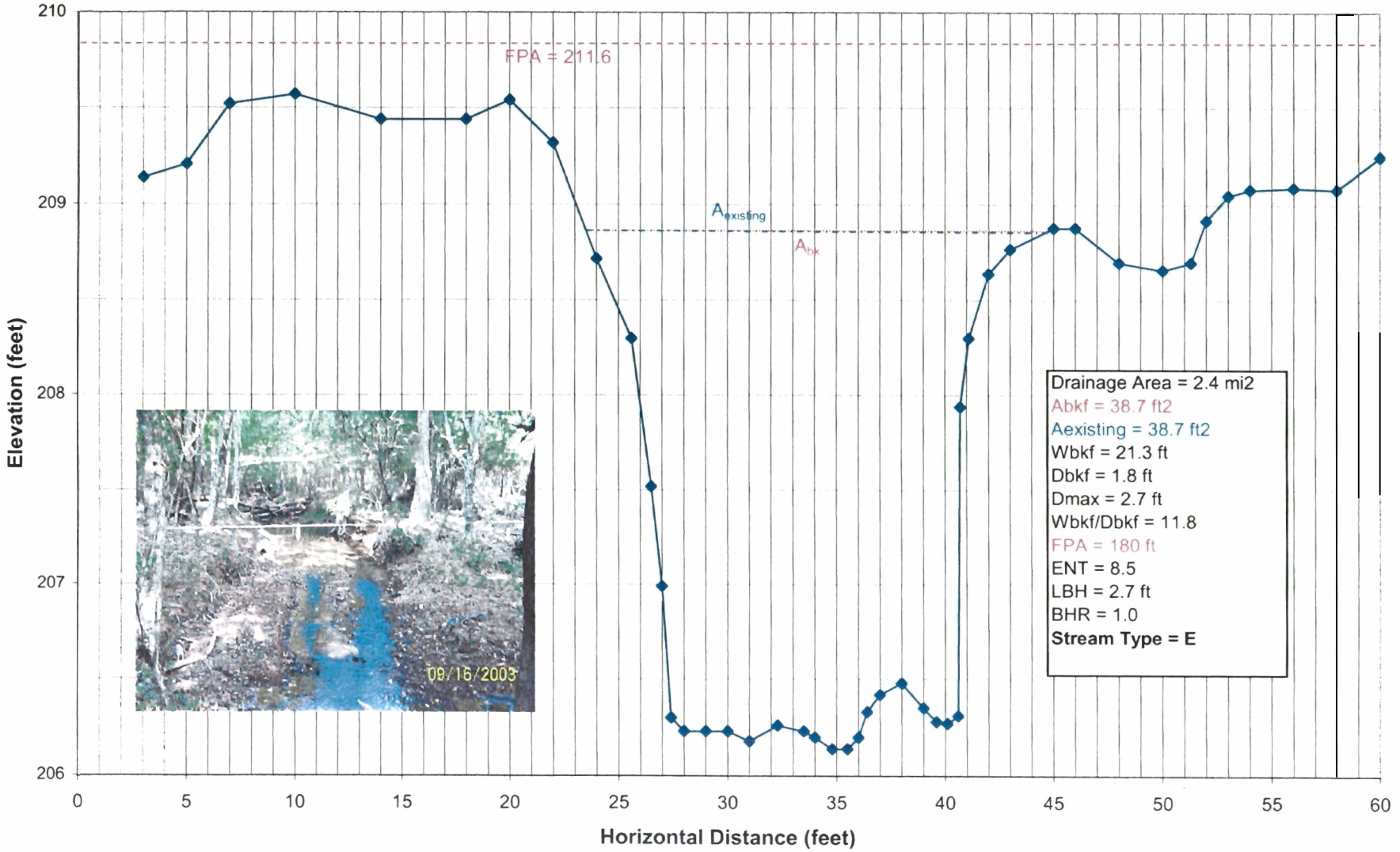
APPENDIX C

EXISTING STREAM DATA

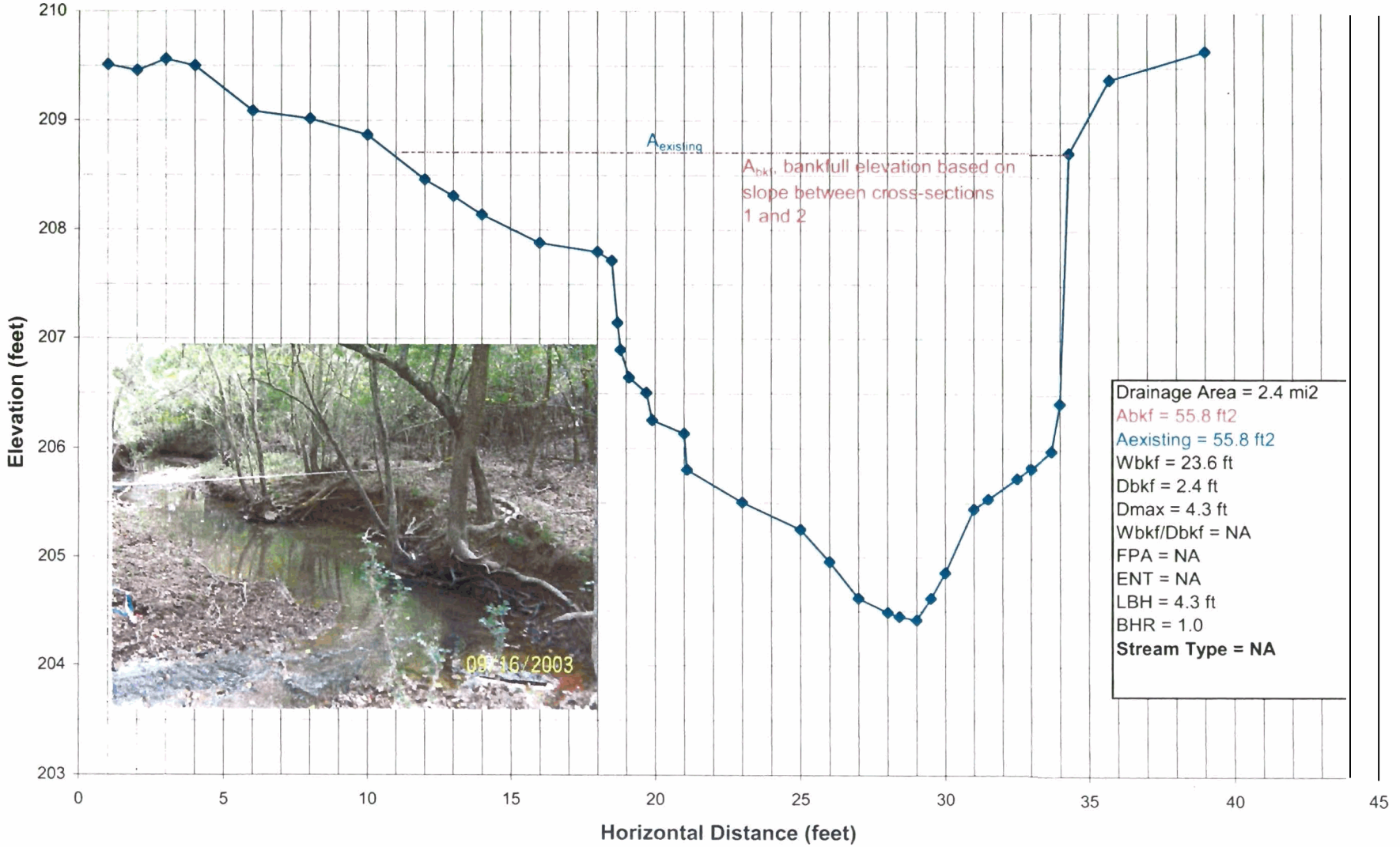
Bishop Property On-Site Dimension: Camp Branch Area

	X-sect	DA (mi^2)	A_{bkf} (ft^2)	$A_{existing}$ (ft^2)	W_{bkf} (ft)	D_{ave} (ft)	D_{max} (ft)	W/D Ratio	FPA	Entrench	LBH (ft)	BHR	Stream Type
	Camp Branch Reach 1 (Upstream of Headcut)												
Riffles	1	2.4	38.7	38.7	21.3	1.8	2.7	11.8	180	8.5	2.7	1	E
	3		38.7	52.8	19.6	2	2.4	9.9	75	3.8	3.1	1.3	
	5		36	44.1	16.5	2.2	2.6	7.5	110	6.6	3.1	1.2	
	average	**2.4**	**37.8**	**45.2**	**19.1**	**2.0**	**2.6**	**9.7**	**121.7**	**6.3**	**3.0**	**1.2**	
	min	**2.4**	**36.0**	**38.7**	**16.5**	**1.8**	**2.4**	**7.5**	**75.0**	**3.8**	**2.7**	**1.0**	
	max	**2.4**	**38.7**	**52.8**	**21.3**	**2.2**	**2.7**	**11.8**	**180.0**	**8.5**	**3.1**	**1.3**	
Pools	2	2.4	55.8	55.8	23.6	2.4	4.3	---	---	---	4.3	1	---
	Camp Branch Reach 2 (Headcut to Ford)												
Riffles	4	2.4	38.7	62.2	18.3	2.1	2.7	8.7	100	5.5	4	1.5	E
Pools	6	2.4	29.2	51.4	12.9	2.3	3.2	---	---	---	4.8	1.5	---
	Camp Branch Reach 3 (Downstream of Ford)												
Riffles	8	2.7	42	104.1	16	2.6	3	6.2	17.2	1.1	6.7	2.2	G
	9	2.7	42	124.3	19.5	2.2	2.5	8.9	24.3	1.2	6.1	2.4	G
	average	**2.7**	**42**	**114.2**	**17.75**	**2.4**	**2.75**	**7.55**	**20.75**	**1.15**	**6.4**	**2.3**	
	min	**2.7**	**42**	**104.1**	**16**	**2.2**	**2.5**	**6.2**	**17.2**	**1.1**	**6.1**	**2.2**	
	max	**2.7**	**42**	**124.3**	**19.5**	**2.6**	**3**	**8.9**	**24.3**	**1.2**	**6.7**	**2.4**	
Pools	10	2.7	57.8	130.2	19.4	3	4.1	---	---	---	7.4	1.8	---
	7	2.7	38.4	89.2	13.4	2.9	3.3	---	---	---	6.8	2.1	---
	average	**2.7**	**48.1**	**109.7**	**16.4**	**2.95**	**3.7**	**---**	**---**	**---**	**7.1**	**1.95**	
	min	**2.7**	**38.4**	**89.2**	**13.4**	**2.9**	**3.3**	**---**	**---**	**---**	**6.8**	**1.8**	
	max	**2.7**	**57.8**	**130.2**	**19.4**	**3**	**4.1**	**---**	**---**	**---**	**7.4**	**2.1**	
	Unnamed Tributary to Camp Branch												
Riffles	1	0.3	9.2	9.2	15.7	0.6	1.4	26.17	100	6.4	1.4	1	C
	2	0.3	9.4	13.3	6	1.6	2.7	3.75	100	16.6	1.5	1.07	E
	average	**0.3**	**9.3**	**11.25**	**10.85**	**1.1**	**2.05**	**14.96**	**100**	**11.5**	**1.45**	**1.04**	
	min	**0.3**	**9.2**	**9.2**	**6**	**0.6**	**1.4**	**3.75**	**100**	**6.4**	**1.4**	**1**	
	max	**0.3**	**9.4**	**13.3**	**15.7**	**1.6**	**2.7**	**26.17**	**100**	**16.6**	**1.5**	**1.07**	

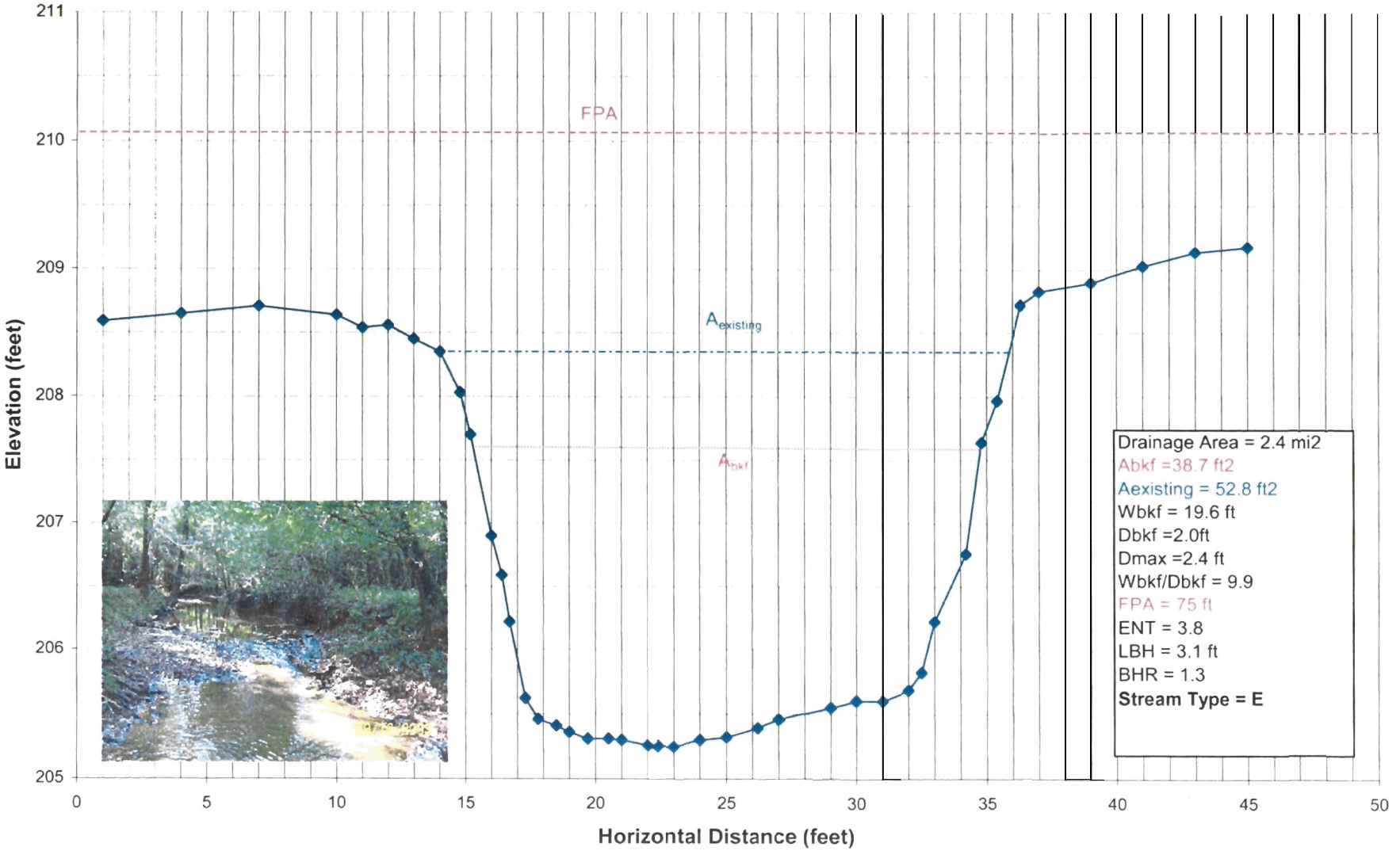
Cross-section 1: riffle, Camp Branch



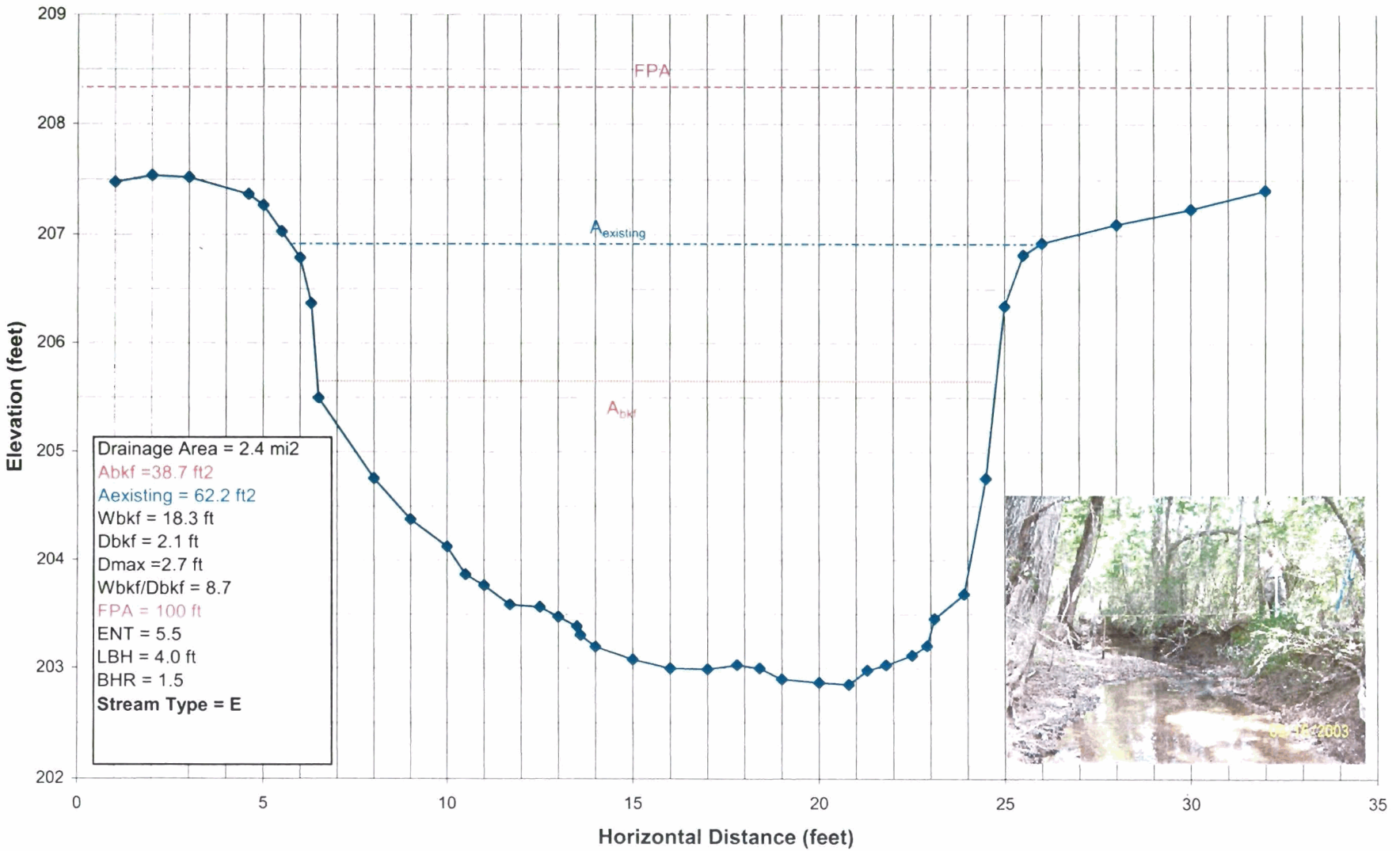
Cross-section 2: pool, Camp Branch



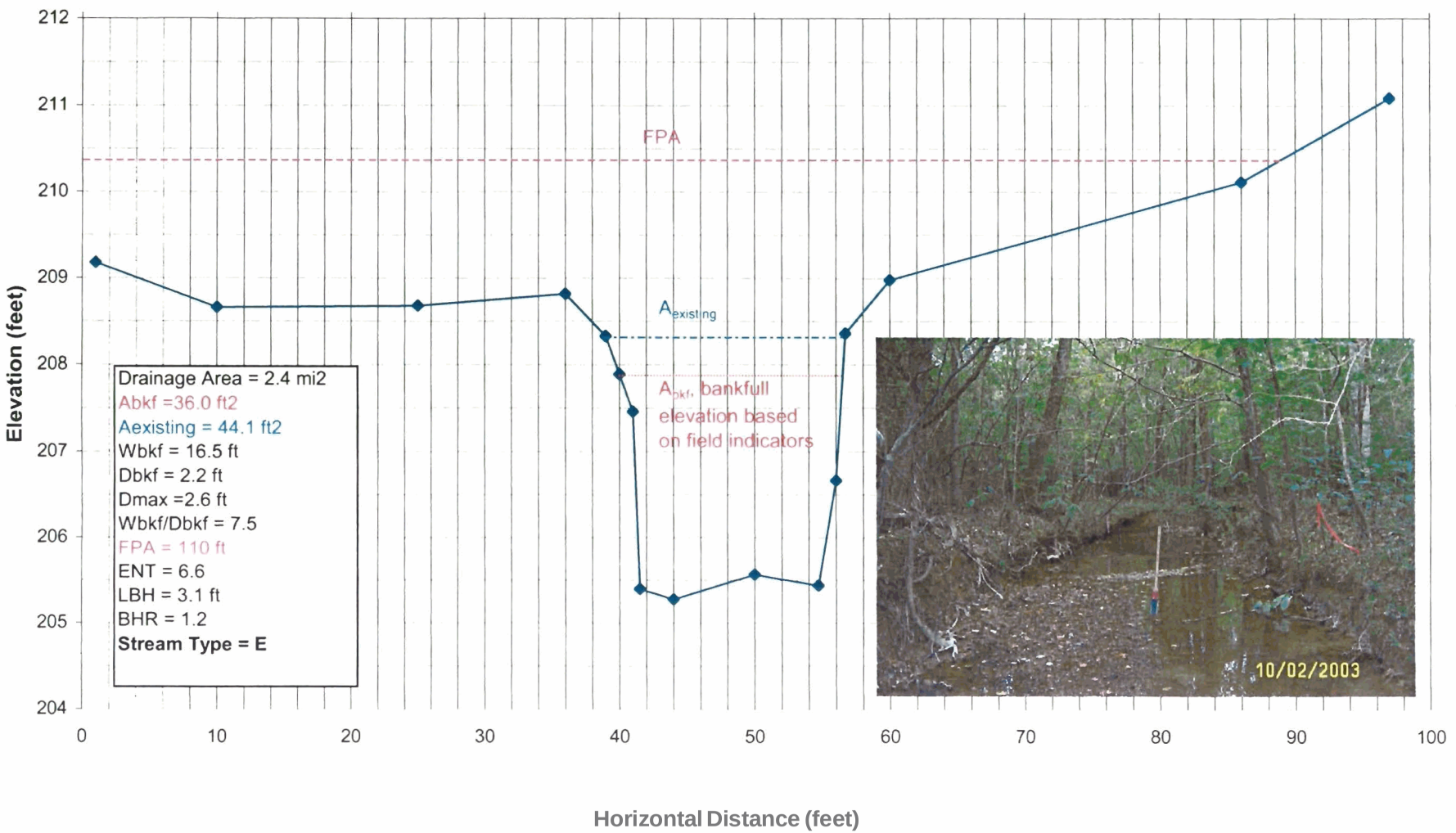
Cross-section 3: riffle, Camp Branch



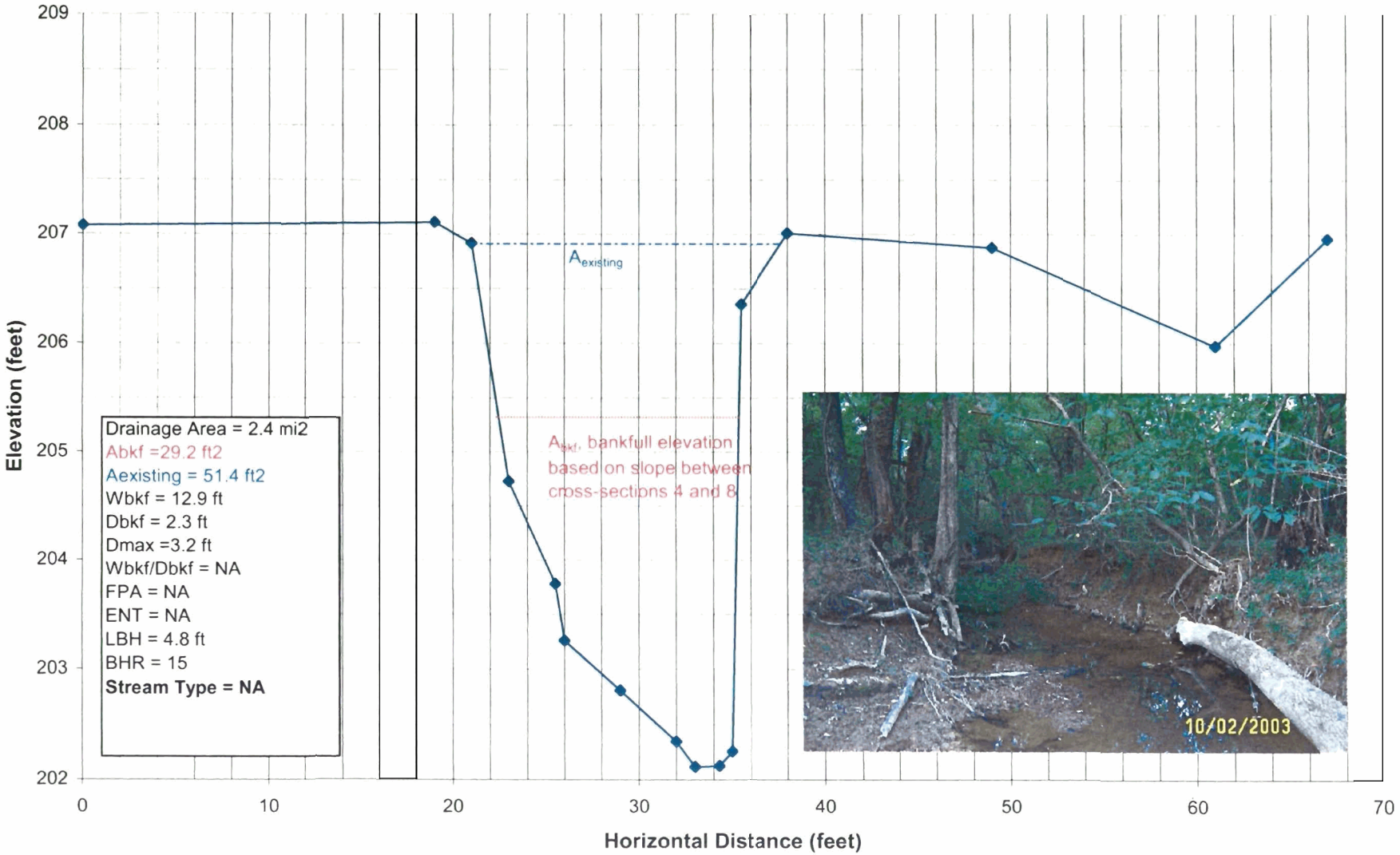
Cross-section 4: riffle, Camp Branch



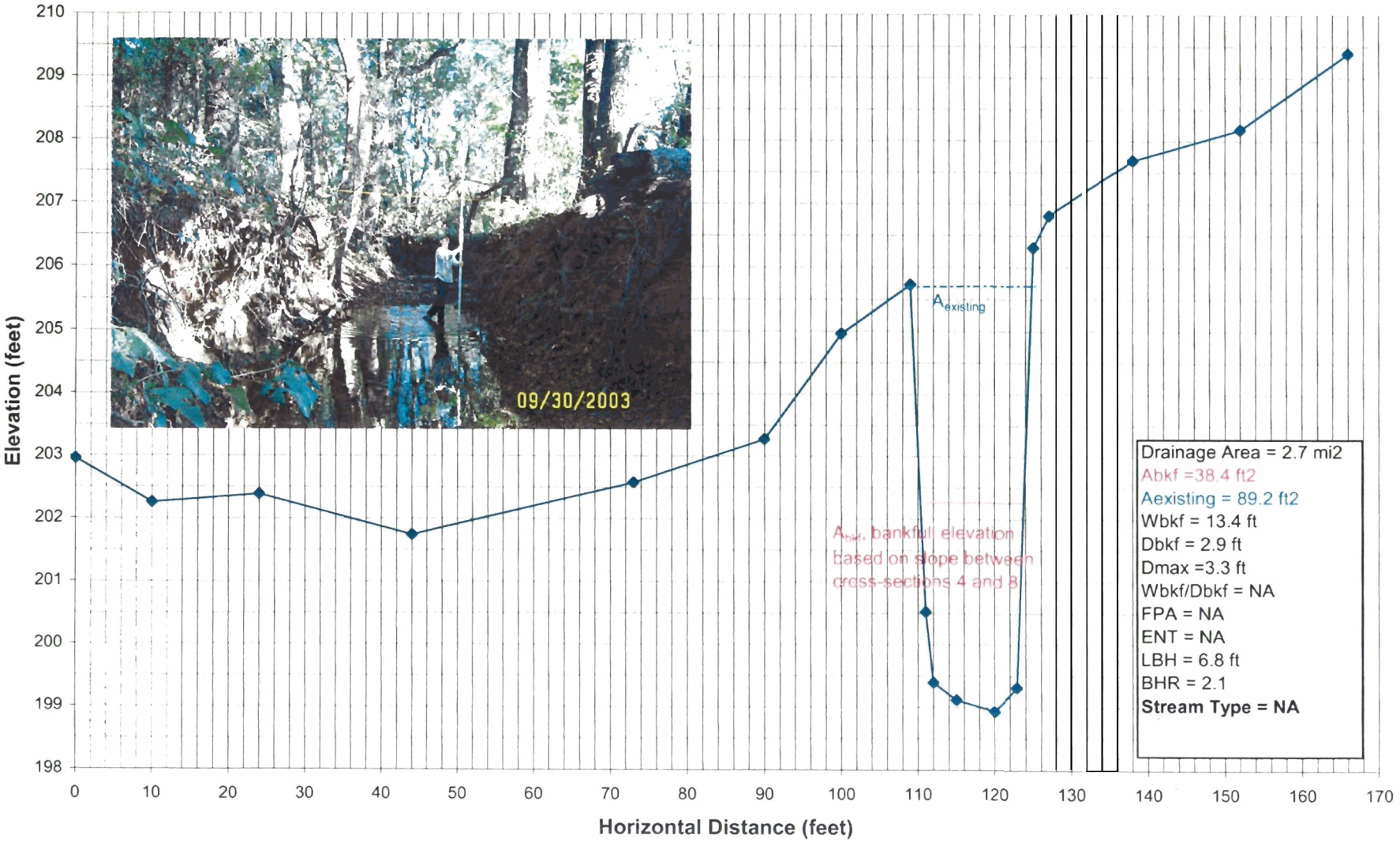
Cross-section 5: riffle, Camp Branch



Cross-section 6: pool, Camp Branch

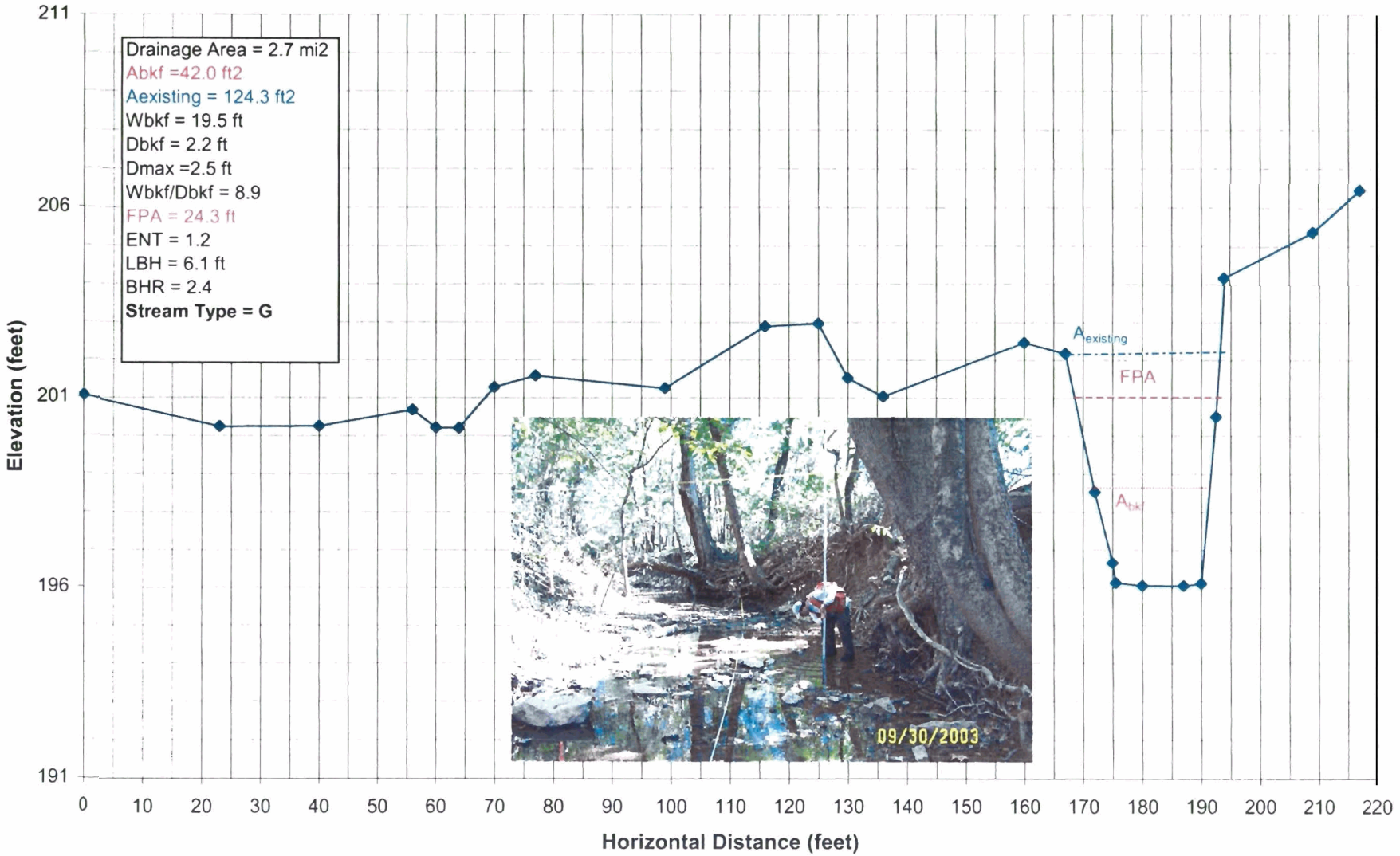


Cross-section 7: pool, Camp Branch

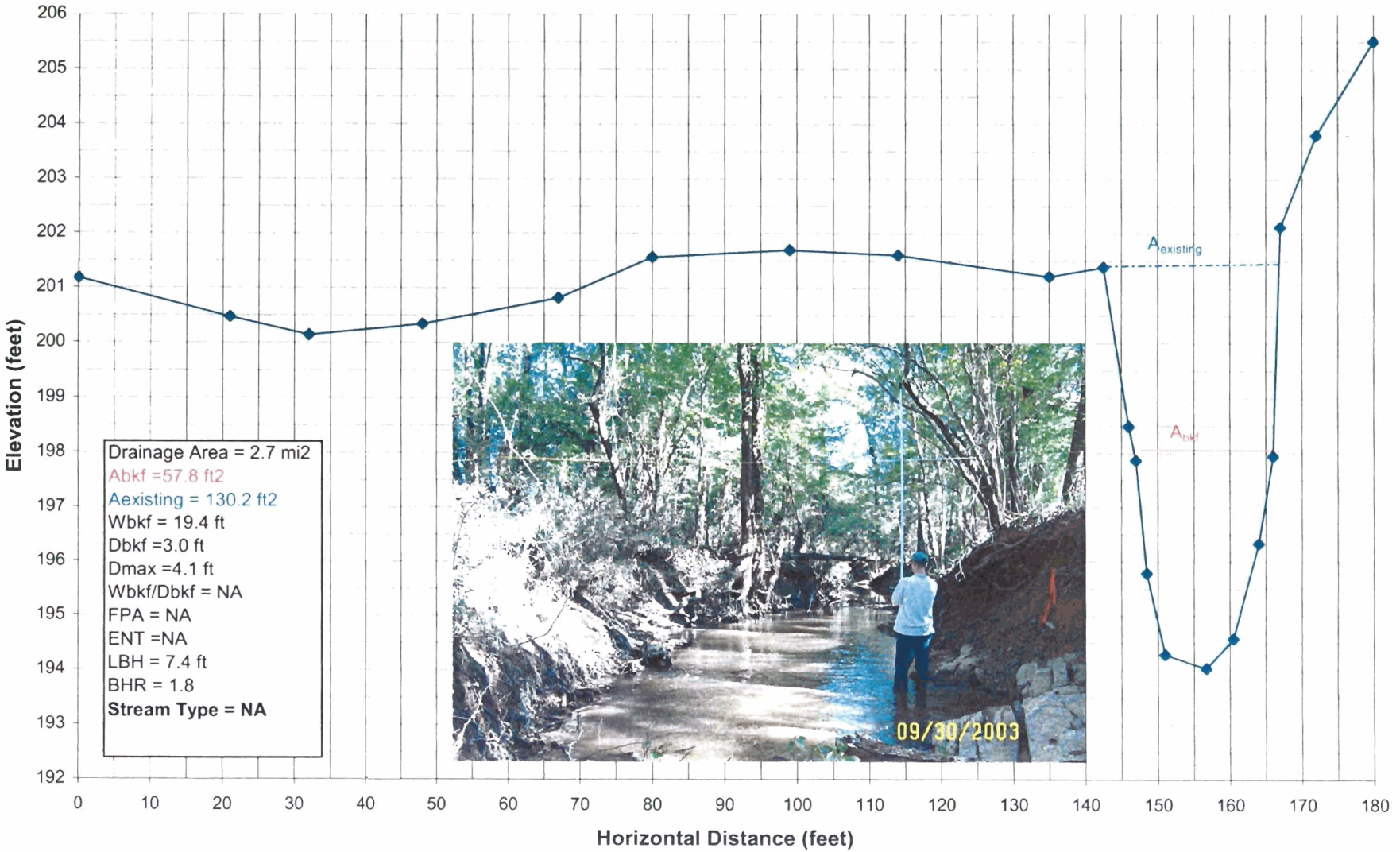


Cross-section 8: riffle, Camp Branch

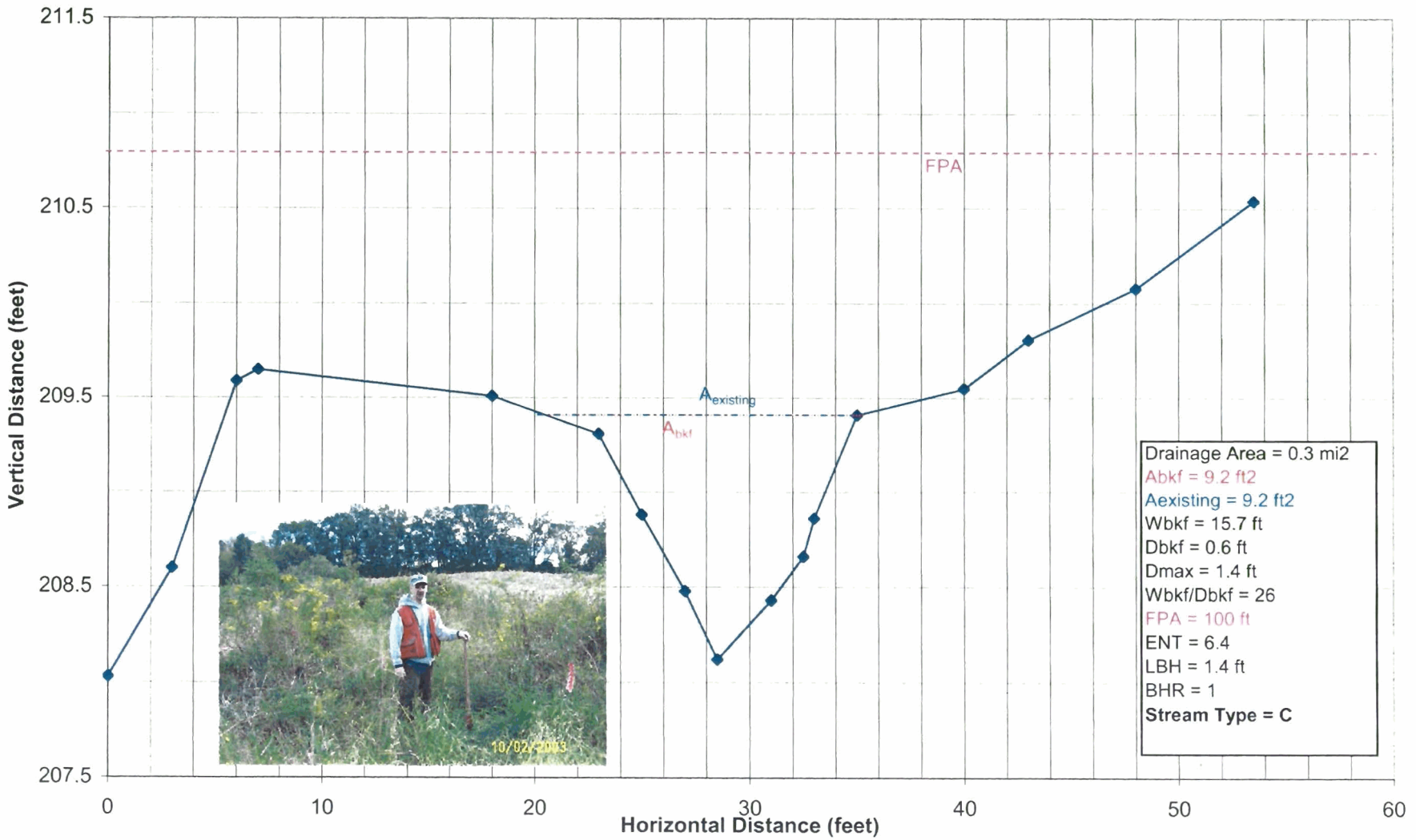
Cross-section 9: riffle, Camp Branch



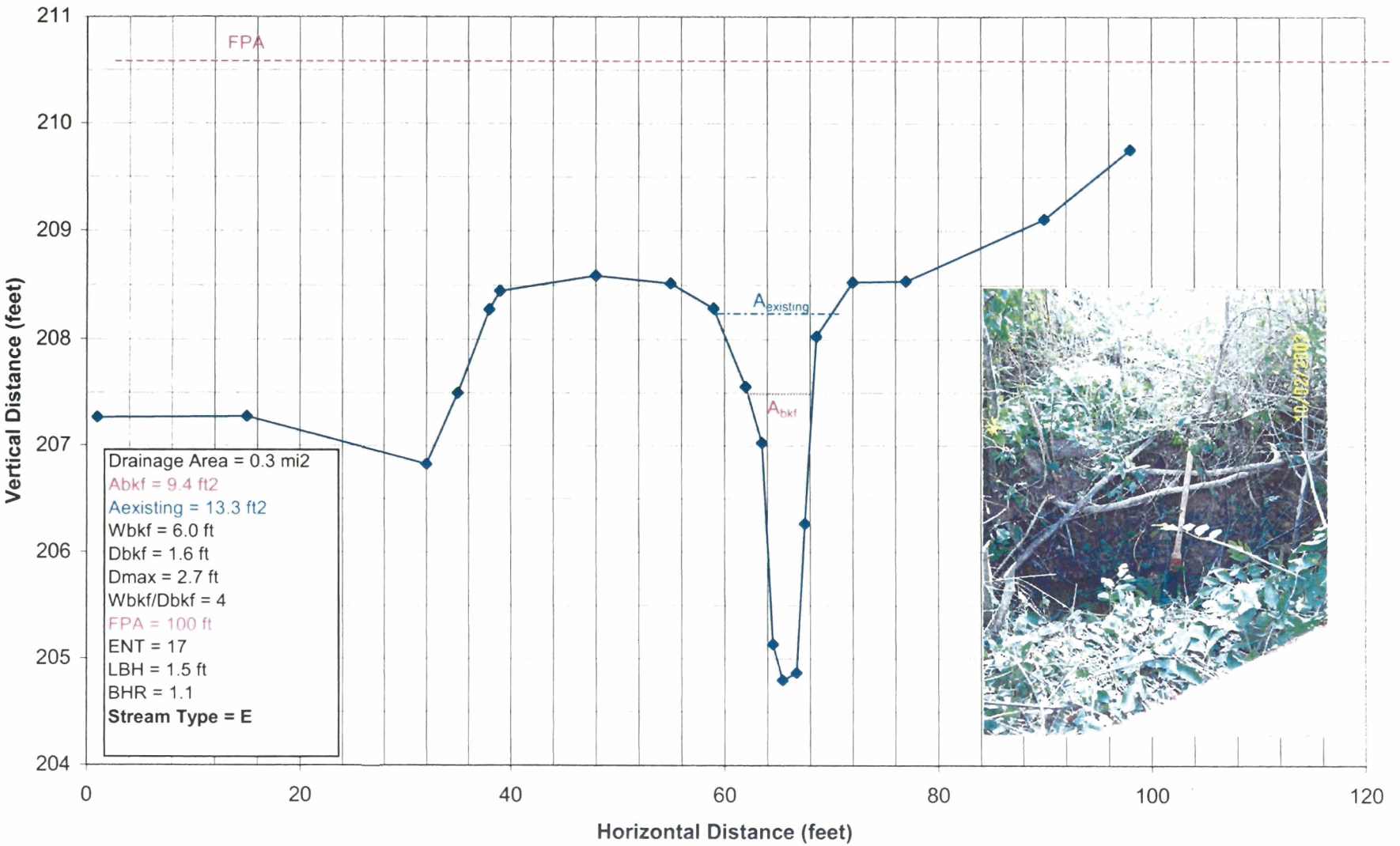
Cross-section 10: pool, Camp Branch



Cross-section 1UTCB: UT to Camp Branch



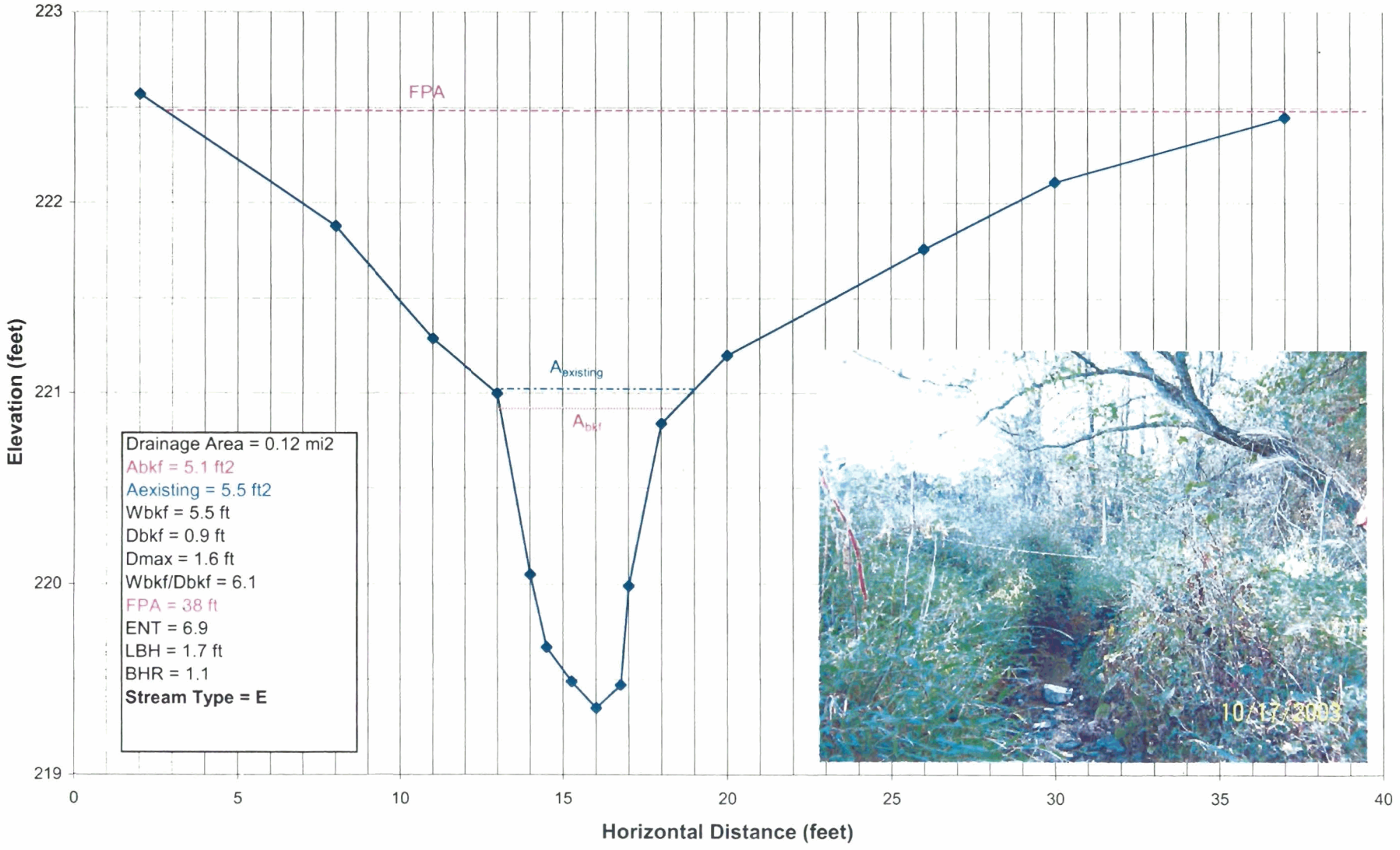
Cross-section 2UTCB: UT to Camp Branch



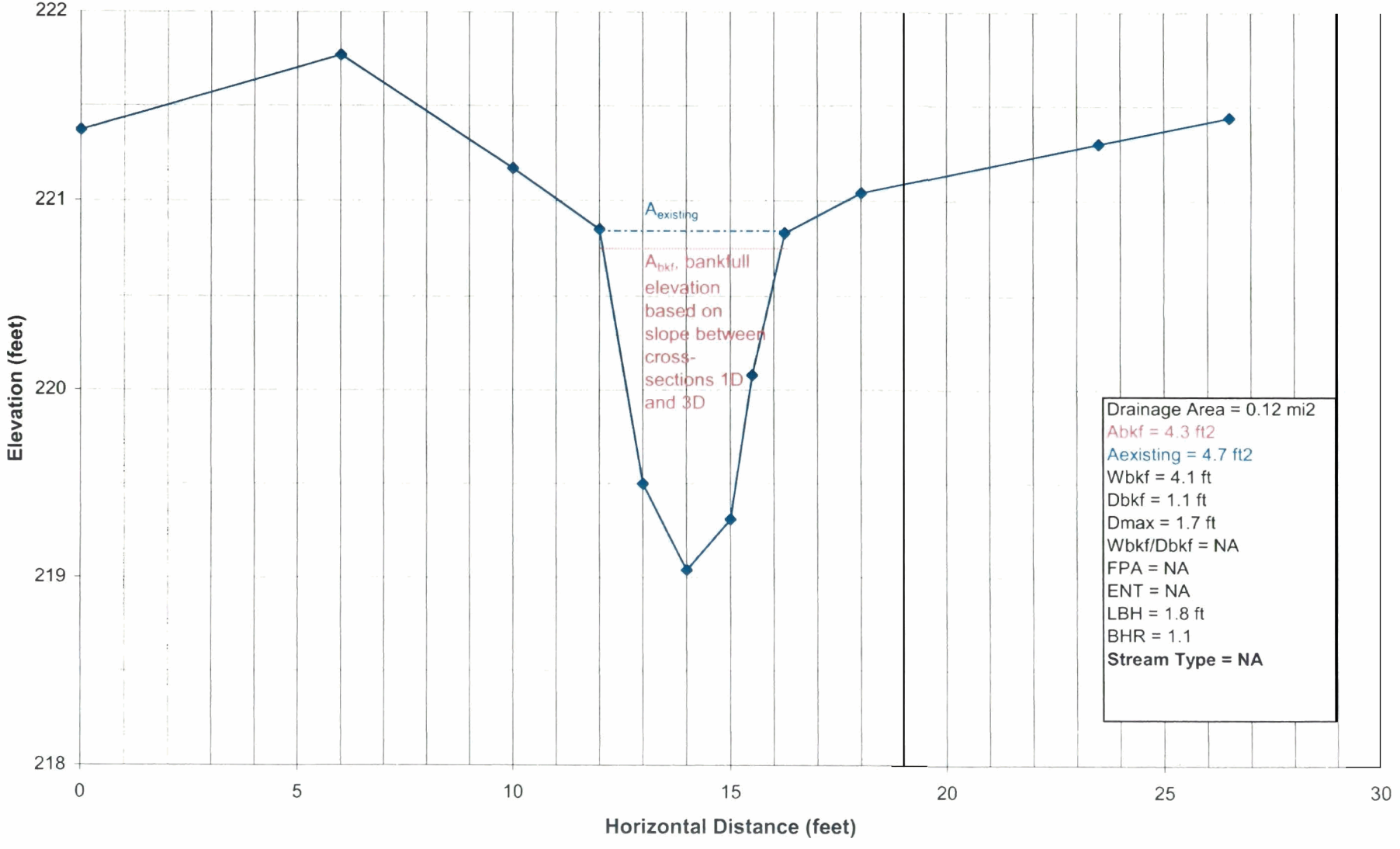
Bishop Property On-Site Dimension: Dula Thoroughfare Area

	X-sect	DA (mi^2)	A_{bkf} (ft^2)	$A_{existing}$ (ft^2)	W_{bkf} (ft)	D_{ave} (ft)	D_{max} (ft)	W/D Ratio	FPA	Entrench	LBH (ft)	BHR	Stream Type
	Dula Thoroughfare												
Riffles	1D	0.12	5.1	5.5	5.5	0.9	1.6	6.1	38	6.9	1.7	1.1	E
	3D	0.12	5.1	5.1	6.4	0.8	1.5	8	50	7.8	1.5	1	
	average	**0.12**	**5.1**	**5.3**	**5.95**	**0.85**	**1.55**	**7.05**	**44**	**7.35**	**1.6**	**1.05**	
	min	**0.12**	**5.1**	**5.1**	**5.5**	**0.8**	**1.5**	**6.1**	**38**	**6.9**	**1.5**	**1**	
	max	**0.12**	**5.1**	**5.5**	**6.4**	**0.9**	**1.6**	**8**	**50**	**7.8**	**1.7**	**1.1**	
Pools	2D	0.12	4.3	4.7	4.1	1.1	1.7	---	---	---	1.8	1.1	---
Wet Area	4D	0.14	5.7	5.7	12.3	0.5	0.9	27	150	12.1	0.9	1	C
	5D	0.14	5.7	5.7	15.9	0.4	0.8	40	50	3.1	0.8	1	
	6D	0.25	8.4	19.7	14	0.6	0.8	23.3	34.9	2.5	1.6	2	
	average	**0.18**	**6.60**	**10.37**	**14.07**	**0.50**	**0.83**	**30.10**	**78.30**	**5.90**	**1.1**	**1.3**	
	min	**0.14**	**5.7**	**5.7**	**12.3**	**0.4**	**0.8**	**23.3**	**34.9**	**2.5**	**0.8**	**1**	
	max	**0.25**	**8.4**	**19.7**	**15.9**	**0.6**	**0.9**	**40**	**150**	**12.1**	**1.6**	**2**	
	Unnamed Tributary to Dula Thoroughfare												
Riffles	1UTD	0.11	4.8	12.8	3.7	1.3	1.8	2.8	5.8	1.6	3.5	1.9	G
	2UTD	0.12	5.1	6.9	4.4	1.2	1.9	3.6	40	9.1	2.3	1.2	E
	3UTD	0.13	4.4	6.9	6.2	0.7	1.2	8.9	40	6.5	1.5	1.3	E
	average	**0.12**	**4.77**	**8.87**	**4.77**	**1.07**	**1.63**	**5.10**	**28.60**	**5.73**	**2.4**	**1.5**	
	min	**0.11**	**4.4**	**6.9**	**3.7**	**0.7**	**1.2**	**2.8**	**5.8**	**1.6**	**1.5**	**1.2**	
	max	**0.13**	**5.1**	**12.8**	**6.2**	**1.3**	**1.9**	**8.9**	**40**	**9.1**	**3.5**	**1.9**	

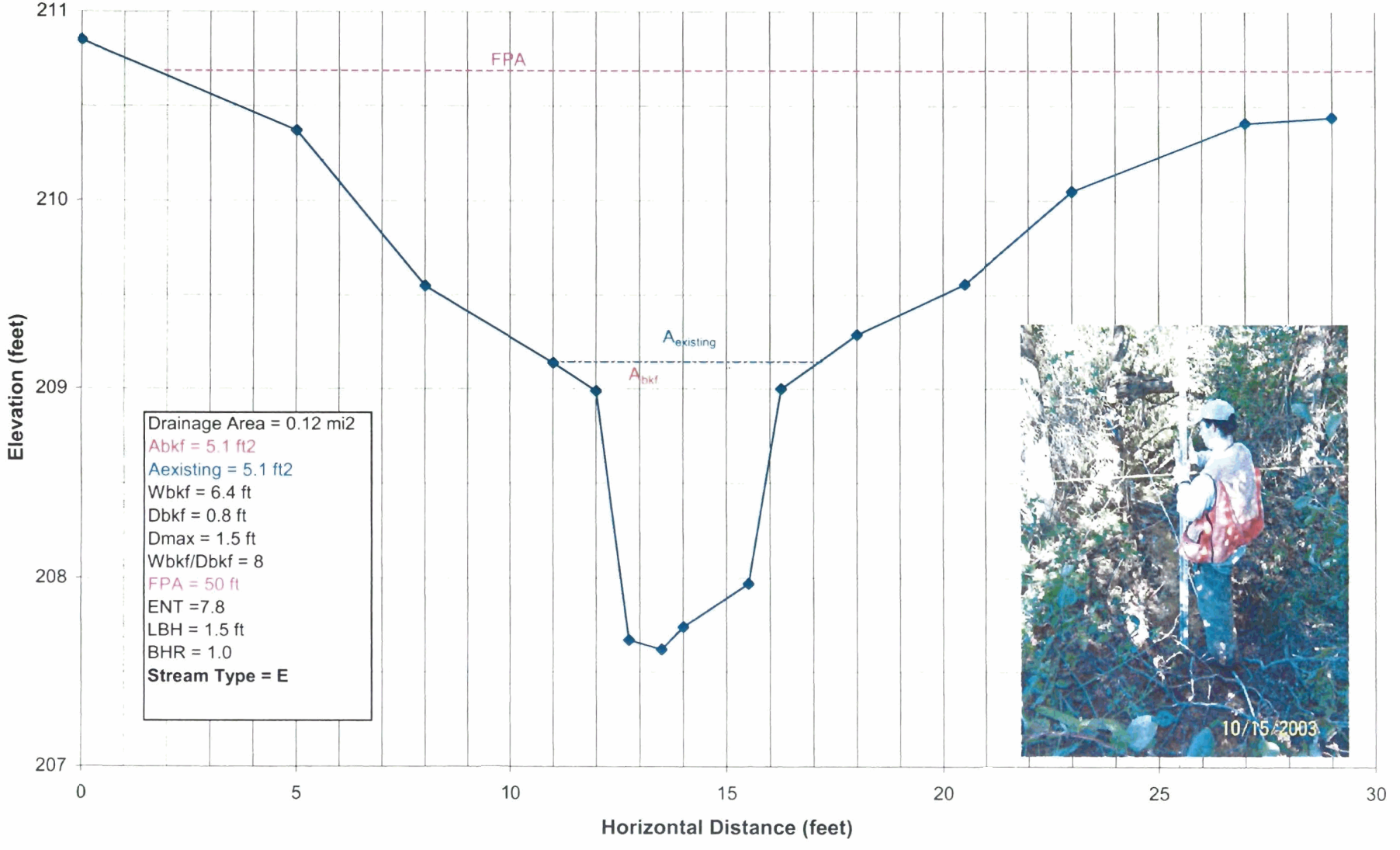
Cross-section 1D: riffle, Dulla



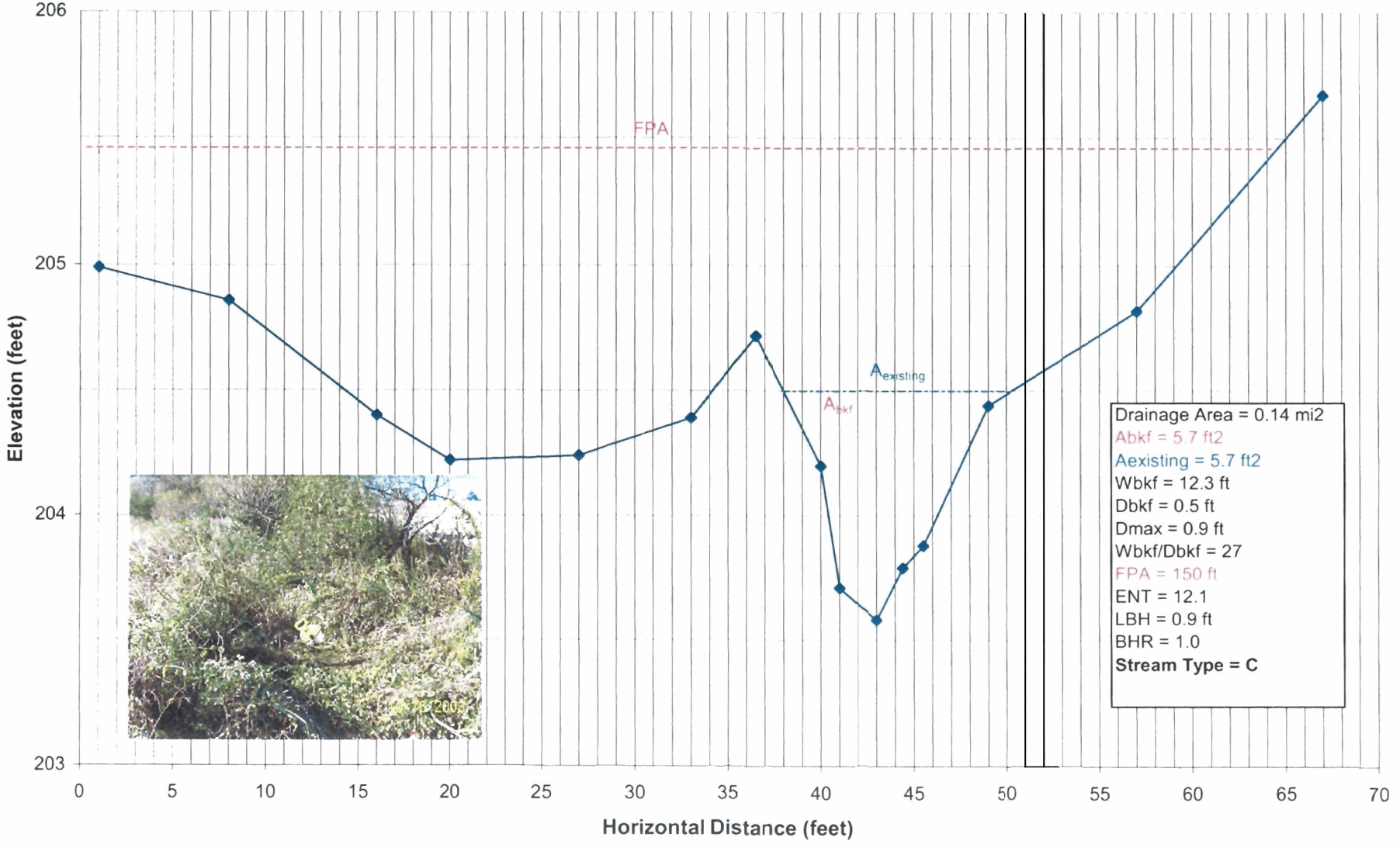
Cross-section 2D: pool, Dulla



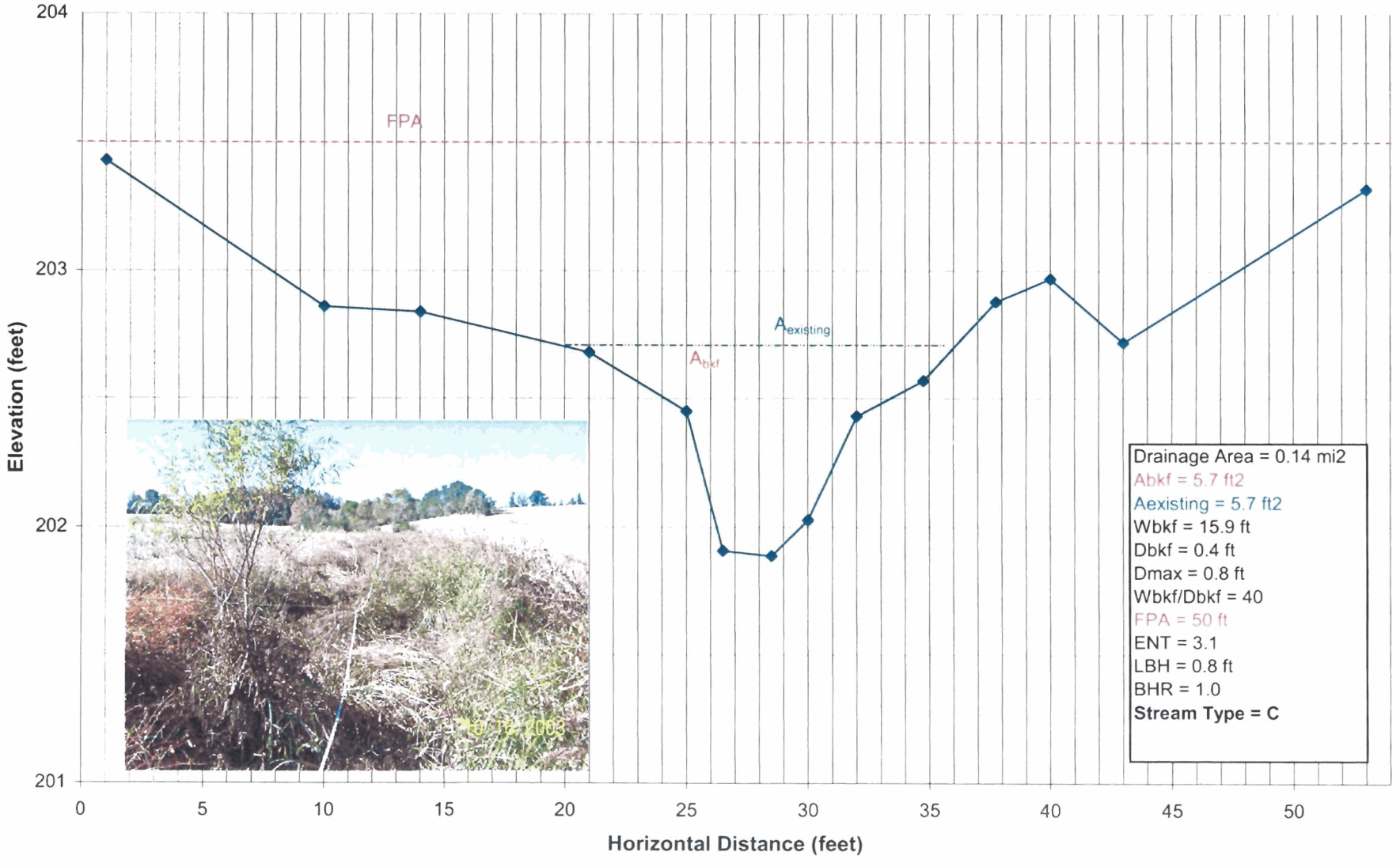
Cross-section 3D: riffle, Dulla



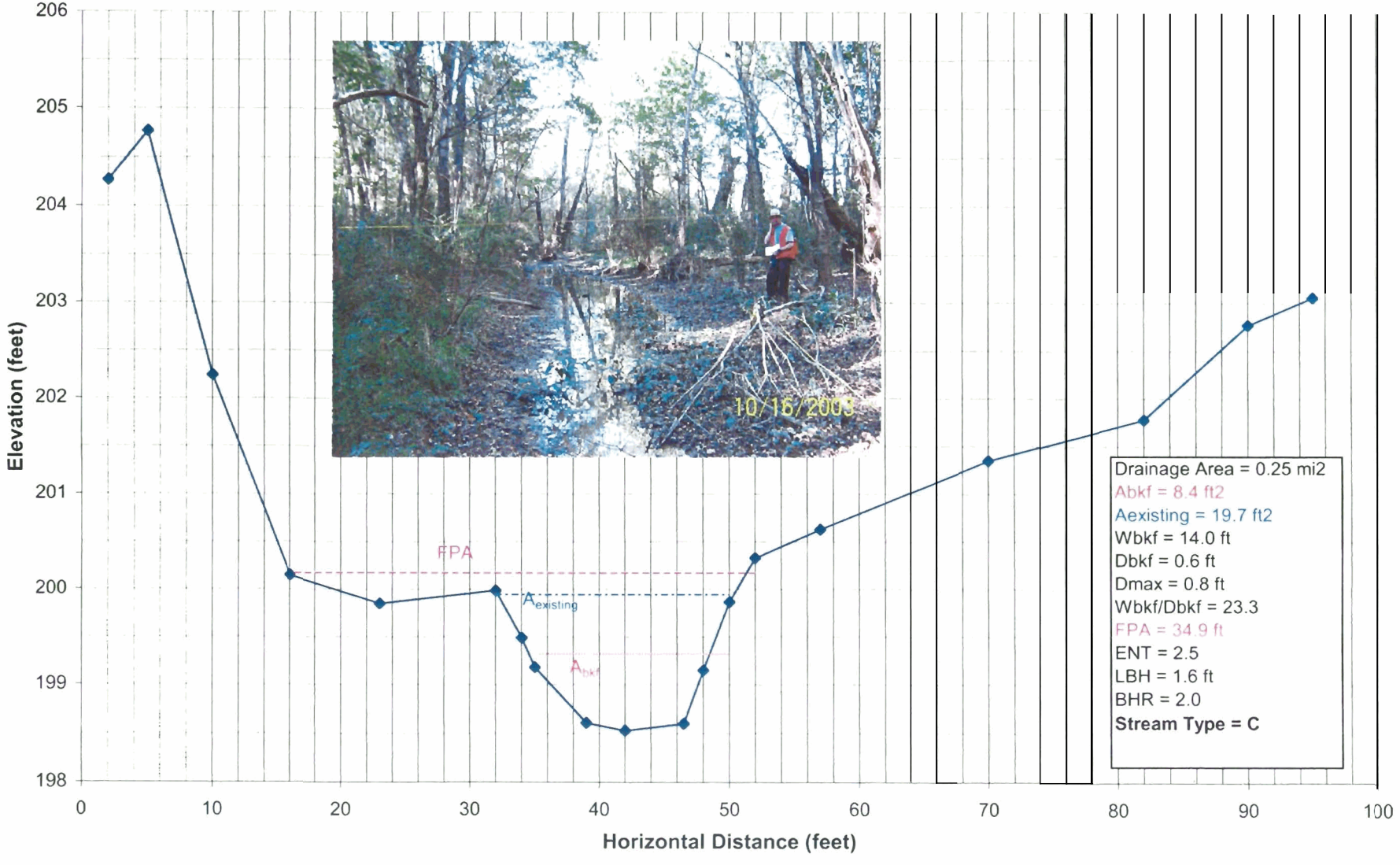
Cross-section 4D: wetland area, Dulla



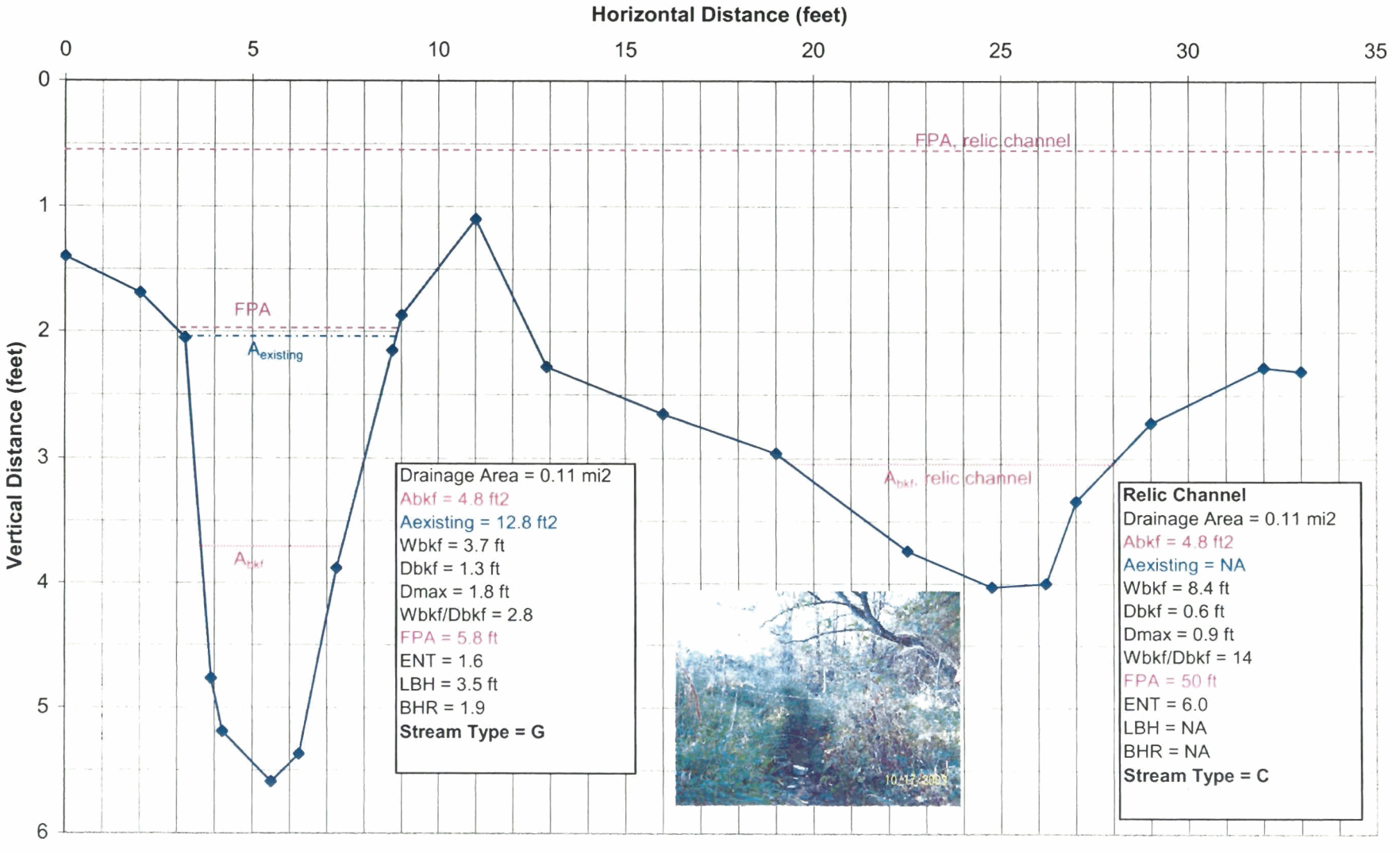
Cross-section 5D: wetland area, Dulla



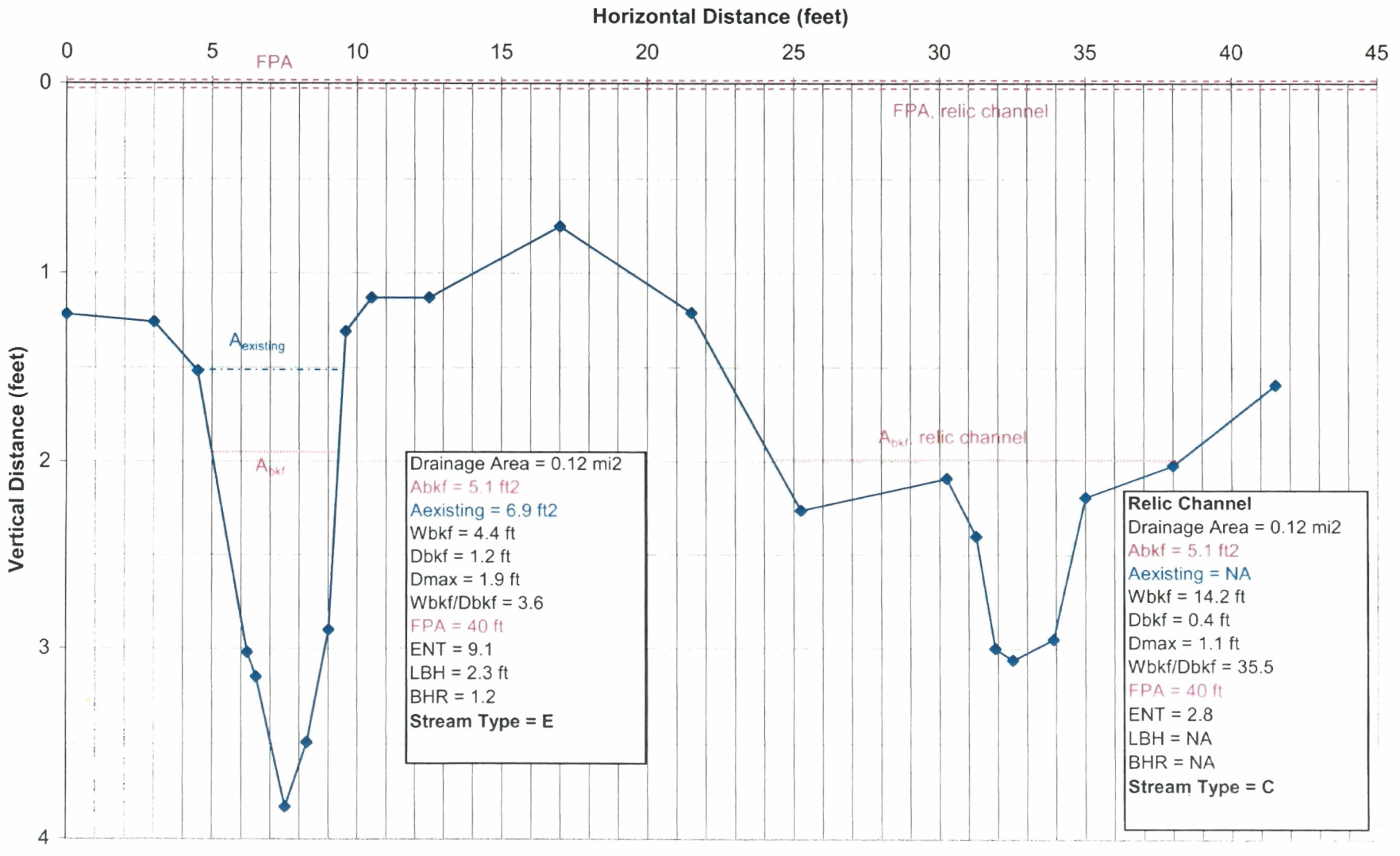
Cross-section 6D: wetland area, Dulla



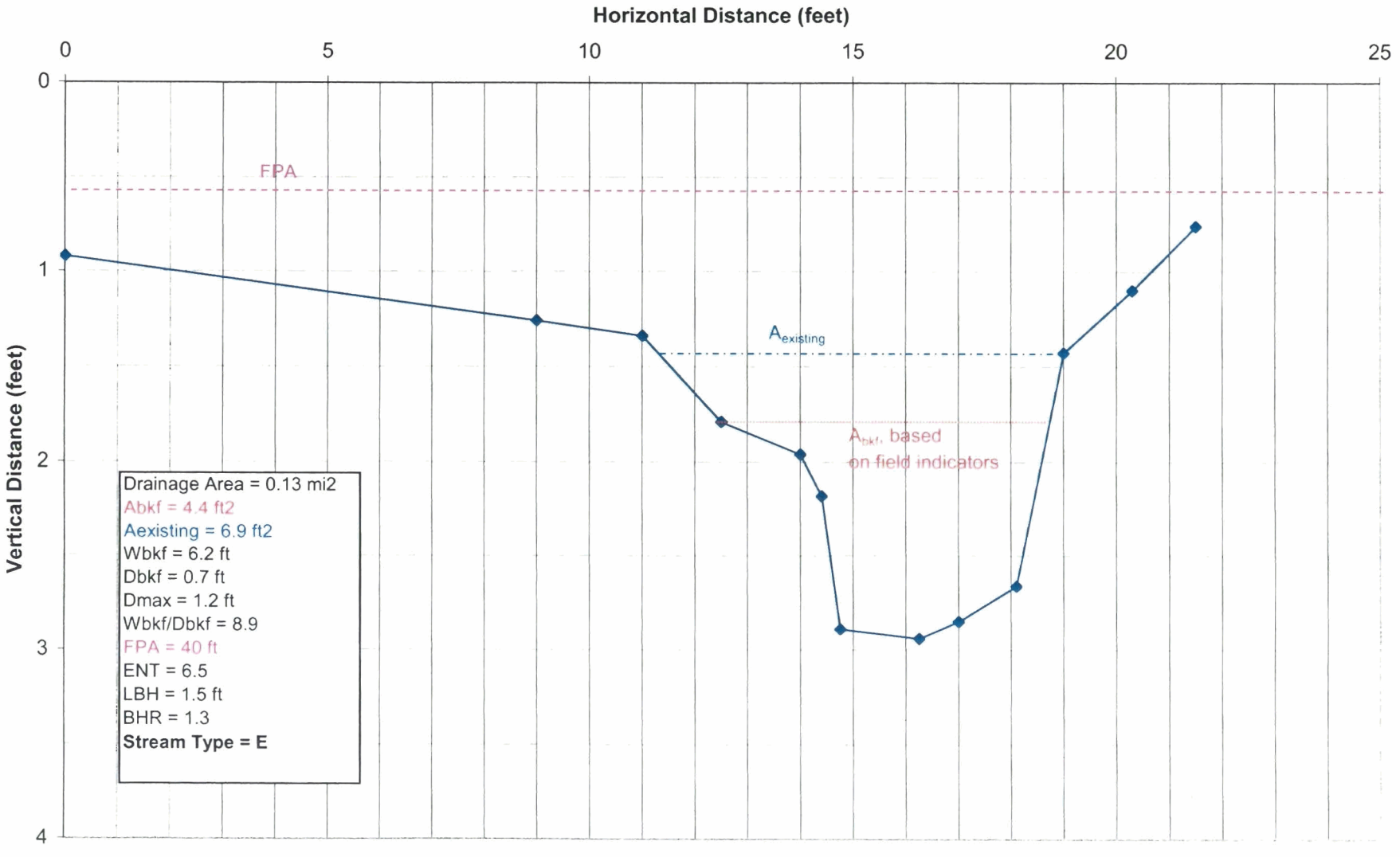
Cross-section 1UTD: riffle, UT to Dulla



Cross-section 2UTD: riffle, UT to Dulla



Cross-section 3UTD: riffle, UT to Dulla



Pattern: Camp Branch

Reaches 1 and 2 Camp Branch Upstream to Ford				
	Pool to pool spacing (feet)	Meander Length (feet)	Beltwidth (feet)	Radius of curv (feet)
	45	66	30	16.7
	46	85	31	23.4
	50	88	33	27.1
	51	89	34	27.1
	53	92	34	28.1
	55	95	35	28.6
	56	101	36	29.2
	58	102	38	29.7
	61	103	39	29.7
	62	112	40	32.3
	64	116	42	32.8
	65	123	43	36.5
	73	126	46	40.6
	73	133	46	40.6
	75	135	46	50.0
	79	137	52	53.3
	79	143	52	53.3
	79	147	57	100.0
	79	155	63	106.7
	89	159	68	116.7
	95	172	89	120.0
	112	175	97	133.3
	118	182		133.3
	120	200		133.3
	122	209		200.0
	122	237		
	140	240		
	145			
Median	**74**	**133**	**42.5**	**40.6**
Range	**45-145**	**66-240**	**30-97**	**17-200**

Reach 3 Camp Branch Downstream of Ford			
	Pool to pool spacing (feet)	Meander Length (feet)	Beltwidth (feet)
	No repetitive riffle and pool pattern.		19
			22
			25
			27
			28
			28
			32
			34
			36
			36
			36
			37
			37
			37
			37
			39
			40
			44
			44
			45
			45
			47
			68
			79
Median	**NA**	**NA**	**37**
Range	**NA**	**NA**	**19-79**

Pattern: Dula Thoroughfare

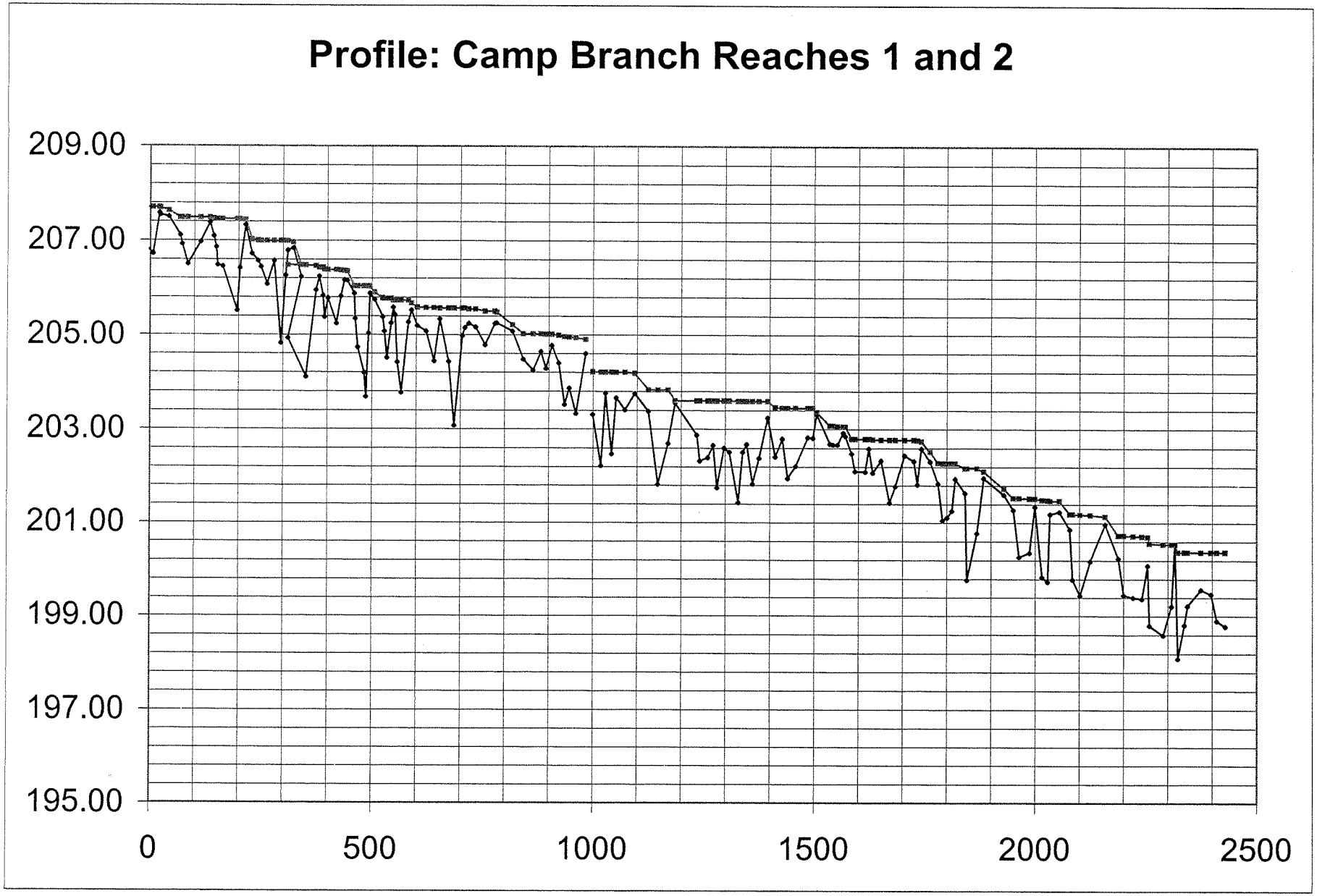
Reach 1 Dulla				
Upstream/Stream Reach				
	Pool to pool spacing (feet)	Meander Length (feet)	Beltwidth (feet)	Beltwidth/ bkf
	No repetitive riffle and pool pattern		6	
			7	
			7	
			7	
			7	
			8	
			8	
			8	
			8	
			8	
			8	
			8	
			9	
			10	
			10	
			13	
			14	
			16	
			20	
			20	
Median	NA	NA	8	1.33333333
Low	NA	NA	6	1
High	NA	NA	20	3.33333333

Reach 2 Dulla			
Downstream/Wet Area Reach			
	Pool to pool spacing (feet)	Meander Length (feet)	Beltwidth (feet)
	No repetitive riffle and pool pattern		
Median	NA	NA	NA
Low	NA	NA	NA
High	NA	NA	NA

Pattern: Unnamed Tributary to Dula Thoroughfare

Reach 2 UT Dulla Downstream E-type Reach				
	Pool to pool spacing (feet)	Meander Length (feet)	Beltwidth (feet)	Radius of Curv (feet)
	23	40	10	13.1
	26	42	14	19.7
	27	45	16	21.9
	28	46	16	24.1
	32	49	17	24.1
	33	53	18	24.1
	33	53	18	26.3
	34	61	19	30.6
	35	62	19	30.6
	37	67	20	35.0
	37	68	21	35.0
	41	71	22	39.4
	42	74	24	43.8
	43	77	25	48.1
	43	80	29	48.1
	46	81	29	48.1
	46	83	31	61.3
	48	97	32	61.3
	54	97	38	70.0
	54	100	41	70.0
	56	100		
	58	106		
	63			
Median	**41**	**69.5**	**20.5**	**35.0**
Low	**23**	**40**	**10**	**13.1**
High	**63**	**106**	**41**	**70**

Reach 1 UT Dulla Upstream G-type Reach				
	Pool to pool spacing (feet)	Meander Length (feet)	Beltwidth (feet)	Beltwidth/ bkf
	No repetitive riffle and pool pattern		22	5.9
			18	4.9
			21	5.7
Median	**NA**	**NA**	**21**	**5.7**
Low	**NA**	**NA**	**18**	**4.9**
High	**NA**	**NA**	**22**	**5.9**


Profile: Camp Branch Reaches 1 and 2
209.00
207.00
205.00
203.00
201.00
199.00
197.00
195.00
0
500
1000
1500
2000
2500

Camp Branch Profile - Reach 1 & 2

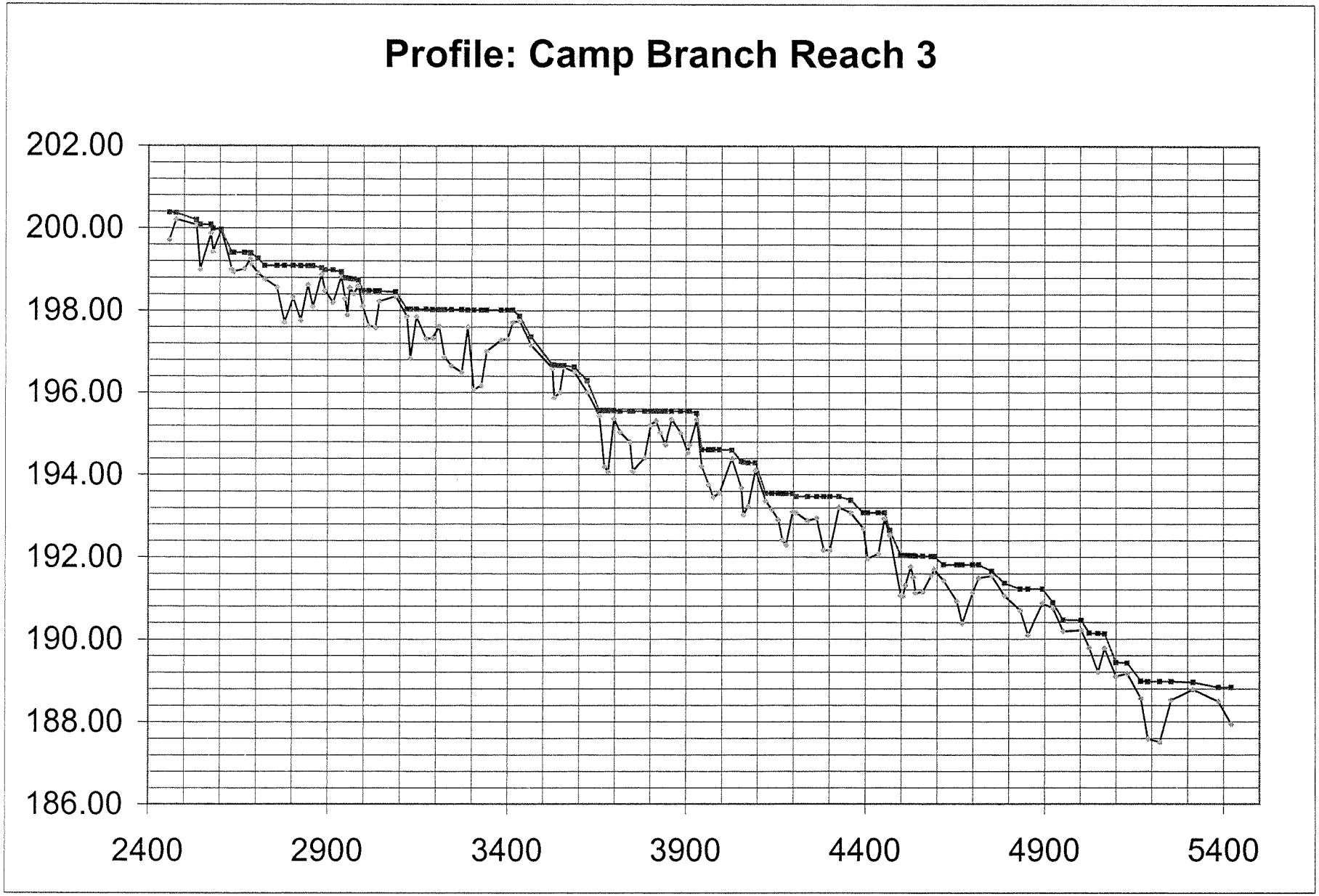
Survey conducted by Corri & Kendrick (to sta 602) and Grant, Heather, & Ben (rest of stream)

The following calculations are a result of printing out the profile graph (as originally surveyed) and amending point by point

Station	Revised Feature	Bed Elevation	Revised WS Elevation
-3		206.81	207.70
6.4		206.72	207.70
21		207.58	207.70
23	TR1	207.54	207.69
42		207.50	207.63
68	BR1	207.11	207.48
72		206.92	207.48
85.5	P1	206.50	207.48
114		206.97	207.48
135	TR2	207.38	207.48
144		207.09	207.46
149.4	BR2	206.86	207.45
152.5		206.48	207.45
164		206.45	207.45
197	P2	205.51	207.45
203		206.42	207.44
216	TR3	207.33	207.43
230		206.72	207.02
243.5		206.57	207.00
250.5	BR3	206.44	206.99
264		206.07	206.99
280		206.57	206.99
295.5	P3	204.82	206.99
306		206.26	206.99
310.5	TR4	206.79	206.99
323		206.84	206.96
341	BR4	206.23	206.48
311		204.93	206.48
351.5	P4	204.10	206.47
374		205.95	206.46
381.5	TR5	206.24	206.43
390		205.83	206.43
393		205.38	206.39
401	BR5	205.78	206.38
420		205.24	206.38
430	P5	205.82	206.37
438	TR6	206.16	206.36
444		206.15	206.35
460	BR6	205.88	206.03
462		205.35	206.03
468		204.73	206.03
482	P6	204.19	206.03
486.5		203.68	206.03
492		205.03	206.03
495	TR7	205.88	206.02
506		205.75	205.90
524	BR7	205.38	205.78
528		205.07	205.77
533.5	P7	204.51	205.77
543	TR8	205.25	205.77
548		205.58	205.73
552	BR8	205.42	205.73
557		204.42	205.73
566	P8	203.77	205.73
582	TR9	205.27	205.73
589		205.52	205.67
602	BR9	205.19	205.58
622		205.07	205.57

640		204.44	205.57
653		205.34	205.56
673	P9	204.43	205.56
686		203.07	205.56
704		204.98	205.56
710	TR9b	205.15	205.56
719		205.24	205.54
734	BR9b	205.16	205.54
756	P9b	204.78	205.50
778	TR10	205.24	205.50
782		205.25	205.48
818		205.07	205.21
842	BR10	204.48	205.02
864		204.24	205.02
882	P10	204.64	205.02
893		204.28	205.01
907	TR11	204.77	205.01
922		204.40	204.99
935	BR11	203.52	204.96
946		203.87	204.95
961	P11	203.33	204.94
983	TR12	204.60	204.90
999	BR12	203.31	204.21
1018		202.22	204.20
1028		203.76	204.20
1042	P12	202.47	204.20
1052		203.66	204.20
1072		203.41	204.20
1094	TR13	203.75	204.18
1125	BR13	203.38	203.83
1147	P13	201.82	203.83
1170	TR14	202.70	203.83
1186	BR14	203.56	203.60
1235		202.87	203.60
1242		202.32	203.60
1260		202.39	203.60
1272		202.66	203.60
1281		201.75	203.60
1297	P14	202.60	203.60
1309		202.51	203.60
1329		201.43	203.59
1339		202.51	203.59
1348		202.68	203.59
1361		201.83	203.59
1376		202.38	203.59
1395	TR15	203.24	203.59
1412		202.41	203.46
1428	BR15	202.79	203.45
1440		201.95	203.45
1458	P15	202.21	203.45
1485		202.82	203.45
1497	TR16	202.81	203.45
1505		203.32	203.36
1535	BR16	202.69	203.07
1542		202.67	203.07
1552	P16	202.67	203.06
1565	TR17	202.92	203.05
1570		202.85	203.05
1584	BR17	202.48	202.79
1592		202.10	202.79
1615		202.09	202.79
1623		202.59	202.79
1632		202.07	202.78
1651		202.33	202.77
1670	P17	201.43	202.77
1683		201.78	202.77
1704		202.44	202.77
1725		202.32	202.77
1733		201.82	202.76
1742	TR18	202.59	202.74
1762		202.31	202.52
1780	BR18	201.84	202.28
1790		201.05	202.27
1800	P18	201.11	202.27

1811		201.26	202.27
1819	TR19	201.94	202.27
1841	BR19	201.64	202.17
1845	P19	199.78	202.17
1868	TR20	200.78	202.17
1883		201.96	202.10
1929		201.60	201.73
1950	BR20	201.28	201.53
1963		200.27	201.53
1987		200.36	201.52
1999	P20	201.35	201.52
2015		199.84	201.49
2028		199.74	201.48
2033	TR21	201.19	201.47
2054		201.24	201.47
2078	BR21	200.86	201.19
2084		199.79	201.19
2101	P21	199.44	201.18
2124		200.18	201.17
2158	TR22	200.97	201.14
2188	BR22	200.24	200.73
2200		199.45	200.73
2221	P22	199.40	200.72
2241		199.37	200.71
2254	TR23	200.09	200.70
2258		198.80	200.56
2289		198.59	200.54
2308		199.21	200.54
2316		200.54	200.54
2322	BR23	198.09	200.37
2337		198.81	200.37
2344		199.22	200.37
2374	P23	199.57	200.37
2397		199.47	200.37
2410		198.90	200.37
2429		198.78	200.37

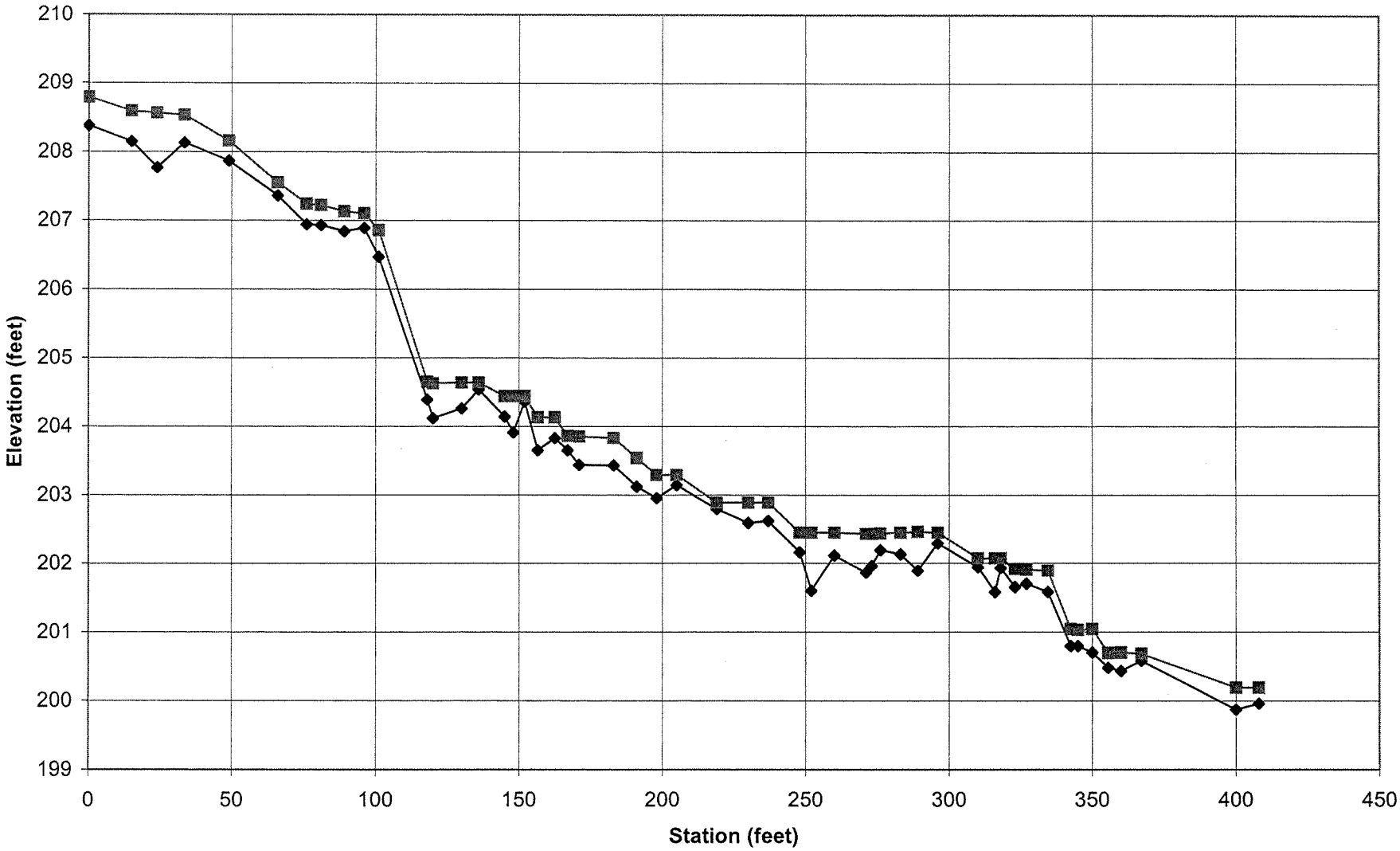

Profile: Camp Branch Reach 3
202.00
200.00
198.00
196.00
194.00
192.00
190.00
188.00
186.00
2400
2900
3400
3900
4400
4900
5400

Camp Branch Profile - Reach 3

Station	Revised Feature	Bed Elevation	Revised WS Elevation
2458		199.71	200.37
2477	TR24	200.21	200.36
2534		200.07	200.19
2544	BR24	199.00	200.08
2574		199.87	200.08
2580	P24	199.42	199.98
2603	TR25	199.96	199.96
2633	BR25	199.00	199.40
2638		198.94	199.40
2668	P25	199.01	199.40
2684	TR26	199.25	199.39
2686		199.13	199.38
2706		198.91	199.26
2725	BR26	198.76	199.09
2759		198.56	199.09
2780		197.71	199.09
2804	P26	198.31	199.09
2825		197.76	199.08
2845		198.63	199.08
2859		198.08	199.08
2883	TR27	198.88	199.03
2892	BR27	198.49	198.98
2915	P27	198.19	198.98
2938	TR28	198.83	198.93
2948	BR28	198.29	198.79
2955	P28	197.90	198.78
2961	TR29	198.55	198.77
2972		198.41	198.76
2985		198.59	198.74
2997	BR29	198.10	198.48
3014		197.63	198.48
3032	P29	197.58	198.47
3043	TR30	198.22	198.47
3088		198.35	198.45
3120	BR30	197.85	198.03
3129		196.84	198.03
3146		197.85	198.03
3173		197.31	198.03
3191		197.33	198.02
3209		197.61	198.02
3224		196.86	198.02
3243		196.65	198.02
3272		196.49	198.02
3289	P30	197.60	198.01
3306		196.07	198.01
3327		196.18	198.01
3342		197.01	198.01
3382		197.28	198.01
3400		197.30	198.01
3415	TR31	197.71	198.01
3434		197.75	197.86
3466		197.16	197.35
3526	BR31	196.59	196.68
3531		195.87	196.67
3546	P31	196.00	196.66
3558	TR32	196.61	196.66
3587		196.50	196.62
3623		196.01	196.29
3657	BR32	195.44	195.56
3671		194.20	195.56
3682		194.06	195.56
3698		195.37	195.56
3716		195.03	195.55
3743		194.79	195.55
3751		194.08	195.55
3784		194.41	195.55
3801	P32	195.21	195.55
3816		195.31	195.55

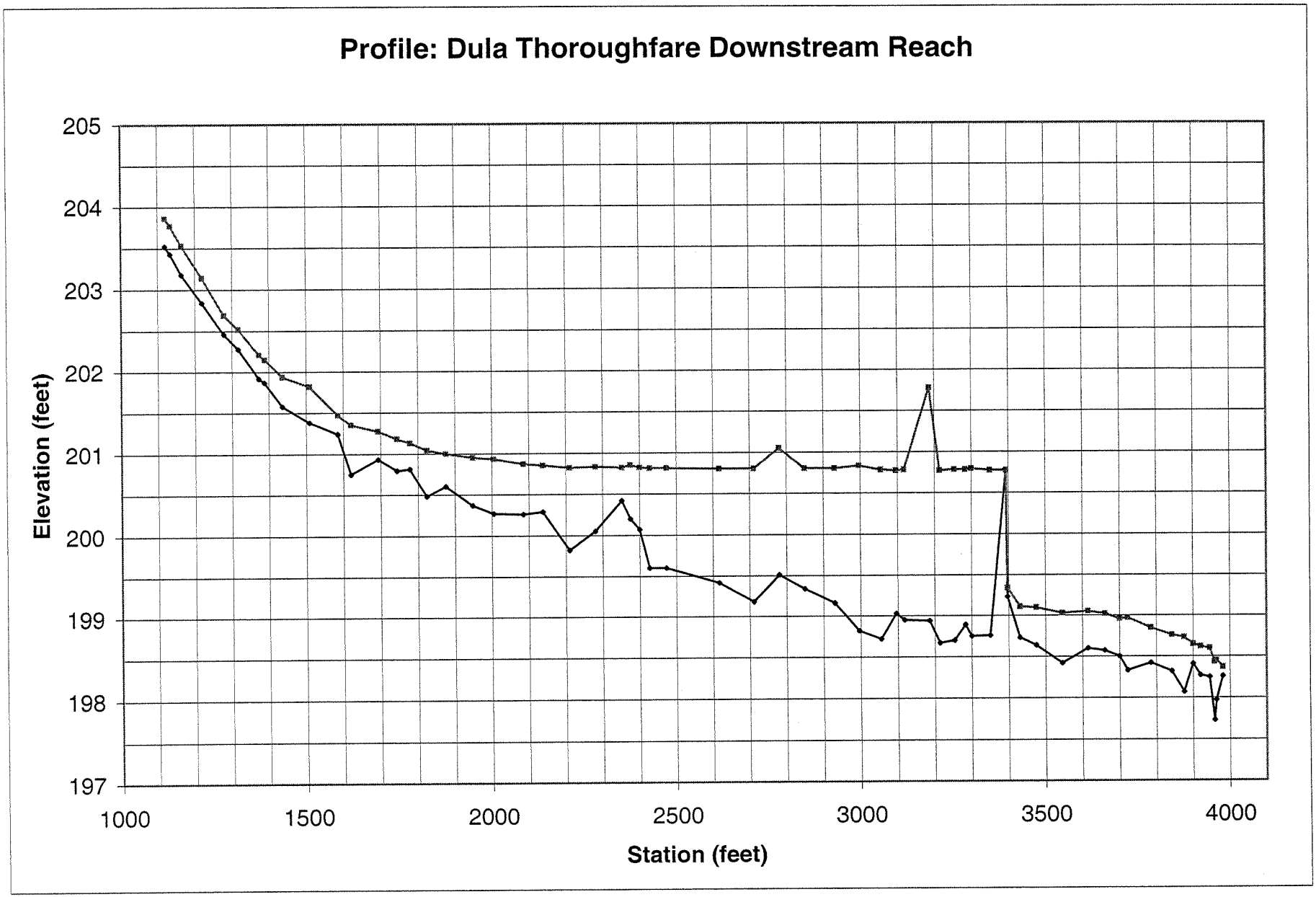
3828		195.02	195.55
3842		194.73	195.55
3860		195.35	195.55
3885		195.02	195.55
3905		194.54	195.55
3910		194.71	195.55
3929.5	TR33	195.34	195.50
3944	BR33	194.20	194.61
3963		193.76	194.61
3976	P33	193.45	194.61
3994		193.56	194.61
4028.5	TR34	194.39	194.60
4055	BR34	193.67	194.32
4060		193.03	194.30
4074	P34	193.23	194.29
4094	TR35	194.10	194.29
4123	BR35	193.36	193.55
4140		193.16	193.55
4158		192.91	193.55
4169		192.41	193.54
4180	P35	192.29	193.54
4198	TR36	193.10	193.54
4208	BR36	193.08	193.47
4240		192.88	193.47
4265		192.94	193.47
4285	P36	192.16	193.47
4302		192.16	193.47
4327	TR37	193.21	193.47
4360		193.08	193.38
4395	BR37	192.69	193.08
4407		191.96	193.08
4437	P37	192.08	193.08
4454	TR38	192.93	193.08
4468		192.53	192.65
4499	BR38	191.06	192.04
4505		191.04	192.04
4512		191.31	192.04
4526		191.77	192.03
4534	P38	191.51	192.03
4540		191.12	192.02
4560		191.15	192.02
4584		191.55	192.01
4591.5	TR39	191.70	192.01
4618	BR39	191.42	191.81
4655		190.92	191.81
4670	P39	190.37	191.81
4699		191.13	191.81
4716	TR40	191.49	191.81
4752		191.54	191.66
4788		191.05	191.36
4832	BR40	190.69	191.22
4853	P40	190.10	191.22
4894	TR41	190.86	191.22
4923		190.75	190.88
4952		190.19	190.46
5003		190.22	190.45
5025	BR41	189.79	190.15
5050	P41	189.20	190.14
5068	TR42	189.77	190.13
5100		189.09	189.43
5131		189.16	189.42
5169	BR42	188.57	188.98
5189		187.59	188.97
5222	P42	187.51	188.97
5254	TR43	188.52	188.97
5315		188.78	188.95
5385	BR43	188.49	188.83
5421		187.95	188.83
		106.01	

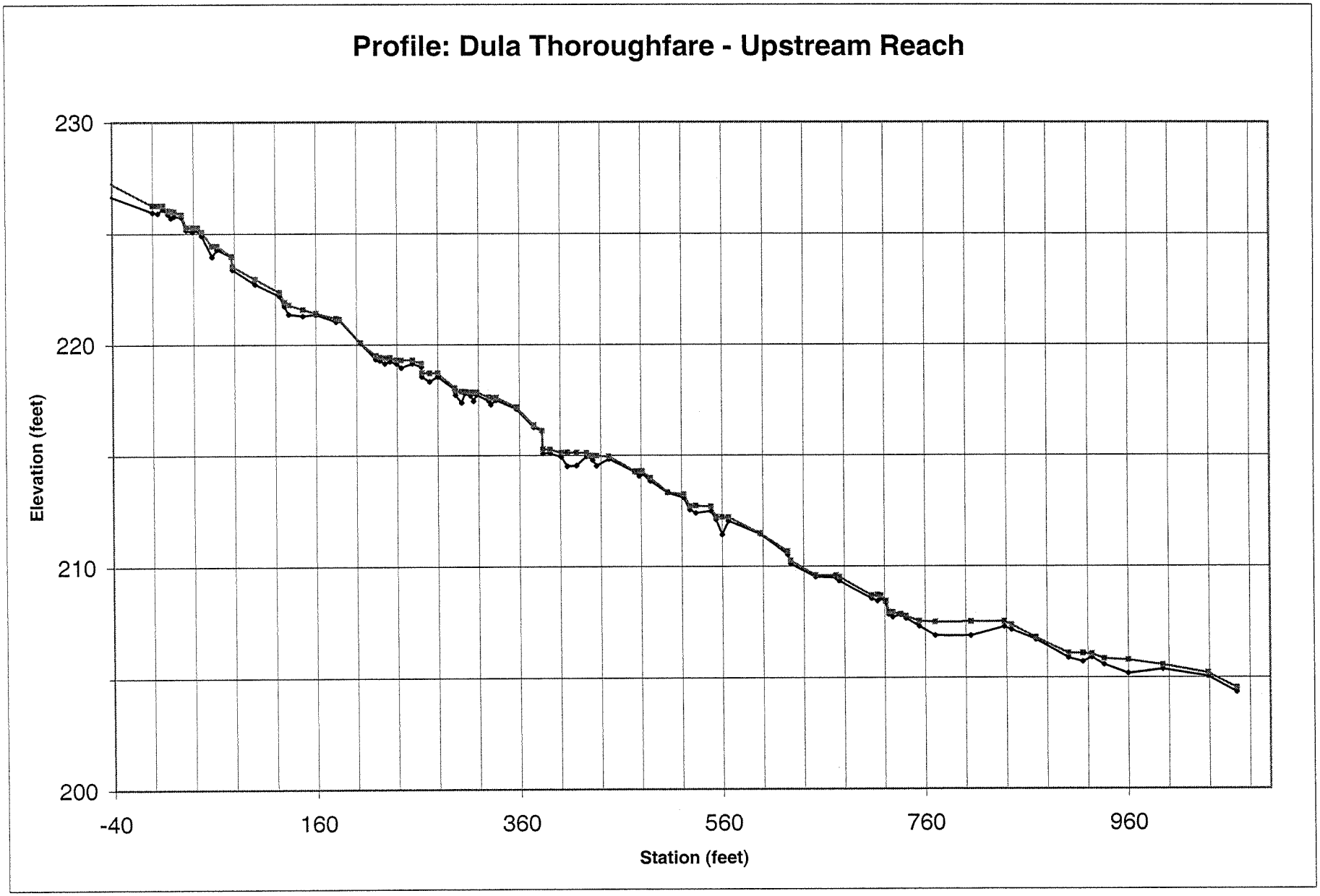
Profile: UT to Camp Branch



UT to Camp Branch

Station	Station reversed	Bed Elevation	WS Elevation	Feature Amended
0	408	199.96	200.19	
8	400	199.87	200.19	br14
41	367	200.58	200.68	tr14
48	360	200.43	200.7	p13
52.5	355.5	200.48	200.69	br13
58	350	200.7	201.04	tr13
63	345	200.79	201.03	p12
65.5	342.5	200.79	201.04	br12
73.5	334.5	201.58	201.89	tr12
81	327	201.7	201.9	p11
85	323	201.65	201.91	br11
90	318	201.93	202.07	tr11
92	316	201.58	202.07	p10
98	310	201.94	202.07	br10
112	296	202.29	202.45	tr10
119	289	201.89	202.46	p9c
125	283	202.13	202.45	
132	276	202.19	202.44	
135	273	201.96	202.43	p9b
137	271	201.86	202.43	
148	260	202.11	202.45	
156	252	201.6	202.45	p9a
160	248	202.16	202.45	br9
171	237	202.62	202.89	tr9
178	230	202.59	202.89	p8
189	219	202.79	202.89	br8
203	205	203.14	203.29	tr8
210	198	202.95	203.29	br7
217	191	203.12	203.54	
225	183	203.43	203.83	tr7
237	171	203.44	203.85	p6
241	167	203.65	203.86	br6
245.5	162.5	203.83	204.13	tr6
251.5	156.5	203.65	204.13	br5
256	152	204.36	204.44	tr5
260	148	203.91	204.44	p4
263	145	204.14	204.44	br4
272	136	204.54	204.64	tr4
278	130	204.26	204.64	
288	120	204.12	204.63	p3
290	118	204.39	204.65	br3
307	101	206.47	206.86	
312	96	206.89	207.1	tr3
319	89	206.84	207.13	p2
327	81	206.93	207.22	
332	76	206.94	207.24	br2
342	66	207.36	207.55	
359	49	207.87	208.16	
374.5	33.5	208.13	208.53	tr2
384	24	207.77	208.56	p1
393	15	208.15	208.59	br1
408	0	208.38	208.79	tr1


Profile: Dula Thoroughfare Downstream Reach
Elevation (feet)
205
204
203
202
201
200
199
198
197
1000
1500
2000
2500
3000
3500
4000
Station (feet)


Profile: Dula Thoroughfare - Upstream Reach
230
220
210
200
Elevation (feet)
-40
160
360
560
760
960
Station (feet)

Dulla Throughfare Profile

Composite Station	Bed Elevation	Water Surface Elevation	Feature
-41.5	226.66	227.25	upstream culvert
0	225.94	226.24	downstream culvert KX01
5	225.9	226.25	glide
10	226.09	226.24	TR KX02
15	225.87	226.03	BR
18	225.69	225.99	KX03
21	225.77	225.97	TR
28	225.74	225.84	MR
33	225.15	225.27	BR
39	225.08	225.28	P
44	225.16	225.26	TR
48	224.9	225.07	MR
58	223.96	224.44	P
63	224.28	224.44	HC
77	223.97	223.98	THC
78	223.37	223.52	BHC
100	222.72	222.95	MR KX06
124	222.19	222.35	MR KX07
129	221.72	221.91	BR
133	221.37	221.78	P
147	221.29	221.57	
160	221.36	221.41	TR
180	221.03	221.18	P
183	221.12	221.14	TR
204	220.07	220.09	MR
219	219.35	219.5	x-sect 1D
223	219.29	219.43	BR
228	219.15	219.41	P
233	219.24	219.42	TR
239.5	219.15	219.31	BR KX14
244	218.96	219.31	P
255	219.15	219.31	TR
264	219.01	219.15	THC
264.5	218.57	218.74	BHC
272	218.35	218.72	P
280	218.57	218.72	TR
296.5	218.01	218.07	BR, THC formed by fallen tree
297.5	217.74	217.93	BHC
303.5	217.39	217.9	P
306.5	217.81	217.89	TR
312	217.72	217.87	BR
315	217.47	217.86	P
318	217.75	217.87	TR
330	217.48	217.63	BR
332	217.31	217.61	P
337	217.51	217.62	TR
357	217.11	217.19	MR
374	216.27	216.37	TR/KX21
382	216.11	216.12	THC
383	215.08	215.29	BHC
390	215.1	215.26	
401	214.92	215.13	BR
407	214.5	215.14	P
416	214.53	215.12	P
426	214.95	215.1	TR
429	214.96	215	MR KX29
432	214.78	214.98	BR
436	214.52	214.98	P
448	214.82	214.95	G/TR KX29
474	214.25	214.27	BR
478	214.05	214.28	P
481	214.18	214.29	TR KX28
489	213.82	213.97	MR
506	213.31	213.33	BR
522	213.09	213.23	DEBRIS JAM
528	212.54	212.7	BASE OF DEBRIS JAM
534	212.39	212.72	P KX30
549	212.48	212.69	TR
554	212.09	212.21	BR
560	211.42	212.2	P
566	212.02	212.19	TR
597	211.45	211.47	MR
624	210.53	210.65	MR,TOP OF ROOT GRADE CONTROL
627	210.1	210.25	MR, TOP AT 1.3
651.5	209.51	209.58	BR, MOUTH OF CULVERT
671.7	209.48	209.58	MOUTH OF CULVERT
675	209.33	209.51	BR
707	208.53	208.68	BR
713	208.42	208.69	P
716	208.54	208.66	TR
721	208.34	208.42	THC
724	207.81	207.93	BHC
728	207.69	207.91	P KX37
736	207.79	207.81	TR
741	207.64	207.73	MR X-SECT 3D
754	207.29	207.51	BR
770	206.87	207.47	P, AGGREGATION REACH STARTS
805	206.86	207.48	SLACKWATER POOL
838	207.26	207.49	BOTTOM OF SLACK WATER
845	207.13	207.34	TR
869	206.69	206.77	MR
901	205.88	206.08	P
915	205.7	206.08	GLIDE
924	205.9	206.04	TR KX 47
936	205.56	205.84	BR KX48
960	205.17	205.77	P KX50

Composite Station	Bed Elevation	Water Surface Elevation	Feature
994	205.36	205.54	KX52
1038.5	205.04	205.19	FK7.5 WETLAND
1067	204.33	204.52	FK8
1119	203.52	203.86	
1134	203.43	203.77	X-SECT4D
1164	203.18	203.53	
1219	202.84	203.14	
1278	202.46	202.69	
1317	202.28	202.52	
1373	201.92	202.21	
1388	201.87	202.15	X-SECT5D
1436	201.58	201.94	
1509	201.38	201.82	
1585	201.24	201.47	
1620	200.75	201.35	CONVERGENCE OF DULLA W/DITCH
1693	200.93	201.27	
1744	200.79	201.18	
1778	200.81	201.13	KY28
1824	200.48	201.04	
1875	200.6	201	
1948	200.37	200.95	KY29
2005	200.27	200.93	
2085	200.26	200.87	
2138	200.29	200.85	
2210	199.82	200.82	
2280	200.05	200.83	
2352	200.42	200.82	KY33
2375	200.2	200.85	FL01 DOWNSTREAM SIDE OF DAM
2400	200.07	200.82	
2427	199.6	200.81	FL02
2473	199.6	200.81	
2617	199.42	200.8	
2711	199.18	200.8	
2780	199.51	201.05	
2849	199.34	200.8	FL08
2930	199.16	200.8	
2996	198.82	200.83	CONV. OF DULLA W/DITCH, BEAVER IMP.
3055	198.72	200.78	
3096	199.03	200.77	
3118	198.95	200.78	
3186	198.94	201.78	
3214	198.67	200.77	FH25 BEAVER DEN
3253	198.7	200.78	FH23
3283	198.89	200.78	
3300	198.75	200.79	FH21
3350	198.76	200.77	
3394	200.77	200.77	TOP OF BEAVER DAM/H2O SURFACE
3397	199.23	199.34	BASE OF BEAVER DAM
3431	198.73	199.11	SF11
3475	198.64	199.1	
3545	198.42	199.03	
3615	198.6	199.05	
3660	198.57	199.02	
3700	198.5	198.96	
3722	198.33	198.97	
3785	198.42	198.85	FH08
3842	198.32	198.76	SG04
3875	198.07	198.73	
3900	198.41	198.65	
3920	198.27	198.62	TR FH03
3945	198.25	198.6	BR
3958	197.73	198.43	P(BEHIND LOG JAM)
3963	197.97	198.45	
3981	198.26	198.37	

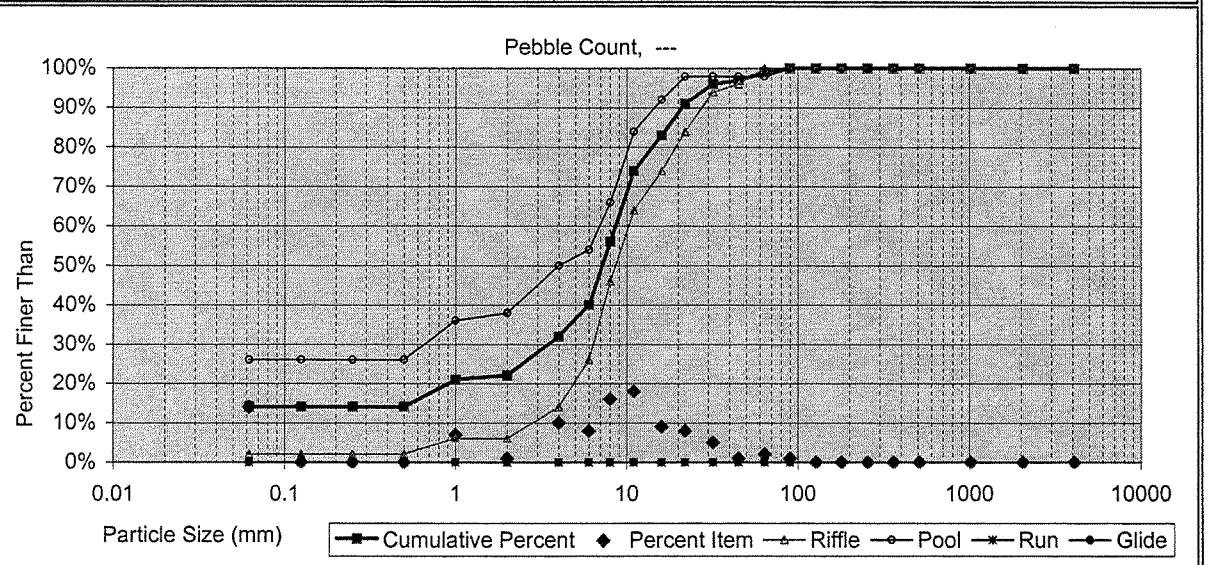
Weighted Pebble Count

Percent Riffle:	50	Percent Run:	
Percent Pool:	50	Percent Glide:	

Pebble Count,

Note: **Camp Branch Reference Reach (Reach 1)**

Material	Size Range (mm)		Total #	
silt/clay	0	0.062	14.0	#
very fine sand	0.062	0.13	0.0	#
fine sand	0.13	0.25	0.0	#
medium sand	0.25	0.5	0.0	#
coarse sand	0.5	1	7.0	#
very coarse sand	1	2	1.0	#
very fine gravel	2	4	10.0	#
fine gravel	4	6	8.0	#
fine gravel	6	8	16.0	#
medium gravel	8	11	18.0	#
medium gravel	11	16	9.0	#
coarse gravel	16	22	8.0	#
coarse gravel	22	32	5.0	#
very coarse gravel	32	45	1.0	#
very coarse gravel	45	64	2.0	#
small cobble	64	90	1.0	#
medium cobble	90	128	0.0	#
large cobble	128	180	0.0	#
very large cobble	180	256	0.0	#
small boulder	256	362	0.0	#
small boulder	362	512	0.0	#
medium boulder	512	1024	0.0	#
large boulder	1024	2048	0.0	#
very large boulder	2048	4096	0.0	#
bedrock			0.0	#
		Weighted Count:	100	
		True Total Particle Count:	100	



Size percent less than (mm)					Percent by substrate type					
D16	D35	D50	D84	D95	silt/clay	sand	gravel	cobble	boulder	bedrock
0.610	4.66	7.2	17	30	14%	8%	77%	1%	0%	0%

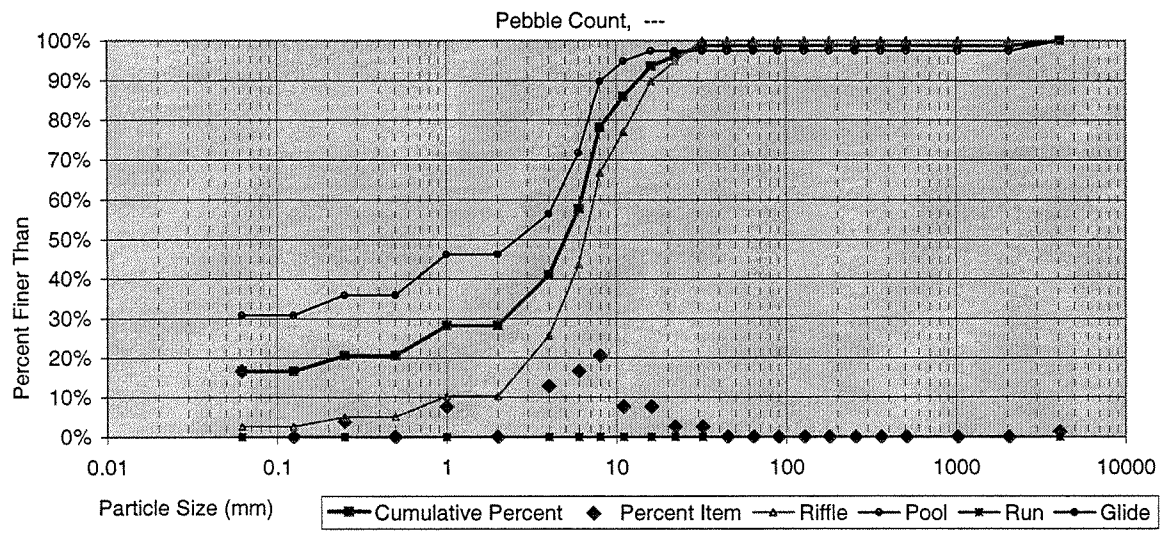
Weighted Pebble Count

Percent Riffle:	50	Percent Run:	
Percent Pool:	50	Percent Glide:	

Pebble Count,

Note: **Camp Branch (Reach 2)**

Material	Size Range (mm)		Total #	
silt/clay	0	0.062	16.7	#
very fine sand	0.062	0.13	0.0	#
fine sand	0.13	0.25	3.8	#
medium sand	0.25	0.5	0.0	#
coarse sand	0.5	1	7.7	#
very coarse sand	1	2	0.0	#
very fine gravel	2	4	12.8	#
fine gravel	4	6	16.7	#
fine gravel	6	8	20.5	#
medium gravel	8	11	7.7	#
medium gravel	11	16	7.7	#
coarse gravel	16	22	2.6	#
coarse gravel	22	32	2.6	#
very coarse gravel	32	45	0.0	#
very coarse gravel	45	64	0.0	#
small cobble	64	90	0.0	#
medium cobble	90	128	0.0	#
large cobble	128	180	0.0	#
very large cobble	180	256	0.0	#
small boulder	256	362	0.0	#
small boulder	362	512	0.0	#
medium boulder	512	1024	0.0	#
large boulder	1024	2048	0.0	#
very large boulder	2048	4096	1.3	#
bedrock			0.0	#
		Weighted Count:	100	
		True Total Particle Count:	78	



Size percent less than (mm)				
D16	D35	D50	D84	D95
#N/A	2.89	5.0	10	19

Percent by substrate type					
silt/clay	sand	gravel	cobble	boulder	bedrock
17%	12%	71%	0%	1%	0%

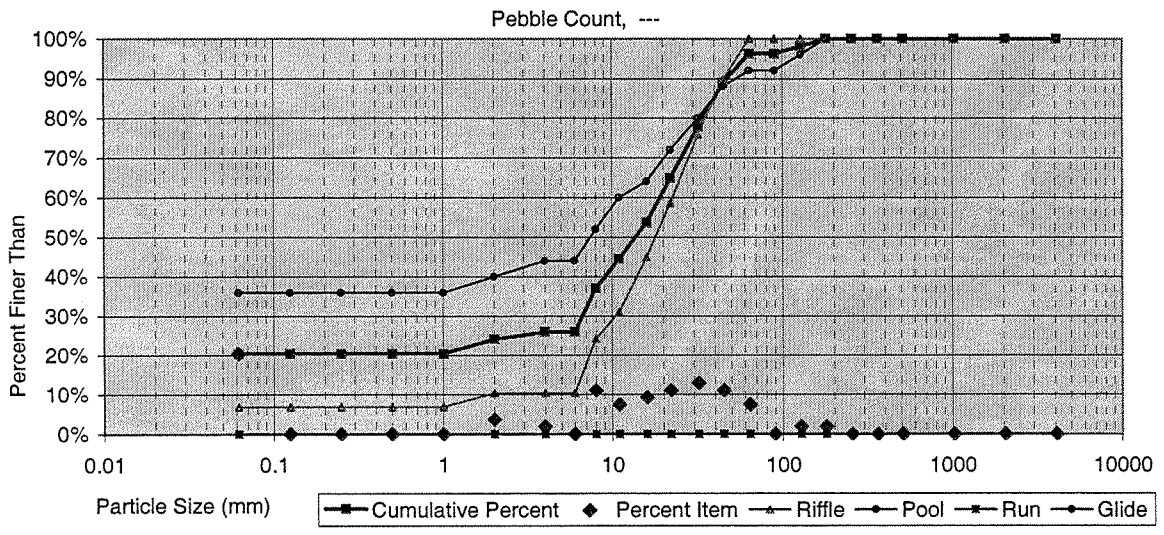
Weighted Pebble Count

Percent Riffle:	50	Percent Run:	
Percent Pool:	50	Percent Glide:	

Pebble Count,

Note: **Camp Branch (Reach 3)**

Material	Size Range (mm)		Total #	
silt/clay	0	0.062	13.8	# #
very fine sand	0.062	0.13	0.0	# #
fine sand	0.13	0.25	0.0	# #
medium sand	0.25	0.5	0.0	# #
coarse sand	0.5	1	0.0	# #
very coarse sand	1	2	2.5	# #
very fine gravel	2	4	1.3	# #
fine gravel	4	6	0.0	# #
fine gravel	6	8	7.5	# #
medium gravel	8	11	5.0	# #
medium gravel	11	16	6.3	# #
coarse gravel	16	22	7.5	# #
coarse gravel	22	32	8.8	# #
very coarse gravel	32	45	7.5	# #
very coarse gravel	45	64	5.0	# #
small cobble	64	90	0.0	# #
medium cobble	90	128	1.3	# #
large cobble	128	180	1.3	# #
very large cobble	180	256	0.0	# #
small boulder	256	362	0.0	# #
small boulder	362	512	0.0	# #
medium boulder	512	1024	0.0	# #
large boulder	1024	2048	0.0	# #
very large boulder	2048	4096	0.0	# #
bedrock			32.5	#
		Weighted Count:	100	
		True Total Particle Count:	80	



Size percent less than (mm)					Percent by substrate type					
D16	D35	D50	D84	D95	silt/clay	sand	gravel	cobble	boulder	bedrock
#N/A	7.59	13.8	39	60	14%	3%	49%	3%	0%	33%

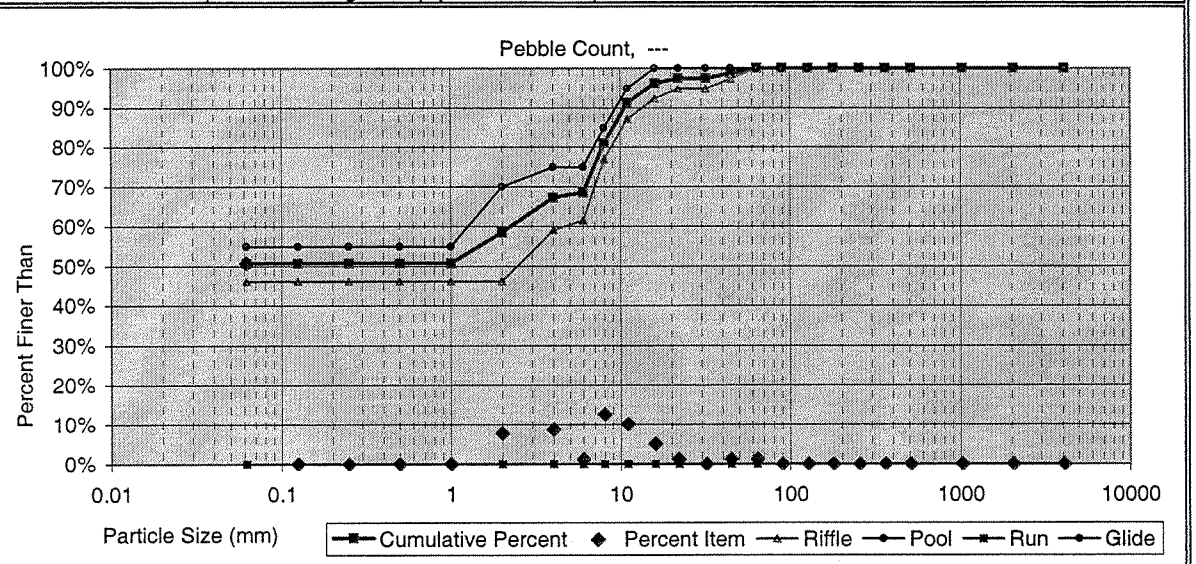
Weighted Pebble Count

Percent Riffle:	50	Percent Run:	
Percent Pool:	50	Percent Glide:	

Pebble Count,

Note: **Dulla Thoroughfare (Upstream Reach)**

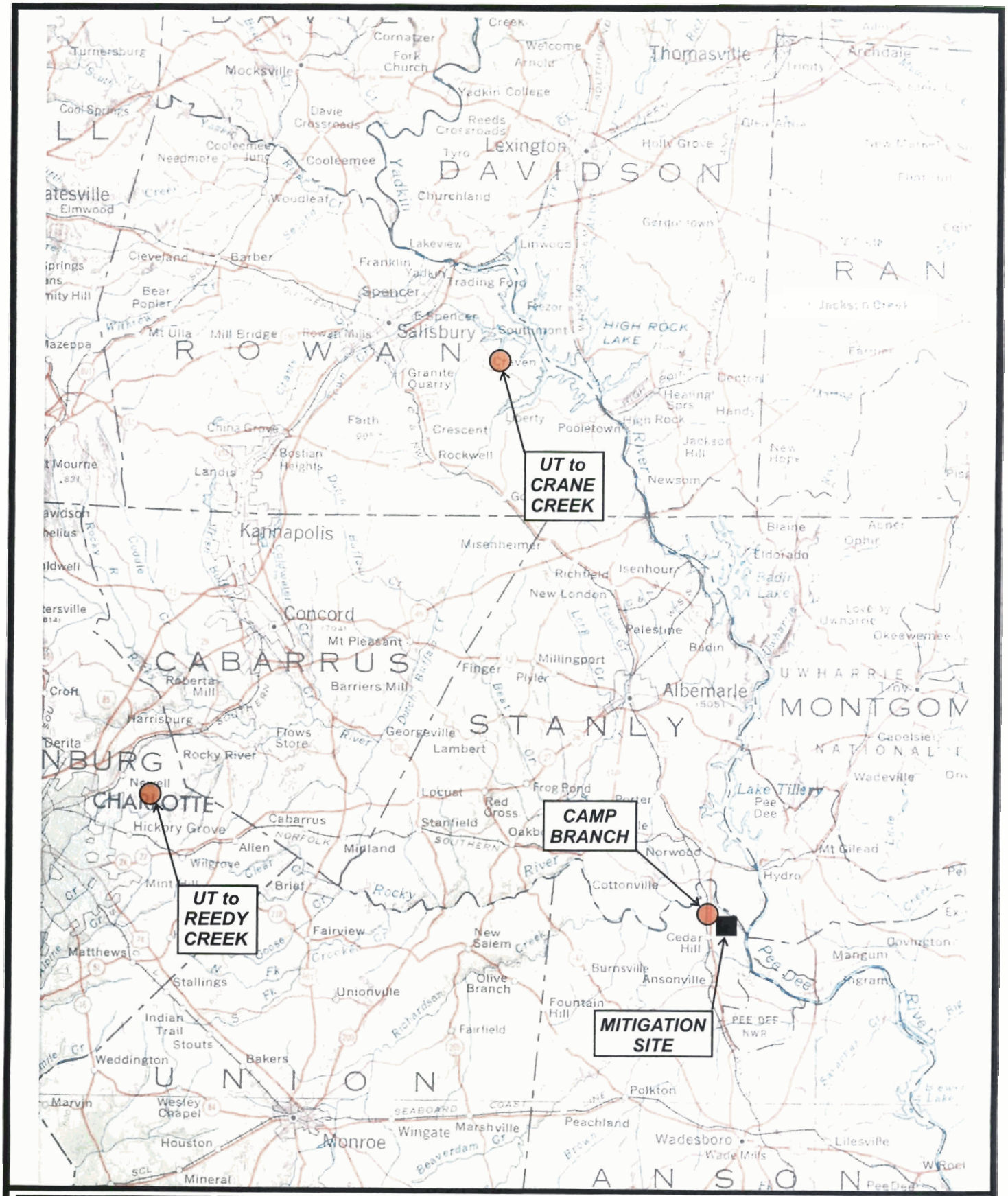
Material	Size Range (mm)		Total #	
silt/clay	0	0.062	48.9	#
very fine sand	0.062	0.13	0.0	#
fine sand	0.13	0.25	0.0	#
medium sand	0.25	0.5	0.0	#
coarse sand	0.5	1	0.0	#
very coarse sand	1	2	7.5	#
very fine gravel	2	4	8.5	#
fine gravel	4	6	1.2	#
fine gravel	6	8	12.1	#
medium gravel	8	11	9.8	#
medium gravel	11	16	4.9	#
coarse gravel	16	22	1.2	#
coarse gravel	22	32	0.0	#
very coarse gravel	32	45	1.2	#
very coarse gravel	45	64	1.2	#
small cobble	64	90	0.0	#
medium cobble	90	128	0.0	#
large cobble	128	180	0.0	#
very large cobble	180	256	0.0	#
small boulder	256	362	0.0	#
small boulder	362	512	0.0	#
medium boulder	512	1024	0.0	#
large boulder	1024	2048	0.0	#
very large boulder	2048	4096	0.0	#
bedrock			3.6	#
		Weighted Count:	100	
		True Total Particle Count:	62	



Size percent less than (mm)					Percent by substrate type					
D16	D35	D50	D84	D95	silt/clay	sand	gravel	cobble	boulder	bedrock
#N/A	#N/A	#N/A	9	15	49%	8%	40%	0%	0%	4%

APPENDIX D

REFERENCE DATA

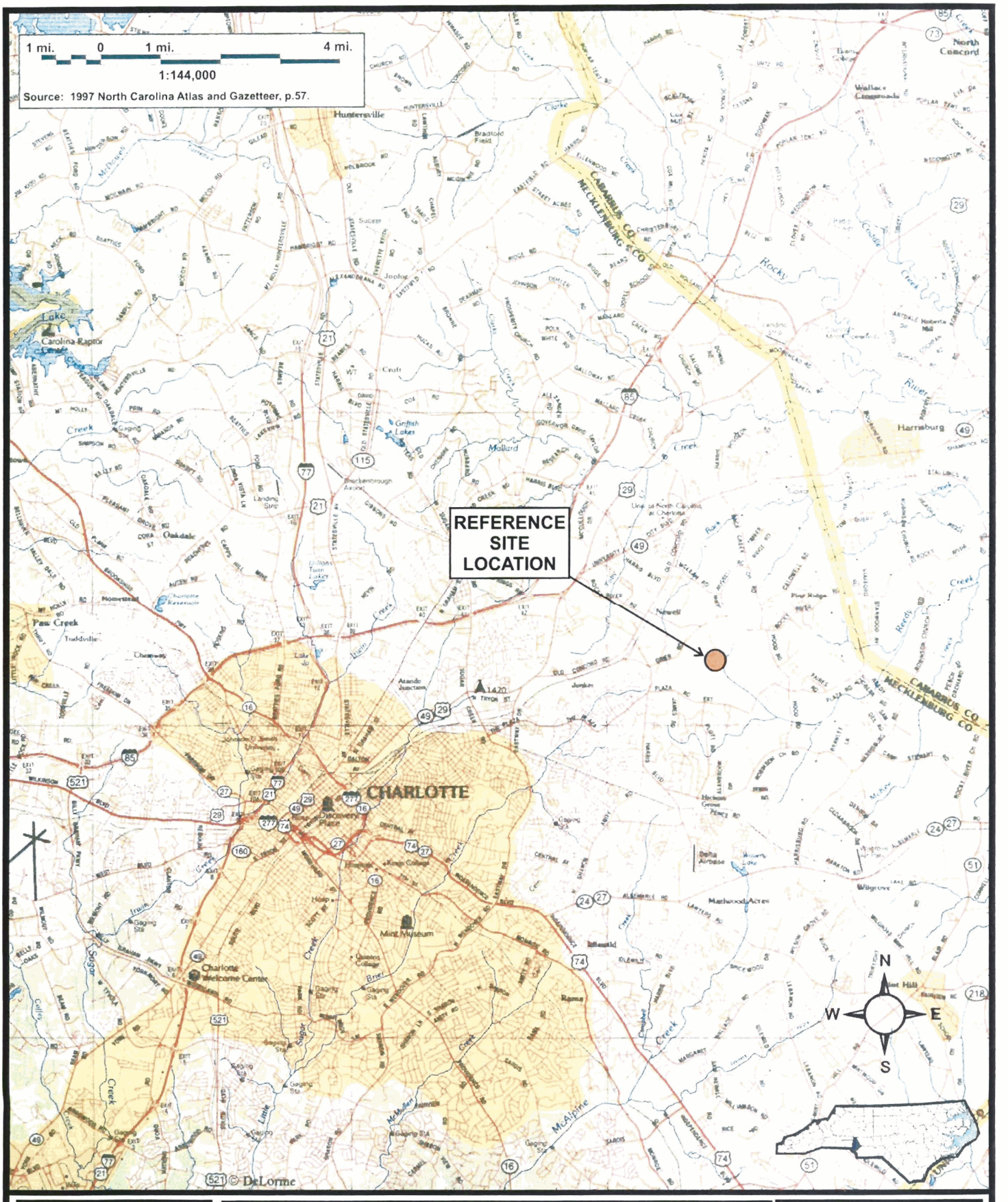


EcoScience Corporation
Raleigh, North Carolina

REFERENCE SITE LOCATIONS
Bishop Site
DETAILED MITIGATION STUDIES
Anson County, North Carolina

Dwn. by:	MAF
Ckd by:	WGL
Date:	July 2004
Project:	02-0113.34

APPENDIX
Figure
1



EcoScience Corporation
Raleigh, North Carolina

UT to REEDY CREEK
Reference Site
Mecklenburg County, North Carolina

Dwn. by:	MAF
Ckd by:	WGL
Date:	July 2004
Project:	02-113.34

APPENDIX
Figure
2A

Idlers: Reedy Creek Nature Preserve

Regional Curve Data

DA	A	W	D	Q
0.4	11.5 ft²	9.5 ft	1.2 ft	45.9 cfs

Helms! Reedy Creek Nature Park
Reference Dimension

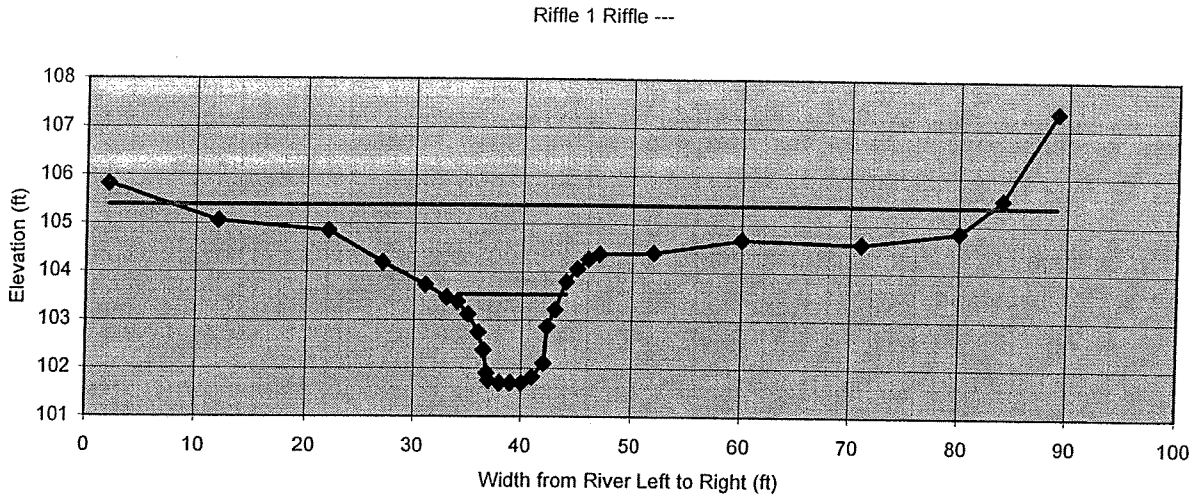
Riffles

X Sect #	A Bkfl	W Bkfl	D Ave	Pmax	W/D	FPA	Ent. Ratio	LBH	BHR	Dmax/Dave	Stream Type
1	11.8	9.6	1.2	1.8	8	70.5	7.4	1.8	1.0	1.5	E
2	17.1	10.4	1.6	2.2	6	58	5.6	2.6	1.2	1.4	E
3	15.5	11.2	1.4	2.2	8	42	3.7	2.0	1.0	1.6	E
Ave	14.8	10.4	1.4	2.1	7	56.8	5.6	2.1	1.1	1.4	
Comm	15.5	10.4	1.4	2.2	8	58	5.6	2.0	1.0	1.4	

Pools

X-Sect	A	W	Dave	Pmax	LBH	BHR
2	17.1	14.7	1.2	2.3	2.3	1.0
4	18.8	13.7	1.4	2.2	2.3	1.0
Ave	18.0	14.2	1.3	2.3	2.3	1.0

Cross Section



section: **Riffle 1**

Riffle

---

description: Reedy Creek

height of instrument (ft): **110.44**

notes	omit pt.	distance (ft)	FS (ft)	elevation
	☑	2	4.62	105.82
	☑	12	5.38	105.06
	☑	22	5.58	104.86
	☑	27	6.24	104.2
	☑	31	6.71	103.73
	☑	33	6.97	103.47
	☐	34	7.06	103.38
	☐	35	7.32	103.12
	☐	36	7.69	102.75
	☐	36.5	8.06	102.38
	☐	36.8	8.54	101.9
	☐	37	8.69	101.75
	☐	38	8.74	101.7
	☐	39	8.74	101.7
	☐	40	8.75	101.69
	☐	41	8.62	101.82
	☐	42	8.33	102.11
	☐	42.3	7.57	102.87
	☐	43	7.22	103.22
	☐	44	6.64	103.8
	☑	45	6.37	104.07
	☑	46	6.17	104.27
	☑	47	6.06	104.38
	☑	52	6.03	104.41
	☑	60	5.75	104.69
	☑	71	5.83	104.61
	☑	80	5.58	104.86
	☑	84	4.9	105.54
	☑	89	3.08	107.36
	☐			

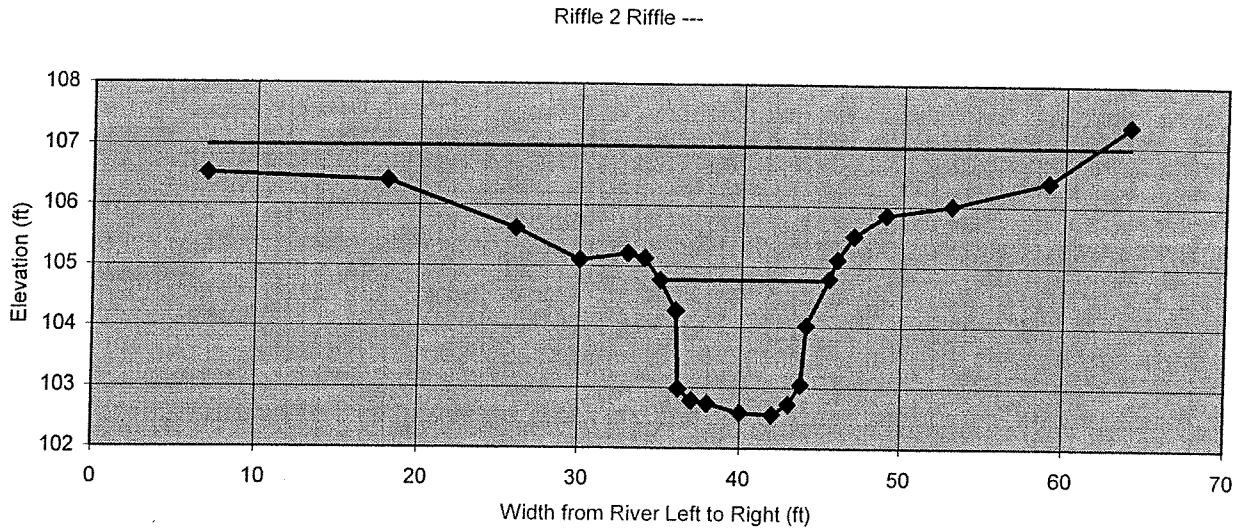
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.9	6.9	70.5		
103.54	103.54			

dimensions			
11.8	x-section area	1.2	d mean
9.6	width	10.8	wet P
1.8	d max	1.1	hyd radi
1.9	bank ht	7.8	w/d ratio
70.5	W flood prone area	7.4	ent ratio

hydraulics	
0.0	velocity (ft/sec)
0.0	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
0.000	unit stream power (lbs/ft/sec)
0.00	Froude number
0.0	friction factor u/u*
0.0	threshold grain size (mm)

check from channel material			
12	measured D84 (mm)		
30.2	relative roughness	11.3	fric. factor
0.000	Manning's n from channel material		

Cross Section



section: **Riffle 2**

Riffle

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description:

height of instrument (ft): **111.72**

notes	omit pt	distance (ft)	FS (ft)	elevation
	✓	7	5.2	106.52
	✓	18	5.32	106.4
	✓	26	6.1	105.62
	✓	30	6.62	105.1
	✓	33	6.51	105.21
	✓	34	6.59	105.13
		35	6.95	104.77
		36	7.45	104.27
		36.2	8.74	102.98
		37	8.93	102.79
		38	8.98	102.74
		40	9.13	102.59
		42	9.16	102.56
		43	8.99	102.73
		43.8	8.67	103.05
		44.1	7.7	104.02
		45.5	6.92	104.8
	✓	46	6.6	105.12
	✓	47	6.21	105.51
	✓	49	5.86	105.86
	✓	53	5.71	106.01
	✓	59	5.31	106.41
	✓	64	4.38	107.34

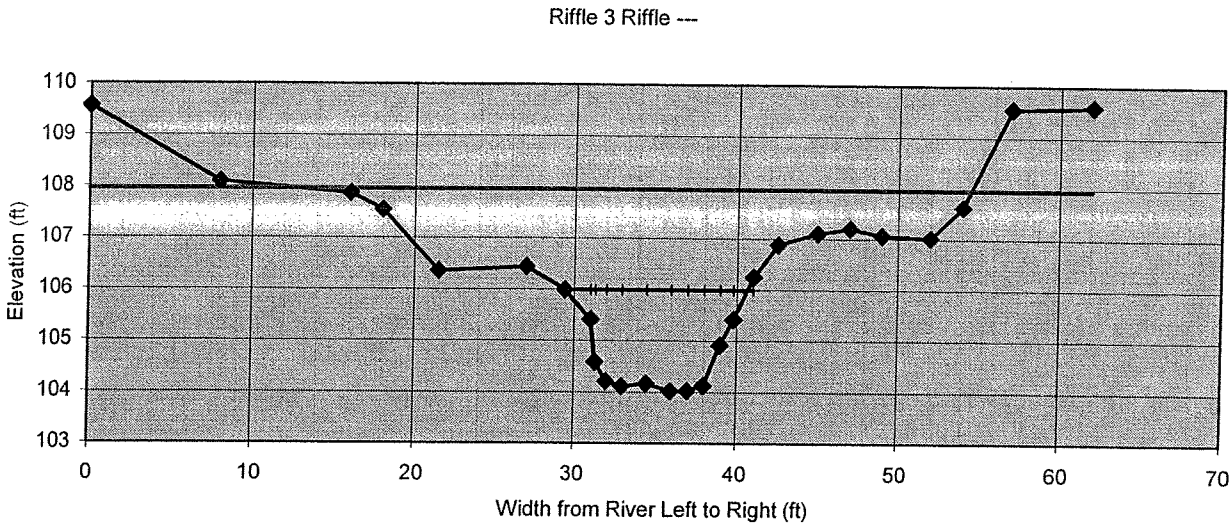
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.95	6.59	58.0		
104.77	105.13			

dimensions			
17.1	x-section area	1.6	d mean
10.4	width	12.7	wet P
2.2	d max	1.3	hyd radi
2.6	bank ht	6.4	w/d ratio
58.0	W flood prone area	5.6	ent ratio

hydraulics	
0.0	velocity (ft/sec)
0.0	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
0.000	unit stream power (lbs/ft/sec)
0.00	Froude number
0.0	friction factor u/u*
0.0	threshold grain size (mm)

check from channel material			
12	measured D84 (mm)		
40.2	relative roughness	12.0	fric. factor
0.000	Manning's n from channel material		

Cross Section



section:	Riffle 3
	Riffle

	---
description:	
height of instrument (ft):	112.42

notes	omit pt	distance (ft)	FS (ft)	elevation
	✓	0	2.85	109.57
	✓	8	4.32	108.1
	✓	16	4.55	107.87
	✓	18	4.87	107.55
	✓	21.5	6.06	106.36
	✓	27	5.98	106.44
		29.4	6.43	105.99
		31	7.01	105.41
		31.3	7.83	104.59
		32	8.21	104.21
		33	8.3	104.12
		34.5	8.25	104.17
		36	8.4	104.02
		37	8.39	104.03
		38	8.29	104.13
		39	7.5	104.92
		39.8	7	105.42
		41	6.17	106.25
	✓	42.5	5.53	106.89
	✓	45	5.31	107.11
	✓	47	5.21	107.21
	✓	49	5.35	107.07
	✓	52	5.39	107.03
	✓	54	4.79	107.63
	✓	57	2.86	109.56
	✓	62	2.82	109.6

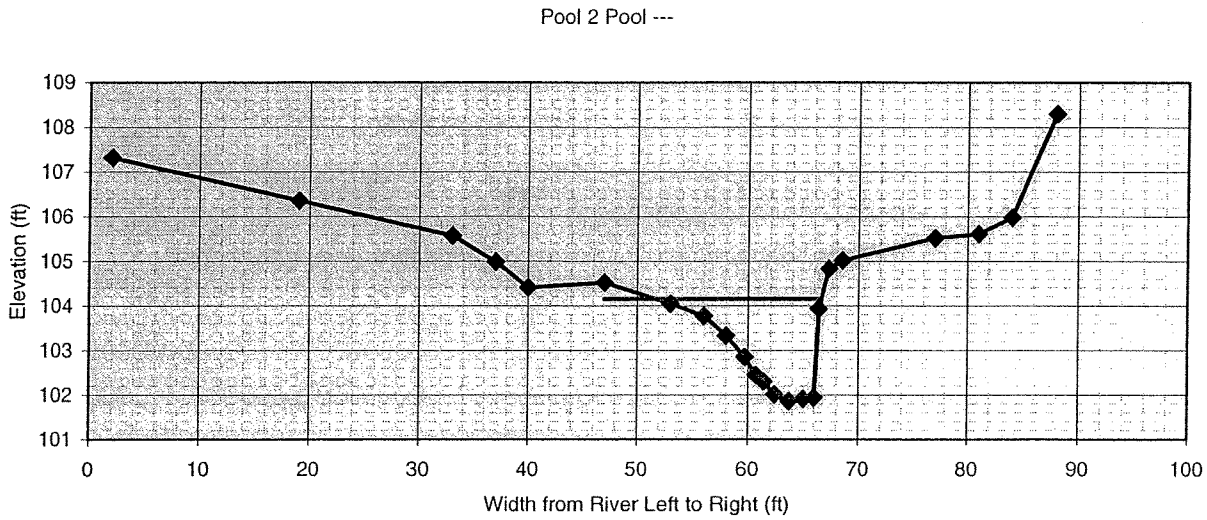
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.43	6.43	42.0	0.0029	0.034
105.99	105.99			

dimensions			
15.5	x-section area	1.4	d mean
11.2	width	12.6	wet P
2.0	d max	1.2	hyd radi
2.0	bank ht	8.1	w/d ratio
42.0	W flood prone area	3.7	ent ratio

hydraulics	
0.3	velocity (ft/sec)
4.2	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.03	shear velocity (ft/sec)
0.001	unit stream power (lbs/ft/sec)
0.00	Froude number
8.0	friction factor u/u*
0.1	threshold grain size (mm)

check from channel material			
12	measured D84 (mm)		
34.0	relative roughness	11.6	fric. factor
0.024	Manning's n from channel material		

Cross Section



section:	Pool 2
	Pool --- ---
description:	
height of instrument (ft):	111.05

notes	omit pt.	distance (ft)	FS (ft)	elevation
	# ☑ #	2	3.73	107.32
	# ☑ #	19	4.69	106.36
	# ☑ #	33	5.48	105.57
	# ☑ #	37	6.07	104.98
	# ☑ #	40	6.64	104.41
	# ☐ #	47	6.53	104.52
	# ☐ #	53	7	104.05
	# ☐ #	56	7.28	103.77
	# ☐ #	58	7.72	103.33
	# ☐ #	59.7	8.2	102.85
	# ☐ #	60.7	8.6	102.45
	# ☐ #	61.4	8.75	102.3
	# ☐ #	62.4	9.04	102.01
	# ☐ #	63.7	9.19	101.86
	# ☐ #	65	9.14	101.91
	# ☐ #	66	9.11	101.94
	# ☐ #	66.4	7.12	103.93
	# ☑ #	67.3	6.22	104.83
	# ☑ #	68.5	6.03	105.02
	# ☑ #	77	5.53	105.52
	# ☑ #	81	5.44	105.61
	# ☑ #	84	5.07	105.98
	# ☑ #	88	2.75	108.3
	# ☐ #			

☐

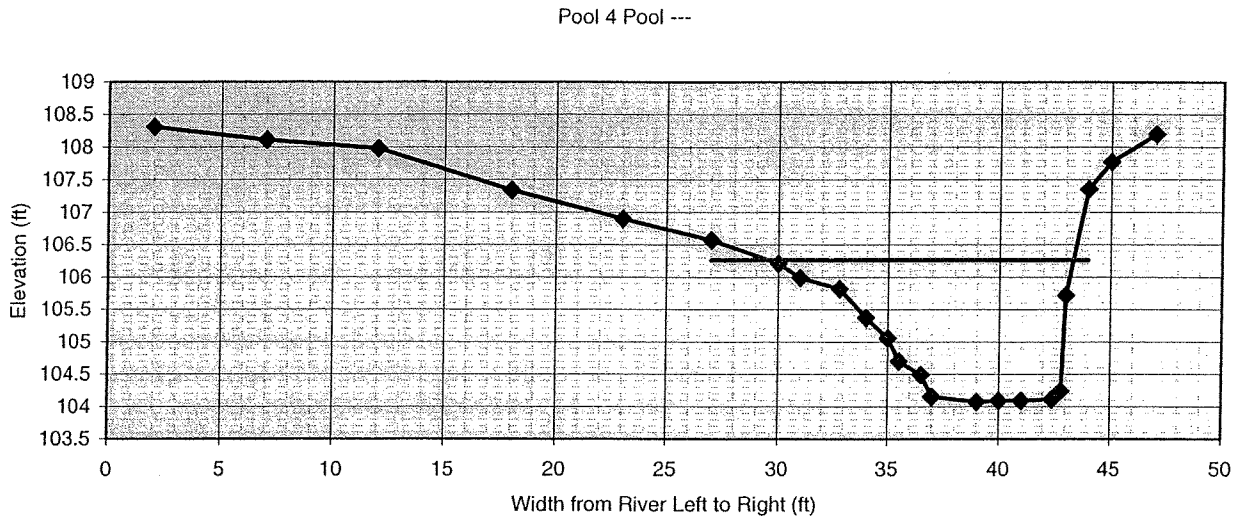
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.9	6.9			
104.15	104.15			

dimensions			
17.1	x-section area	1.2	d mean
14.7	width	16.6	wet P
2.3	d max	1.0	hyd radi
2.3	bank ht	~~12.6~~	w/d ratio
~~0.0~~	W flood prone area	~~0.0~~	ent ratio

hydraulics	
~~0.0~~	velocity (ft/sec)
~~0.0~~	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
~~0.000~~	unit stream power (lbs/ft/sec)
~~0.00~~	Froude number
~~0.0~~	friction factor u/u*
~~0.0~~	threshold grain size (mm)

check from channel material			
~~12~~	measured D84 (mm)		
~~28.6~~	relative roughness	~~11.1~~	fric. factor
~~0.000~~	Manning's n from channel material		

Cross Section



section:	Pool 4
	Pool --- ---
description:	
height of instrument (ft):	113.51

notes	omit pt.	distance (ft)	FS (ft)	elevation
	# ☑ #	2	5.2	108.31
	# ☑ #	7	5.4	108.11
	# ☑ #	12	5.53	107.98
	# ☑ #	18	6.17	107.34
	# ☑ #	23	6.61	106.9
	# ☐ #	27	6.94	106.57
	# ☐ #	30	7.3	106.21
	# ☐ #	31	7.52	105.99
	# ☐ #	32.8	7.69	105.82
	# ☐ #	34	8.14	105.37
	# ☐ #	35	8.45	105.06
	# ☐ #	35.5	8.81	104.7
	# ☐ #	36.5	9.02	104.49
	# ☐ #	37	9.36	104.15
	# ☐ #	39	9.44	104.07
	# ☐ #	40	9.42	104.09
	# ☐ #	41	9.42	104.09
	# ☐ #	42.4	9.4	104.11
	# ☐ #	42.8	9.27	104.24
	# ☐ #	43	7.79	105.72
	# ☐ #	44	6.16	107.35
	# ☑ #	45	5.74	107.77
	# ☑ #	47	5.31	108.2
	# ☐ #			

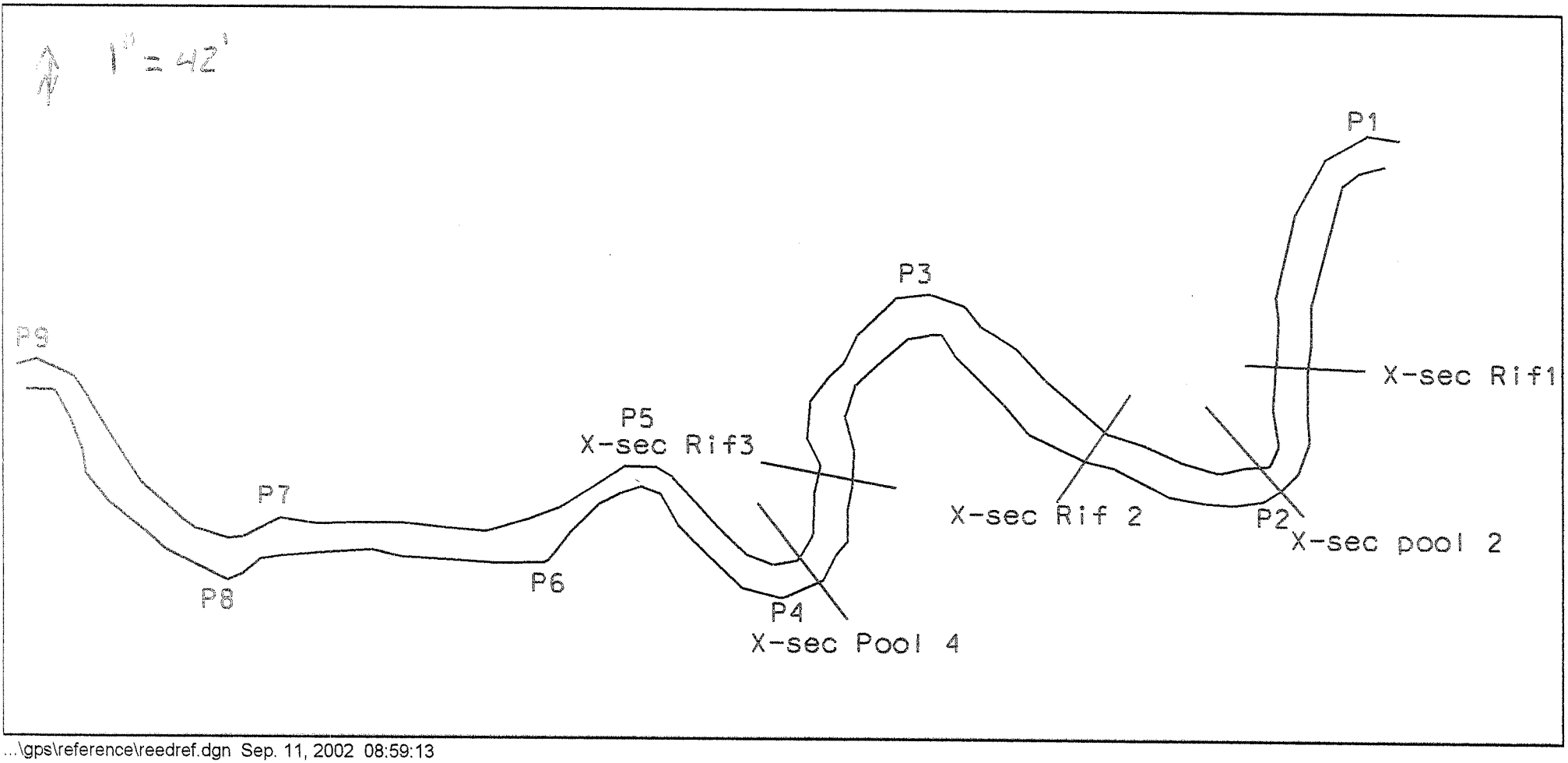
☐

FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
7.25	6.16			
106.26	107.35			

dimensions			
18.8	x-section area	1.4	d mean
13.7	width	15.8	wet P
2.2	d max	1.2	hyd radi
3.3	bank ht	~~10.0~~	w/d ratio
~~0.0~~	W flood prone area	~~0.0~~	ent ratio

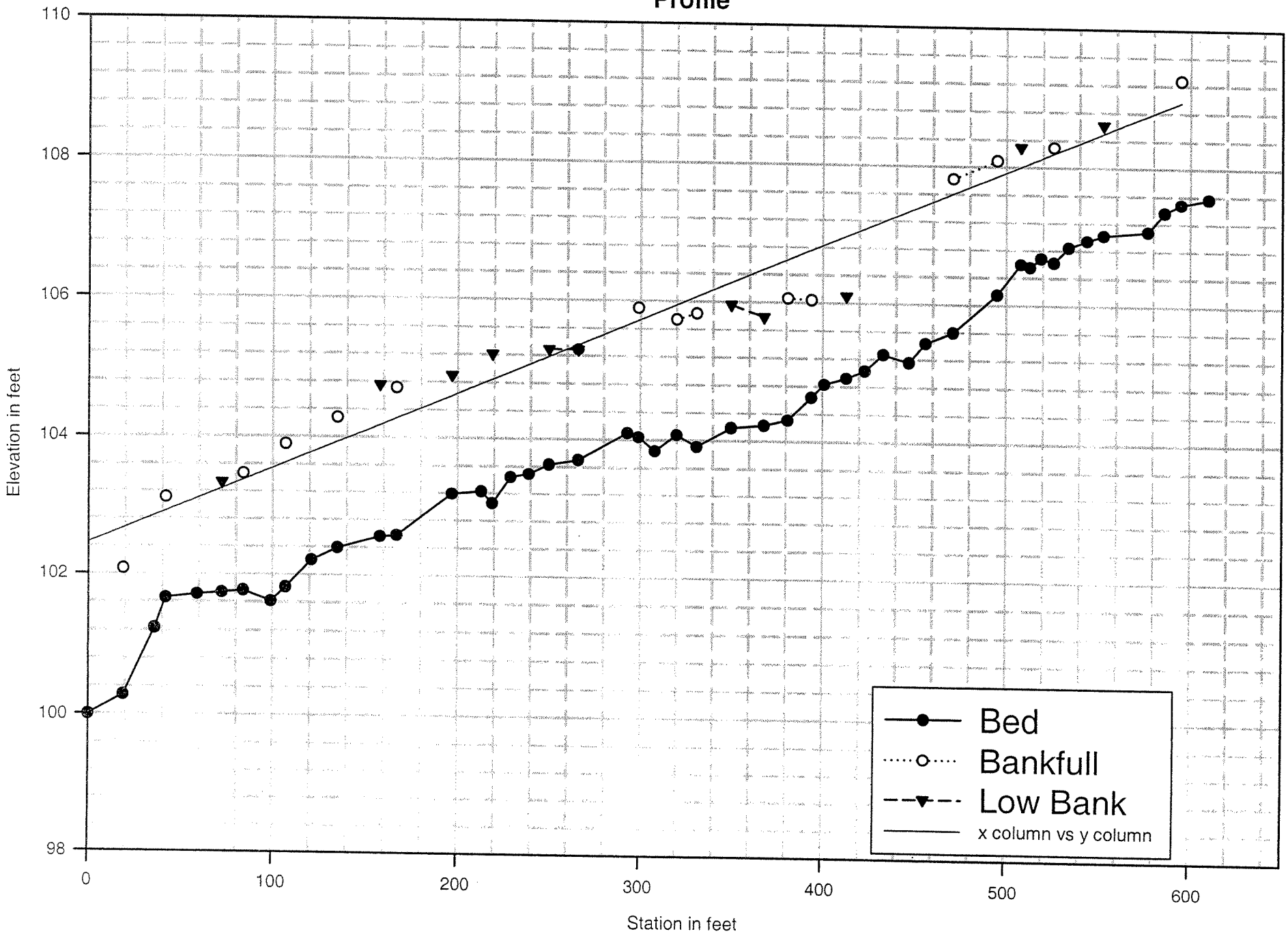
hydraulics	
~~0.0~~	velocity (ft/sec)
~~0.0~~	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
~~0.000~~	unit stream power (lbs/ft/sec)
~~0.00~~	Froude number
~~0.0~~	friction factor u/u*
~~0.0~~	threshold grain size (mm)

check from channel material			
~~12~~	measured D84 (mm)		
~~33.7~~	relative roughness	~~11.5~~	fric. factor
~~0.000~~	Manning's n from channel material		



...\gps\reference\reedref.dgn Sep. 11, 2002 08:59:13

Reedy Creek Nature Park
Reference Stream
Profile



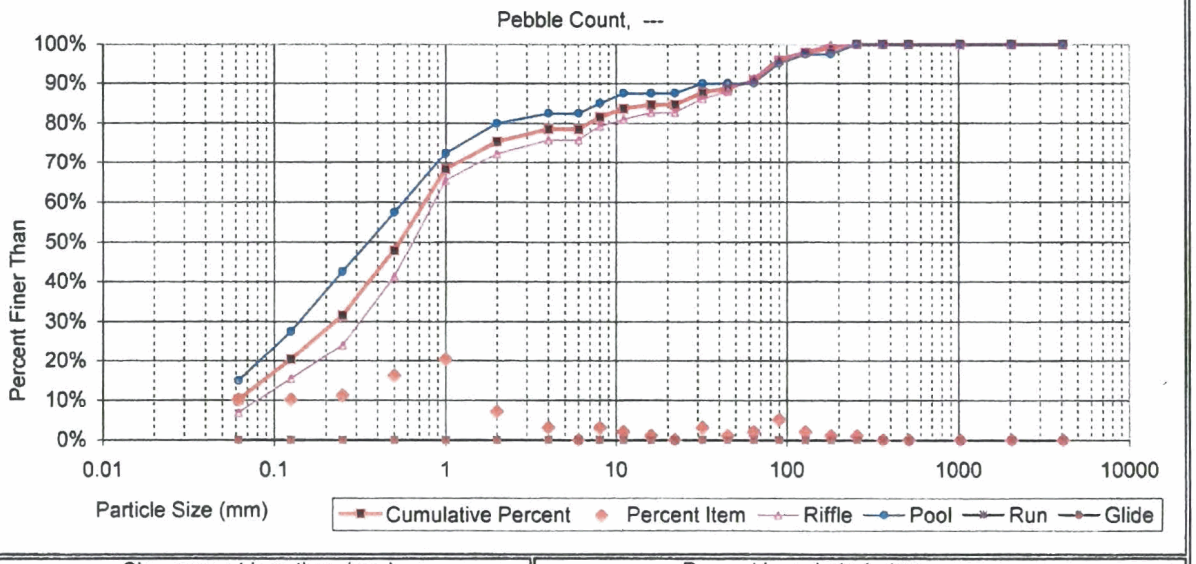
Weighted Pebble Count

Percent Riffle:	60	Percent Run:	0
Percent Pool:	40	Percent Glide:	0

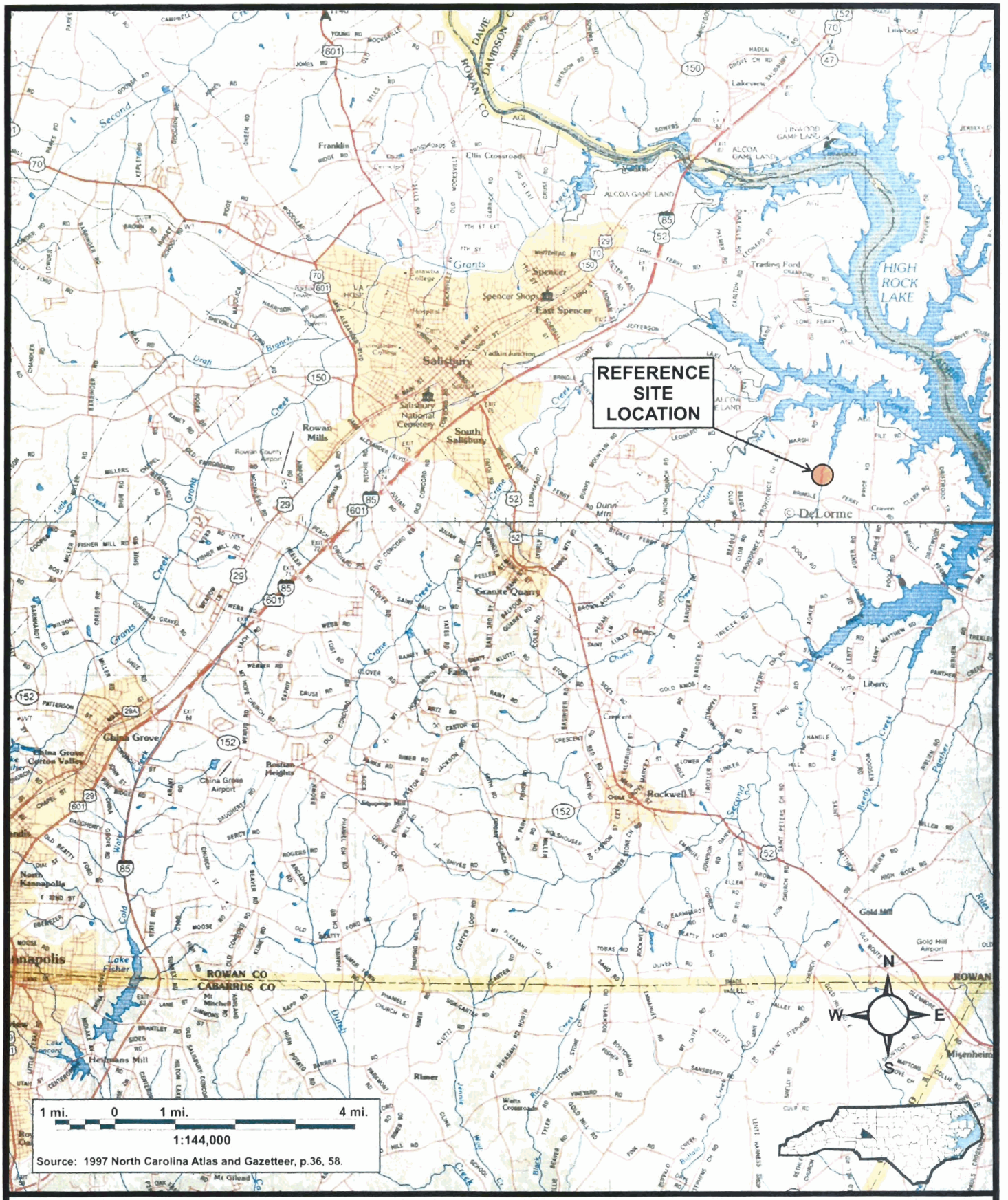
Pebble Count,

Material	Size Range (mm)		Total #	
silt/clay	0	0.062	10.0	#
very fine sand	0.062	0.13	10.0	#
fine sand	0.13	0.25	11.0	#
medium sand	0.25	0.5	16.0	#
coarse sand	0.5	1	20.0	#
very coarse sand	1	2	7.0	#
very fine gravel	2	4	3.0	#
fine gravel	4	6	0.0	#
fine gravel	6	8	3.0	#
medium gravel	8	11	2.0	#
medium gravel	11	16	1.0	#
coarse gravel	16	22	0.0	#
coarse gravel	22	32	3.0	#
very coarse gravel	32	45	1.0	#
very coarse gravel	45	64	2.0	#
small cobble	64	90	5.0	#
medium cobble	90	128	2.0	#
large cobble	128	180	1.0	#
very large cobble	180	256	1.0	#
small boulder	256	362	0.0	#
small boulder	362	512	0.0	#
medium boulder	512	1024	0.0	#
large boulder	1024	2048	0.0	#
very large boulder	2048	4096	0.0	#
bedrock			2.0	#
		Weighted Count:	100	
		True Total Particle Count:	100	

Note: **Reedy Creek Composite Pebble Count**



Size percent less than (mm)					Percent by substrate type					
D16	D35	D50	D84	D95	silt/clay	sand	gravel	cobble	boulder	bedrock
0.092	0.29	0.5	12	85	10%	64%	15%	9%	0%	2%



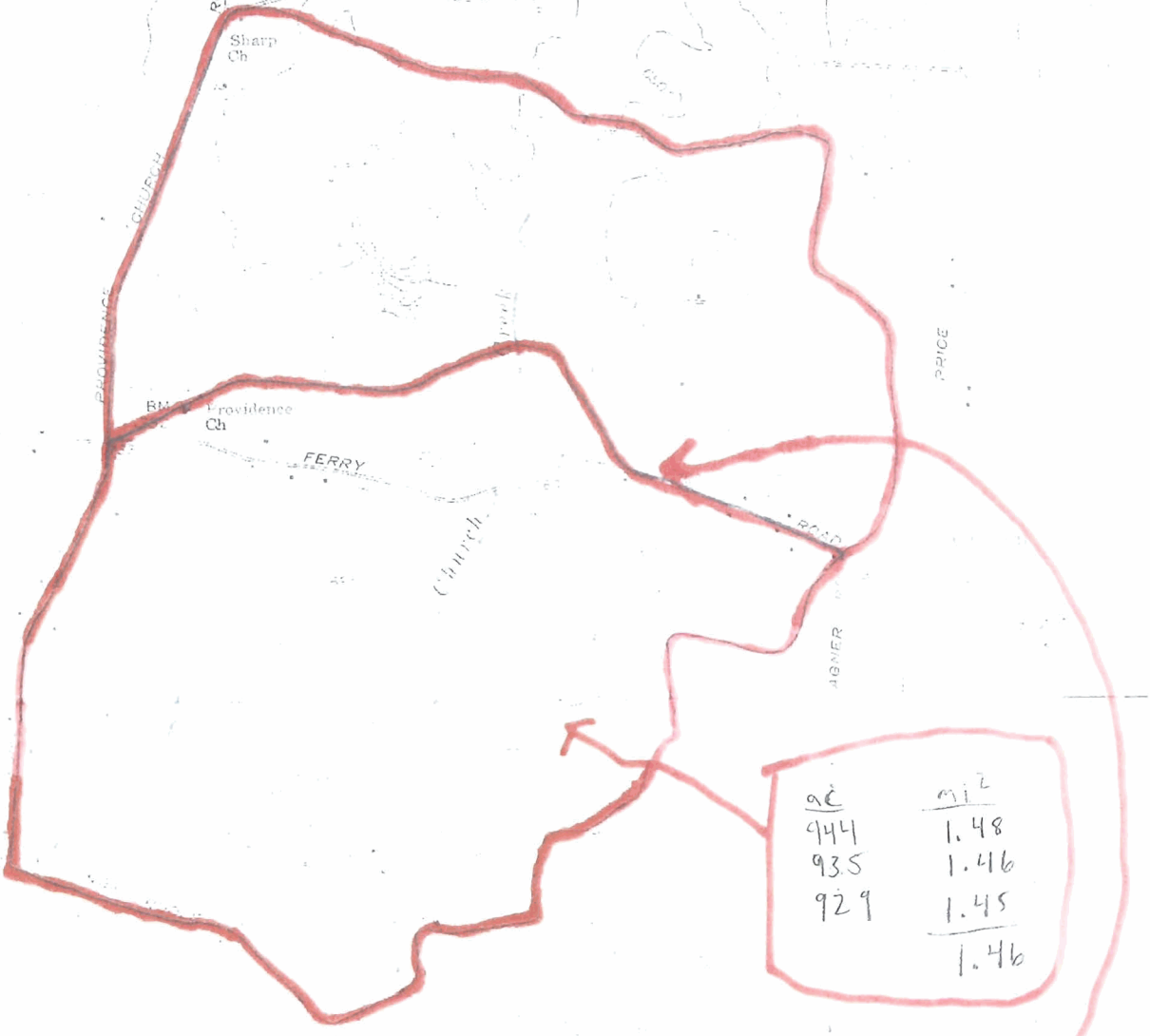
EcoScience Corporation
Raleigh, North Carolina

UT to CRANE CREEK
Reference Site
Rowan County, North Carolina

Dwn. by:	MAF
Ckd by:	WGL
Date:	July 2004
Project:	02-113.34

APPENDIX
Figure
2B

DAN NICHOLAS PARK - HELMS REFERENCE
REGIONAL CURVE DATA
UT TO CRANE CREEK



ac	mi²
944	1.48
935	1.46
929	1.45
	1.46

ac	mi²
1621	2.53
1624	2.54
1625	2.54
	2.5

DA	A	W	D	Q
1.5	28.2 ft²	16.0 ft	1.8 ft	119 cfs
2.5	39.8 ft²	19.5 ft	2.0 ft	173 cfs
1.46	27.7	15.8 ft	1.8	117 cfs

Helms: Dan Nicholas Park (UT to Crane Cr.)

Reference Dimension

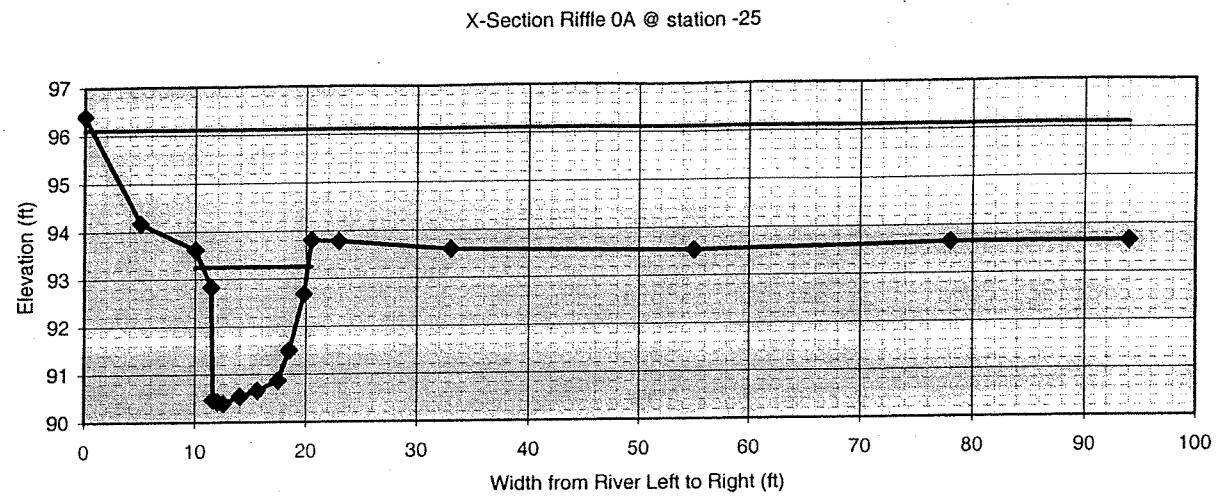
Riffles

X Sec #	A BKFL	W BKFL	Dave	Dmay	w/D	FPA	Ent Ratio	Low Bank Height	Bank Height Ratio	Dmax/Dave	Stream Type
A	19.8	9.5	2.1	2.9	4.5	237	25.0	3.2	1.1	1.4	E
B	25.0	11.9	2.1	2.6	5.7	237	20.0	3.1	1.2	1.2	E
	20.5	10.1	2.0	2.5	5.1	232	23.0	2.9	1.2	1.3	E
	19.3	10.0	1.9	2.5	5.3	345	34.5	3.1	1.2	1.3	E
	21.2	10.4	2.0	2.6	5.2	263	25.6	3.1	1.2	1.3	
2	20.5	10.1	2.0	2.6	5.1	237	25.0	3.1	1.2	1.3	E
ge	19.3-25.0	9.5-11.9	1.9-2.1	2.5-2.9	4.5-5.7	232-345	20.0-34.5	2.9-3.2	1.1-1.2	1.2-1.4	

Pools

Project	A BKFL	W BKFL	Dave	Dmax	LBH	BHR	Dmax/Dave	L Pool
	20.6	11.7	1.8	2.8	3.3	1.2	1.6	
A	19.5	10.5	1.9	3.0	4.0	1.3	1.6	
	20.1	11.1	1.9	2.9	3.7	1.3	1.6	
AN	19.5	11.7	1.9	3.0	4.0	1.7	1.6	

Cross Section



section: **X-Section Riffle 0A**

Riffle

---

description:

height of instrument (ft): **99.76**

notes	omit pt.	distance (ft)	FS (ft)	elevation
FP extends	☑	0	3.36	96.4
	☑	5	5.58	94.18
TOB	☐	10	6.14	93.62
	☐	11.4	6.93	92.83
	☐	11.6	9.29	90.47
	☐	12	9.33	90.43
thalweg	☐	12.5	9.37	90.39
	☐	14	9.22	90.54
water eleva	☐	15.6	9.1	90.66
	☐	17.5	8.89	90.87
	☐	18.5	8.26	91.5
	☐	19.8	7.08	92.68
TOB	☐	20.5	5.95	93.81
	☑	23	5.98	93.78
	☑	33	6.16	93.6
	☑	55	6.23	93.53
	☑	78	6.1	93.66
	☑	94	6.1	93.66
up steepist	☐			
	☐			
stk: 3.95	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			

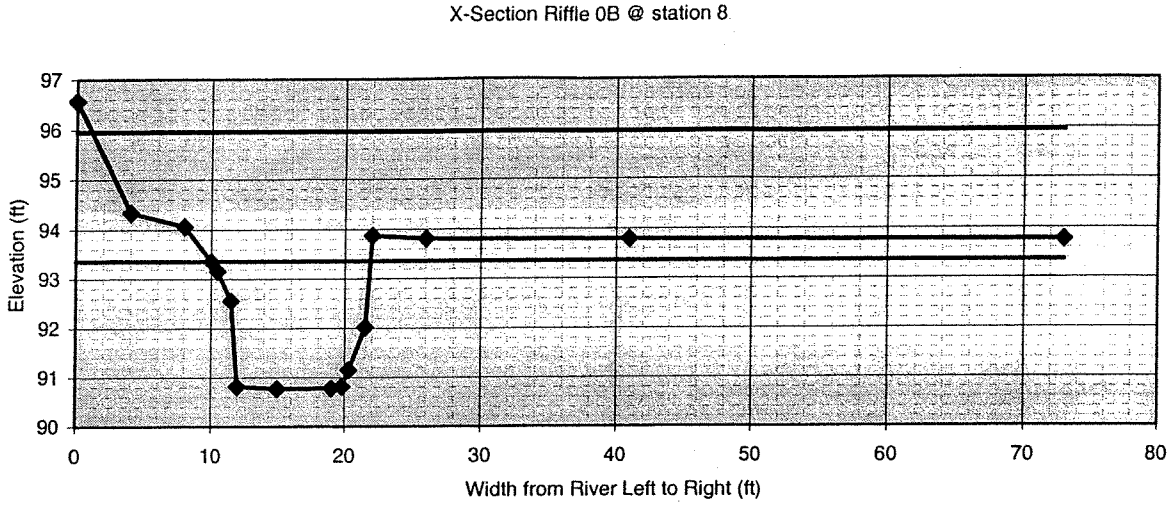
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.51	6.14	16.0		
93.25	93.62			

dimensions			
19.8	x-section area	2.1	d mean
9.5	width	12.8	wet P
2.9	d max	1.6	hyd radi
3.2	bank ht	4.5	w/d ratio
~~16.0~~	W flood prone area	~~17~~	ent ratio
237		25	

hydraulics	
0.0	velocity (ft/sec)
0.0	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
0.000	unit stream power (lbs/ft/sec)
0.00	Froude number
0.0	friction factor u/u*
~~0.0~~	threshold grain size (mm)

check from channel material			
0	measured D84 (mm)		
0.0	relative roughness	0.0	fric. factor
0.000	Manning's n from channel material		

Cross Section



section: **X-Section Riffle 0B**

Riffle

---

description:

height of instrument (ft): **99.77**

notes	omit pt.	distance (ft)	FS (ft)	elevation
up steep	☐	0	3.2	96.57
	☐	4	5.43	94.34
	☐	8	5.71	94.06
bankfull	☐	10	6.41	93.36
	☐	10.5	6.61	93.16
	☐	11.5	7.21	92.56
	☐	12	8.95	90.82
	☐	15	9	90.77
water depth	☐	19	8.99	90.78
water edge	☐	19.8	8.95	90.82
	☐	20.3	8.62	91.15
	☐	21.5	7.75	92.02
TOB	☐	22	5.9	93.87
	☐	26	5.96	93.81
	☐	41	5.98	93.79
	☐	73	6	93.77
	☐			
stk: 3.94	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			
	☐			

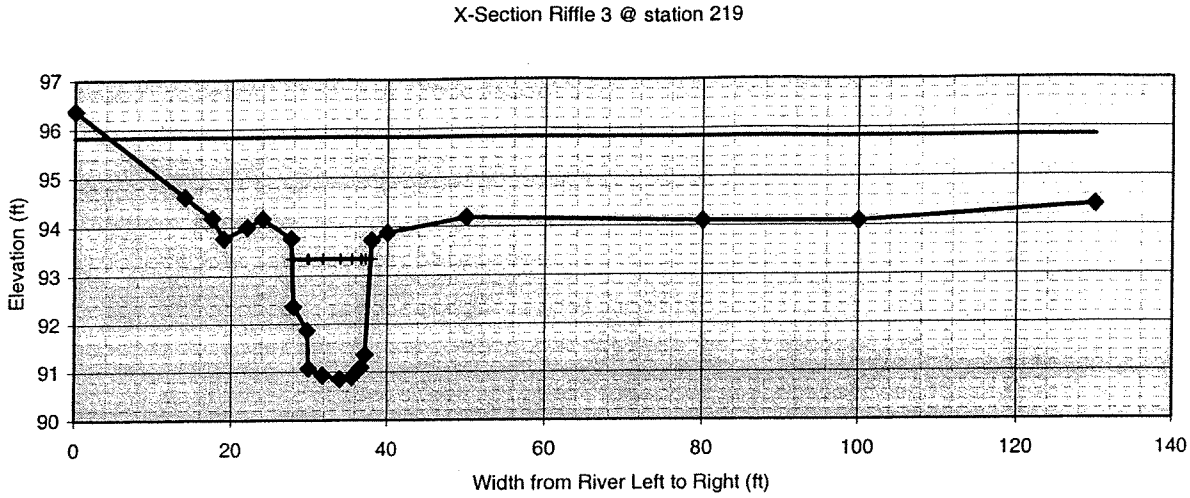
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.41	5.9			
93.36	93.87			

dimensions			
25.0	x-section area	2.1	d mean
11.9	width	14.8	wet P
2.6	d max	1.7	hyd radi
3.1	bank ht	5.6	w/d ratio
~~0.0~~	W flood prone area	~~0.0~~	ent ratio
23.1		20.0	

hydraulics	
0.0	velocity (ft/sec)
0.0	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
0.000	unit stream power (lbs/ft/sec)
0.00	Froude number
0.0	friction factor u/u*
~~0.0~~	threshold grain size (mm)

check from channel material			
0	measured D84 (mm)		
0.0	relative roughness	0.0	fric. factor
0.000	Manning's n from channel material		

Cross Section



section: **X-Section Riffle 3**

Riffle

---

description:

height of instrument (ft): **100.14**

notes	omit pt.	distance (ft)	FS (ft)	elevation
up steep	☑	0	3.77	96.37
	☑	14	5.52	94.62
	☑	17.5	5.95	94.19
	☑	19	6.37	93.77
	☑	22	6.14	94
	☑	24	5.97	94.17
TOB	☐	27.7	6.38	93.76
MB	☐	28	7.78	92.36
MB	☐	29.8	8.27	91.87
	☐	30	9.07	91.07
EOW	☐	31.8	9.21	90.93
thawleg	☐	34	9.29	90.85
	☐	35.5	9.25	90.89
	☐	36.7	9.05	91.09
MB	☐	37.2	8.78	91.36
TOB	☐	38	6.42	93.72
	☑	40	6.26	93.88
	☑	50	5.96	94.18
	☑	80	6.04	94.1
	☑	100	6.05	94.09
	☑	130	5.73	94.41
FP extends	☐			
	☐			
stk: 4.30	☐			
	☐			
	☐			
	☐			
	☐			

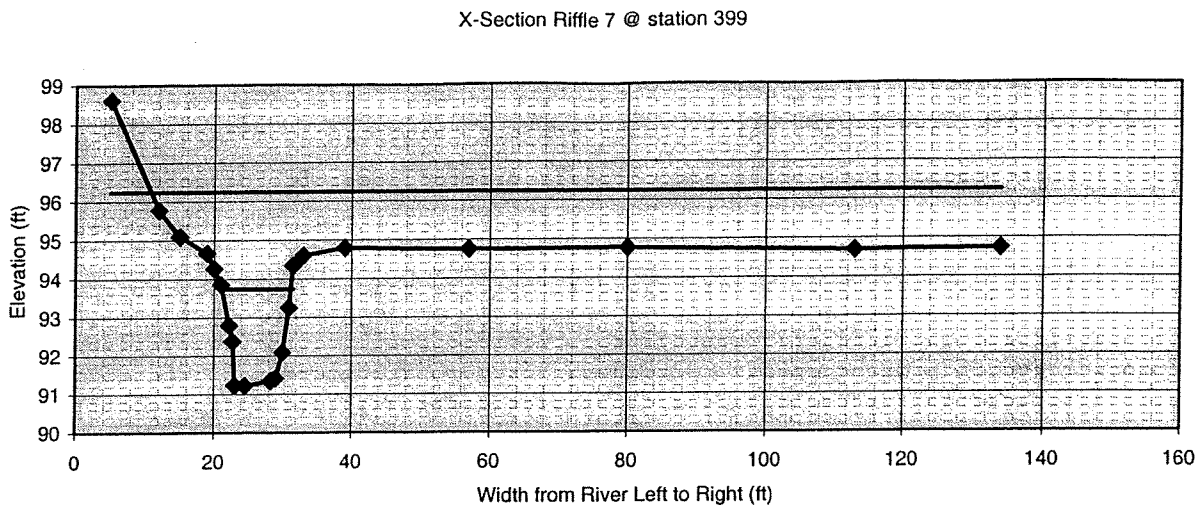
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.8	**6.42**	**150.0**		**0.034**
93.34	93.72			

dimensions			
20.5	x-section area	2.0	d mean
10.1	width	13.1	wet P
2.5	d max	1.6	hyd radi
2.9	bank ht	5.0	w/d ratio
~~150.0~~ 232.0	W flood prone area	~~14.9~~ 23.0	ent ratio

hydraulics	
0.0	velocity (ft/sec)
0.0	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
0.000	unit stream power (lbs/ft/sec)
0.00	Froude number
0.0	friction factor u/u*
~~0.0~~	threshold grain size (mm)

check from channel material			
0	measured D84 (mm)		
0.0	relative roughness	0.0	fric. factor
0.000	Manning's n from channel material		

Cross Section



section: **X-Section Riffle 7**

Riffle

---

description:

height of instrument (ft): **100.76**

notes	omit pt.	distance (ft)	FS (ft)	elevation
up steep	☑	5	2.14	98.62
	☑	12	4.98	95.78
	☑	15	5.66	95.1
	☑	19	6.09	94.67
	☑	20	6.49	94.27
	☐	21	6.91	93.85
	☐	22.2	7.97	92.79
	☐	22.7	8.38	92.38
EOW: depl	☐	23	9.53	91.23
	☐	24.5	9.54	91.22
EOW	☐	28.2	9.42	91.34
	☐	29	9.34	91.42
MB	☐	30	8.67	92.09
MB	☐	30.9	7.51	93.25
TOB	☐	31.5	6.42	94.34
	☑	33	6.15	94.61
	☑	39	5.96	94.8
	☑	57	6	94.76
	☑	80	5.99	94.77
	☑	113	6.06	94.7
	☑	134	6.02	94.74
	☐			
stk: 3.99	☐			
	☐			
	☐			
	☐			
	☐			
	☐			

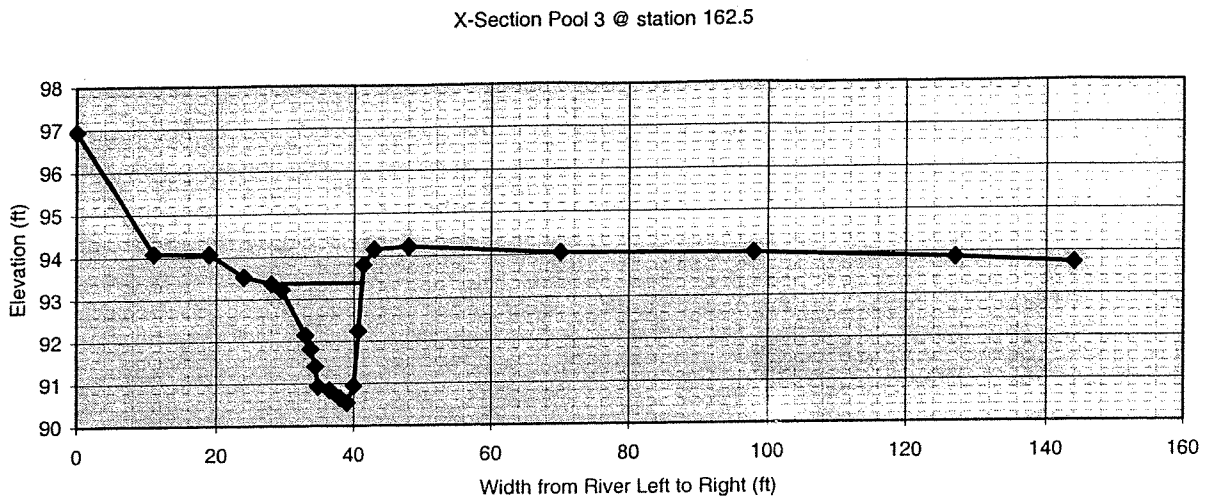
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
7.03	**6.42**	**18.5**		
93.73	94.34			

dimensions			
19.3	x-section area	1.9	d mean
10.0	width	12.5	wet P
2.5	d max	1.5	hyd radi
3.1	bank ht	5.2	w/d ratio
~~18.5~~ 345.0	W flood prone area	~~1.8~~	ent ratio

hydraulics	
0.0	velocity (ft/sec)
0.0	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
0.000	unit stream power (lbs/ft/sec)
0.00	Froude number
0.0	friction factor u/u*
~~0.0~~	threshold grain size (mm)

check from channel material			
0	measured D84 (mm)		
0.0	relative roughness	0.0	fric. factor
0.000	Manning's n from channel material		

Cross Section



section: Pool

description: ---

height of instrument (ft): 100.17

notes	omit pt.	distance (ft)	FS (ft)	elevation
up steep	☑	0	3.22	96.95
	☑	11	6.08	94.09
	☑	19	6.1	94.07
	☑	24	6.64	93.53
	☑	28	6.8	93.37
	☐	29.5	6.95	93.22
	☐	33	8.03	92.14
	☐	33.7	8.35	91.82
	☐	34.4	8.77	91.4
EOW	☐	34.8	9.24	90.93
	☐	36.5	9.33	90.84
	☐	38	9.51	90.66
thalweg	☐	39	9.63	90.54
EOW	☐	40	9.23	90.94
	☐	40.7	7.93	92.24
TOB	☐	41.4	6.37	93.8
	☑	43	6.01	94.16
	☑	48	5.95	94.22
	☑	70	6.13	94.04
	☑	98	6.16	94.01
	☑	127	6.31	93.86
	☑	144	6.44	93.73
	☐			
stk: 5.99	☐			
	☐			

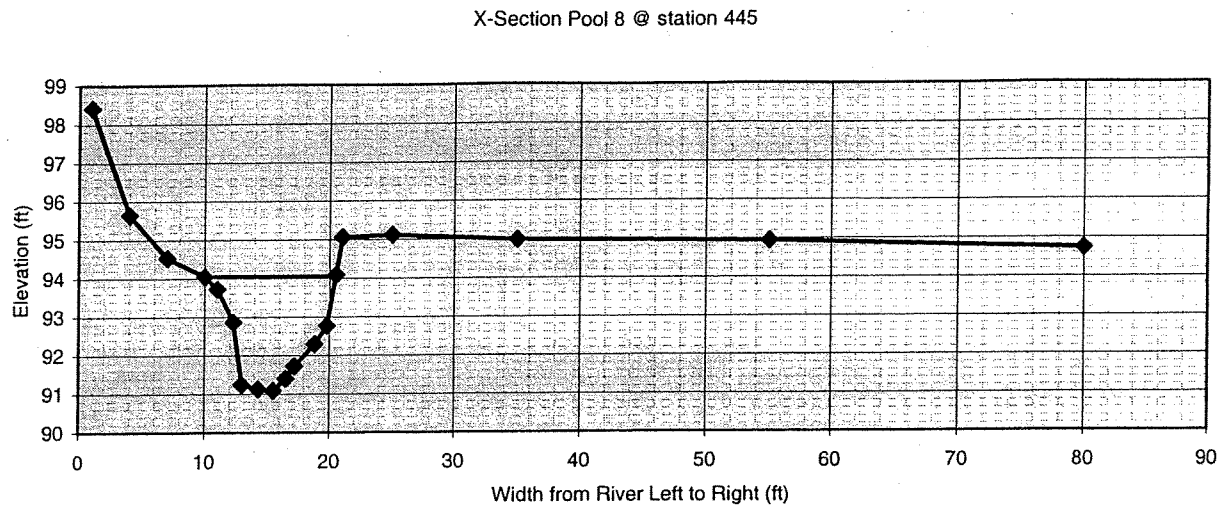
FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.8	6.37			
93.37	93.8			

dimensions			
20.6	x-section area	1.8	d mean
11.7	width	13.9	wet P
2.8	d max	1.5	hyd radi
3.3	bank ht	~~6.7~~	w/d ratio
~~0.0~~	W flood prone area	~~0.0~~	ent ratio

hydraulics	
~~0.0~~	velocity (ft/sec)
~~0.0~~	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
~~0.000~~	unit stream power (lbs/ft/sec)
~~0.00~~	Froude number
~~0.0~~	friction factor u/u*
~~0.0~~	threshold grain size (mm)

check from channel material			
~~12~~	measured D84 (mm)		
~~46.2~~	relative roughness	~~12.3~~	fric. factor
~~0.000~~	Manning's n from channel material		

Cross Section



section:	
	Pool

	---
description:	
height of instrument (ft):	101.02

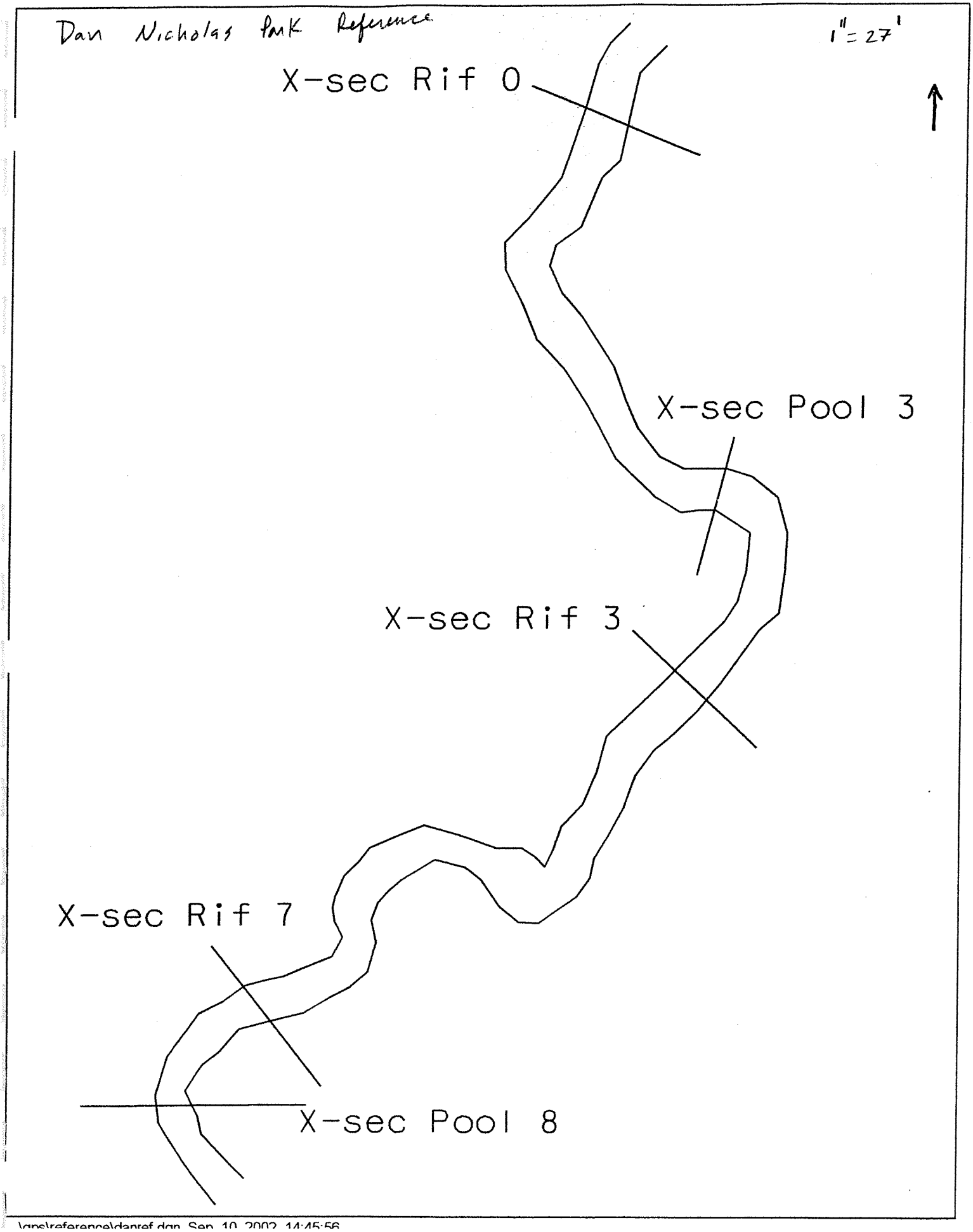
notes	omit pt.	distance (ft)	FS (ft)	elevation
up steep	☑	1	2.61	98.41
	☑	4	5.37	95.65
	☑	7	6.48	94.54
	☐	10	6.97	94.05
	☐	11	7.3	93.72
	☐	12.3	8.16	92.86
EOW: depl	☐	13	9.77	91.25
	☐	14.3	9.89	91.13
	☐	15.5	9.93	91.09
EOW	☐	16.5	9.62	91.4
	☐	17.2	9.29	91.73
	☐	18.8	8.72	92.3
MB	☐	19.8	8.25	92.77
MB	☐	20.5	6.93	94.09
TOB	☑	21	5.95	95.07
	☑	25	5.9	95.12
	☑	35	6.03	94.99
	☑	55	6.08	94.94
	☑	80	6.28	94.74
	☐			
stk: 3.78	☐			
	☐			

FS bankfull	FS top of bank	W fpa (ft)	channel slope (%)	Manning's "n"
6.97	5.95			
94.05	95.07			

dimensions			
19.5	x-section area	1.9	d mean
10.5	width	12.9	wet P
3.0	d max	1.5	hyd radi
4.0	bank ht	~~5.6~~	w/d ratio
~~0.0~~	W flood prone area	~~0.0~~	ent ratio

hydraulics	
~~0.0~~	velocity (ft/sec)
~~0.0~~	discharge rate, Q (cfs)
0.00	shear stress ((lbs/ft sq)
0.00	shear velocity (ft/sec)
~~0.000~~	unit stream power (lbs/ft/sec)
~~0.00~~	Froude number
~~0.0~~	friction factor u/u*
~~0.0~~	threshold grain size (mm)

check from channel material



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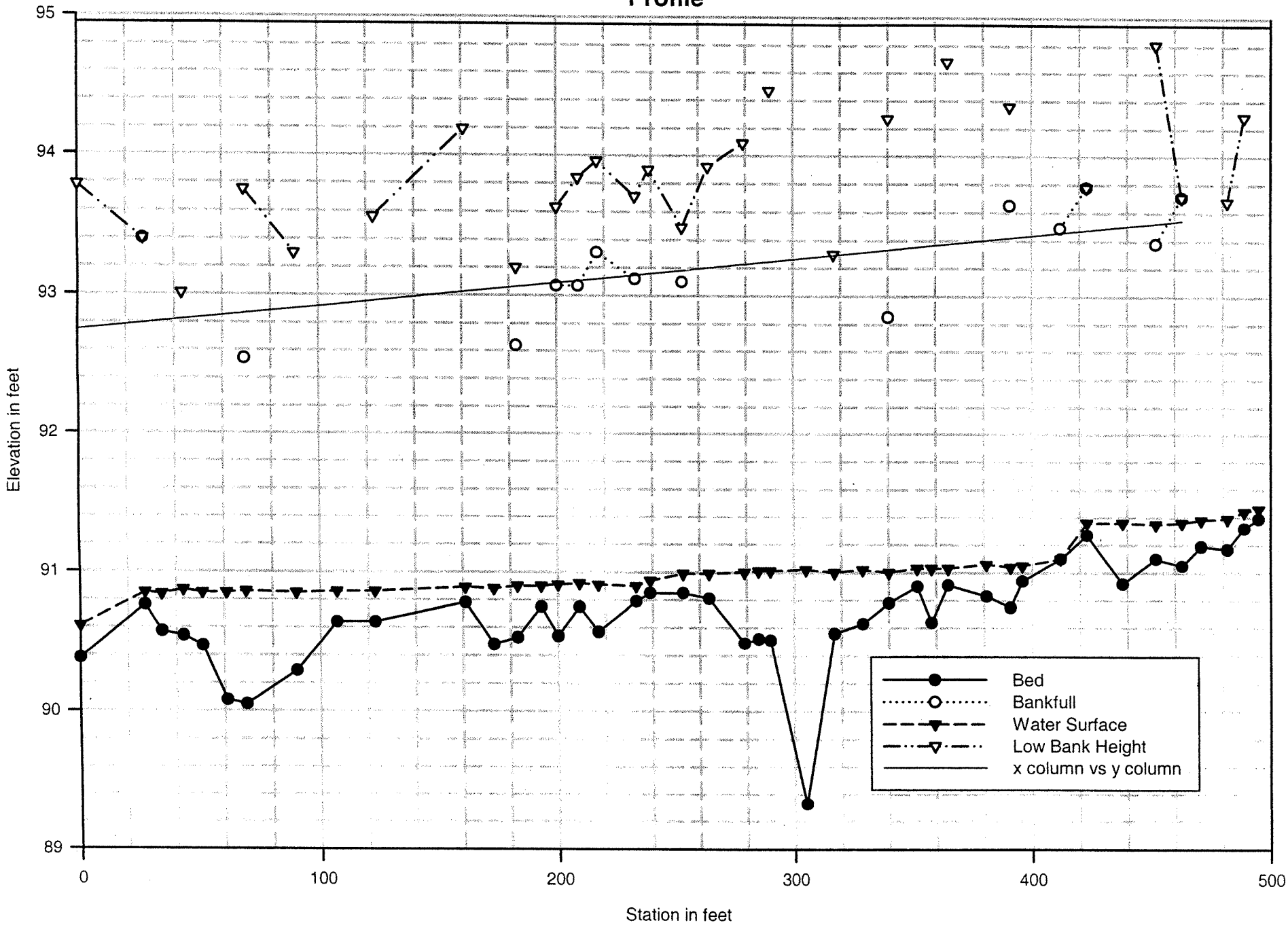
Dan Nicholas Park
Reference Stream
Profile



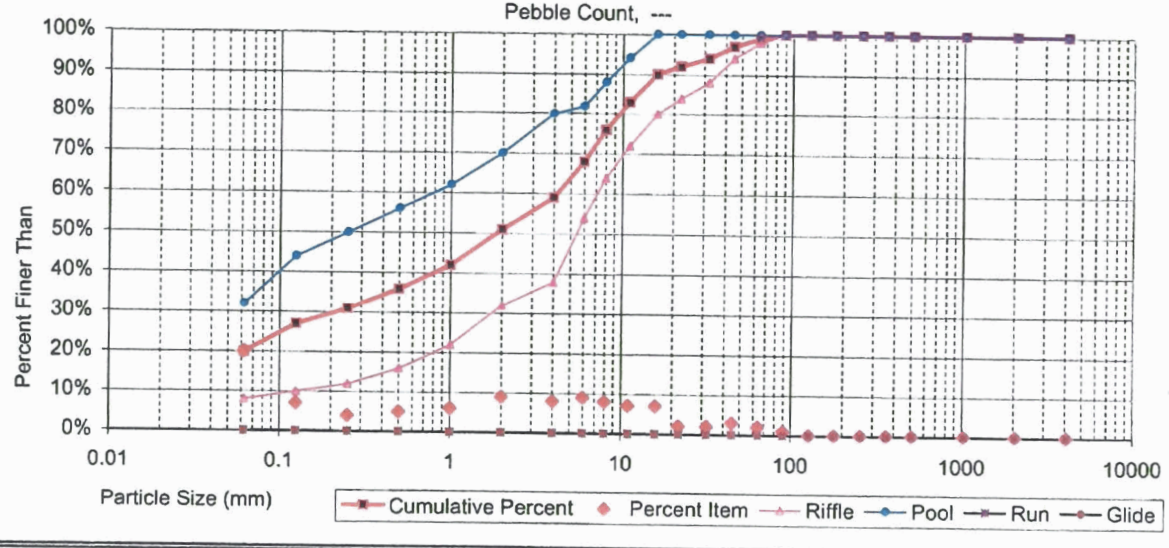
Weighted Pebble Count

Percent Riffle:	50	Percent Run:	0
Percent Pool:	50	Percent Glide:	0

Pebble Count, ---

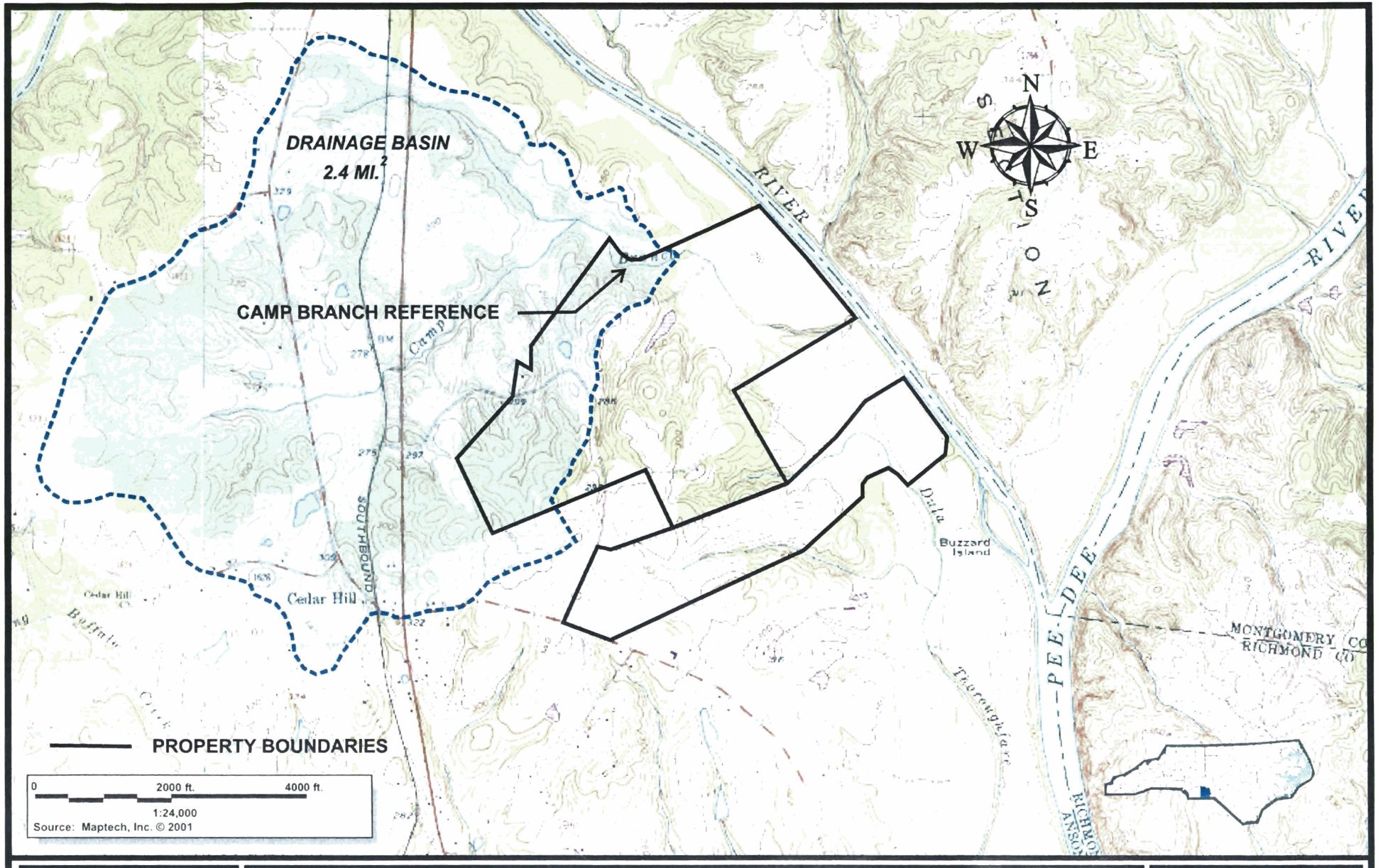
Note: **Dan Nicholas Weighted**

Material	Size Range (mm)		Total #	
silt/clay	0	0.062	20.0	#
very fine sand	0.062	0.13	7.0	#
fine sand	0.13	0.25	4.0	#
medium sand	0.25	0.5	5.0	#
coarse sand	0.5	1	6.0	#
very coarse sand	1	2	9.0	#
very fine gravel	2	4	8.0	#
fine gravel	4	6	9.0	#
fine gravel	6	8	8.0	#
medium gravel	8	11	7.0	#
medium gravel	11	16	7.0	#
coarse gravel	16	22	2.0	#
coarse gravel	22	32	2.0	#
very coarse gravel	32	45	3.0	#
very coarse gravel	45	64	2.0	#
small cobble	64	90	1.0	#
medium cobble	90	128	0.0	#
large cobble	128	180	0.0	#
very large cobble	180	256	0.0	#
small boulder	256	362	0.0	#
small boulder	362	512	0.0	#
medium boulder	512	1024	0.0	#
large boulder	1024	2048	0.0	#
very large boulder	2048	4096	0.0	#
bedrock			0.0	#
		Weighted Count:	100	
		True Total Particle Count:	100	



Size percent less than (mm)				
D16	D35	D50	D84	D95
#N/A	0.44	1.9	12	36

Percent by substrate type					
silt/clay	sand	gravel	cobble	boulder	bedrock
20%	31%	48%	1%	0%	0%



EcoScience Corporation
Raleigh, North Carolina

Camp Branch
Reference Site
Anson County, North Carolina

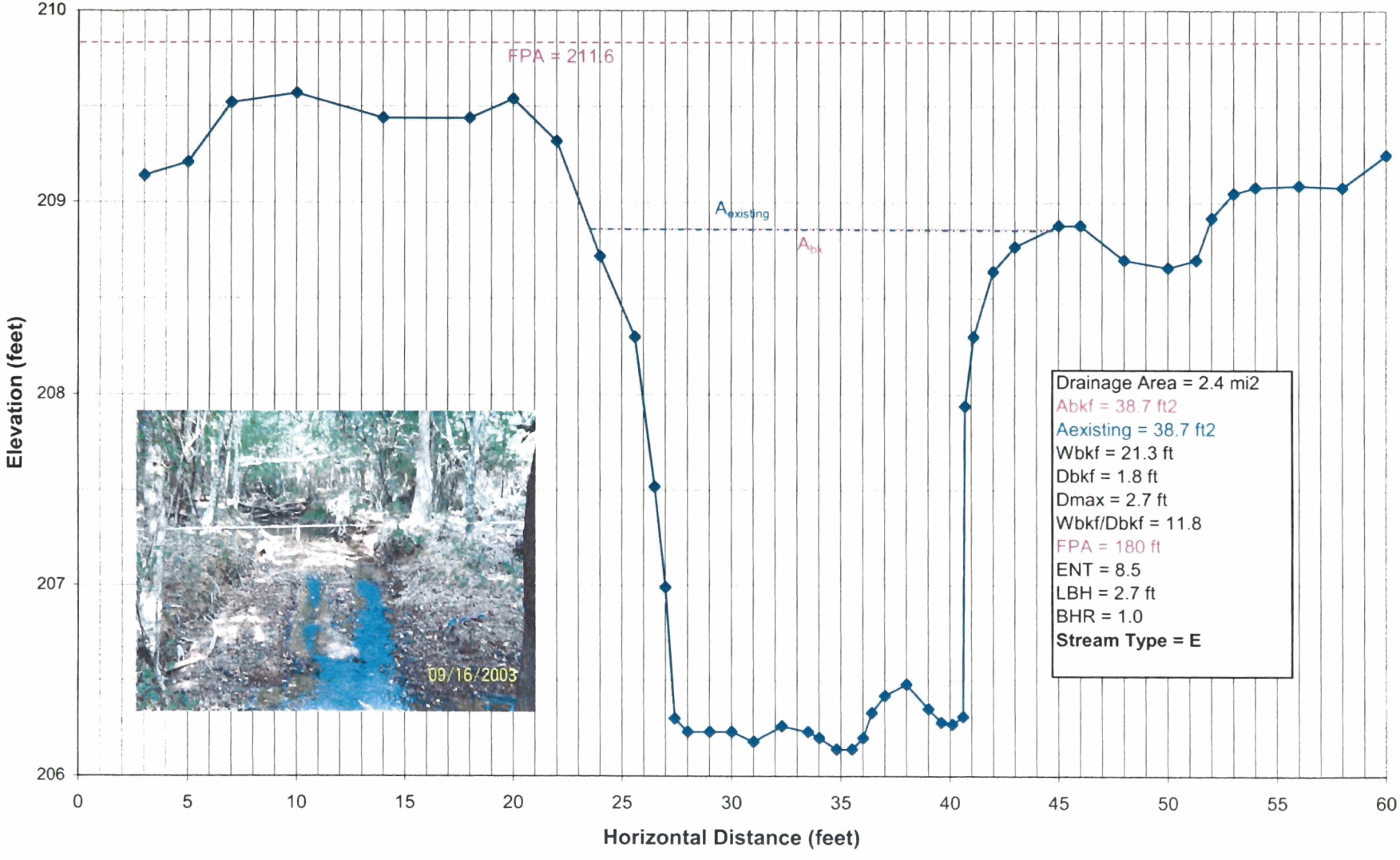
Dwn. by:	MAF
Ckd by:	WGL
Date:	July 2004
Project:	02-113.34

APPENDIX
Figure
2C

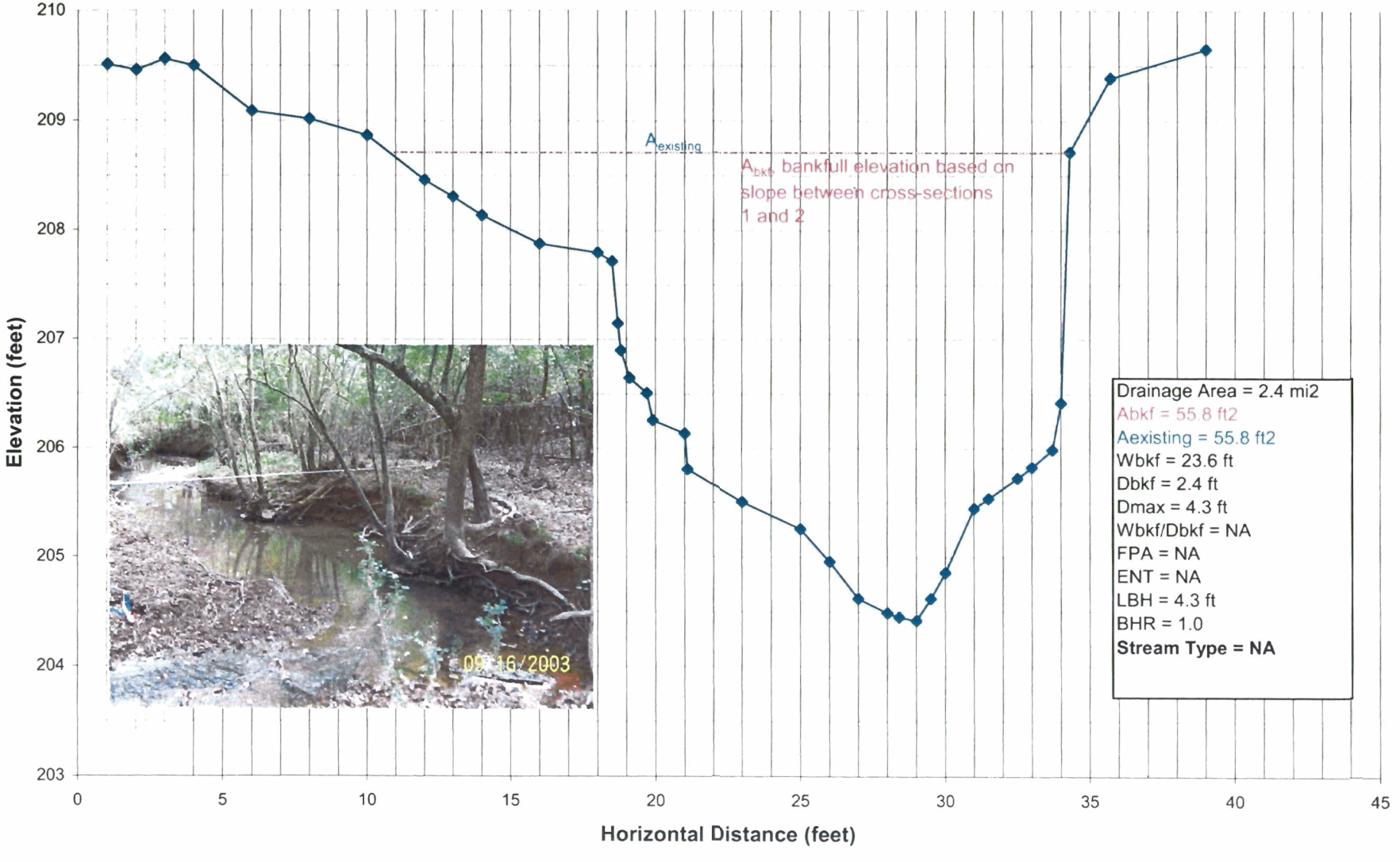
Bishop Property Refence Dimension: Camp Branch Area

	X-sect	DA (mi^2)	A_{bkf} (ft^2)	$A_{existing}$ (ft^2)	W_{bkf} (ft)	D_{ave} (ft)	D_{max} (ft)	W/D Ratio	FPA	Entrench	LBH (ft)	BHR	Stream Type
	Camp Branch Reach 1 (Upstream of Headcut)												
Riffles	1	2.4	38.7	38.7	21.3	1.8	2.7	11.8	180	8.5	2.7	1	E
	5		36	44.1	16.5	2.2	2.6	7.5	110	6.6	3.1	1.2	
	average	**2.4**	**37.4**	**41.4**	**18.9**	**2.0**	**2.7**	**9.7**	**145.0**	**7.6**	**2.9**	**1.1**	
	min	**2.4**	**36.0**	**38.7**	**16.5**	**1.8**	**2.6**	**7.5**	**110.0**	**6.6**	**2.7**	**1.0**	
	max	**2.4**	**38.7**	**44.1**	**21.3**	**2.2**	**2.7**	**11.8**	**180.0**	**8.5**	**3.1**	**1.2**	
Pools	2	2.4	55.8	55.8	23.6	2.4	4.3	---	---	---	4.3	1	---

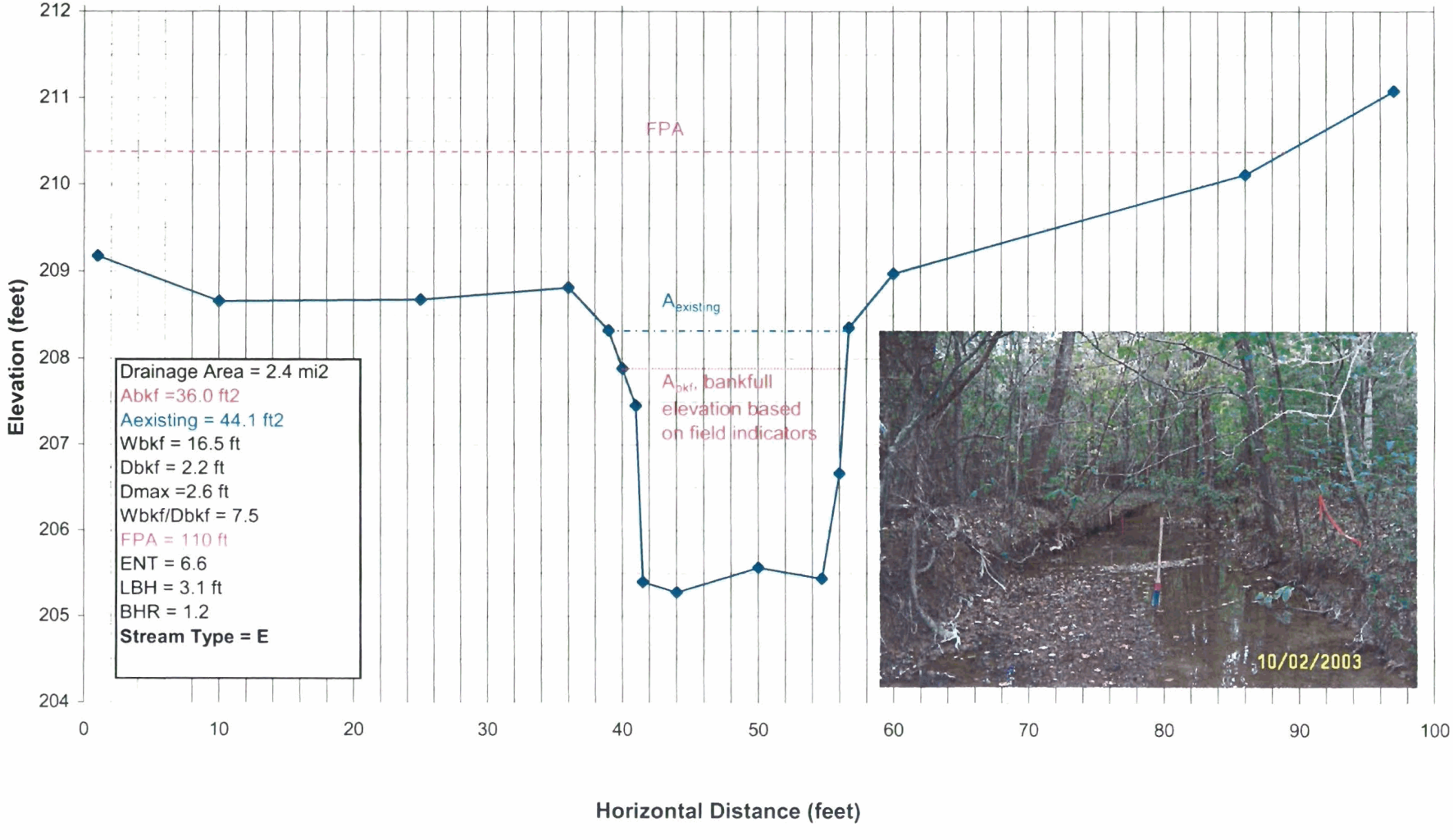
Cross-section 1: riffle, Camp Branch



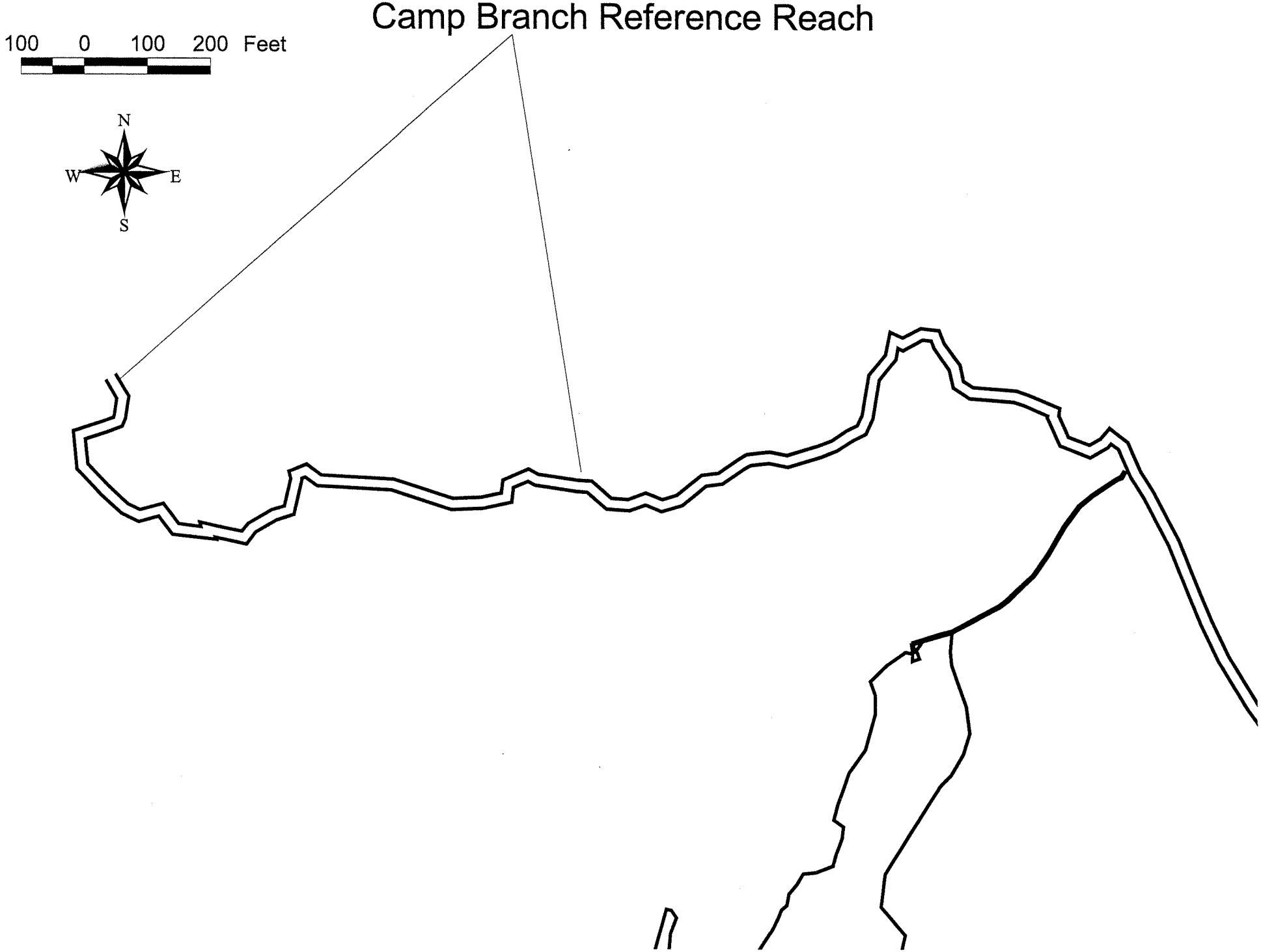
Cross-section 2: pool, Camp Branch



Cross-section 5: riffle, Camp Branch



Camp Branch Reference Reach



Camp Branch Referecne Reach Pattern

Camp Branch		pool to pool spacing	meander length	beltwidth	radius of curv	bkf width	pool to pool/bkf width	meander/ bkf width	beltwidth/ bkf width	rad/bkf width
Ref Reach	Median	74	133	43	41	19.6	3.8	6.8	2.2	2.1
	Range low	45	66	30	17		2.3	3.4	1.5	0.9
	Range high	145	240	97	200		7.4	12.2	4.9	10.2

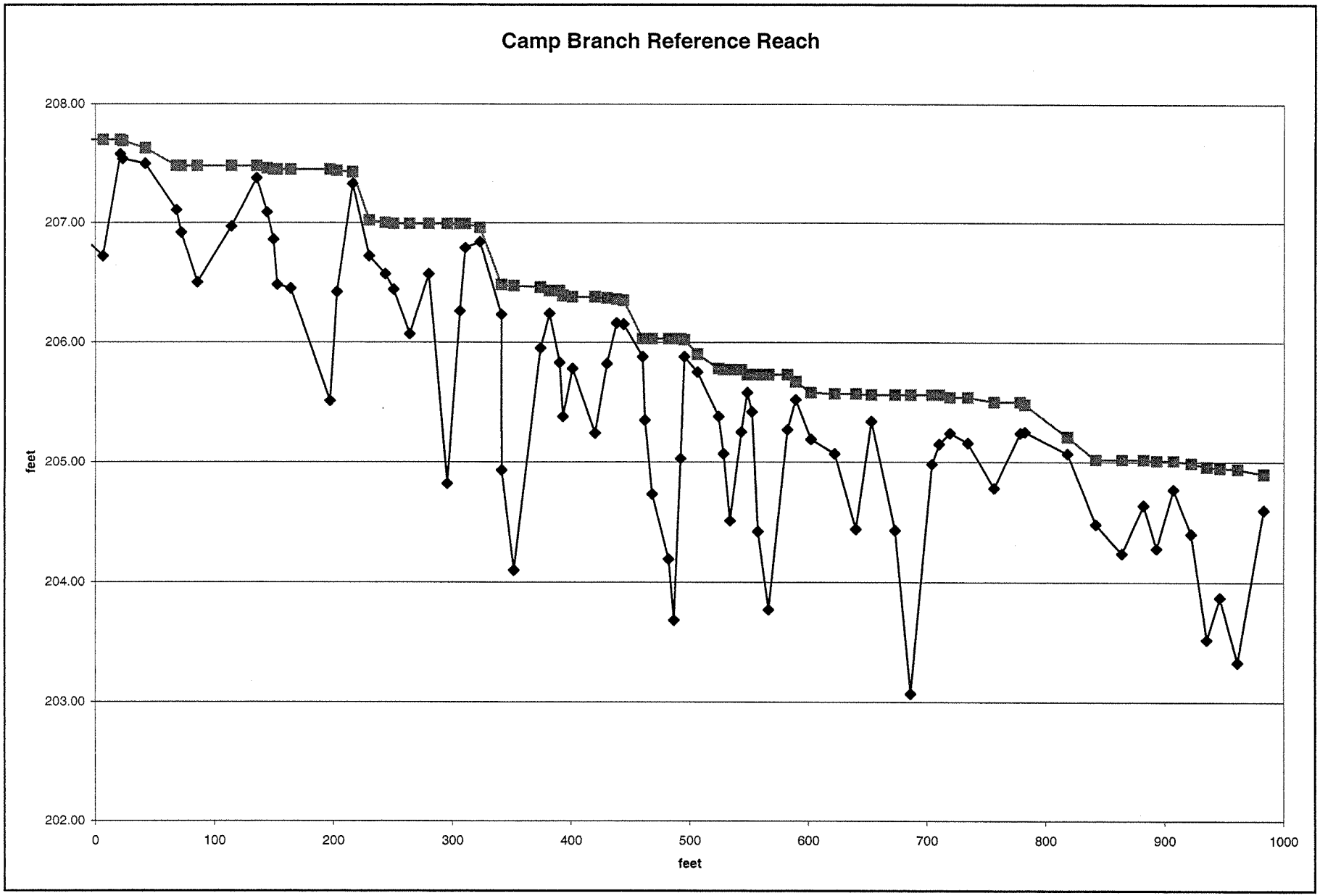
Pattern: Camp Branch

Reference Reach and Reach 2 Camp Branch Upstream to Ford				
	Pool to pool spacing (feet)	Meander Length (feet)	Beltwidth (feet)	Radius of curv (feet)
	45	66	30	16.7
	46	85	31	23.4
	50	88	33	27.1
	51	89	34	27.1
	53	92	34	28.1
	55	95	35	28.6
	56	101	36	29.2
	58	102	38	29.7
	61	103	39	29.7
	62	112	40	32.3
	64	116	42	32.8
	65	123	43	36.5
	73	126	46	40.6
	73	133	46	40.6
	75	135	46	50.0
	79	137	52	53.3
	79	143	52	53.3
	79	147	57	100.0
	79	155	63	106.7
	89	159	68	116.7
	95	172	89	120.0
	112	175	97	133.3
	118	182		133.3
	120	200		133.3
	122	209		200.0
	122	237		
	140	240		
	145			
Median	**74**	**133**	**42.5**	**40.6**
Range	**45-145**	**66-240**	**30-97**	**17-200**

Camp Branch Profile

Survey conducted by Corri & Kendrick (to sta 602) and Grant, Heather, & Ben (rest of stream)
The following calculations are a result of printing out the profile graph (as originally surveyed) and amending point by point

Station	Revised Feature	Bed Elevation	Revised WS Elevation	WS Slope	Riffle Slope	Pool Slope
-3		206.81	207.70			
6.4		206.72	207.70			
21		207.58	207.70			
23	TR1	207.54	207.69			
42		207.50	207.63			
68	BR1	207.11	207.48		0.0047	
72		206.92	207.48			
85.5	P1	206.50	207.48			
114		206.97	207.48			0.0000
135	TR2	207.38	207.48			
144		207.09	207.46			
149.4	BR2	206.86	207.45		0.0021	
152.5		206.48	207.45			
164		206.45	207.45			
197	P2	205.51	207.45			0.0003
203		206.42	207.44			
216	TR3	207.33	207.43			
230		206.72	207.02			
243.5		206.57	207.00			
250.5	BR3	206.44	206.99		0.0128	
264		206.07	206.99			
280		206.57	206.99			
295.5	P3	204.82	206.99			0.0000
306		206.26	206.99			
310.5	TR4	206.79	206.99			
323		206.84	206.96			
341	BR4	206.23	206.48		0.0167	
341.1		204.93	206.48			
351.5	P4	204.10	206.47			0.0012
374		205.95	206.46			
381.5	TR5	206.24	206.43			
390		205.83	206.43			
393		205.38	206.39			
401	BR5	205.78	206.38		0.0026	
420		205.24	206.38			
430	P5	205.82	206.37			0.0005
438	TR6	206.16	206.36			
444		206.15	206.35			
460	BR6	205.88	206.03		0.0150	
462		205.35	206.03			
468		204.73	206.03			
482	P6	204.19	206.03			0.0003
486.5		203.68	206.03			
492		205.03	206.03			
495	TR7	205.88	206.02			
506		205.75	205.90			
524	BR7	205.38	205.78		0.0083	
528		205.07	205.77			
533.5	P7	204.51	205.77			0.0005
543	TR8	205.25	205.77			
548		205.58	205.73			
552	BR8	205.42	205.73		0.0044	
557		204.42	205.73			
566	P8	203.77	205.73			0.0000
582	TR9	205.27	205.73			
589		205.52	205.67			
602	BR9	205.19	205.58		0.0075	
622		205.07	205.57			
640		204.44	205.57			
653		205.34	205.56			
673	P9	204.43	205.56			0.0002
686		203.07	205.56			
704		204.98	205.56			
710	TR9b	205.15	205.56			
719		205.24	205.54			
734	BR9b	205.16	205.54		0.0008	
756	P9b	204.78	205.50			0.0009
778	TR10	205.24	205.50			
782		205.25	205.48			
818		205.07	205.21			
842	BR10	204.48	205.02		0.0075	
864		204.24	205.02			
882	P10	204.64	205.02			0.0002
893		204.28	205.01			
907	TR11	204.77	205.01			
922		204.40	204.99		0.0018	
935	BR11	203.52	204.96			
946		203.87	204.95			
961	P11	203.33	204.94			0.0013
983	TR12	204.60	204.90			
upstream to headcut:			**ave**	**0.0029**	**0.0070**	**0.0004**
			min		**0.0008**	**0.0000**
			max		**0.0167**	**0.0013**


Camp Branch Reference Reach
208.00
207.00
206.00
205.00
204.00
203.00
202.00
feet
0
100
200
300
400
500
600
700
800
900
1000
feet

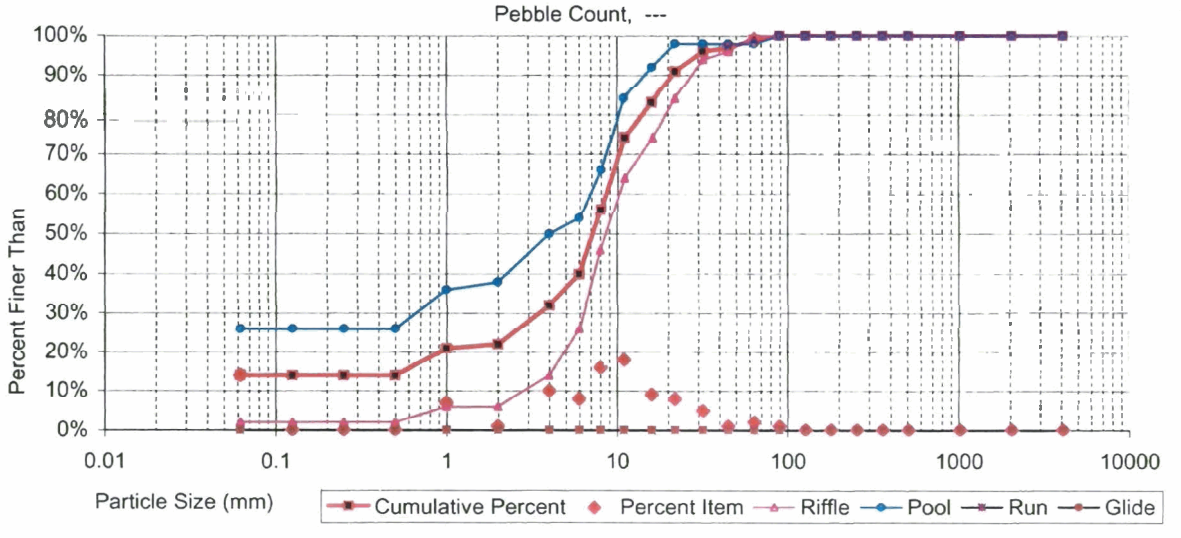
Weighted Pebble Count

Percent Riffle:	50	Percent Run:	
Percent Pool:	50	Percent Glide:	

Pebble Count,

Note:	**Camp Branch Reference Reach (Reach 1)**

Material	Size Range (mm)		Total #	
silt/clay	0	0.062	14.0	#
very fine sand	0.062	0.13	0.0	#
fine sand	0.13	0.25	0.0	#
medium sand	0.25	0.5	0.0	#
coarse sand	0.5	1	7.0	#
very coarse sand	1	2	1.0	#
very fine gravel	2	4	10.0	#
fine gravel	4	6	8.0	#
fine gravel	6	8	16.0	#
medium gravel	8	11	18.0	#
medium gravel	11	16	9.0	#
coarse gravel	16	22	8.0	#
coarse gravel	22	32	5.0	#
very coarse gravel	32	45	1.0	#
very coarse gravel	45	64	2.0	#
small cobble	64	90	1.0	#
medium cobble	90	128	0.0	#
large cobble	128	180	0.0	#
very large cobble	180	256	0.0	#
small boulder	256	362	0.0	#
small boulder	362	512	0.0	#
medium boulder	512	1024	0.0	#
large boulder	1024	2048	0.0	#
very large boulder	2048	4096	0.0	#
bedrock			0.0	#
		Weighted Count:	100	
		True Total Particle Count:	100	



Size percent less than (mm)					Percent by substrate type					
D16	D35	D50	D84	D95	silt/clay	sand	gravel	cobble	boulder	bedrock
0.610	4.66	7.2	17	30	14%	8%	77%	1%	0%	0%

APPENDIX E

CATENA GROUP FRESHWATER MUSSEL SURVEY

The Catena Group

410-B Millstone Drive
Hillsborough, NC 27278
(919) 732-1300

Freshwater Mussel Survey

Bishop Property Stream Restoration Mitigation Site
Anson County
North Carolina

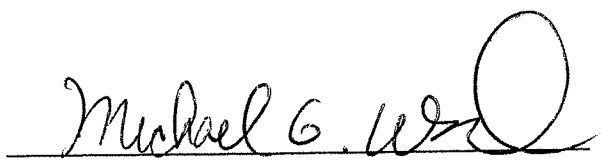
Prepared For:

EcoScience Corporation
1101 Haynes Street, Suite 101
Raleigh, North Carolina 27604

Prepared By:

The Catena Group, Inc.
Hillsborough, North Carolina

January 24, 2004



Michael G. Wood

INTRODUCTION

The North Carolina Ecosystem Enhancement Program (NCEEP) has contracted EcoScience Corporation to evaluate the Bishop Property (Bishop Site) for its potential as a mitigation site. The Bishop Site is in the Rocky River Subbasin of the Yadkin/Pee Dee River Basin in Anson County (Figure 1). The proposed mitigation on this property will include the restoration of an estimated total of 7600 linear feet of stream on Camp Branch, an Unnamed Tributary (UT) to Camp Branch, Dulla Thoroughfare, and UT to Dulla Throughfare. Although no restoration is planned for the mainstem of the Rocky River, there is potential for its waters to be impacted as a result of restoration efforts planned for Dulla Throughfare just above where it joins with the mainstem Rocky River. The federally endangered Carolina heelsplitter (*Lasmigona decorata*) is known to occur in the Rocky River Subbasin of the Yadkin/Pee Dee River Basin and is listed by the US Fish and Wildlife Service as occurring in Anson County, thus The Catena Group, Inc. was retained by EcoScience Corporation to conduct surveys for this species.

WATERS IMPACTED: Camp Branch, UT to Camp Branch, Dulla Thoroughfare, UT to Dulla Thoroughfare, and Rocky River

Camp Branch originates at the westernmost portion of the property, approximately 1.5 river miles (RM) from its confluence with Rocky River. The upstream portion of Camp Branch (the section upstream of its confluence with UT Camp Branch) meanders through a wooded area with a 1-2 meter (3-6.5 foot) wide channel and 1-3 meter (3.5-10 feet) high moderately eroded clay banks. The substrate in this portion of the stream was a sand-cobble mix.

The confluence with the UT is near the farm road that used to cross Camp Branch. The road crossing has been removed, however a beaver dam has been recently constructed that has ponded approximately 600 feet of channel. From below the beaver dam downstream to the Rocky River, the channel widens to an average of 6 meters (19.7 feet) and the banks become deeply incised, up to 7 meters (23 feet) high in some places. The sand-cobble substrate includes large areas of bedrock. The riparian corridor in this section is very narrow, flanked on both sides with active crop fields. Stream flow ranged from shallow riffles to slow moving runs with beaver activity observed throughout the reach.

UT to Camp Branch originates approximately 1200 meters upstream of its confluence with Camp Branch. This shallow stream meanders through a wooded lot for about 600 meters before entering a small impoundment. UT to Camp Branch exits the pond to the northeast where it has been ditched through its remaining length before converging with Camp Branch. Within the area surveyed, the UT ranges from 0.5-1.0 meters (2-3.5 feet) in width.

Dulla Thoroughfare and **UT to Dulla Thoroughfare** occur in the southeastern portion of the tract with the UT connecting Dulla to the Rocky River. Cursory habitat examinations revealed the streams to be heavily degraded and often ditched through out the majority of the property. Due to these factors and their relatively small size, it was determined that they contained no appropriate habitat for freshwater mussels.

The Catena Group	**Bishop Property Mitigation Site** Freshwater Mussel Survey Locations Anson County, North Carolina	Date: January 2005 Scale: As Shown Job No.: 3143	Figure 1

Rocky River originates in Cabarrus County over 30 RM to the northwest of the Bishop Property. It flows east, forming the southern border of Stanley County until it joins the Pee-Dee River just downstream of the survey area. Within the surveyed reach, the Rocky River was approximately 80 meters (260 feet) wide with a maximum depth of approximately 7 feet. Substrate ranged from compact gravel-cobble in the main channel to silty clay along the banks. River banks were approximately 3 meters (10 feet) high and often vertical. A moderate amount of windthrow and the resulting woody debris was apparent along the rivers edge. There was a narrow wooded buffer separating the large tracts of surrounding agricultural land from the Rocky River within the surveyed reach.

SPECIES DESCRIPTION

CAROLINA HEELSPLITTER (*Lasmigona decorata*) ***Lea 1852***

Status: Endangered
Family: Unionidae
Listed: July-24-1992

Characteristics

The Carolina heelsplitter (*Lasmigona decorata*), originally described as *Unio decoratus* by (Lea 1852), synonymized with *Lasmigona subviridis Conrad*, (Johnson 1970), and later separated as a distinct species (Clarke 1985), is a federally Endangered freshwater mussel, historically known from several locations within the Catawba and Pee Dee River systems in North Carolina and the Pee Dee, Savannah and possibly the Saluda River systems in South Carolina.

The Carolina heelsplitter is characterized as having an ovate, trapezoid-shaped, unsculptured shell. The outer surface of the shell ranges from greenish brown to dark brown in color, with younger specimens often having faint greenish brown or black rays. The shell's nacre is often pearly white to bluish white, grading to orange in the area of the umbo (Keferl 1991). The hinge teeth are well developed and heavy and the beak sculpture is double looped (Keferl and Shelly 1988). Morphologically, the shell of the Carolina heelsplitter is very similar to the shell of the green floater (Clarke 1985), with the exception of a much larger size and thickness in *L. decorata* (Keferl and Shelly 1988).

Prior to collections in 1987 and 1990 by Keferl (1991), *L. decorata* had not been collected in the 20th century and was known only from shell characteristics. Because of its rarity, very little information of this species biology, life history, and habitat requirements was known. Feeding strategy and reproductive cycle of the Carolina heelsplitter have not been documented, but are likely similar to other native freshwater mussels (USFWS 1996).

The feeding processes of freshwater mussels are specialized for the removal (filtering) of suspended microscopic food particles from the water column (Pennak 1989). Documented food sources for freshwater mussels include detritus, diatoms, phytoplankton and zooplankton (USFWS 1996).

Freshwater mussels have complex reproductive cycles, which include a larval stage (glochidium) that is an obligatory parasite on a fish (Pennak 1989). The glochidia develop into juvenile mussels and detach from the "fish host" and sink to the stream bottom where they continue to develop, provided suitable substrate and water conditions are available (USFWS 1996). Many species of naiades require a particular species of fish to serve as the host. The host species(s) for the Carolina heelsplitter is unknown (USFWS 1996).

Distribution and Habitat Requirements

Currently the Carolina heelsplitter has a very fragmented, relict distribution. Until recently, it was known to be surviving in only six streams and one small river (USFWS 1996):

1. Waxhaw Creek (Catawba River system) in Union County, North Carolina
2. Goose Creek (Pee Dee River system) in Union County, North Carolina
3. Lynches River (Pee Dee River system), in Chesterfield, Lancaster and Kershaw Counties, South Carolina
4. Flat Creek, a tributary to the Lynches River in Lancaster County, South Carolina
5. Turkey Creek (Savannah River system) in Edgefield County, South Carolina
6. Mountain Creek (tributary to Turkey Creek) in Edgefield County, South Carolina
7. Beaverdam Creek (tributary to Turkey Creek) in Edgefield County, South Carolina

In the summer of 2004, a population of this species was discovered in Little Fishing Creek (Catawba River system) in Chester County, South Carolina (personal observations). Additionally, a range extension of the Waxhaw Creek population was documented into Lancaster County, South Carolina (John Alderman, personal Communication 2004).

Habitat for this species has been reported from small to large streams and rivers as well as ponds. These ponds are believed to be millponds on some of the smaller streams within the species' historic range (Keferl 1991). Most individuals have been found along well-shaded streambanks with mud, muddy sand, or muddy gravel substrates. The stability of stream banks appears to be very important to this species ((Keferl 1991).

Threats to Species

The low numbers of individuals and the restricted range of each of the surviving populations make them extremely vulnerable to extirpation from a single catastrophic event or activity (USFWS 1996). The cumulative effects of several factors, including sedimentation, point and non-point discharge, and stream modification (impoundments, channelization, etc.) has contributed to the decline of this species throughout its range (USFWS 1996).

Siltation resulting from improper sedimentation control of various land usages, including agricultural, forestry, and developmental activities, has been recognized as a major contributing factor to degradation of mussel populations (USFWS 1996). Siltation has been documented to be extremely detrimental to mussel populations by degrading substrate and

water quality, increasing potential exposure to other pollutants, and by direct smothering of mussels (Ellis 1936), (Markings and Bills 1979)). Sediment accumulations of less than 1 inch have been shown to cause high mortality in most mussel species (Ellis 1936).

Sewage treatment effluent has been documented to significantly affect the diversity and abundance of mussel fauna (Goudreau, Neves et al. 1988). Goudreau, Neves et al. (1988) found that recovery of mussel populations might not occur for up to two miles below points of chlorinated sewage effluent.

The impact of impoundments on freshwater mussels has been well-documented (USFWS 1992 a), Neves 1993). Construction of dams transforms lotic habitats into lentic habitats, which results in changes with aquatic community composition. Muscle Shoals on the Tennessee River in northern Alabama, once the richest site for naiads (mussels) in the world, is now at the bottom of Wilson Reservoir and covered with 19 feet of muck (USFWS 1992 b). Large portions of all of the river basins within the Carolina heelsplitter's range have been impounded and this is believed to be a major factor contributing to the species decline (USFWS 1996).

The introduction of exotic species such as the Asiatic clam (*Corbicula fluminea*) and zebra mussel (*Dreissena polymorpha*) has also been shown to pose significant threats to native freshwater mussels. The Asiatic clam is now established in most of the major river systems in the United States (Fuller and Powell 1973); including those streams still supporting surviving populations of the Carolina heelsplitter (USFWS 1996). Concern has been raised over competitive interactions for space, food and oxygen with this species and native mussels, possibly at the juvenile stages (Neves and Widlak 1987), (Alderman 1995). The zebra mussel is not known from any waterbodies supporting the Carolina heelsplitter (USFWS 1996).

SURVEY EFFORTS

Pre Survey Investigation

Prior to conducting in-stream surveys, a review of previous surveys that had taken place in the project area was conducted. Sources consulted include the North Carolina Natural Heritage Program (NCNHP) systematic inventory (database) of rare plant and animal species and the North Carolina Wildlife Resources Commission (NCWRC). While there were no records within one mile of the areas to be impacted, there is a historical record of the Carolina heelsplitter from the mainstem of the Yadkin-Pee Dee River near Leak Island, approximately 3 miles downstream from the Bishop Tract.

Mussel Surveys

Michael Wood, Shay Garriock, Kate Montieth, and Sharon Snider of The Catena Group investigated the Bishop Tract Stream Restoration site on January 3, 2005. Where appropriate mussel habitat was present, surveys were conducted using the standard USFWS recommendations for aquatic species of 100 meters upstream of the most upstream point of impact to 400 meters downstream of the most downstream point of impact.

Methodology and Results

Visual surveys were conducted using batiscopes and tactile methods in each stream except the mainstem Rocky River, which required SCUBA surveys. Searches for relic shells were also conducted concurrently with in-stream surveys. No freshwater mussels were found during the 12 person hours spent surveying the Bishop property. The specific results of each survey reach (Figure 1) are detailed below.

Camp Branch:

Deeply incised throughout most of the survey reach, especially in its lower portion, Camp Branch was likely heavily impacted by the past and current agricultural practices in its watershed. Additionally, the lower portions are heavily impacted by beaver activity. Within the upper surveyed portion (above its UT confluence) one *Pysella sp.* snail was found in Camp Branch. Below the UT confluence, one shell of the introduced Asian clam (*Corbicula fluminea*) was found. No freshwater mussels were located in the surveyed reach of Camp Branch.

UT Camp Branch:

Due to its predominantly wooded surroundings, this UT to Camp Branch remains relatively stable in its upper reach. Below the man made impoundment, however, the stream is ditched. Throughout the surveyed area the UT was very small, rarely over 3 feet in width making freshwater mussel habitat marginal. No freshwater mussels, snails, or the Asian clam were found in this UT.

Dulla Thoroughfare and UT to Dulla Thoroughfare:

The approximately 100 meters of the Dulla Thoroughfare connection to the mainstem Rocky River surveyed was an agricultural ditch characterized by unconsolidated sand, silt and mud substrate. No mollusks were observed here and freshwater mussel habitat was not appropriate. Cursory habitat examinations in several other locations revealed the stream to be degraded and often ditched, especially in the reaches intended for restoration. Due to these factors and the relatively small size of the streams, especially in the UT, it was determined that Dulla Thoroughfare and its UT contained no appropriate habitat for freshwater mussels.

Rocky River:

The proposed restoration efforts in Dulla Thoroughfare extend to its confluence with the mainstem Rocky River, thus the Rocky River was surveyed approximately 400 meters downstream of this confluence. A short reach above the confluence was also surveyed for habitat comparison. A variety of appropriate mussel habitats persists in this reach of the Rocky River and represents the best potential habitat that may be impacted as a result of the restoration efforts. Despite this fact and the acceptable survey conditions, no freshwater mussels were found in this reach. The only freshwater mollusk located was the Asian clam (*Corbicula fluminea*), which was common.

DISCUSSION

The streams within the Bishop tract proposed for restoration efforts are, for the most part, not appropriate habitat for freshwater mussels. This is due to their generally degraded, altered states resulting from the surrounding agricultural land use. Within the UT to Camp Branch and UT Dulla Thoroughfare, their small size seems to be the main factor limiting appropriate mussel habitat. The Rocky River represents the best freshwater mussel habitat within the vicinity of the Bishop tract, however, no mussels were found during the survey. It is possible that a remnant population of freshwater mussels exists downstream of the project area in the Rocky River as mussel populations within the mainstem of the Rocky River have been documented as recently as 2004. However, due to the sensitive nature of the Carolina heelsplitter, it is very unlikely that it is part of the freshwater mussel fauna potentially present in the Rocky River downstream of the Bishop Tract. It is therefore anticipated that the proposed stream mitigation within the Bishop Tract is **"Not Likely To Adversely Effect"** the Carolina heelsplitter.

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APPENDIX F

NOTIFICATION OF JURISDICTIONAL DETERMINATION

COPY

U.S. ARMY CORPS OF ENGINEERS
Wilmington District

Action ID: 200430199 County: **Anson**

Notification of Jurisdictional Determination

Property Owner: NCDOT
Address: Gregory J. Thorpe, Project Development and Environmental Analysis
1548 Mail Service Center
Raleigh, NC 27699-1548
Telephone: 919-733-3141

Authorized Agent: EcoScience Corporation
Attn: W. Grant Lewis
Address: 1101 Haynes Street
Suite 101, Raleigh, NC 27604
Telephone:919-828-3433

Size and Location of Property (waterbody, Highway name/number, town, etc.):
Bishop Property Stream and Wetland Mitigation Site, Approximately 930-acre parcel adjacent to the Rocky River off Carpenter Road north of Ansonville in the Yadkin/Pee Dee River Basin

Basis for Determination: Delineation Maps and GPS surveys dated January 27, 2004 with accompanying Wetland Data Forms and Stream Assessment Worksheets from August and September 2003 identifying hydric soil, wetland hydrology, hydrophytic vegetation, stream flow, an ordinary high waterline and surface hydrologic connections to the Yadkin/Pee Dee River System.

Indicate Which of the Following apply:

◊ The wetlands and surface waters on this project have been delineated and the limits of the Corps jurisdiction have been explained to you. Unless there is a change in the law or our published regulations, this determination may be relied upon for a period not to exceed five years from the date of this notification.

Placement of dredged or fill material in streams and wetlands on this property without a Department of the Army permit is in most cases a violation of Section 301 of the Clean Water Act (33 USC 1311). A permit is not required for work on the property restricted entirely to existing high ground. If you have any questions regarding the Corps of Engineers regulatory program, please contact
Steven W. Lund **at** 828-271-7980 x 223.

Project Manager Signature Steven W. Lund
Date: January 13, 2004 **Expiration Date: January 13, 2009**

SURVEY PLAT OR FIELD SKETCH OF DESCRIBED PROPERTY AND THE WETLAND DELINEATION FORM MUST BE ATTACHED TO THIS FORM.