

AIR EMISSION TEST REPORT
Wiggins, Mississippi Wood Pellet Production Facility
Enviva Pellets Wiggins, LLC

Submitted to

Enviva Pellets Wiggins, LLC

Submitted by

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Definitions

Total Hydrocarbons All organic compounds containing hydrogen and carbon that are detected by a flame ionization detector operated in accordance with U.S. EPA Method 25A.

Volatile Organic Compounds

All organic compounds that are emitted to the atmosphere in a gaseous or vapor form that can participate in photochemical reactions to produce ozone. All volatile organic compounds are considered VOCs unless specifically exempted in 40 CFR 51.100(s). Relevant excluded compounds include methane, ethane, and acetone.

VOC Emissions Mass emissions of VOC measured on a pounds of carbon basis.

Acronyms

EPA	U.S. Environmental Protection Agency
FID	Flame Ionization Detector
FTIR	Fourier Transform Infrared Spectrometer
HAP	Hazardous Air Pollutant
MC	Moisture Content
MDEQ	Mississippi Department of Environmental Quality
ODT	Oven Dried Tons
THC	Total Hydrocarbons
VOC	Volatile Organic Compounds
C1	Carbon

Units of Measure

ppm	Parts per million (wet basis)
ppmvd	Parts per million (dry basis)
ppm C ₃	Parts per million as propane
ppm C ₁	Parts per million as carbon
mg	Milligram
kg	Kilogram
µg	Micrograms

Permit Designations/Titles

Dryer 1	AA-001, 30 MMBTU Wood-Fired Dryer (No. 1) with a Multiclone
Dryer 2	AA-002, 45 MMBTU Wood Fired Dryer (No. 2) with a Cyclone
Dry Hammermill 1	AA-006, No. 1 Secondary Hammermill w/High-Eff. Cyclone
Dry Hammermill 2	AA-007, No. 2 Secondary Hammermill w/High-Eff. Cyclone
Pellet Cooler 1	AA-004, Includes Line 1 Press Aspiration (AA-012)
Pellet Cooler 2	AA-014, Pellet Cooler 2 w/Hi-Efficiency Cyclone
Aspiration System	AA-013, Line 2 Pellet Mill Aspiration System
Green Hammermill	AA-016 (Hammermill Bin)

Air Emission Test Report Wiggins, Mississippi Wood Pellet Production Facility

1. SUMMARY

Enviva Pellets, Wiggins, LLC (Enviva) has sponsored air emission testing to satisfy the requirements of Agreed Order 6366-13 dated June 16, 2013 (the "Order"). These test results are being submitted to the Mississippi Department of Environmental Quality (MDEQ) by October 31, 2013 in accordance with the Order.

The scope of the testing program included volatile organic compounds (VOCs) and six organic hazardous air pollutants (HAPs). Annual emissions of each analyte have been calculated and compared to applicable permit limits. The results of the testing program are summarized in Table 1-1 based on the present maximum permitted production limit of 185,550 ODT per year in the permit.

Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	66.3	57.6	11.1	21.1	15.7	7.8	46.4	7.4	233.5
Organic HAPs									
Methanol	1.85	7.26	0.08	0.27	0.16	0.24	0.34	0.05	10.3
Acetaldehyde	0.00	1.40	0.25	0.61	0.39	0.35	0.23	0.17	2.0
Acrolein	1.03	2.32	0.43	1.24	0.77	0.68	0.20	0.29	7.0
Formaldehyde	2.01	3.48	0.39	0.37	0.49	0.34	0.03	0.26	7.4
Phenol	0.00	0.00	0.00	0.00	0.39	0.00	0.00	0.00	0.4
Propionaldehyde	1.06	1.82	0.17	0.09	0.16	0.11	0.00	0.11	3.5
Total HAPS	5.96	14.87	1.32	2.59	2.35	1.72	0.80	0.88	31.89

At the current maximum permitted production limit, VOC emissions remain below the PSD threshold of 250 tons per year. However, HAP emissions exceed the 25 ton per year threshold for major source classification, and methanol exceeds the 10 ton per year single compound threshold for major source classification. Importantly, the plant has never operated at the maximum permitted production limit of 185,550 ODT per year.

Enviva plans to propose to MDEQ a new maximum permitted production limit of 140,000 ODT/year. VOC and HAP emissions based on this proposed maximum permitted production limit are summarized in Table 1-2. Like the current limit of 185,000 ODT/year, to date, the Wiggins plant has also never achieved 140,000 ODT/year.

VOC emissions at the newly proposed production rate limit would be well below the PSD threshold of 250 tons per year. Furthermore, combined HAPs emissions are less than 25 tons per year, and none of the HAPs are emitted at more than 10 tons per year. Because the plant has never achieved a production rate of 140,000 ODT/year, the plant has never exceeded the major source threshold for VOCs or HAPs.

Table 1-2. Total Emissions at Plant Permit Limit of 140,000 ODT/Year

Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	50.1	43.4	8.4	15.9	11.7	5.9	35.0	5.6	175.9
Organic HAPs									
Methanol	1.40	5.48	0.06	0.21	0.12	0.18	0.26	0.04	7.7
Acetaldehyde	0.00	1.06	0.19	0.46	0.29	0.26	0.17	0.12	2.6
Acrolein	0.78	1.75	0.33	0.93	0.58	0.51	0.15	0.22	5.3
Formaldehyde	1.52	2.62	0.30	0.28	0.37	0.26	0.03	0.20	5.6
Phenol	0.00	0.00	0.00	0.00	0.29	0.00	0.00	0.00	0.3
Propionaldehyde	0.80	1.37	0.13	0.07	0.12	0.08	0.00	0.08	2.7
Total HAPS	4.50	12.28	0.99	1.95	1.78	1.30	0.61	0.66	24.06

These tests were conducted in accordance with the emission test protocol^[1] submitted to MDEQ on July 31, 2013. The scope of the emission test program was increased since submittal of the test program protocol in order to ensure that Enviva evaluated emissions from all possible sources of VOCs and HAPs.

The air emission tests were conducted by Air Control Techniques, P.C. using EPA Reference Methods 1, 2, 3, 4, 25A, and 320. The emission tests were conducted from Thursday, October 10 through Sunday, October 13, 2013. This report summarizes the emissions test data, quality assurance data, test method procedures, sampling equipment calibrations, process operating conditions, and test program participants.

2. EMISSION TEST PROGRAM DESCRIPTION

2.1 Wiggins, Mississippi Plant Description

Enviva operates a plant producing wood pellets. The plant consists of a wood receiving yard, log debarkers and chippers, two rotary dryers, two hammermills, two pellet presses and coolers, and an aspiration system. The plant processes wood composed of a range of hardwoods and softwoods.

2.2 Purpose and Scope of the Emission Test Program

Based on a voluntary self-evaluation, Enviva reported to the Mississippi Department of Environmental Quality (MDEQ) that it may have underreported emissions of volatile organic compounds (VOCs) in its permit application. Enviva's concern was based on a set of engineering-oriented tests^[2] conducted in November 2012 that indicated that VOC emissions from a hammermill source and a press cooler aspiration vent may be higher than previously known. While emissions from specific wood pellet plants are highly dependent on the specific equipment employed and to a lesser degree the hardwood/softwood mix of raw material, Enviva's preliminary findings in the November 2012 engineering test are generally consistent with other recent findings in the Wood Pellet Industry, specifically the engineering-oriented tests^[3] at a Georgia Biomass, Inc. plant in Waycross, Georgia and Green Circle Bio Energy in Cottondale, Florida.

This air emission testing program is intended to address Enviva's concern and fulfills the requirements of the Order. Specifically, Enviva agreed to generate VOC emissions data for the following sources.

- Dryer 1 multiclone stack
- Dryer 2 cyclone stack
- Secondary Hammermill 2 cyclone outlet
- Pellet Mill 2 Aspiration System

Since signing the Order, Enviva has determined that it would be beneficial to expand the scope of the emission testing program to include these three additional sources.

- Green Hammermill
- Pellet Cooler 1
- Pellet Cooler 2

The tests at Secondary Hammermill 2 cyclone outlet also represent emissions from Secondary Hammermill 1. Secondary Hammermill 2 is identical to Secondary Hammermill 1 except for the larger capacity of Secondary Hammermill 2.

2.3 Test Participants

The Enviva project manager for this project was Mr. Michael Doniger, Director of Plant Operations. He was assisted by Mr. Joe Harrell, Environmental Manager, Mr. Mike Jones, and Mr. Gary Williams, Wiggins Plant Manager.

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Legal counsel for Enviva is Mr. Alan McConnell. Mr. McConnell participated in this study to ensure that it addressed the requirements of the Order.

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Enviva retained Air Control Techniques, P.C. to conduct the air emission testing program at the Wiggins plant. The Air Control Techniques, P.C. project manager was John Richards, Ph.D., P.E., QSTI. He was assisted by David Goshaw, P.E., QSTI, Todd Brozell, P.E., QSTI, and Jonas Gilbert. Tom Holder, QSTI provided quality assurance services for the test program. Contact information for Air Control Techniques, P.C. includes the following.

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Enthalpy, Inc. provided the laboratory analyses of the samples. The Enthalpy project manager for this project was Mr. Bryan Tyler. He was assisted by Dr. Grant Plummer, Mr. Clint Thrasher, and Mr. Steve Eckert, President.

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3. TEST MATRIX AND TEST RESULTS

3.1 Test Matrix

Table 3-1 summarizes the test program analytes, sampling methods, and analytical methods used for the seven sources listed in Section 1.1

Analyte	Test Method	Number of Runs	Run Length	Analytical Method
Acetaldehyde, Acrolein, Formaldehyde, Methanol, Phenol, Propionaldehyde	EPA Method 320	3	60 min	FTIR
Gas Flow	EPA Method 2	3	60 min	Manometer
Gas Molecular Weight, Oxygen, Carbon Dioxide	EPA Method 3	3	60 min	Fyrite® Analyzer
Gas Moisture	EPA Method 4	3	60 min	Gravimetric
Total Hydrocarbons (THC)	EPA Method 25A	3	60 min	FID

The tests were conducted on Thursday, October 10 through Sunday October 13, 2013. During all of the tests, the plant operated with a 60% softwood/40% hardwood feed.

3.2 Test Results

The VOC and organic HAP test results and calculated annual emission rates are summarized in Tables 3-2 through 3-8. VOC and HAP emissions were measured simultaneously at each of the seven emission units tested.

The VOC emissions have been calculated based on the total hydrocarbon data provided by Method 25A. The Method 25A data have been converted from a wet to a dry basis to account for the moisture in the stack gas stream. Total hydrocarbon concentrations (THC) has been used as a surrogate for VOCs.

The VOC emission calculations do not include any corrections for methane, ethane, or acetone despite the fact that these compounds are detected by Method 25A but are not classified as VOCs. Accordingly, the reported VOC emissions are biased to higher-than-true levels to the extent that these three compounds affected the Method 25A results.

The Method 25A data reflect the combined THC concentrations consisting of (1) alpha and beta pinene, (2) numerous other terpenes such as limonene and 3-carene, and (3) the organic HAPs. The organic HAP emissions discussed later in this report are also classified as VOCs and represent a small fraction of the total VOC emissions reported.

Method 320 was used to measure six organic compounds. Several of the organic compounds were below the detection limits of Method 320 in this matrix of gaseous constituents. These non-detection concentrations are designated by shading in Tables 3-2 through 3-8.

Table 3-2. Green Hammermill ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/10/2013	10/10/2013	10/10/2013	N/A
Start	9:17	10:36	11:50	N/A
Stop	10:17	11:36	12:50	N/A
Throughput, tons/hour	36	36	36	36.0
Moisture Content Outlet, %wt.	47.15	47.15	47.15	47.2
Throughput, ODT/hour	19.026	19.026	19.026	19.0
ACFM	27,642	27,273	27,189	27,368.0
DSCFM	25,184	24,803	25,031	25,006
Stack Temperature, °F	70.8	70.6	70.9	70.8
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	3.41	3.62	2.37	3.1
VOC, ppmvd as Propane	31.9	33.4	27	30.8
VOC, ppmvd as C1	95.7	100.3	81.1	92.4
VOC, lbs/hour as C1	4.5	4.7	3.8	4.3
VOC, lbs/ODT	0.24	0.25	0.20	0.2
Methanol, ppmvd	0.53	0.48	0.39	0.46
Acetaldehyde, ppmvd	0.79	0.75	0.74	0.76
Acrolein, ppmvd	1.17	1.25	1.18	1.20
Formaldehyde, ppmvd	0.77	0.65	0.57	0.66
Phenol, ppmvd	0.91	0.91	0.90	0.91
Propionaldehyde, ppmvd	0.24	0.24	0.26	0.247
Methanol, lbs/hour	0.066	0.060	0.049	0.058
Acetaldehyde, lbs/hour	0.136	0.129	0.127	0.131
Acrolein, lbs/hour	0.257	0.274	0.259	0.263
Formaldehyde, lbs/hour	0.090	0.077	0.068	0.078
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.000	0.000	0.058	0.019
Methanol, lbs/ODT	0.003	0.003	0.002	0.003
Acetaldehyde, lbs/ODT	0.007	0.007	0.006	0.007
Acrolein, lbs/ODT	0.013	0.014	0.013	0.013
Formaldehyde, lbs/ODT	0.005	0.004	0.003	0.004
Phenol, lbs/ODT	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/ODT	0.000	0.000	0.003	0.001

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Parameter	Run 1	Run 2	Run 3	Average
Date	10/10/2013	10/11/2013	10/11/2013	N/A
Start	17:38	10:00	11:37	N/A
Stop	18:38	11:00	12:37	N/A
Throughput, tons/hour	8.5	8.45	9	8.7
Moisture Content Outlet, %wt.	15.5	14.36	18.9	16.3
Throughput, ODT/hour	7.18	7.24	7.30	7.2
ACFM	44,448	42,243	42,593	43,095
DSCFM	32,404	31,700	31,215	31,773
Stack Temperature, °F	146.3	150.1	147.3	147.9
O ₂ , %	19.0	17.0	17.0	17.7
% Moisture	16.07	12.79	15.23	14.7
VOC, ppmvd as Propane	79.5	71	67.4	72.6
VOC, ppmvd as C1	238.8	213.3	202.6	218.2
VOC, lbs/hour as C1	14.4	12.6	11.8	12.93
VOC, lbs/ODT	2.00	1.74	1.62	1.79
Methanol, ppmvd	3.00	1.95	1.88	2.28
Acetaldehyde, ppmvd	1.51	1.46	1.50	1.49
Acrolein, ppmvd	2.13	1.97	2.03	2.04
Formaldehyde, ppmvd	3.96	1.83	2.10	2.63
Phenol, ppmvd	2.43	2.34	2.41	2.39
Propionaldehyde, ppmvd	0.76	0.81	0.59	0.72
Methanol, lbs/hour	0.483	0.308	0.292	0.36
Acetaldehyde, lbs/hour	0.0	0.0	0.0	0.000
Acrolein, lbs/hour	0.598	0.0	0.0	0.199
Formaldehyde, lbs/hour	0.597	0.272	0.307	0.392
Phenol, lbs/hour	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/hour	0.222	0.233	0.167	0.207
Methanol, lbs/ODT	0.067	0.043	0.040	0.050
Acetaldehyde, lbs/ODT	0.0	0.0	0.0	0.000
Acrolein, lbs/ODT	0.083	0.0	0.0	0.028
Formaldehyde, lbs/ODT	0.083	0.038	0.042	0.054
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.031	0.032	0.023	0.029

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-4. Pellet Cooler 1 ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/12/2013	10/12/2013	10/12/2013	N/A
Start	8:58	10:22	11:41	N/A
Stop	9:58	11:22	12:41	N/A
Throughput, tons/hour	4	4	4	4.0
Moisture Content Outlet, %wt.	7.9	7.9	7.9	7.9
Throughput, ODT/hour	3.68	3.68	3.68	3.68
ACFM	16,168	16,246	16,134	16,182.7
DSCFM	15,189	14,870	14,825	14,961
Stack Temperature, °F	82.3	94.8	97.7	91.6
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	3.35	3.68	2.79	3.27
VOC, ppmvd as Propane	40.4	34.6	36.7	37.2
VOC, ppmvd as C1	121.2	103.8	110.1	111.7
VOC, lbs/hour as C1	3.44	2.88	3.05	3.12
VOC, lbs/ODT	0.93	0.78	0.83	0.85
Methanol, ppmvd	0.56	0.34	0.36	0.42
Acetaldehyde, ppmvd	0.71	0.73	0.78	0.74
Acrolein, ppmvd	1.01	1.06	1.39	1.15
Formaldehyde, ppmvd	1.49	1.30	1.30	1.36
Phenol, ppmvd	1.03	1.02	1.01	1.02
Propionaldehyde, ppmvd	0.39	0.30	0.25	0.31
Methanol, lbs/hour	0.042	0.026	0.027	0.032
Acetaldehyde, lbs/hour	0.074	0.076	0.081	0.077
Acrolein, lbs/hour	0.135	0.141	0.184	0.153
Formaldehyde, lbs/hour	0.105	0.092	0.092	0.096
Phenol, lbs/hour	0.2	0.0	0.0	0.077
Propionaldehyde, lbs/hour	0.054	0.041	0.000	0.032
Methanol, lbs/ODT	0.011	0.007	0.007	0.009
Acetaldehyde, lbs/ODT	0.020	0.021	0.022	0.021
Acrolein, lbs/ODT	0.037	0.038	0.050	0.042
Formaldehyde, lbs/ODT	0.029	0.025	0.025	0.026
Phenol, lbs/ODT	0.063	0.000	0.0	0.021
Propionaldehyde, lbs/ODT	0.015	0.011	0.000	0.009

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Parameter	Run 1	Run 2	Run 3	N/A
Date	10/13/2013	10/13/2013	10/13/2013	N/A
Start	9:21	11:14	12:31	N/A
Stop	10:21	12:52	13:47	N/A
Throughput, tons/hour	14.5	11.2	11.3	12.3
Moisture Content Outlet, %wt.	18.5	13.45	13.75	15.2
Throughput, ODT/hour	11.82	9.69	9.75	10.4
ACFM	24,998	25,318	25,278	25,198.0
DSCFM	14,745	15,224	14,842	14,937
Stack Temperature, °F	174.3	154.9	171.8	167.0
O ₂ , %	16.5	17	17	16.8
% Moisture	29.04	29.86	29.64	29.5
VOC, ppmvd as Propane	129.4	115.8	138.1	127.8
VOC, ppmvd as C1	388.2	347.4	414.3	383.3
VOC, lbs/hour as C1	10.70	9.88	11.49	10.69
VOC, lbs/ODT	0.91	1.02	1.18	1.03
Methanol, ppmvd	26.5	14.5	15.3	18.795
Acetaldehyde, ppmvd	1.4	4.7	1.4	2.498
Acrolein, ppmvd	2.7	3.7	3.5	3.303
Formaldehyde, ppmvd	9.0	9.4	9.6	9.336
Phenol, ppmvd	3.9	4.0	4.0	3.944
Propionaldehyde, ppmvd	3.3	2.0	2.4	2.575
Methanol, lbs/hour	1.949	1.070	1.129	1.383
Acetaldehyde, lbs/hour	0.138	0.473	0.147	0.253
Acrolein, lbs/hour	0.345	0.476	0.456	0.425
Formaldehyde, lbs/hour	0.622	0.647	0.662	0.644
Phenol, lbs/hour	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/hour	0.445	0.262	0.322	0.343
Methanol, lbs/ODT	0.165	0.110	0.116	0.130
Acetaldehyde, lbs/ODT	0.012	0.049	0.015	0.025
Acrolein, lbs/ODT	0.029	0.049	0.047	0.042
Formaldehyde, lbs/ODT	0.053	0.067	0.068	0.062
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.038	0.027	0.033	0.033

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-6. Dry Hammermill 2¹ Emission Test Results

Parameter	Run 1	Run 2	Run 3	Average
Date	10/11/2013	10/11/2013	10/11/2013	N/A
Start	18:11	19:35	20:48	N/A
Stop	19:11	20:35	21:48	N/A
Throughput, tons/hour	11.18	11.22	11.12	11.2
Moisture Content Outlet, %wt.	10.2	10.3	10.2	10.2
Throughput, ODT/hour	10.04	10.06	9.99	10.0
ACFM	15,197	14,385	15,165	14,916
DSCFM	13,183	12,366	13,303	12,951
Stack Temperature, °F	122.4	128.4	116.4	122.4
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	4.25	4.18	4.18	4.20
VOC, ppmvd as Propane	26.3	31.0	25.5	27.6
VOC, ppmvd as C1	78.9	93	76.5	82.8
VOC, lbs/hour as C1	1.94	2.15	1.90	2.00
VOC, lbs/ODT	0.19	0.21	0.19	0.20
Methanol, ppmvd	0.20	0.22	0.21	0.21
Acetaldehyde, ppmvd	0.75	0.74	0.74	0.74
Acrolein, ppmvd	1.02	1.02	1.01	1.02
Formaldehyde, ppmvd	1.09	1.19	1.16	1.14
Phenol, ppmvd	1.13	1.13	1.13	1.13
Propionaldehyde, ppmvd	0.24	0.25	0.27	0.254
Methanol, lbs/hour	0.013	0.014	0.014	0.014
Acetaldehyde, lbs/hour	0.067	0.067	0.000	0.045
Acrolein, lbs/hour	0.118	0.118	0.000	0.078
Formaldehyde, lbs/hour	0.067	0.073	0.071	0.071
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.029	0.030	0.032	0.030
Methanol, lbs/ODT	0.001	0.001	0.001	0.0014
Acetaldehyde, lbs/ODT	0.007	0.007	0.000	0.0045
Acrolein, lbs/ODT	0.012	0.012	0.000	0.0078
Formaldehyde, lbs/ODT	0.007	0.007	0.007	0.0070
Phenol, lbs/ODT	0.000	0.000	0.000	0.0000
Propionaldehyde, lbs/ODT	0.003	0.003	0.003	0.0030

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-7. Pellet Cooler 2 Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/11/2013	10/11/2013	10/11/2013	N/A
Start	13:43	15:08	16:39	N/A
Stop	14:43	16:08	17:39	N/A
Throughput, tons/hour	15.0	15.0	15.0	15.0
Moisture Content Outlet, %wt.	7.12	7.36	7.17	7.2
Throughput, ODT/hour	13.93	13.90	13.92	13.9
ACFM	13,252	12,718	12,831	12,934
DSCFM	10,938	10,543	10,488	10,656
Stack Temperature, °F	148.9	143.2	152.3	148.1
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	4.86	4.64	4.54	4.68
VOC, ppmvd as Propane	25.0	22.3	26.0	24.4
VOC, ppmvd as C1	75	66.9	78	73.3
VOC, lbs/hour as C1	1.53	1.32	1.53	1.46
VOC, lbs/ODT	0.11	0.09	0.11	0.10
Methanol, ppmvd	0.84	0.71	0.88	0.81
Acetaldehyde, ppmvd	0.90	0.87	0.83	0.87
Acrolein, ppmvd	1.36	1.27	1.39	1.34
Formaldehyde, ppmvd	1.12	0.69	1.93	1.25
Phenol, ppmvd	1.14	1.13	1.13	1.13
Propionaldehyde, ppmvd	0.26	0.26	0.38	0.30
Methanol, lbs/hour	0.046	0.039	0.048	0.044
Acetaldehyde, lbs/hour	0.068	0.065	0.062	0.065
Acrolein, lbs/hour	0.130	0.121	0.133	0.128
Formaldehyde, lbs/hour	0.058	0.035	0.099	0.064
Phenol, lbs/hour	0	0	0	0.000
Propionaldehyde, lbs/hour	0.026	0.000	0.037	0.021
Methanol, lbs/ODT	0.003	0.003	0.003	0.003
Acetaldehyde, lbs/ODT	0.005	0.005	0.004	0.005
Acrolein, lbs/ODT	0.009	0.009	0.010	0.009
Formaldehyde, lbs/ODT	0.004	0.003	0.007	0.005
Phenol, lbs/ODT	0.0	0.0	0.0	0.000
Propionaldehyde, lbs/ODT	0.002	0.000	0.003	0.002

i. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

Table 3-8. Aspiration System ¹ Emission Test Results				
Parameter	Run 1	Run 2	Run 3	Average
Date	10/12/2013	10/12/2013	10/12/2013	N/A
Start	15:09	16:36	18:00	N/A
Stop	16:09	17:36	19:00	N/A
Throughput, tons/hour	15	15	15	15.0
Moisture Content Outlet, %wt.	7.12	8.83	7.85	7.93
Throughput, ODT/hour	13.93	13.68	13.82	13.8
ACFM	1,756	1,692	1,624	1,691
DSCFM	1,079	1,016	985	1,027
Stack Temperature, °F	148.6	148.3	152.1	149.7
O ₂ , %	20.9	20.9	20.9	20.9
% Moisture	27.67	29.33	28.19	28.4
VOC, ppmvd as Propane	1485.8	1354.2	1671.1	1,503.7
VOC, ppmvd as C1	4457.4	4062.6	5013.3	4,511.1
VOC, lbs/hour as C1	8.99	7.71	9.23	8.64
VOC, lbs/ODT	0.65	0.56	0.67	0.63
Methanol, ppmvd	11.5	12.6	11.4	11.81
Acetaldehyde, ppmvd	6.4	5.5	5.2	5.73
Acrolein, ppmvd	4.4	4.4	3.1	3.97
Formaldehyde, ppmvd	1.5	2.2	1.5	1.72
Phenol, ppmvd	3.8	3.9	3.8	3.81
Propionaldehyde, ppmvd	4.1	4.2	4.2	4.19
Methanol, lbs/hour	0.062	0.068	0.061	0.064
Acetaldehyde, lbs/hour	0.048	0.041	0.039	0.042
Acrolein, lbs/hour	0.041	0.042	0.030	0.037
Formaldehyde, lbs/hour	0.000	0.011	0.007	0.006
Phenol, lbs/hour	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/hour	0.000	0.000	0.000	0.000
Methanol, lbs/ODT	0.004	0.005	0.004	0.005
Acetaldehyde, lbs/ODT	0.003	0.003	0.003	0.003
Acrolein, lbs/ODT	0.003	0.003	0.002	0.003
Formaldehyde, lbs/ODT	0.000	0.001	0.001	0.000
Phenol, lbs/ODT	0.000	0.000	0.000	0.000
Propionaldehyde, lbs/ODT	0.000	0.000	0.000	0.000

1. Note: Shaded area indicates a calculated minimum detection limit. Emissions were calculated based on zero for non-detect values.

3.3 Emissions Data Evaluation

Method 25A VOC Concentrations

The VOC emissions from the various process units ranged from 0.10 to 1.79 pounds per ODT. VOC emissions were highest from the two dryers.

Dryer 1 had an emission rate of 1.79 pounds per ODT, and Dryer 2 had an emission rate of 1.03 pounds per ODT. This is equivalent to a 79% difference despite the fact that the dryers were handling similar hardwood/softwood blends and were generating wood with similar outlet moisture levels. The dryer outlet temperatures were also similar. These data clearly demonstrate that VOC emissions from the dryers are due to two factors: (1) the performance of the wood waste burner supplying the heat to the dryer, and (2) volatilization of VOCs from the wood in the dryer. Of these two sources, contributions of the burner are most important.

Due to the dominance of the burner in establishing the VOC emission rates from the combined burner/dryer source, the importance of the hardwood/softwood ratio is less important than previously thought. Changes in the hardwood/softwood ratio do not necessarily affect the VOC emissions from the burner.

The emissions of organic HAP compounds are not sensitive to the hardwood/softwood ratio. The data summarized in the Phase I report indicate that emissions of organic HAPs decreased slightly as the softwood content increased from 10% to 100%.

The data summarized in Tables 3-2 through 3-8 indicate that the total VOC emissions from the Wiggins Plant exceed 100 tons per year calculated as carbon. These tests confirm that the plant is a major source for VOCs.

The accuracy of the VOC data is demonstrated by a Method 25A response factor of approximately 1 for the group of compounds present in the gas stream. The Method 25A response is expressed in terms of a response factor that is defined as the observed Method 25A concentration divided by the true concentration. The Method 25A FID has a response factor close to 1.0 for a large set of organic compounds. Some high molecular weight organics have a response factor larger than 1, and in some cases, approaching 1.5. For these compounds, Method 25A is biased to higher-than-true concentrations. Some low molecular weight highly oxygenated organic compounds such as methanol and formaldehyde have very low response factors in the range of 0.1 to 0.4. For these compounds, Method 25A is biased to lower-than-true concentrations.

As part of the laboratory tests reported to MDEQ in Enviva's Phase I emission study dated July 31, 2013⁽⁴⁾ (the "Phase I Study"). Air Control Techniques, P.C. has taken the following two independent approaches in assessing the Method 25A response factors: (1) direct measurement of the Method 25A response factor using an alpha-pinene gas standard, the dominant organic compound measured during the laboratory tests and (2) a comparison of the Method 25A concentration data with the summed concentrations of all of the specific organics measured simultaneously using NCASI Method 98.01 and EPA Method 18. The results of these response factor analyses are presented in Tables 3-9 and 3-10.

Alpha-Pinene Gas Standard, as C ₁₀ H ₁₆	259 ppm
Alpha-Pinene Gas Standard, as C ₃	863 ppm
FID Response, as C ₃	888 ppm
Response Factor as C ₃	1.03

1. Note: This table was included in the Phase I Study report to MDEQ.

Run	Process Type	Softwood Content, %	Method 25A versus Combined NCASI 98.01 and Method 18	Dominant Compounds	Other Important Compounds
4	Dryer	10	0.72	α-and β-Pinene	Acetone, Methanol
5	Dryer	10	0.70	α-and β-Pinene	Acetone, Methanol
6	Dryer	10	0.75	α-and β-Pinene	Methanol, Formaldehyde
21	Dryer	10	1.23	α-and β-Pinene	Acetone, Methanol
22	Press	10	1.05	α-and β-Pinene	Acetone, Methanol
7	Dryer	70	0.85	α-and β-Pinene	Acetone
8	Dryer	70	0.90	α-and β-Pinene	Acetone
9	Dryer	70	1.02	α-and β-Pinene	Acetone
10	Dryer	70	0.91	α-and β-Pinene	Acetone
24	Press	70	1.51	α-and β-Pinene	Acetone, Methanol
11	Dryer	100	0.99	α-and β-Pinene	Acetone
12	Dryer	100	0.96	α-and β-Pinene	Acetone
13	Dryer	100	0.85	α-and β-Pinene	Acetone
14	Dryer	100	0.87	α-and β-Pinene	Acetone
16	Dryer	100	1.09	α-and β-Pinene	Methanol, Acetone
19	Dryer	100	1.21	α-and β-Pinene	Methanol, Acetone
20	Press	100	1.13	α-and β-Pinene	Methanol, Acetone
Test Program Average			0.98		

1. Note: This table was included in the Phase I Study report to MDEQ.

The excellent agreement between the Method 25A total concentration and the combined concentrations of all of the organics measured by NCASI 98.01 and EPA Method 18 demonstrate that Method 25A is an appropriate VOC measurement technique for wood pellet production facilities.

Method 320 HAP Concentrations

At the maximum permitted production limit of 185,550 ODT per year, five of the six organic HAP compounds measured by Method 320 were each emitted at a rate less than 10 tons per year. The methanol emission rate at this production level was 11.0 tons per year. The combined emission rate of all six organic HAPs was slightly over 31.1 tons per year at the maximum permitted production rate.

The list of HAPs specifically included in the test protocol included methanol, acetaldehyde, acrolein, formaldehyde, phenol, and propionaldehyde. This list was compiled based on (1) the organic compounds identified in laboratory analyses of pellet production facilities emissions, (2) previous emission tests conducted in the Pellet Manufacturing Industry, and (3) organic HAPs identified in studies of other wood products industries—specifically, MDF production.

The results of this test program indicate that this list of HAPs compounds needs to be amended. Phenol was detected at low concentration in only one of the tests of the seven process units. Furthermore, propionaldehyde was not detected in most of the tests.

The low to non-detectable phenol emissions data are consistent with the results of the Phase I Study. Phenol was not identified at detectable concentrations in any of the laboratory studies summarized in the Phase I Study report. The emission rates of phenol reported in the November 2012 Wiggins report ^[2] ranged from 0.0002 to 0.0018 pounds per hour—all insignificant emission rates. Phenol was also not listed in previous emission tests reviewed in preparation for this test program. Phenol was included in the test protocol primarily because other researchers such as Beauchemin and Tampier, ^[5] Milot, ^[6] and Milot and Mosher ^[7] listed phenol due to its inclusion in tests conducted at MDF and particleboard facilities. However, phenol emissions in MDF and particleboard production are due to the use of phenolic resins and similar binders. There is no reason to expect any appreciable phenol formation in pellet production considering (1) the lack of binders of any type in pellet production, (2) the higher moisture levels in pellet production as compared to MDF and particleboard processes, and (3) the lower material temperatures in pellet process equipment. Air Control Techniques, P.C. has assigned zero values to non-detected concentrations.

Acetaldehyde, propionaldehyde, and acrolein had very low concentrations in most of the emission tests summarized in this report. The IR absorption spectra of both water and the terpene compounds overlap the absorption spectra of acetaldehyde, propionaldehyde, and acrolein. Accordingly, the reported concentrations of these three compounds are biased to higher-than-true levels to the extent that this interference could not be avoided by Method 320 spectral absorption modeling. Zero values have been assigned when these concentrations were below detection limits of Method 320 due, in part, to the interference bias.

The use of zero values for non-detected compounds is an appropriate approach for any source, such as pellet production, where there are a few dominant compounds (i.e. methanol and formaldehyde) and a large number of possible compounds at extremely low levels such as phenol, acetaldehyde, and propionaldehyde. The use of non-detect or one-half non-detect concentrations in emission calculations for a large number of compounds potentially present at trace levels inherently makes any source “major” regardless of the actual emissions, size, or operations characteristics of the emission unit.

3.4 VOC and Organic HAP Emission Summary

Table 3-11 summaries annual emissions of VOC and organic HAP compounds. The annual emission rates are based on operation at the permit limited production rate of 185,550 ODT.

As discussed, the plant has never operated at the maximum permitted production limit of 185,550 ODT per year. The VOC and HAP emissions based on the newly proposed maximum production rate of 140,000 ODT/year are summarized in Table 3-12.

The VOC emissions at the lower production rate are well below the PSD threshold of 250 tons per year. The combined HAPs emissions are less than 25 tons per year, and none of the HAPs are emitted at more than 10 tons per year. Accordingly, at this production limit, the plant is not above the major source threshold for HAPs.

Table 3-11. Total Emissions at Plant Permit Limit of 185,550 ODT/Year

Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
Total VOC	66.3	57.6	11.1	21.1	15.7	7.8	46.4	7.4	233.5
Organic HAPs									
Methanol	1.85	7.26	0.08	0.27	0.16	0.24	0.34	0.05	10.3
Acetaldehyde	0.00	1.40	0.25	0.61	0.39	0.35	0.23	0.17	2.0
Acrolein	1.03	2.32	0.43	1.24	0.77	0.68	0.20	0.29	7.0
Formaldehyde	2.01	3.48	0.39	0.37	0.49	0.34	0.03	0.26	7.4
Phenol	0.00	0.00	0.00	0.00	0.39	0.00	0.00	0.00	0.4
Propionaldehyde	1.06	1.82	0.17	0.09	0.16	0.11	0.00	0.11	3.5
Total HAPS	5.96	14.87	1.32	2.59	2.35	1.72	0.80	0.88	31.89

Table 3-12. Total Emissions at Plant Permit Limit of 140,000 ODT/Year

Analyte	Dryer 1	Dryer 2	Dry Hammermill 2	Green Hammermill	Pellet Cooler 1	Pellet Cooler 2	Aspirator	Dry Hammermill 1	Total
VOC Total	50.1	43.4	8.4	15.9	11.7	5.9	35.0	5.6	175.9
Organic HAPs									
Methanol	1.40	5.48	0.06	0.21	0.12	0.18	0.26	0.04	7.7
Acetaldehyde	0.00	1.06	0.19	0.46	0.29	0.26	0.17	0.12	2.6
Acrolein	0.78	1.75	0.33	0.93	0.58	0.51	0.15	0.22	5.3
Formaldehyde	1.52	2.62	0.30	0.28	0.37	0.26	0.03	0.20	5.6
Phenol	0.00	0.00	0.00	0.00	0.29	0.00	0.00	0.00	0.3
Propionaldehyde	0.80	1.37	0.13	0.07	0.12	0.08	0.00	0.08	2.7
Total HAPS	4.50	12.28	0.99	1.95	1.78	1.30	0.61	0.66	24.06

4. SAMPLING LOCATIONS

4.1 Dryer # 1 Stack Sampling Location

The Dryer 1 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-1. Twelve sampling points were used to measure the gas flow rate.

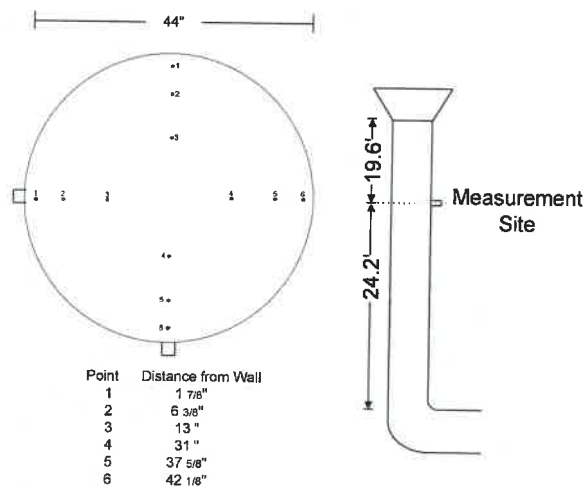


Figure 4-1 Dryer # 1 Stack Sampling Location

The downstream¹ flow disturbance is the stack discharge. The upstream flow disturbance is the duct from the fan entering the base of the stack.

During the sampling program, only the port facing south was used. The port facing east was blocked by the stack support equipment and the Dry Hammermill 1 ductwork. Test personnel reached all of the sampling ports by angling the probe inserted through the south port.

No cyclonic flow conditions were observed in the Dryer 1 stack. The point-by-point cyclonic flow checks indicated an average flow angle 3.1 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dryer 1 stack is shown in Figure 4-2.



Figure 4-2. Photograph of the Dryer 1 Stack

¹ "Upstream" and "downstream" are defined based on the sampling location as the reference point.

4.2 Dryer 2 Stack Sampling Location

The Dryer 2 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-2. Twelve sampling points were used to measure the gas flow rate.

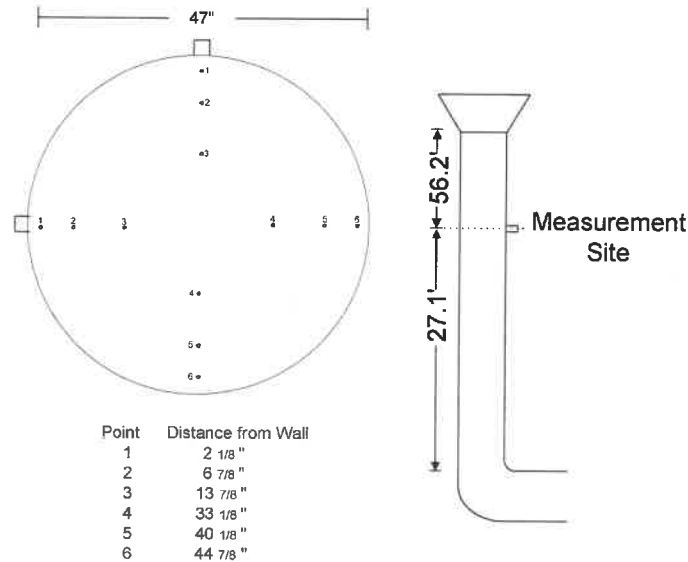


Figure 4-3. Dryer # 2 Stack Sampling Location

The downstream flow disturbance is the stack discharge. The upstream flow disturbance is the duct from the fan entering the base of the stack.

During the sampling program, only the port facing west was used in the test program. The port facing north could not be reached without potentially interrupting operation of the CEM sampling equipment. Test personnel reached all of the sampling ports by angling the probe inserted through the west port.

No cyclonic flow conditions were observed in the Dryer 2 stack. The point-by-point cyclonic flow checks indicated an average flow angle 2.4 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dryer 2 stack is shown in Figure 4-4.



Figure 4-4. Photograph of the Dryer 2 Stack

4.3 Dry Hammermill 2 Cyclone Outlet Sampling Location

The Dry Hammermill 2 sampling location meets EPA Method 1 location requirements as indicated in Figure 4-5. Twelve sampling points were used to measure the gas flow rate.

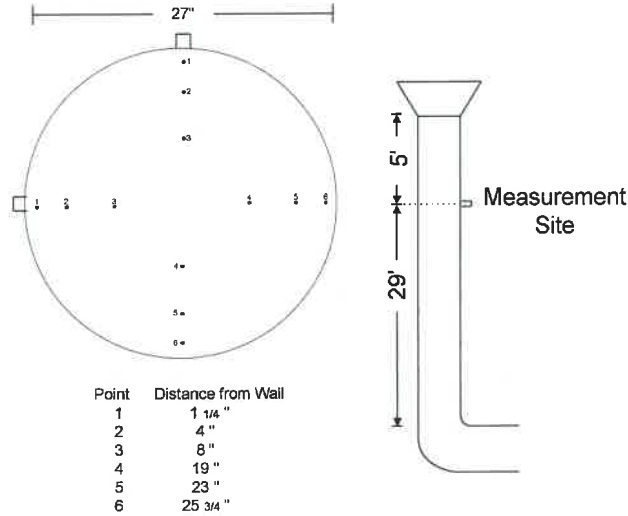


Figure 4-5. Dry Hammermill 2 Sampling Location

The downstream flow disturbance is an elbow in the fan outlet duct. The upstream flow disturbance is the fan discharge. During the sampling program both ports were accessible.

No cyclonic flow conditions were observed in the Dry Hammermill 2 stack. The point-by-point cyclonic flow checks indicated an average flow angle of 0.6 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Dry Hammermill 2 stack is shown in Figure 4-6.



Figure 4-6. Photograph of the Dry Hammermill 2 Sampling Location

4.4 Pellet Mill Aspiration System Sampling Location

The Pellet Mill Aspiration System has a six-inch diameter. Gas flow rate sampling was performed in general accordance with EPA Method 1A. The sampling port location met EPA Method 1 location requirements as indicated in Figure 4-7. A total of eight sampling points were used—four in a horizontal direction and four reached by an angled probe in the vertical direction. Due to the position of the duct and surrounding equipment, it was not possible to sample from any orientation except horizontal.

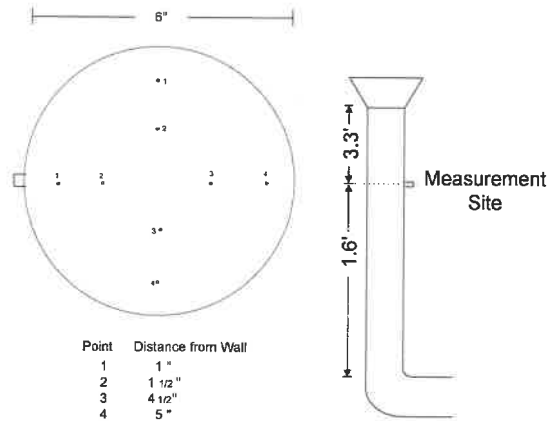


Figure 4-7. Pellet Mill Aspiration System Sampling Location

The upstream flow disturbance was an entry duct from Pellet Mill 6. The downstream flow disturbance was the fan inlet.

No cyclonic flow conditions were observed in the Pellet Mill Aspiration System outlet duct. The point-by-point cyclonic flow checks indicated an average flow angle of 0.75 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Mill Aspiration System sampling location is shown in Figure 4-8.



Figure 4-8. Photograph of the Pellet Mill Aspiration System Sampling Location

4.5 Pellet Mill 2 Cooler Stack Sampling Location

The Pellet Mill 2 Cooler stack sampling location meets the minimum requirements specified in Method 1, Section 11.1. As indicated in Figure 4-9, the downstream² disturbance (stack exit) is 0.6 stack diameters from the sampling location. The minimum allowed by Method 1 is 0.5 stack diameters. The upstream flow disturbance was the fan outlet duct. The distance to the upstream flow disturbance meets Method 1 requirements. Both sampling ports were used in the test program.

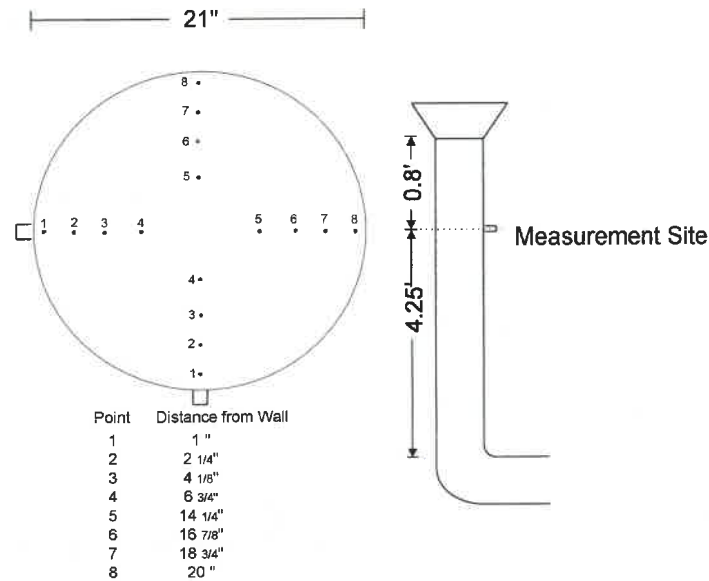


Figure 4-9. Pellet Mill 2 Cooler Stack Sampling Location

No cyclonic flow conditions were observed in the Pellet Mill 2 Cooler stack. The point-by-point cyclonic flow checks indicated an average flow angle of 1.5 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Cooler 2 stack is shown in Figure 4-10



Figure 4-10. Photograph of the Pellet Cooler 2 Stack

² The terms “upstream” and “downstream” are defined based on the test location as the reference point. A recent change in a figure in EPA Method 1 has these terms incorrectly stated.

4.6 Pellet Mill 1 Cooler Stack

The Pellet Mill 1 Cooler stack sampling location meets the minimum requirements specified in Method 1, Section 11.1. As indicated in Figure 4-11, the downstream disturbance (stack exit) is 0.6 stack diameters from the sampling location. The minimum allowed is 0.5 stack diameters. The upstream flow disturbance is the fan outlet duct. The distance to the upstream flow disturbance meets Method 1 requirements. Four of the six sampling ports were used in the test program. The plugs in two of the ports could not be removed.

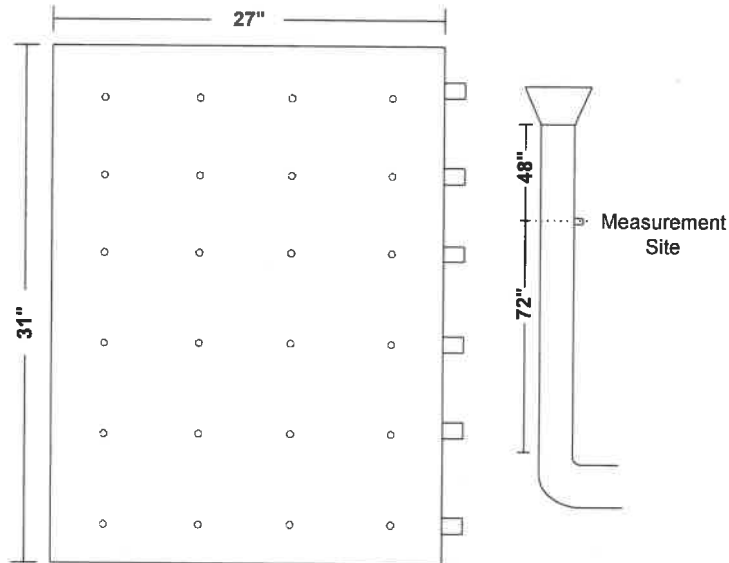


Figure 4-11. Pellet Mill 1 Cooler Stack Sampling Location

No cyclonic flow conditions were observed in the Pellet Mill 1 Cooler stack. The point-by-point cyclonic flow checks indicated an average flow angle of 2.0 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Pellet Mill 1 Cooler Stack is shown in Figure 4-12.



Figure 4-12. Photograph of the Pellet Mill 1 Cooler Stack

4.7 Green Hammermill Stack Sampling Location

The Green Hammermill stack sampling location shown in Figure 4-13 meets the minimum requirements for a downstream flow disturbance specified in Method 1, Section 11.1. The upstream flow disturbance is the fan outlet duct. The downstream flow disturbance is the stack discharge. The distance to the upstream flow disturbance meets Method 1 requirements. Only one sampling port could be reached safely. All of the sampling ports were reached by angling the Pitot tube inserted through the port facing south.

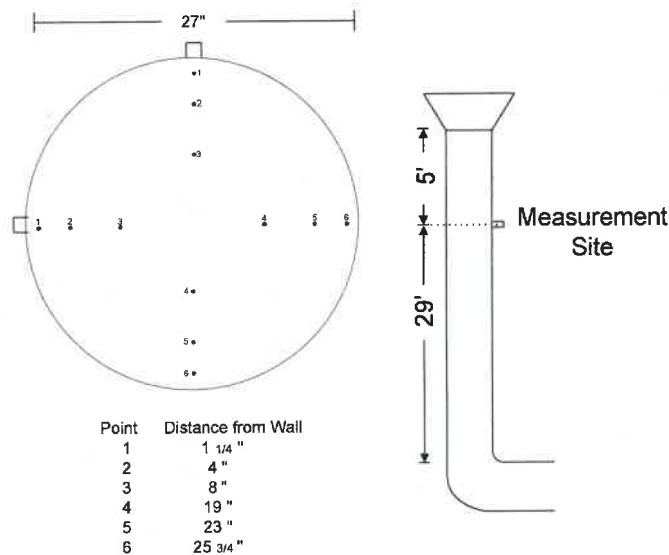


Figure 4-13. Green Hammermill Stack Sampling Location

No cyclonic flow conditions were observed in the Green Hammermill stack. The point-by-point cyclonic flow checks indicated an average flow angle of 1.7 degrees. This meets the requirements of Section 11.4 of Method 1. A photograph of the Green Hammermill stack is shown in Figure 4-14.



Figure 4-14. Photograph of the Green Hammermill Fan Inlet

5. TESTING PROCEDURES

5.1 Flue Gas Velocity and Volumetric Flow Rate - EPA Method 2

The flue gas velocities and volumetric flow rates during all of the emission tests were determined according to the procedures outlined in U.S. EPA Reference Method 2. Velocity measurements were made using S-Type Pitot tubes conforming to the geometric specifications outlined in Method 2. Accordingly, each Pitot was assigned a coefficient of 0.84. Velocity pressures were measured with fluid manometers. Effluent gas temperatures were measured with chromel-alumel thermocouples attached to digital readouts.

5.2 Flue Gas Composition and Molecular Weight - EPA Method 3

Flue gas analyses and calculation of flue gas dry molecular weights were performed in accordance with EPA Method 3. A stainless steel probe was inserted into the gas stream to collect a representative sample of the flue gas during each test run. The samples were analyzed using a Fyrite gas analyzer. Moisture was removed from the sample gas by means of a knockout jar located prior to the sample pump.

5.3 Flue Gas Moisture Content - EPA Method 4

The flue gas moisture content was determined in conjunction with each test run according to the sampling and analytical procedures outlined in EPA Method 4. Wet impinger sampling trains were used to withdraw and analyze the stack gas. The impingers were connected in series and contained water in the first two impingers followed by an empty impinger and then a silica gel impinger. The impingers were contained in an ice bath to assure condensation of the flue gas stream moisture. Any moisture that was not condensed in the impingers was captured in the silica gel; therefore, all moisture was weighed and entered into moisture content calculations.

5.4 Total Hydrocarbons – EPA Method 25A

Continuous emissions monitoring was conducted for volatile organic compounds. The sampling and analytical procedures for VOCs were conducted in accordance with EPA 25A. The CEM system consisted of a sample acquisition system, the THC emission monitor, and a data acquisition system (DAS). A California Analytical Model 300 flame ionization detector was used for the Method 25A tests.

The sample acquisition system included an in-stack probe, a heated out-of-stack glass mat filter for particulate matter removal, a heat-traced Teflon® sample line, a Teflon® heated-head pump, and a gas manifold board. All components of the sample acquisition system that contacted the sampled gas were constructed of Type 316 stainless steel or Teflon®. The sample gas was continuously extracted from a central point within the duct at a constant rate ($\pm 10\%$) for the duration of each test run. The wet, filtered gas was transported to a heated-head pump located at the CEM laboratory. The sample gas was sent directly to the VOC analyzer. Care was taken to ensure that the sample gas was greater than 250°F during transport from the stack to the VOC monitor. All pretest and posttest calibration procedures were performed as outlined in the EPA Reference Method 25A.

Total organic hydrocarbon concentrations were measured on a wet basis using a California Analytical 300 FID continuous emission monitor. The THC concentrations were monitored on a propane (C₃) basis using a flame ionization detector (FID). The FID was fueled by a gas mixture consisting of 40% helium and 60% hydrogen to reduce the effect of oxygen synergism. The

THC analyzer was calibrated with a set of at least four gas standards. Calibration tests were performed prior to and following each test run.

Outputs from the individual emission monitors were connected to a computerized data acquisition system. Outputs from the analyzer were sent to a portable computer via a National Instruments™ FieldPoint controller. The signals were downloaded to a STRATA® software program every two seconds. The two-second readings were averaged for the duration of the test run.

Total mass emissions of VOCs were determined based on the Method 25A total hydrocarbon concentration data. The mass emissions were expressed on a pounds mass of carbon per hour.

5.5 Organic HAP Compounds – EPA Method 320

Testing for wet-basis organic HAP concentrations was conducted by extractive Fourier transform infrared (FTIR) spectroscopy using EPA Method 320 (40CFR, Part 63, Appendix A). Sample gas was continuously passed through the sampling system, which included an in-stack probe, a heated out-of-stack glass mat filter for particulate matter removal, a Teflon® heat-traced sample line, a MIDAC Fourier Transform Infrared (FTIR) spectrometer, a Teflon® heated-head pump, and a gas manifold board as shown in Figure 5-1. All components of the sample acquisition system that contacted the sampled gas were Type 316 stainless steel or Teflon®. All components of the sampling system and the FTIR cell were maintained at or above 120° C. Air Control Techniques, P.C. took great care to ensure that the sampling system contained no “cold spots” to prevent organic HAP loss. The sampling rate was maintained at approximately 10 liters per minute.

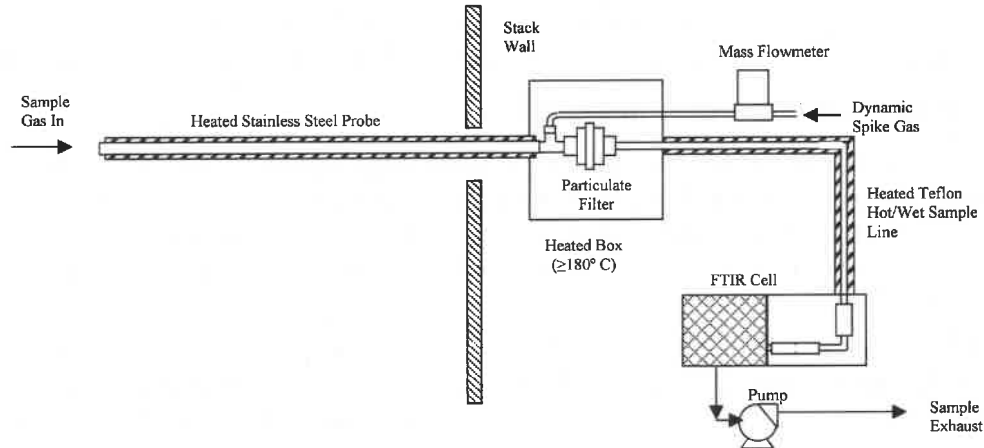


Figure 5-1. Method 320 Organic HAP Sampling System

The FTIR system included a MIDAC Corporation I-1301 spectrometer equipped with a heated, nominal 10-meter path absorption cell, a potassium bromide (KBr) beam splitter, zinc selenide (ZnSe) non-hygroscopic windows, and a liquid nitrogen-cooled Mercury Cadmium Telluride detector. Measurements were made using a MIDAC Model I-1301 high resolution Michelson interferometer with AutoQuant Pro software. Sample gas continuously passed through the sampling system, and sample spectra (based on 50 co-added interferograms) were recorded every

minute. The system's nominal spectral resolution was 0.5 cm^{-1} . Samples and standards were analyzed at temperatures greater than 120°C and near ambient pressures.

The inside walls of the cells were polished stainless steel to minimize interaction of the sample with the cell walls, and the cell mirrors were of bare gold. The gas pressure in the FTIR sample cell was monitored with a pressure transducer connected directly to the sample cell. The heated sample cell was wrapped in an insulating thermal jacket, and the temperature was controlled with type J thermocouples. The absorption cell volume was approximately 2 liters.

The FTIR system was operated via a portable computer, and a data archive storage system (USB Mass Storage Drive) was used for data backup. All interferograms, single beams, absorbance spectra, and background single beams were stored and have been archived. The filename, time, pressure and temperature of the sample cell, scan rate, background identification and other pertinent information was recorded by hand during the test program.

Air Control Techniques used the program AutoquantPro™ Version 4.5.0.195, (©Midac Corporation, 2012) to collect and analyze all the infrared field data. The program allows the development and storage of analytical "methods" for analysis of spectral data (absorbance) files. The reference spectra used for these analyses were developed by MIDAC Corporation, EPA, and Enthalpy Analytical, Inc. One "model" was developed for determining the absorption path length and one additional "method" for determining the concentrations of the target compounds for each source.

The concentration uncertainty reported by AutoquantPro is called the Standard Error of the Estimated Concentration, or SEC; it is also known as the Marginal Standard Deviation. The uncertainties in the concentration are proportional to the square root of the sums of the squares of the residual. After the residual spectrum is obtained, which we will call R, the error variance for the case of a single reference spectrum is calculated as follows.

$$\sigma^2 = \frac{\sum_i R_i^2}{(n-1)}$$

Where n is the number of observations. The SEC is given by the following.

$$SEC = \frac{\sigma C}{\sqrt{\sum_i A_i^2}}$$

Where A is the spectrum and C is the known concentration of the reference.

The 95% confidence interval is 1.96 times the SEC.

6. QUALITY ASSURANCE

6.1 Method 1 Quality Assurance

All S-type Pitot tubes used in this project conformed to EPA guidelines concerning construction and geometry. Pitot tubes were inspected prior to use. Information pertaining to S-type Pitot tubes is presented in detail in Section 3.1.1 of EPA Publication No. 600/4-77-027b. Only S-type Pitot tubes meeting the required EPA specifications were used in this project.

The thermocouples used in this project were calibrated using the procedures described in Section 3.4.2 of EPA Publication No. 600/4-77-027b. Each temperature sensor was calibrated at a minimum of three points over the anticipated range of use against NIST-traceable mercury in glass thermometer.

6.2 Method 4 Quality Assurance

Pretest and posttest leak checks were conducted on each Method 4 sampling train used. The observed leak rates for the sampling trains were below 0.02 actual cubic feet per minute as required by Method 4.

All dry gas meters were fully calibrated to determine the volume correction factor prior to field use. Post-tests calibration checks were performed as soon as possible after the equipment was returned to the laboratory. Pre-and post-test calibrations agreed within ± 5 percent. The calibration procedure is documented in Section 3.3.2 of EPA Publication No. 600/4-77-237b.

The scales used at the test location to determine flue gas moisture content were calibrated using a standard set of weights.

6.3 Method 25A Quality Assurance

At the beginning of the test day, a linearity calibration test was performed on each analyzer. The continuous emission monitoring instrument response did not differ by more ± 5 from the propane calibration standard. Linearity results for the test program are provided in Table 6-1 through 6-8.

Prior to and following each test run, a system calibration test was performed. The system test was performed to verify that the sampling system did not contain leaks (system bias) and to measure a change in analyzer response during the test program (system drift). The system bias was less than $\pm 5\%$ of full-scale, and system drift was less than $\pm 3\%$ of full scale. System calibration results for the test program are provided in Tables 6-1 through 6-8.

Table 6-1. Dryer 1 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.8	0.1
Zero Bias (Post), %	±5	0.9	0.1	0.0
Up-scale Bias (Pre), %	±5	0.0	-0.2	-0.6
Up-scale Bias (Post), %	±5	0.1	-0.6	-1.0
Zero Drift, %	±3	0.9	-0.7	-0.2
Up-scale Drift, %	±3	0.1	-0.4	-0.4
Response Time, sec	N/A			

Table 6-2. Pellet Cooler 1 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.4		
Mid, %	±5	0.8		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.3	0.2
Zero Bias (Post), %	±5	0.3		0.3
Up-scale Bias (Pre), %	±5	0.1	-0.1	-0.1
Up-scale Bias (Post), %	±5	-0.1		0.3
Zero Drift, %	±3	0.3	-0.1	0.1
Up-scale Drift, %	±3	-0.1	0.0	-0.1
Response Time, sec	N/A			

Table 6-3. Dryer 2 Quality Assurance Results, Total Hydrocarbons, Method 25A, High Range				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.3		
Mid, %	±5	-0.1		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	-0.1
Zero Bias (Post), %	±5	0.1	-0.1	-0.1
Up-scale Bias (Pre), %	±5	0.0	-0.3	-0.4
Up-scale Bias (Post), %	±5	-0.3	-0.4	-0.3
Zero Drift, %	±3	0.1	-0.1	0.0
Up-scale Drift, %	±3	-0.3	-0.1	0.1
Response Time, sec	N/A	28		

Table 6-4. Dryer 2 Quality Assurance Results, Total Hydrocarbons, Method 25A, Low Range				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±8	1.0		
Low, %	±8	1.5		
Mid, %	±8	0.7		
High, %	±8	0.1		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.6	-0.6
Zero Bias (Post), %	±5	0.6	-0.6	-0.7
Up-scale Bias (Pre), %	±5	0.0	0.3	0.1
Up-scale Bias (Post), %	±5	0.3	0.1	-0.1
Zero Drift, %	±3	0.6	-1.2	-0.1
Up-scale Drift, %	±3	0.3	-0.2	-0.2
Response Time, sec	N/A	28		

Table 6-5. Dry Hammermill 2 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.2	0.0	0.2
Zero Bias (Post), %	±5	0.0	0.2	0.2
Up-scale Bias (Pre), %	±5	-1.3	-1.1	-1.3
Up-scale Bias (Post), %	±5	-1.1	-1.3	-1.2
Zero Drift, %	±3	-0.1	0.1	0.0
Up-scale Drift, %	±3	0.2	-0.1	0.0
Response Time, sec	N/A	28		

Table 6-6 Pellet Cooler 2 Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0		
Low, %	±5	0.4		
Mid, %	±5	2.2		
High, %	±5	0.0		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.3	0.1
Zero Bias (Post), %	±5	0.3	0.1	0.2
Up-scale Bias (Pre), %	±5	-1.0	-0.9	-1.0
Up-scale Bias (Post), %	±5	-0.9	-1.0	-1.3
Zero Drift, %	±3	0.3	-0.2	0.0
Up-scale Drift, %	±3	0.1	-0.1	-0.3
Response Time, sec	N/A	28		

Table 6-7. Aspiration Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.1		
Low, %	±5	0.7		
Mid, %	±5	0.0		
High, %	±5	0.1		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	0.0
Zero Bias (Post), %	±5	0.1	0.0	0.1
Up-scale Bias (Pre), %	±5	0.0	-0.1	-0.1
Up-scale Bias (Post), %	±5	-0.1	-0.1	-0.3
Zero Drift, %	±3	0.1	-0.1	0.1
Up-scale Drift, %	±3	-0.1	0.1	-0.3
Response Time, sec	N/A	28		

Table 6-8. Green Hammermill Quality Assurance Results, Total Hydrocarbons, Method 25A				
Linearity Tests				
Parameter	Allowable	Test Series		
Zero, %	±5	0.0		
Low, %	±5	1.1		
Mid, %	±5	1.6		
High, %	±5	0.4		
System Tests				
Parameter	Allowable	Run 1	Run 2	Run 3
Zero Bias (Pre), %	±5	0.0	0.1	0.1
Zero Bias (Post), %	±5	0.1	0.1	0.1
Up-scale Bias (Pre), %	±5	0.0	-0.1	-0.7
Up-scale Bias (Post), %	±5	-0.1	-0.7	-1.0
Zero Drift, %	±3	0.1	-0.1	0.1
Up-scale Drift, %	±3	-0.1	-0.5	-0.3
Response Time, sec	N/A	28		

6.4 Method 320 Quality Assurance

Air Control Techniques, P.C. performed daily quality assurance checks. Background scans and calibration transfer standard (CTS) spectra tests were performed prior to and following each test series. An analyte spike was performed using methanol.

The flow rate at the outlet of the pump was measured while the probe was plugged to verify that the sampling system was leaks. The flow rate was less than 200 ml/min.

The FTIR cell was tested for leaks by closing the valve while the cell was at minimum absolute pressure.

Background Spectra

Sample spectra were divided point-by-point by a 128-scan background recorded using N₂. The single beam spectrum was constantly monitored, and a new background was generated approximately following each test series or when residual and absorbance spectra indicated component build-up on the optical surfaces or alignment-related baseline shifts.

Calibration Transfer Standards and Absorption Path Lengths

A cylinder of 100 ppm ethylene in nitrogen served as the CTS. A CTS gas was introduced to the FTIR and allowed to reach steady state. The CTS was used to determine effective cell path length based on comparisons of the “field” CTS spectra to a laboratory CTS spectrum recorded by MIDAC. As shown in Table 6-9, the maximum path length deviation was less than 5% of the average.

Date	Time	CTS Scan (pathlength)	SEC (ppm)	Cell Press. (psi)	Cell Temp (deg C)	Deviation from Previous	Deviation from Average
10-Oct	806	8.78	0.137	14.7	121	NA	-0.6%
	1927	8.68	0.120	14.89	121	1.1%	0.5%
11-Oct	1121	8.73	0.134	14.8	121	-0.6%	-0.1%
	1301	8.73	0.133	14.7	121	0.0%	-0.1%
	1755	8.75	0.133	14.6	121	-0.3%	-0.3%
	2204	8.72	0.133	14.8	121	0.4%	0.1%
12-Oct	0809	8.59	0.133	14.9	121	1.4%	1.5%
	1300	8.77	0.137	14.6	121	-2.1%	-0.5%
	1940	8.78	0.134	14.72	121	-0.1%	-0.6%
13-Oct	0810	8.71	0.134	14.82	121	0.7%	0.1%
	1435	8.73	0.135	14.85	121	-0.1%	0.0%
Average		8.725	0.133				

Background Spectra

On-site test personnel performed matrix spiking using a certified calibration standard of methanol and SF₆. The methanol gas standard was introduced into the sampling system upstream of the particulate matter filter at an average dilution ratio of less than 10% of the total sample volume. Analyte spiking was performed to demonstrate the suitability of the sampling system. The dilution factor was calculated based on the ratio of the SF₆ tracer gas analyzed directly by the FTIR and the in-stack measured concentration.

$$\frac{SF_6 \text{ during spike}}{SF_6 \text{ direct}} = DF$$

The recovery was calculated using the mean concentration of the spiked analyte (S_m), the native concentration of the analyte in the stack (S_u), the dilution factor (DF), and the cylinder concentration (C_s).

$$\text{Recovery}(\%) = \frac{S_m - S_u (1 - DF)}{DF \times C_s}$$

As shown in Table 6-10, the percent recovery was 100±30% as required by Method 320.

Table 6-10. Spike Recovery Results Summary

Direct Cylinder Spike, ppm		System Spiked Gas, ppm		Native Concentration, ppm		Recovery, %
methanol	SF ₆	methanol	SF ₆	methanol	SF ₆	
101.26	2.84	9.867	0.272	0.496	-0.00789	94.6

Minimum Detectable Concentration

EPA Method 320 and the equivalent ASTM Standard D6348-03 specify a number of analytical uncertainty parameters that the analyst may calculate to characterize the FTIR system performance.

QA Review

Before the test program began, an analysis of possible analytical interferents (e.g., H₂O, CO₂, CO, pinenes) based on previous stack test data. Analytical wavelengths were determined to minimize analytical uncertainty and detection limits using reference spectra and the FTIR instrument that was used for the field testing.

At the conclusion of the testing a quality assurance review of the test data was performed. This review included examination of the sample spectra and the quantitative analytical results. It also included spot-checking the analysis results by hand. These examinations included visual comparisons of the sample and reference spectra.

7. PROCESS DOCUMENTATION

Enviva Pellets Wiggins, LLC personnel logged the following process data during each test run of each process unit.

- Throughput in tons per hour (all process units)
- Inlet temperature (dryer)
- Outlet temperature (dryer)
- Cyclone static pressure drop (dryer, hammermill, presses)
- Wood feed % softwood content

8. REFERENCES

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4. Richards, J., D. Goshaw, and T. Holder. "Laboratory Evaluation of VOC Emissions from Wood Pellet Processes." Report to Enviva, LP. July 31, 2013.
5. Beauchemin, P. and M. Tampier. "Emissions and Air Pollution Control for the Biomass Pellet Manufacturing Industry." Report submitted to the British Columbia Ministry of the Environment. May 12, 2010.
6. Milota, M.R. "Emissions from Wood Drying" Forest Projects Journal, Volume 50, Number 6, Pages 10-19, June 2000.
7. Milota, M. and P. Mosher. "Emissions of Hazardous Air Pollutants from Lumber Drying." Forest Products Journal, Volume 58, No. 7/8, Pages 50-55, July/August 2008.

APPENDIX A
Moisture and Gas Flow Rate Data

Air Control Techniques, PC: Emissions Calculations
 Job # 1911

Enviva

Wiggins

PARAMETER

NOMENCLATURE

Sampling Location

	Green Hammermill 1	Green Hammermill 2	Green Hammermill 3	Dryer 1 4	Dryer 1 5	Dryer 1 6
Date	10/10/2013	10/10/2013	10/10/2013	10/10/2013	10/11/2013	10/11/2013
Run Time	60	60	60	60	60	60
Nozzle Diameter	N/A	N/A	N/A	N/A	N/A	N/A
Stack Area	3.98	3.98	3.98	10.56	10.56	10.56
Pitot Tube Coefficient	0.84	0.84	0.84	0.84	0.84	0.84
Meter Calibration Factor	0.9828	0.9828	0.9828	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	29.90	29.90	29.90	29.90	29.80	29.80
Static Pressure	-20.8	-20.8	-20.8	-0.75	-0.71	-0.71
Stack Pressure	28.37	28.37	28.37	29.84	29.75	29.75
Meter Box Pressure Differential	1.00	1.00	1.00	1.00	1.00	1.00
Average Velocity Head	3.961	3.854	3.847	1.283	1.172	1.185
Volume of Gas Sampled	33.868	33.981	33.156	33.201	33.221	32.565
Dry Gas Meter Temperature	66.0	70.8	75.5	81.250	76.5	87.0
Stack Temperature	70.8	70.6	70.9	146.3	150.1	147.3
Liquid Collected	25.1	26.5	16.6	129.5	99.8	117.5
Carbon Dioxide	0	0	0	2	4	4
Oxygen	20.9	20.9	20.9	19	17	17
Carbon Monoxide	0	0	0	0	0	0
Nitrogen	79.1	79.1	79.1	79	79	79
Volume of Gas Sampled, Dry	33.472	33.283	32.187	31.888	32.082	30.845
Volume of Water Vapor	1.183	1.249	0.783	6.106	4.706	5.540
Moisture Content	3.41	3.62	2.37	16.07	12.79	15.23
Saturation Moisture	2.7	2.7	2.7	23.1	25.4	23.7
Dry Mole Fraction	0.966	0.964	0.976	0.839	0.872	0.848
Fuel Factor	#DIV/0!	#DIV/0!	#DIV/0!	0.950	0.975	0.975
Gas Molecular Weight, Dry	28.84	28.84	28.84	29.08	29.32	29.32
Gas Molecular Weight, Wet	28.47	28.44	28.58	27.30	27.87	27.60
Gas Velocity	115.87	114.32	113.97	70.16	66.68	67.23
Volumetric Air Flow, Actual	27,642	27,273	27,189	44,448	42,243	42,593
Volumetric Air Flow, Standard	25,184	24,803	25,031	32,404	31,700	31,215

Air Control Techniques, PC: Emissions Calculations
1911

PARAMETER	Enviva	Wiggins	NOMENCLATURE					
Sampling Location								
Date	Dry Hammermill 2 10/11/2013	Dry Hammermill 2 10/11/2001	Dry Hammermill 2 10/11/2013	Dry Hammermill 2 10/11/2013	Dry Hammermill 2 10/12/2013	Dry Hammermill 2 10/12/2013	Dry Hammermill 2 10/12/2013	
Run Time	60	60	60	60	60	60	60	
Nozzle Diameter	N/A	N/A	N/A	N/A	N/A	N/A	N/A	
Stack Area	2.64	2.64	2.64	2.64	2.64	2.64	2.64	
Pitot Tube Coefficient	0.84	0.84	0.84	0.84	0.84	0.84	0.84	
Meter Calibration Factor	0.9828	0.9828	0.9828	0.9828	0.9828	0.9828	0.9828	
Barometric Pressure, inches Hg	29.80	29.80	29.80	29.80	29.85	29.85	29.85	
Static Pressure	1.4	1.4	1.4	1.4	-7.5	-7.5	-7.5	
Stack Pressure	29.90	29.90	29.90	29.90	29.30	29.30	29.30	
Meter Box Pressure Differential	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Average Velocity Head	2.601	2.308	2.618	2.618	5.359	4.944	4.547	
Volume of Gas Sampled	33.419	33.679	33.876	33.876	33.241	32.149	34.408	
Dry Gas Meter Temperature	80.3	78.8	78.3	78.3	85.0	84.8	81.8	
Stack Temperature	122.4	128.2	116.4	116.4	148.6	148.3	152.1	
Liquid Collected	30.2	30	30.2	30.2	256.8	269.6	274.4	
Carbon Dioxide	0	0	0	0	0	0	0	
Oxygen	20.9	20.9	20.9	20.9	20.9	20.9	20.9	
Carbon Monoxide	0	0	0	0	0	0	0	
Nitrogen	79.1	79.1	79.1	79.1	79.1	79.1	79.1	
Volume of Gas Sampled, Dry	32.050	32.389	32.609	32.609	31.654	30.628	32.962	
Volume of Water Vapor	1.424	1.415	1.424	1.424	12.108	12.712	12.938	
Moisture Content	4.25	4.18	4.18	4.18	27.67	29.33	28.19	
Saturation Moisture	12.3	14.4	10.4	10.4	24.9	24.7	27.2	
Dry Mole Fraction	0.957	0.958	0.958	0.958	0.723	0.707	0.718	
Fuel Factor	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	#DIV/0!	
Gas Molecular Weight, Dry	28.84	28.84	28.84	28.84	28.84	28.84	28.84	
Gas Molecular Weight, Wet	28.38	28.38	28.38	28.38	25.84	25.66	25.78	
Gas Velocity	95.95	90.82	95.74	95.74	149.06	143.63	137.85	
Volumetric Air Flow, Actual	15,197	14,385	15,165	15,165	1,756	1,692	1,624	
Volumetric Air Flow, Standard	13,183	12,366	13,303	13,303	1,079	1,016	985	

Air Control Techniques, PC: Emissions Calculations
 Job # 1911

Enviva		Wiggins	
PARAMETER		NOMENCLATURE	
Sampling Location		Dryer 2	Dryer 2
Date		19	20
Run Time		10/13/2013	10/13/2013
Nozzle Diameter	θ	60	60
Stack Area	inches	N/A	N/A
Pitot Tube Coefficient	As - sq. ft.	12.05	12.05
Meter Calibration Factor	Cp	0.84	0.84
Barometric Pressure, inches Hg	Y	0.9828	0.9828
Static Pressure	Bp - in Hg	29.90	29.90
Stack Pressure	Pg - in. H ₂ O	-0.33	-0.33
Meter Box Pressure Differential	Ps	29.88	29.88
Average Velocity Head	Δ H - in. H ₂ O	1.00	1.00
Volume of Gas Sampled	Δ p - in. H ₂ O	0.285	0.300
Dry Gas Meter Temperature	Vm - cu. ft.	31.888	33.650
Stack Temperature	Tm - °F	77.5	89.5
Liquid Collected	Ts - °F	174.3	154.9
Carbon Dioxide	grams	267.7	287.5
Oxygen	% CO ₂	4.5	4
Carbon Monoxide	% O ₂	16.5	17
Nitrogen	% CO	0	0
Volume of Gas Sampled, Dry	% N ₂	79	79
Volume of Water Vapor	Vmstd - cu. ft.	30.841	31.834
Moisture Content	Vwstd - cu. ft.	12.622	13.556
Saturation Moisture	% H ₂ O	29.04	29.86
Dry Mole Fraction	% H ₂ O	44.9	28.5
Fuel Factor	Mfd	0.710	0.701
Gas Molecular Weight, Dry	Fo	0.978	0.975
Gas Molecular Weight, Wet	Md	29.38	29.32
Gas Velocity	Ms	26.08	25.94
Volumetric Air Flow, Actual	vs - ft./sec.	34.58	35.02
Volumetric Air Flow, Standard	Qaw - ACFM	24,998	25,318
	Qsd - DSCFM	14,745	15,224
			29.094
			12.259
			29.64
			42.4
			0.704
			0.975
			29.32
			25.96
			34.97
			25,278
			14,842

Method 1 - Air Control Techniques, P.C.

Date

10/10/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Dryer 1
No. of Ports Available	2
No. of Ports Used	1
Port Inside Diameter, inches	4
Distance From Far Wall To Outside Of Port, Inches	46
Nipple Length And/OR Wall Thickness, Inches	2
Depth Of Stack Or Duct, Inches	44
Stack Or Duct Width (if rectangular), inches	44
Equiv. Diameter = $2DW/(D+W)$, Inches	44
Stack/Duct Area, Square Feet	10.6
($D \times R^2$ or $L \times W$)	
Distance to Flow Disturbances, inches	Upstream 290.4
Diameters	Downstream 235.2
	6.60
	5.35

Velocity	Diameters		Down		Particulate	
	UP	DOWN	2	1.75	1.5	1.25
12	8	7	2	1.75	1.5	1.25
12	7	6	1.5	1.5	1.5	1.5
12	6	5	1.25	1.25	1.25	1.25
16	5	4	1.0	1.0	1.0	1.0
16	4	3	0.75	0.75	0.75	0.75
20	3	2	0.5	0.5	0.5	0.5
24 or 25	2	1	0.25	0.25	0.25	0.25

Point	Location of Points in Circular Stacks or Ducts											
	4	6	8	10	12	14	16	18	20	22	24	26
1	67	44	32	28	21	18	16	14	12	10	8	6
2	250	148	108	82	67	57	49	42	36	30	25	21
3	750	296	184	148	118	99	85	72	60	50	42	35
4	953	704	323	226	177	146	125	109	97	87	79	72
5		664	677	342	250	201	169	146	129	116	103	92
6		668	666	342	250	201	169	146	129	116	103	92
7		668	666	342	250	201	169	146	129	116	103	92
8		668	666	342	250	201	169	146	129	116	103	92
9		668	666	342	250	201	169	146	129	116	103	92
10		668	666	342	250	201	169	146	129	116	103	92
11		668	666	342	250	201	169	146	129	116	103	92
12		668	666	342	250	201	169	146	129	116	103	92
13		668	666	342	250	201	169	146	129	116	103	92
14		668	666	342	250	201	169	146	129	116	103	92
15		668	666	342	250	201	169	146	129	116	103	92
16		668	666	342	250	201	169	146	129	116	103	92
17		668	666	342	250	201	169	146	129	116	103	92
18		668	666	342	250	201	169	146	129	116	103	92
19		668	666	342	250	201	169	146	129	116	103	92
20		668	666	342	250	201	169	146	129	116	103	92
21		668	666	342	250	201	169	146	129	116	103	92
22		668	666	342	250	201	169	146	129	116	103	92
23		668	666	342	250	201	169	146	129	116	103	92
24		668	666	342	250	201	169	146	129	116	103	92

Point	Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12	
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2	
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.6	
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8	
4			87.5	70.0	58.3	50	43.8	38.9	35.0	31.8	29.2	
5				90.0	75	64.3	56.3	50	45.0	40.9	37.5	
6					91.7	76.8	68.8	61.1	55.0	50	46.6	
7						92.9	81.8	72.2	65.0	59.1	54.2	
8							94.8	83.3	75.0	68.2	62.5	
9								96.4	85.0	77.3	70.8	
10									97.0	86.4	79.2	
11										97.5	80.0	
12											98.2	

Point Location Data

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	4.4	1 7/8	3 7/8
2	14.6	6 3/8	8 3/8
3	29.6	13	15
4	70.4	31	33
5	85.4	37 5/8	39 5/8
6	95.6	42 1/8	44 1/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

- 0.0000 - 0.0625 - 0
- 0.0625 - 0.1875 - 1/8
- 0.1875 - 0.3125 - 1/4
- 0.3125 - 0.4375 - 3/8
- 0.4375 - 0.5625 - 1/2
- 0.5625 - 0.6875 - 5/8
- 0.6875 - 0.8125 - 3/4
- 0.8125 - 0.9375 - 7/8
- 0.9375 - 1.0000 - 1

Method 1 - Air Control Techniques, P.C.

Date

10/13/2013

Client	ENVIVA
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Dryer 2

No. of Ports Available	2
No. of Ports Used	1
Port Inside Diameter, inches	4
Distance From Far Wall To Outside Of Port, Inches	55.5
Nipple Length And/Or Wall Thickness, Inches	8.5
Depth Of Stack Or Duct, Inches	47
Stack Or Duct Width (if rectangular), Inches	47
Equip. Diameter = 2DW/(D+W), Inches	12.05
Stack/Duct Area, Square Feet	
(D x R ² or L x W)	
Distance to Flow Disturbances, inches	Upstream 325.2
Diameters	Downstream 674.4
	6.92 14.35

2 diff nipples probe marked to inside of port

Point	% of Duct Depth	Distance From	
		Inside Wall	Outside of Port
1	4.4	2 1/8	10 5/8
2	14.6	6 7/8	15 3/8
3	29.6	13 7/8	22 3/8
4	70.4	33 1/8	41 5/8
5	85.4	40 1/8	48 5/8
6	95.6	44 7/8	53 3/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Velocity	Diameters					Particulate In
	UP	Down	2	1.75	1.5	
12	8	2	12	16	24	22
12	7	1.75	18	24	36	32
12	6	1.5	24	36	54	48
16	5	1.25	30	48	72	64
20	4	1.0	36	60	90	80
24	3	0.75	48	80	120	108

Point	Location of Points in Circular Stacks or Ducts											
	4	5	6	7	8	9	10	11	12	13	14	15
1	67	44	32	26	21	18	16	14	12	10	8	6
2	25.9	14.6	10.6	8.2	6.7	5.7	4.9	4.2	3.6	3.1	2.6	2.2
3	75.0	25.6	19.4	14.6	11.8	9.8	8.5	7.5	6.0	5.1	4.3	3.5
4	93.3	76.4	32.3	22.8	17.7	14.6	12.5	10.9	9.7	8.7	7.9	7.3
5	85.4	67.7	34.2	25.0	20.1	18.9	14.6	12.8	11.5	10.5	9.8	9.2
6	85.6	65.6	35.9	25.9	21.0	19.8	14.6	12.8	11.5	10.5	9.8	9.2
7		69.5	77.4	64.4	38.8	29.3	23.6	20.4	18.6	18.1	18.1	18.1
8		96.6	85.4	75.0	63.4	37.5	29.8	25.0	21.8	18.4	18.4	18.4
9		91.8	82.3	73.1	62.5	38.2	30.9	26.2	23.0	20.0	18.4	18.4
10		87.4	86.2	79.9	71.7	61.6	38.8	31.5	27.2	23.0	20.0	18.4
11			93.3	85.4	78.0	70.4	61.2	38.3	32.3	28.8	25.0	21.8
12			97.9	90.1	83.1	76.4	68.4	59.4	50.7	39.8	30.8	25.0
13			94.3	87.6	81.2	75.0	68.4	59.4	50.7	39.8	30.8	25.0
14			96.2	91.5	85.4	79.6	73.8	67.8	61.8	55.8	50.0	45.0
15			93.1	88.1	83.5	79.2	73.8	67.8	61.8	55.8	50.0	45.0
16			98.4	93.5	87.1	82.0	77.0	71.0	66.0	61.0	56.0	51.0
17				95.6	90.3	85.4	80.6	75.4	70.4	65.4	60.4	55.4
18				96.6	91.5	86.6	81.4	76.4	71.4	66.4	61.4	56.4
19				96.1	91.3	86.4	81.4	76.4	71.4	66.4	61.4	56.4
20				95.7	91.0	86.5	81.4	76.4	71.4	66.4	61.4	56.4
21				96.5	92.1	87.5	82.4	77.4	72.4	67.4	62.4	57.4
22				94.5	89.5	84.5	79.5	74.5	69.5	64.5	59.5	54.5
23				98.5	93.5	88.5	83.5	78.5	73.5	68.5	63.5	58.5
24				98.9	93.9	88.9	83.9	78.9	73.9	68.9	63.9	58.9

Point	Location of Points in Rectangular Stacks or Ducts											
	2	3	4	5	6	7	8	9	10	11	12	
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2	
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5	
3	83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8	20.0	
4	87.5	70.0	58.3	50	43.8	38.8	34.6	31.6	29.0	26.4	24.2	
5	86.3	68.3	56.3	48.3	41.3	36.3	32.3	29.3	26.3	23.3	21.3	
6	86.3	68.3	56.3	48.3	41.3	36.3	32.3	29.3	26.3	23.3	21.3	
7	86.3	68.3	56.3	48.3	41.3	36.3	32.3	29.3	26.3	23.3	21.3	
8	86.3	68.3	56.3	48.3	41.3	36.3	32.3	29.3	26.3	23.3	21.3	
9	86.3	68.3	56.3	48.3	41.3	36.3	32.3	29.3	26.3	23.3	21.3	
10	86.3	68.3	56.3	48.3	41.3	36.3	32.3	29.3	26.3	23.3	21.3	
11	86.3	68.3	56.3	48.3	41.3	36.3	32.3	29.3	26.3	23.3	21.3	
12	86.3	68.3	56.3	48.3	41.3	36.3	32.3	29.3	26.3	23.3	21.3	

- 0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
- 0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
- 0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
- 0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
- 0.4375 - 0.5625 - 1/2

Dryer 2 Run 1

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	19
Plant	Wiggins		Date	10/13/2013
City/State	Wiggins, MS		Gauge ID	909033
Location	Dryer 2		Pitot ID	6Pext
Averages	0.285	174.3	Thermocouple ID	TC25
Point No.	Delta P In Water	Temp Deg F	Angle	
A-1	0.200	168	5	Oxygen % 16.5
2	0.280	173	2	
3	0.330	175	0	Carbon Dioxide % 4.5
4	0.330	175	5	
5	0.300	174	0	Moisture % 29.04
6	0.230	170	0	
B-1	0.210	174	6	Stack Area sq.in. 1734.94
2	0.360	176	3	
3	0.350	177	0	Pbar 29.90
4	0.330	177	0	
5	0.300	177	-4	Static Pressure -0.33
6	0.230	175	4	
0				Pitot Coef. 0.84
0				
0				Start Time 843
0				
0				Stop Time 859
2				
3				Absolute Gas Pressure inches water Ps = 29.88
4				
5				Dry Mole Fraction of Gas Mfd = 0.70959
6				
7				Dry Molecular Weight of Gas lb/lb Mole Md = 29.38
8				
D-1				Wet Molecular Weight of Gas lb/lb Mole Ms = 26.08
2				
3				Average Gas Velocity ft/sec vs = 34.58
4				
5				Dry Volumetric Gas Flow Rate at Standard Conditions SCFM Qsd = 14745
6				
7				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM Qaw = 24998
8				
E-1				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH WSCFH = 1246788
2				
3				
4				
5				
6				LKCH
7				Pre 6-5 good
8				Post 5-3 good

Dryer 2 Run 2

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client Enviva			ACT Run Number	20
Plant Wiggins			Date	10/13/13
City/State Wiggins, MS			Gauge ID	909033
Location Dryer 2			Pitot ID	6Pext
Averages 0.300 154.9			Thermocouple ID	TC25
Point	No.	Delta P In Water	Temp Deg F	
A-1	0.200	167		Oxygen % 17
2	0.800	167		Carbon Dioxide % 4
3	0.310	167		Moisture % 29.86
4	0.330	168		Stack Area sq.in. 1734.94
5	0.340	169		Pbar 29.90
6	0.200	167		Static Pressure -0.33
B-1	0.220	170		Pitot Coef. 0.84
2	0.310	170		Start Time 1047
3	0.310	2		Stop Time 1051
4	0.290	170		
5	0.260	171		
6	0.190	171		
0				
0				
0				
0				
0				
2				
3				Absolute Gas Pressure inches water Ps = 29.88
4				Dry Mole Fraction of Gas Mfd = 0.70135
5				Dry Molecular Weight of Gas lb/lb Mole Md = 29.32
6				Wet Molecular Weight of Gas lb/lb Mole Ms = 25.94
7				Average Gas Velocity ft/sec vs = 35.02
8				Dry Volumetric Gas Flow Rate at Standard Conditions SCFM Qsd = 15224
D-1				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM Qaw = 25318
2				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH WSCFH = 1302430
2				
3				
4				
5				
6				LKCH
7				Pre 6-5 good
8				Post 5-3 good

Dryer 2 Run 3

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	21
Plant	Wiggins		Date	10/13/13
City/State	Wiggins, MS		Gauge ID	909033
Location	Dryer 2		Pitot ID	6Pext
Averages	0.291	171.8	Thermocouple ID	TC25
	Delta P	Temp		
Point No.	In Water	Deg F		
A-1	0.220	169	Oxygen %	17
2	0.250	172	Carbon Dioxide %	4
3	0.320	173	Moisture %	29.64
4	0.320	174	Stack Area sq.in.	1734.94
5	0.330	174	Pbar	29.90
6	0.260	168	Static Pressure	-0.33
B-1	0.240	168	Pitot Coef.	0.84
2	0.310	171	Start Time	1208
3	0.340	172	Stop Time	1215
4	0.330	172		
5	0.310	173		
6	0.280	175		
0				
0				
0				
0				
0				
2				
3			Absolute Gas Pressure inches water	Ps = 29.88
4			Dry Mole Fraction of Gas	Mfd = 0.70356
5			Dry Molecular Weight of Gas lb/lb Mole	Md = 29.32
6			Wet Molecular Weight of Gas lb/lb Mole	Ms = 25.96
7			Average Gas Velocity ft/sec	vs = 34.97
8			Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 14842
D-1			Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 25278
2			Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 1265741
3				
4				
5				
6			LKCH	
7			Pre	3-4 good
8			Post	5-3 good

Method 1 - Air Control Techniques, P.C.

Date

10/10/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Green Hammill

No. of Ports Available	2
No. of Ports Used	1
Port Inside Diameter, inches	30
Distance From Far Wall To Outside Of Port, inches	3
Nipple Length And/Or Wall Thickness, inches	27
Depth Of Stack Or Duct, inches	27
Stack Or Duct Width (if rectangular), inches	3.9761
Equip. Diameter = 2DW/(D+W), inches	
Stack/Duct Area, Square Feet	
(□ x R ² or L x W)	
Upstream	348
Downstream	60
Distance to Flow Disturbances, inches	12.69
Diameters	2.22

Point Location Data

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	4.4	1 2/8	4 2/8
2	14.6	4	7
3	29.6	8	11
4	70.4	19	22
5	85.4	23	26
6	95.6	25 6/8	28 6/8
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

2 diff nipples probe marked to inside of port

Velocity	UP	Down	Particulate
12	8	2	
12	7	1.75	
12	6	1.5	
16	5	1.25	
16	2	0.5	

Note: If more than 8 and 2 diameters and if exact dia is less than 24" use 8 or 9 points

Location of Points in Circular Stacks or Ducts

	4	8	12	16	20	24
1	8.7	4.4	3.2	2.6	2.1	1.8
2	25.0	14.6	10.8	8.2	6.7	5.7
3	75.0	29.6	19.4	14.6	11.8	9.9
4	93.3	79.4	32.3	21.6	17.7	14.8
5		85.4	67.7	34.2	25.0	20.1
6		95.6	60.6	65.6	35.6	28.9
7		88.5	77.4	64.4	36.6	29.8
8		86.8	85.4	75.0	37.5	29.6
9		91.8	97.4	82.3	73.1	62.5
10		97.4	97.4	88.2	79.9	61.9
11			93.3	85.4	76.5	62.2
12			97.9	89.4	79.4	66.7
13			94.3	87.6	81.2	69.5
14			98.2	91.5	85.4	73.8
15			98.1	89.1	83.5	78.2
16			98.4	92.5	87.1	82.0
17			98.4	96.6	90.3	85.4
18			98.4	99.9	93.3	88.4
19			98.4	98.7	91.3	86.8
20			98.4	94.0	88.7	84.0
21			98.4	96.5	92.1	87.5
22			98.4	96.9	92.1	87.5
23			98.4	96.9	92.1	87.5
24			98.4	96.9	92.1	87.5
25			98.4	96.9	92.1	87.5

Location of Points in Rectangular Stacks or Ducts

	2	3	4	5	6	7	8	9	10	11	12
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5
3		83.3	62.5	50.0	41.7	35.7	31.3	27.6	25.0	22.7	20.8
4			87.5	70.0	58.3	50	43.8	38.9	35.0	31.8	29.2
5				80.0	75	64.3	56.3	50	45.0	40.9	37.5
6					81.7	78.8	68.8	61.1	55.0	50	45.8
7						82.9	72.2	65.0	58.3	54.2	50.0
8							83.8	75.0	68.8	64.2	60.0
9								84.4	77.3	70.9	66.2
10									85.0	77.3	73.0
11										86.4	79.2
12											87.5

- 0.0000 - 0.0625 - 0 0.5625 - 0.6875 - 5/8
- 0.0625 - 0.1875 - 1/8 0.6875 - 0.8125 - 3/4
- 0.1875 - 0.3125 - 1/4 0.8125 - 0.9375 - 7/8
- 0.3125 - 0.4375 - 3/8 0.9375 - 1.0000 - 1
- 0.4375 - 0.5625 - 1/2

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	
Client	Enviva		ACT Run Number	1911
Plant	Wiggins		Date	10/10/2013
City/State	Wiggins, MS		Gauge ID	909033
Location	Green Hammermill		Pitot ID	4Pext
			Thermocouple ID	TC25
Averages	3.961	70.8		
Point No.	Delta P In Water	Temp Deg F	Angle	
A-1	2.800	71	0	Oxygen % 20.9
2	3.900	71	1	Carbon Dioxide % 0
3	4.400	71	1	Moisture % 3.41
4	3.800	71	2	Stack Area sq.in. 572.5552696
5	3.800	70	4	Pbar 29.90
6	3.000	70	3	Static Pressure -20.8
B-1	4.200	72	0	Pitot Coef. 0.84
2	4.500	71	0	Start Time 855
3	4.600	71	0	Stop Time 908
4	4.600	70	2	
5	4.400	71	4	
6	3.800	70	3	
0				
0				
0				
0				
0				
2				
3				
4				
5				
6				
7				
8				
D-1				
2				
3				
4				
5				
6				
7				
8				
E-1				
2				
3				
4				
5				
6				
7				
8				
0				
0				

Absolute Gas Pressure inches water	Ps =	28.37
Dry Mole Fraction of Gas	Mfd =	0.96585
Dry Molecular Weight of Gas lb/lb Mole	Md =	28.84
Wet Molecular Weight of Gas lb/lb Mole	Ms =	28.47
Average Gas Velocity ft/sec	vs =	115.87
Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd =	25184
Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw =	27642
Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH =	1564487

LKCH		
Pre	3-4	good
Post	5-3	good

GHM Run 2

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911	
Client	Enviva		ACT Run Number	2	
Plant	Wiggins		Date	10/10/2013	
City/State	Wiggins, MS		Gauge ID	909033	
Location	Green Hammermill		Pitot ID	4Pext	
Averages	3.854	70.6	Thermocouple ID	TC25	
Point	No.	Delta P In Water	Temp Deg F		
A-1		2.700	71	Oxygen %	20.9
2		3.800	71	Carbon Dioxide %	0
3		4.400	71	Moisture %	3.62
4		3.800	70	Stack Area sq.in.	572.5552696
5		3.300	70	Pbar	29.90
6		3.100	68	Static Pressure	-20.8
B-1		3.900	72	Pitot Coef.	0.84
2		4.200	70	Start Time	1026
3		4.400	70	Stop Time	1030
4		4.400	70		
5		4.300	71		
6		4.200	73		
0					
0					
0					
0					
0					
2					
3				Absolute Gas Pressure inches water	Ps = 28.37
4				Dry Mole Fraction of Gas	Mfd = 0.96382
5				Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
6				Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.44
7				Average Gas Velocity ft/sec	vs = 114.32
8				Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 24803
D-1				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 27273
2					
3				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 1544072
4					
5					
6				LKCH	
7				Pre	3-4 good
8				Post	5-3 good
0					
0					

GHM Run 3

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	3
Plant	Wiggins		Date	10/10/2013
City/State	Wiggins, MS		Gauge ID	909033
Location	Green Hammermill		Pitot ID	4Pext
Averages	3.847	70.9	Thermocouple ID	TC25
Point No.	Delta P In Water	Temp Deg F		
A-1	2.700	71	Oxygen %	20.9
2	3.600	71	Carbon Dioxide %	0
3	4.400	71	Moisture %	2.37
4	3.700	71	Stack Area sq.in.	572.5552696
5	3.200	71	Pbar	29.90
6	3.300	69	Static Pressure	-20.8
B-1	4.000	72	Pitot Coef.	0.84
2	4.300	71	Start Time	1141
3	4.300	71	Stop Time	1144
4	4.300	71		
5	4.300	71		
6	4.300	71		
0				
0				
0				
0				
0				
2				
3			Absolute Gas Pressure inches water	Ps = 28.37
4			Dry Mole Fraction of Gas	Mfd = 0.97626
5			Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
6			Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.58
7			Average Gas Velocity ft/sec	vs = 113.97
8			Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 25031
D-1			Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 27189
2			Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 1538379
3				
4				
5				
6			LKCH	
7			Pre	3-4 good
8			Post	6-4 good
0				
0				

Method 1 - Air Control Techniques, P.C.

Date

10/12/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Pellet Mill 2 Aspiration

No. of Ports Available	1
No. of Ports Used	1
Port Inside Diameter, Inches	1
Distance From Far Wall To Outside Of Port, Inches	6
Nipple Length And/Or Wall Thickness, Inches	0
Depth Of Stack Or Duct, Inches	6
Stack Or Duct Width (if rectangular), Inches	6
Equiv. Diameter = 2DW(D+W), Inches	0.20
Stack/Duct Area, Square Feet	
($D^2 \times R^2$ or L x W)	
Distance to Flow Disturbances, inches	19
Upstream	3.17
Downstream	6.50

Note: If more than 8 and 2 diameters and 6 duct dia is less than 24" use 8 or 9 points

Point	% of Duct Depth	Distance From		Diameters	Location of Points in Circular Stacks or Ducts																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																														
		Inside Well	Outside of Port		4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																										
1	6.7	3/8	1	6.7	6.7	13.4	20.1	26.8	33.5	40.2	46.9	53.6	60.3	67.0	73.7	80.4	87.1	93.8	100.5	107.2	113.9	120.6	127.3	134.0	140.7	147.4	154.1	160.8	167.5	174.2	180.9	187.6	194.3	201.0	207.7	214.4	221.1	227.8	234.5	241.2	247.9	254.6	261.3	268.0	274.7	281.4	288.1	294.8	301.5	308.2	314.9	321.6	328.3	335.0	341.7	348.4	355.1	361.8	368.5	375.2	381.9	388.6	395.3	402.0	408.7	415.4	422.1	428.8	435.5	442.2	448.9	455.6	462.3	469.0	475.7	482.4	489.1	495.8	502.5	509.2	515.9	522.6	529.3	536.0	542.7	549.4	556.1	562.8	569.5	576.2	582.9	589.6	596.3	603.0	609.7	616.4	623.1	629.8	636.5	643.2	649.9	656.6	663.3	670.0	676.7	683.4	690.1	696.8	703.5	710.2	716.9	723.6	730.3	737.0	743.7	750.4	757.1	763.8	770.5	777.2	783.9	790.6	797.3	804.0	810.7	817.4	824.1	830.8	837.5	844.2	850.9	857.6	864.3	871.0	877.7	884.4	891.1	897.8	904.5	911.2	917.9	924.6	931.3	938.0	944.7	951.4	958.1	964.8	971.5	978.2	984.9	991.6	998.3	1005.0	1011.7	1018.4	1025.1	1031.8	1038.5	1045.2	1051.9	1058.6	1065.3	1072.0	1078.7	1085.4	1092.1	1098.8	1105.5	1112.2	1118.9	1125.6	1132.3	1139.0	1145.7	1152.4	1159.1	1165.8	1172.5	1179.2	1185.9	1192.6	1199.3	1206.0	1212.7	1219.4	1226.1	1232.8	1239.5	1246.2	1252.9	1259.6	1266.3	1273.0	1279.7	1286.4	1293.1	1299.8	1306.5	1313.2	1319.9	1326.6	1333.3	1340.0	1346.7	1353.4	1360.1	1366.8	1373.5	1380.2	1386.9	1393.6	1400.3	1407.0	1413.7	1420.4	1427.1	1433.8	1440.5	1447.2	1453.9	1460.6	1467.3	1474.0	1480.7	1487.4	1494.1	1500.8	1507.5	1514.2	1520.9	1527.6	1534.3	1541.0	1547.7	1554.4	1561.1	1567.8	1574.5	1581.2	1587.9	1594.6	1601.3	1608.0	1614.7	1621.4	1628.1	1634.8	1641.5	1648.2	1654.9	1661.6	1668.3	1675.0	1681.7	1688.4	1695.1	1701.8	1708.5	1715.2	1721.9	1728.6	1735.3	1742.0	1748.7	1755.4	1762.1	1768.8	1775.5	1782.2	1788.9	1795.6	1802.3	1809.0	1815.7	1822.4	1829.1	1835.8	1842.5	1849.2	1855.9	1862.6	1869.3	1876.0	1882.7	1889.4	1896.1	1902.8	1909.5	1916.2	1922.9	1929.6	1936.3	1943.0	1949.7	1956.4	1963.1	1969.8	1976.5	1983.2	1989.9	1996.6	2003.3	2010.0	2016.7	2023.4	2030.1	2036.8	2043.5	2050.2	2056.9	2063.6	2070.3	2077.0	2083.7	2090.4	2097.1	2103.8	2110.5	2117.2	2123.9	2130.6	2137.3	2144.0	2150.7	2157.4	2164.1	2170.8	2177.5	2184.2	2190.9	2197.6	2204.3	2211.0	2217.7	2224.4	2231.1	2237.8	2244.5	2251.2	2257.9	2264.6	2271.3	2278.0	2284.7	2291.4	2298.1	2304.8	2311.5	2318.2	2324.9	2331.6	2338.3	2345.0	2351.7	2358.4	2365.1	2371.8	2378.5	2385.2	2391.9	2398.6	2405.3	2412.0	2418.7	2425.4	2432.1	2438.8	2445.5	2452.2	2458.9	2465.6	2472.3	2479.0	2485.7	2492.4	2499.1	2505.8	2512.5	2519.2	2525.9	2532.6	2539.3	2546.0	2552.7	2559.4	2566.1	2572.8	2579.5	2586.2	2592.9	2600.0	2606.7	2613.4	2620.1	2626.8	2633.5	2640.2	2646.9	2653.6	2660.3	2667.0	2673.7	2680.4	2687.1	2693.8	2700.5	2707.2	2713.9	2720.6	2727.3	2734.0	2740.7	2747.4	2754.1	2760.8	2767.5	2774.2	2780.9	2787.6	2794.3	2801.0	2807.7	2814.4	2821.1	2827.8	2834.5	2841.2	2847.9	2854.6	2861.3	2868.0	2874.7	2881.4	2888.1	2894.8	2901.5	2908.2	2914.9	2921.6	2928.3	2935.0	2941.7	2948.4	2955.1	2961.8	2968.5	2975.2	2981.9	2988.6	2995.3	3002.0	3008.7	3015.4	3022.1	3028.8	3035.5	3042.2	3048.9	3055.6	3062.3	3069.0	3075.7	3082.4	3089.1	3095.8	3102.5	3109.2	3115.9	3122.6	3129.3	3136.0	3142.7	3149.4	3156.1	3162.8	3169.5	3176.2	3182.9	3189.6	3196.3	3203.0	3209.7	3216.4	3223.1	3229.8	3236.5	3243.2	3249.9	3256.6	3263.3	3270.0	3276.7	3283.4	3290.1	3296.8	3303.5	3310.2	3316.9	3323.6	3330.3	3337.0	3343.7	3350.4	3357.1	3363.8	3370.5	3377.2	3383.9	3390.6	3397.3	3404.0	3410.7	3417.4	3424.1	3430.8	3437.5	3444.2	3450.9	3457.6	3464.3	3471.0	3477.7	3484.4	3491.1	3497.8	3504.5	3511.2	3517.9	3524.6	3531.3	3538.0	3544.7	3551.4	3558.1	3564.8	3571.5	3578.2	3584.9	3591.6	3598.3	3605.0	3611.7	3618.4	3625.1	3631.8	3638.5	3645.2	3651.9	3658.6	3665.3	3672.0	3678.7	3685.4	3692.1	3698.8	3705.5	3712.2	3718.9	3725.6	3732.3	3739.0	3745.7	3752.4	3759.1	3765.8	3772.5	3779.2	3785.9	3792.6	3799.3	3806.0	3812.7	3819.4	3826.1	3832.8	3839.5	3846.2	3852.9	3859.6	3866.3	3873.0	3879.7	3886.4	3893.1	3900.0	3906.7	3913.4	3920.1	3926.8	3933.5	3940.2	3946.9	3953.6	3960.3	3967.0	3973.7	3980.4	3987.1	3993.8	4000.5	4007.2	4013.9	4020.6	4027.3	4034.0	4040.7	4047.4	4054.1	4060.8	4067.5	4074.2	4080.9	4087.6	4094.3	4101.0	4107.7	4114.4	4121.1	4127.8	4134.5	4141.2	4147.9	4154.6	4161.3	4168.0	4174.7	4181.4	4188.1	4194.8	4201.5	4208.2	4214.9	4221.6	4228.3	4235.0	4241.7	4248.4	4255.1	4261.8	4268.5	4275.2	4281.9	4288.6	4295.3	4302.0	4308.7	4315.4	4322.1	4328.8	4335.5	4342.2	4348.9	4355.6	4362.3	4369.0	4375.7	4382.4	4389.1	4395.8	4402.5	4409.2	4415.9	4422.6	4429.3	4436.0	4442.7	4449.4	4456.1	4462.8	4469.5	4476.2	4482.9	4489.6	4496.3	4503.0	4509.7	4516.4	4523.1	4529.8	4536.5	4543.2	4549.9	4556.6	4563.3	4570.0	4576.7	4583.4	4590.1	4596.8	4603.5	4610.2	4616.9	4623.6	4630.3	4637.0	4643.7	4650.4	4657.1	4663.8	4670.5	4677.2	4683.9	4690.6	4697.3	4704.0	4710.7	4717.4	4724.1	4730.8	4737.5	4744.2	4750.9	4757.6	4764.3	4771.0	4777.7	4784.4	4791.1	4797.8	4804.5	4811.2	4817.9	4824.6	4831.3	4838.0	4844.7	4851.4	4858.1	4864.8	4871.5	4878.2	4884.9	4891.6	4898.3	4905.0	4911.7	4918.4	4925.1	4931.8	4938.5	4945.2	4951.9	4958.6	4965.3	4972.0	4978.7	4985.4	4992.1	4998.8	5005.5	5012.2	5018.9	5025.6	5032.3	5039.0	5045.7	5052.4	5059.1	5065.8	5072.5	5079.2	5085.9	5092.6	5099.3	5106.0	5112.7	5119.4	5126.1	5132.8	5139.5	5146.2	5152.9	5159.6	5166.3	5173.0	5179.7	5186.4	5193.1	5200.0	5206.7	5213.4	5220.1	5226.8	5233.5	5240.2	5246.9	5253.6	5260.3	5267.0	5273.7	5280.4	5287.1	5293.8	5300.5	5307.2	5313.9	5320.6	5327.3	5334.0	5340.7	5347.4	5354.1	5360.8	5367.5	5374.2	5380.9	5387.6	5394.3	5401.0	5407.7	5414.4	5421.1	5427.8	5434.5	5441.2	5447.9	5454.6	5461.3	5468.0	5474.7	5481.4	5488.1	5494.8	5501.5	5508.2	5514.9	5521.6	5528.3	5535.0	5541.7	5548.4	5555.1	5561.8	5568.5	5575.2	5581.9	5588.6	5595.3	5602.0	5608.7	5615.4	5622.1	5628.8	5635.5	5642.2	5648.9	5655.6	5662.3	5669.0	5675.7	5682.4	5689.1	5695.8	5702.5	5709.2	5715.9	5722.6	5729.3	5736.0	5742.7	5749.4	5756.1	5762.8	5769.5	5776.2	5782.9	5789.6	5796.3	5803.0	5809.7	5816.4	5823.1	5829.8	5836.5	5843.2	5849.9	5856.6	5863.3	5870.0	5876.7	5883.4	5890.1	5896.8	5903.5	5910.2	5916.9	5923.6	5930.3	5937.0	5943.7	5950.4	5957.1	5963.8	5970.5	5977.2	5983.9	5990.6	5997.3	6004.0	6010.7	6017.4	6024.1	6030.8	6037.5	6044.2	6050.9	6057.6	6064.3	6071.0	6077.7	6084.4	6091.1	6097.8	6104.5	6111.2	6117.9	6124.6	6131.3	6138.0	6144.7	6151.4	6158.1	6164.8	6171.5	6178.2	6184.9	6191.6	6198.3	6205.0	6211.7	6218.4	6225.1	6231.8	6238.5	6245.2	6251.9	6258.6	6265.3	6272.0	6278.7	6285.4	6292.1	6298.8	6305.5	6312.2	6318.9	6325.6	6332.3	6339.0	6345.7	6352.4	6359.1	6365.8	6372.5	6379.2	6385.9	6392.6	6399.3	6406.0	6412.7	6419.4	6426.1	6432.8	6439.5	6446.2	6452.9	6459.6	6466.3	6473.0	6479.7	6486.4	6493.1	6500.0	6506.7	6513.4	6520.1	6526.8	6533.5	6540.2	6546.9	6553.6	6560.3	6567.0	6573.7	6580.4	6587.1	6593.8	6600.5	6607.2	6613.9	6620.6	6627.3	6634.0	6640.7	6647.4	6654.1	6660.8	6667.5	6674.2	6680.9	6687.6	6694.3	6701.0	6707.7	6714.4	6721.1	6727.8	6734.5	6741.2	6747.9	6754.6	6761.3	6768.0	6774.7	6781.4	6788.1	6794.8	6801.5	6808.2	6814.9	6821.6	6828.3	6835.0	6841.7	6848.4	6855.1	6861.8	6868.5	6875.2	6881.9	6888.6	6895.3	6902.0	6908.7	6915.4	6922.1	6928.8	6935.5	6942.2	6948.9	6955.6	6962.3</

PMA Run 1

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	16
Plant	Wiggins		Date	10/12/2013
City/State	Wiggins, MS		Gauge ID	909033
Location	Pellet Mill 2 Aspiration		Pitot ID	4Pext
Averages	5.359	148.6	Thermocouple ID	TC25
Point No.	Delta P In Water	Temp Deg F	Angle	
A-1	5.400	149	0	Oxygen % 20.9
2	5.700	148	0	
3	5.100	149	2	Carbon Dioxide % 0
4	5.000	149	1	
B-1	5.700	149	0	Moisture % 27.67
2	5.600	148	1	
3	5.400	149	2	Stack Area sq.in. 28.2743343
4	5.000	148	0	
0				Pbar 29.85
0				
0				Static Pressure -7.5
0				
0				Pitot Coef. 0.84
0				
0				Start Time 1445
0				
0				Stop Time 1448
0				
0				Absolute Gas Pressure inches water Ps = 29.30
0				
0				Dry Mole Fraction of Gas Mfd = 0.72332
0				
0				Dry Molecular Weight of Gas lb/lb Mole Md = 28.84
0				
0				Wet Molecular Weight of Gas lb/lb Mole Ms = 25.84
0				
0				Average Gas Velocity ft/sec vs = 149.06
0				
0				Dry Volumetric Gas Flow Rate at Standard Conditions SCFM Qsd = 1079
0				
0				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM Qaw = 1756
0				
0				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH WSCFH = 89506.7
0				
0				LKCH
0				Pre 4-3 good
8				Post 5-5 good

Method 1 - Air Control Techniques, P.C.

Date

10/11/2013

Client: Enviva
 Job #: 1911
 Plant Name: Wiggins
 State: Mississippi
 City: Wiggins
 Sampling Location: Dry Hammermill 2

No. of Ports Available: 2
 No. of Ports Used: 2
 Port Inside Diameter, Inches: 22
 Distance From Far Wall To Outside Of Port, Inches: 22
 Nipple Length And/Or Wall Thickness, Inches: 0
 Depth Of Stack Or Duct, Inches: 22
 Stack Or Duct Width (if rectangular), Inches: 22
 Equip. Diameter = 2DW/(D+W), Inches: 2.6
 Stack/Duct Area, Square Feet: 2.6
 (D x R² of L x W)
 Distance to Flow Disturbances, Inches: 52
 Diameters: 2.36 0.36

Note: If more than 8 and 2 diameters and if duct dia. is less than 24" use 8 or 9 ports.

Velocity	UP				Down				Particulate
	8	7	6	5	2	1.75	1.5	1.25	
12									12
12									12
12									16
16									20
16									24 or 25

Location of Points in Circular Stacks or Ducts

	4	6	8	10	12	14	16	18	20	22	24
1	6.7	4.4	3.2	2.6	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.8	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2
3	75.0	29.6	19.4	14.8	11.8	9.8	8.5	7.5	6.7	6.0	5.5
4	93.3	70.4	33.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9
5	86.4	67.7	34.2	24.2	25.0	20.1	18.9	14.6	12.9	11.6	10.5
6	86.6	68.6	35.8	25.8	25.0	20.1	18.9	14.6	12.9	11.6	10.5
7	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
8	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
9	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
10	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
11	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
12	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
13	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
14	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
15	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
16	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
17	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
18	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
19	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
20	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
21	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
22	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
23	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0
24	84.4	64.4	34.8	24.4	23.6	20.4	18.0	16.0	14.0	12.0	11.0

2 diff nipples probe marked to inside of port

Point Location Data

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	3.2	6/8	6/8
2	10.6	2 3/8	2 3/8
3	19.4	4 2/8	4 2/8
4	32.3	7 1/8	7 1/8
5	67.7	14 7/8	14 7/8
6	80.6	17 6/8	17 6/8
7	89.5	19 6/8	19 6/8
8	96.8	21 2/8	21 2/8
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Location of Points in Rectangular Stacks or Ducts

	2	3	4	5	6	7	8	9	10	11	12
1	25	10.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.6
3	83.3	62.5	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8
4	17	87.5	87.5	70.0	56.3	50	44.8	39.9	35.0	31.8	29.2
5	80.0	80.0	80.0	75	64.3	64.3	55	45.0	40.9	37.5	37.5
6	91.7	91.7	91.7	91.7	82.9	82.9	72.2	65.0	59.1	54.2	54.2
7	81.3	81.3	81.3	81.3	72.2	72.2	65.0	59.1	54.2	54.2	54.2
8	83.8	83.8	83.8	83.8	75.0	75.0	68.2	62.5	58.0	54.2	54.2
9	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4
10	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4
11	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4
12	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4	84.4

- 0.0000 - 0.0625 - 0
- 0.0625 - 0.1875 - 1/8
- 0.1875 - 0.3125 - 1/4
- 0.3125 - 0.4375 - 3/8
- 0.4375 - 0.5625 - 1/2
- 0.5625 - 0.6875 - 5/8
- 0.6875 - 0.8125 - 3/4
- 0.8125 - 0.9375 - 7/8
- 0.9375 - 1.0000 - 1

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	10
Plant	Wiggins		Date	10/11/2013
City/State	Wiggins, MS		Gauge ID	909033
Location	Dry Hammermill 2		Pitot ID	4Pext
Averages	2.601	122.4	Thermocouple ID	TC25
Point No.	Delta P in Water	Temp Deg F	Angle	
A-1	2.400	121	0	Oxygen % 20.9
2	2.600	122	1	Carbon Dioxide % 0
3	2.550	122	0	Moisture % 4.25
4	2.400	123	0	Stack Area sq.in. 380.13272
5	2.600	123	2	Pbar 29.80
6	3.000	122	0	Static Pressure 1.4
7	3.000	121	0	Pitot Coef. 0.84
8	3.300	120	0	Start Time 1745
B-1	2.200	122	2	Stop Time 1758
2	2.200	122	0	
3	2.300	123	1	Absolute Gas Pressure inches water Ps = 29.90
4	2.300	123	0	Dry Mole Fraction of Gas Mfd = 0.95746
5	2.800	123	2	Dry Molecular Weight of Gas lb/lb Mole Md = 28.84
6	2.700	123	0	Wet Molecular Weight of Gas lb/lb Mole Ms = 28.38
7	2.800	125	1	Average Gas Velocity ft/sec vs = 95.95
8	2.600	124	1	Dry Volumetric Gas Flow Rate at Standard Conditions SCFM Qsd = 13183
0				Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM Qaw = 15197
2				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH WSCFH = 826137
3				
4				
5				
6				LKCH
7				Pre 4-3 good
8				Post 5-5 good
0				
0				

DHM2 Run 2

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva	ACT Run Number	11	
Plant	Wiggins	Date	10/11/2001	
City/State	Wiggins, MS	Gauge ID	909033	
Location	Dry Hammermill 2	Pitot ID	4Pext	
Averages	2.308	128.2	Thermocouple ID	TC25
Point No.	Delta P In Water	Temp Deg F		
A-1	2.200	124	Oxygen %	20.9
2	2.150	127	Carbon Dioxide %	0
3	2.000	129	Moisture %	4.18
4	2.100	129	Stack Area sq.in.	380.132717
5	2.000	129	Pbar	29.80
6	2.600	130	Static Pressure	1.4
7	2.600	130	Pitot Coef.	0.84
8	2.600	129	Start Time	1917
B-1	1.800	129	Stop Time	1923
2	2.200	127		
3	2.200	128	Absolute Gas Pressure inches water	Ps = 29.90
4	2.300	128	Dry Mole Fraction of Gas	Mfd = 0.95816
5	2.600	128	Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
6	2.500	128	Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
7	2.600	128	Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.38
8	2.600	128	Average Gas Velocity ft/sec	vs = 90.82
0			Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 12366
2			Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 14385
3			Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 774351
4				
5				
6			LKCH	
7			Pre	4-3 good
8			Post	5-5 good
0				
0				

DHM2 Run 3

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	12
Plant	Wiggins		Date	10/11/2013
City/State	Wiggins, MS		Gauge ID	909033
Location	Dry Hammermill 2		Pitot ID	4Pext
Averages	2.618	116.4	Thermocouple ID	TC25
	Delta P	Temp		
Point No.	In Water	Deg F		
A-1	2.700	114	Oxygen %	20.9
2	2.700	116	Carbon Dioxide %	0
3	2.700	116	Moisture %	4.18
4	2.500	117	Stack Area sq.in.	380.1327167
5	2.800	117	Pbar	29.80
6	2.800	118	Static Pressure	1.4
7	3.000	117	Pitot Coef.	0.84
8	2.900	116	Start Time	2038
B-1	3.000	117	Stop Time	2043
2	2.900	116		
3	2.600	117	Absolute Gas Pressure inches water	Ps = 29.90
4	2.500	116	Dry Mole Fraction of Gas	Mfd = 0.95816
5	2.300	116	Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
6	2.300	116	Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.38
7	2.100	116	Average Gas Velocity ft/sec	vs = 95.74
8	2.200	117	Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 13303
0			Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 15165
2			Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 833051
3				
4				
5				
6			LKCH	
7			Pre	4-3 good
8			Post	5-5 good
0				
0				

Air Control Techniques, PC: Emissions Calculations

Enviva, Wiggins, MS

Job 1911

PARAMETER NOMENCLATURE

PARAMETER	Sampling Location	Pellet Mill 2 Cooler 7	Pellet Mill 2 Cooler 8	Pellet Mill 2 Cooler 9	Pellet Mill 1 Cooler 13	Pellet Mill 1 Cooler 14	Pellet Mill 1 Cooler 15
Date		10/11/2013	10/11/2013	10/11/2013	10/12/2013	10/12/2013	10/12/2013
Run Time		60	60	60	60	60	60
Nozzle Diameter	inches	N/A	N/A	N/A	N/A	N/A	N/A
Stack Area	As - sq. ft.	2.4	2.4	2.4	5.81	5.8	5.8
Pitot Tube Coefficient	Cp	0.84	0.84	0.84	0.84	0.84	0.84
Meter Calibration Factor	Y	0.9828	0.9828	0.9828	0.9828	0.9828	0.9828
Barometric Pressure, inches Hg	Bp - in Hg	29.80	29.80	29.80	29.90	29.90	29.90
Static Pressure	Pg - in. H ₂ O	-1.2	-1.2	-1.2	-0.4	-0.4	-0.4
Stack Pressure	Ps	29.71	29.71	29.71	29.87	29.87	29.87
Meter Box Pressure Differential	Δ H - in. H ₂ O	1.00	1.00	1	1.00	1.00	1.00
Average Velocity Head	Δ p - in. H ₂ O	2.293	2.102	2.108	0.654	0.644	0.634
Volume of Gas Sampled	Vm - cu. ft.	34,310	34,423	33,681	33,818	35,845	34,567
Dry Gas Meter Temperature	Tm - °F	87.3	89.3	83.8	71.8	82.5	89.0
Stack Temperature	Ts - °F	148.9	143.2	152.3	82.3	94.8	97.7
Liquid Collected	Grams	35.2	33.5	32.4	24.3	27.8	19.9
Carbon Dioxide	% CO ₂	0	0	0	0	0	0
Oxygen	% O ₂	20.9	20.9	20.9	20.9	20.9	20.9
Carbon Monoxide	% CO	0	0	0	0	0	0
Nitrogen	% N ₂	79.1	79.1	79.1	79.1	79.1	79.1
Volume of Gas Sampled, Dry	Vmstd - cu. ft.	32,483	32,472	32,093	33,061	34,348	32,731
Volume of Water Vapor	Vwstd - cu. ft.	1,660	1,580	1,528	1,146	1,311	0,938
Moisture Content	% H ₂ O	4.86	4.64	4.54	3.35	3.68	2.79
Saturation Moisture	% H ₂ O	24.8	21.4	26.9	3.7	5.5	6.0
Dry Mole Fraction	Mfd	0.951	0.954	0.955	0.967	0.963	0.972
Gas Molecular Weight, Dry	Md	28.84	28.84	28.84	28.84	28.84	28.84
Gas Molecular Weight, Wet	Ms	28.31	28.33	28.34	28.47	28.44	28.53
Gas Velocity	vs - ft./sec.	92.52	88.13	88.91	46.36	46.58	46.26
Volumetric Air Flow, Actual	Qaw - ACFM	13,352	12,718	12,831	16,168	16,246	16,134
Volumetric Air Flow, Standard	Qsd - DSCFM	10,938	10,543	10,488	15,189	14,870	14,825

Method 1 - Air Control Techniques, P.C.

Date

10/12/2013

Client	Enviva
Job #	1911
Plant Name	Wiggins
State	Mississippi
City	Wiggins
Sampling Location	Pellet Mill 1 Cooler

No. of Ports Available	6
No. of Ports Used	4
Port Inside Diameter, Inches	30.5
Distance From Far Wall To Outside Of Port, Inches	3.5
Nipple Length And/Or Wall Thickness, Inches	27
Depth Of Stack Or Duct, Inches	31
Stack Or Duct Width (if rectangular), Inches	28.86207
Stack Diameter = 2D/(D+W), Inches	5.8
Stack/Duct Area, Square Feet	
(\square x R ² or L x W)	
Upstream	72
Downstream	48
Distance to Flow Disturbances, Inches	2.49
Diameters	1.66

2 diff nipples probe marked to inside of port

Point	% of Duct Depth	Distance From Inside Wall	Distance From Outside of Port
1	12.5	3.3/8	6.7/8
2	37.5	10.1/8	13.5/8
3	62.5	16.7/8	20.3/8
4	87.5	23.5/8	27.1/8
5			
6			
7			
8			
9			
10			
11			
12			
13			
14			
15			
16			
17			
18			
19			
20			
21			
22			
23			
24			
25			

Velocity	Diameters			
	UP	Down	Particulate	
12	8	2		
12	7	1.75		
12	6	1.5		
16	5	1.25		
16	2	0.5		
				24 or 25

Note: If more than 8 and 2 diameters sized 4 duct size is less than 24 use 8 or 9 points

Location of Points in Circular Stacks or Ducts	Diameters											
	4	6	8	10	12	14	16	18	20	22	24	
1	6.7	4.4	3.2	2.8	2.1	1.8	1.6	1.4	1.3	1.1		
2	25.0	14.6	10.6	8.2	6.7	5.7	4.9	4.4	3.9	3.5		
3	75.0	29.6	19.4	14.6	11.6	9.9	8.5	7.5	6.7	6.0		
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7		
5		85.4	87.7	34.2	25.0	20.1	16.9	14.6	12.9	11.6		
6		95.6	86.6	65.9	35.6	26.9	22.0	18.8	16.5	14.6		
7			85.5	77.4	64.4	36.6	29.3	23.6	20.4	18.0		
8			98.8	85.4	75.0	63.4	37.5	28.6	25.0	21.8		
9				91.8	82.3	72.1	62.5	36.2	30.8	26.2		
10				97.4	86.2	76.9	71.7	61.8	34.5	31.5		
11				93.3	85.4	76.0	70.4	61.2	36.3	32.3		
12				97.9	80.1	83.1	76.4	66.4	60.7	39.8		
13					94.3	87.6	81.2	75.0	68.9	60.2		
14					96.2	91.5	85.4	78.6	73.8	67.7		
15					93.5	89.1	83.5	78.2	72.8	67.2		
16					98.4		92.5	87.1	82.0	77.0		
17							95.6	90.3	85.4	80.8		
18							98.6		93.3	88.4		
19								98.1	91.3	86.6		
20									94.0	89.5		
21										92.1		
22										94.5		
23										96.6		
24										98.9		
25										98.9		

Location of Points in Rectangular Stacks or Ducts	Diameters											
	2	3	4	5	6	7	8	9	10	11	12	
1	25	18.7	12.5	10.0	6.3	7.1	6.3	5.6	5.0	4.5	4.2	
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5	
3		83.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8	
4			87.5	70.0	59.3	50	44.8	28.9	35.0	31.8	29.2	
5				90.0	75	64.3	68.8	50	45.0	40.8	37.5	
6					91.7	78.6	68.8	61.1	55.0	50	45.6	
7						82.6	81.3	72.2	65.0	59.1	54.2	
8							83.8	83.3	75.0	68.2	62.5	
9								84.4	77.3	70.5	66.4	
10									85.0	78.2	73.8	
11										86.6	81.3	
12											88.9	

- 0.0000 - 0.0625 - 0
- 0.0625 - 0.1875 - 1/8
- 0.1875 - 0.3125 - 1/4
- 0.3125 - 0.4375 - 3/8
- 0.4375 - 0.5625 - 1/2
- 0.5625 - 0.6875 - 5/8
- 0.6875 - 0.8125 - 3/4
- 0.8125 - 0.9375 - 7/8
- 0.9375 - 1.0000 - 1

Pellet Mill 1 Run 1

Air Control Techniques EPA Method 2 Data Sheet				ACT Job Number	1911
Client Enviva				ACT Run Number	13
Plant Wiggins				Date	10/12/2013
City/State Mississippi				Gauge ID	909033
Location Pellet Mill 1 Cooler				Pitot ID	4Pext
Averages 0.654 82.3				Thermocouple ID	4Pext
Point No.	Delta P In Water	Temp Deg F	Angle		
A-1	0.380	78	0	Oxygen %	20.9
2	0.340	79	0	Carbon Dioxide %	0
3	0.330	79	0	Moisture %	3.35
4	0.340	77	2	Stack Area sq.in.	837
B-1	0.680	82	8	Pbar	29.90
2	0.650	81	2	Static Pressure	-0.4
3	0.540	82	-5	Pitot Coef.	0.84
4	0.570	82	3	Start Time	830
C-1	0.680	84	-2	Stop Time	847
2	0.700	84	-3	Absolute Gas Pressure inches water	Ps = 29.87
3	0.690	84	0	Dry Mole Fraction of Gas	Mfd = 0.96651
4	0.710	84	3	Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
D-1	1.050	85	0	Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.47
2	1.050	85	-2	Average Gas Velocity ft/sec	vs = 46.36
3	1.050	85	-1	Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 15189
4	1.100	86	2	Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 16168
0				Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 942901
0				LKCH	
0				Pre	3-4 good
0				Post	5-3 good
#REF!					
#REF!					

Pellet Mill 1 Run 2

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	14
Plant	Wiggins		Date	10/12/2013
City/State	Mississippi		Gauge ID	909033
Location	Pellet Mill 1 Cooler		Pitot ID	4PEXT
Averages	0.644	94.8	Thermocouple ID	4PEXT
Point No.	Delta P In Water	Temp Deg F		
A-1	0.380	92	Oxygen %	20.9
2	0.400	93	Carbon Dioxide %	0
3	0.380	93	Moisture %	3.68
4	0.370	93	Stack Area sq.in.	837
B-1	0.530	94	Pbar	29.90
2	0.550	95	Static Pressure	-0.4
3	0.480	95	Pitot Coef.	0.84
4	0.500	95	Start Time	1009
C-1	0.670	95	Stop Time	1015
2	0.690	95		
3	0.660	96	Absolute Gas Pressure inches water	Ps = 29.87
4	0.680	96	Dry Mole Fraction of Gas	Mfd = 0.96324
D-1	1.300	96	Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
2	1.050	96	Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.44
3	1.050	96	Average Gas Velocity ft/sec	vs = 46.58
4	1.050	96	Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 14870
0			Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 16246
0			Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 926248
0				
0			LKCH	
0			Pre	3-4 good
0			Post	5-3 good
#REF!				
#REF!				

Pellet Mill 1 Run 3

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	15
Plant	Wiggins		Date	10/12/2013
City/State	Mississippi		Gauge ID	909033
Location	Pellet Mill 1 Cooler		Pitot ID	4Pext
Averages	0.634	97.7	Thermocouple ID	4Pext
Point No.	Delta P In Water	Temp Deg F		
A-1	0.340	94	Oxygen %	20.9
2	0.290	96	Carbon Dioxide %	0
3	0.280	97	Moisture %	2.79
4	0.330	97	Stack Area sq.in.	837
B-1	0.530	98	Pbar	29.90
2	0.540	98	Static Pressure	-0.4
3	0.500	98	Pitot Coef.	0.84
4	0.480	98	Start Time	1125
C-1	0.730	98	Stop Time	1134
2	0.740	98		
3	0.670	98	Absolute Gas Pressure inches water	Ps = 29.87
4	0.670	99	Dry Mole Fraction of Gas	Mfd = 0.97213
D-1	1.400	98	Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
2	1.050	99	Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.53
3	1.000	99	Average Gas Velocity ft/sec	vs = 46.26
4	1.200	98	Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 14825
0			Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 16134
0			Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 915021
0			LKCH	
0			Pre	3-4 good
0			Post	5-3 good
#REF!				
#REF!				

Method 1 - Air Control Techniques, P.C.

Date

10/11/2013

Client: Enviva
 Job #: 1911
 Plant Name: Wiggins
 State: Mississippi
 City: Wiggins
 Sampling Location: Pellet Mill 2 Cooler

No. of Ports Available: 2
 No. of Ports Used: 2
 Port Inside Diameter, inches: 3
 Distance From Far Wall To Outside Of Port, inches: 21
 Nipple Length And/Or Wall Thickness, inches: 0
 Depth Of Stack Or Duct, inches: 21
 Stack Or Duct Width (if rectangular), inches: 21
 Equip. Diameter = 2DW/(D+W), inches: 2.4
 Stack/Duct Area, Square Feet: 2.4
 (□ x R² or L x W)
 Upstream, Downstream
 Distance to Flow Disturbances, inches: 51, 9.5
 Diameters: 2.43, 0.45

Note: If more than 8 and 2 diameters and if not data is base than 2" use 8 or 9 points

Velocity	Diameters			
	UP	Down	2	Particulate
12	8	2	12	12
12	7	1.75	12	12
12	6	1.5	16	16
16	5	1.25	20	20
16	2	0.5	24 or 25	24 or 25

Location of Points in Circular Stacks or Ducts												
	4	6	8	10	12	14	16	18	20	22	24	
1	6.7	4.4	3.2	2.6	2.1	1.6	1.6	1.4	1.3	20	22	24
2	25.0	14.8	10.8	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2	
3	75.0	29.8	19.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5	
4	93.3	70.4	32.3	22.6	17.7	14.6	12.5	10.9	9.7	8.7	7.9	
5	85.4	67.7	34.2	25.0	20.1	16.8	14.6	12.9	11.5	10.3	10.3	
6	80.6	60.6	35.8	25.6	20.9	17.4	15.2	13.5	12.1	10.8	10.3	
7	89.5	77.4	39.5	28.4	22.6	18.8	16.4	14.6	13.1	11.7	11.2	
8	96.8	86.8	43.4	31.4	25.0	20.4	17.4	15.2	13.5	12.1	11.2	
9	91.8	82.3	37.1	27.5	21.8	17.8	15.2	13.5	12.1	10.8	10.3	
10	97.4	88.2	40.4	29.8	23.6	19.4	16.4	14.6	13.1	11.7	11.2	
11	93.3	85.4	38.4	28.4	22.6	18.8	16.4	14.6	13.1	11.7	11.2	
12	90.1	83.1	36.4	26.6	21.8	17.8	15.2	13.5	12.1	10.8	10.3	
13	84.3	78.6	32.3	23.6	19.4	16.4	14.6	13.1	11.7	10.3	10.3	
14	98.2	91.3	44.4	33.4	26.6	21.8	18.8	16.4	14.6	13.1	12.1	
15	89.1	82.3	37.1	27.5	21.8	17.8	15.2	13.5	12.1	10.8	10.3	
16	98.4	91.3	44.4	33.4	26.6	21.8	18.8	16.4	14.6	13.1	12.1	
17	93.3	85.4	38.4	28.4	22.6	18.8	16.4	14.6	13.1	11.7	11.2	
18	90.1	83.1	36.4	26.6	21.8	17.8	15.2	13.5	12.1	10.8	10.3	
19	84.3	78.6	32.3	23.6	19.4	16.4	14.6	13.1	11.7	10.3	10.3	
20	98.2	91.3	44.4	33.4	26.6	21.8	18.8	16.4	14.6	13.1	12.1	
21	89.1	82.3	37.1	27.5	21.8	17.8	15.2	13.5	12.1	10.8	10.3	
22	98.4	91.3	44.4	33.4	26.6	21.8	18.8	16.4	14.6	13.1	12.1	
23	93.3	85.4	38.4	28.4	22.6	18.8	16.4	14.6	13.1	11.7	11.2	
24	90.1	83.1	36.4	26.6	21.8	17.8	15.2	13.5	12.1	10.8	10.3	

Point Location Data

2 cliff nipples probe marked to inside of port

Point	% of Duct	Depth	Distance From Inside Wall	Distance From Outside of Port
1	3.2	0.672	1	
2	10.6	2.226	2 1/4	
3	19.4	4.074	4 1/8	
4	32.3	6.783	6 3/4	
5	67.7	14.217	14 1/4	
6	80.6	16.926	16 7/8	
7	89.5	18.795	18 3/4	
8	96.8	20.328	20	
9				
10				
11				
12				
13				
14				
15				
16				
17				
18				
19				
20				
21				
22				
23				
24				
25				

Location of Points in Rectangular Stacks or Ducts												
	2	3	4	5	6	7	8	9	10	11	12	
1	25	16.7	12.5	10.0	8.3	7.1	6.3	5.6	5.0	4.5	4.2	
2	75	50	37.5	30.0	25	21.4	18.8	16.7	15.0	13.6	12.5	
3	80.3	62.5	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8	20.8	
4	87.5	70.0	56.3	46.3	39.6	34.2	29.8	26.6	23.6	21.2	20.8	
5	90.0	75	60.0	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8	
6	91.7	76.0	61.3	50.0	41.7	35.7	31.3	27.8	25.0	22.7	20.8	
7	92.8	77.2	62.5	51.7	43.0	36.7	31.9	28.4	25.5	23.0	21.2	
8	93.8	78.3	63.6	52.8	44.1	37.8	32.9	29.2	26.0	23.2	21.4	
9	94.4	79.0	64.3	53.5	45.0	38.5	33.6	30.0	26.5	23.5	21.6	
10	94.4	79.0	64.3	53.5	45.0	38.5	33.6	30.0	26.5	23.5	21.6	
11	94.4	79.0	64.3	53.5	45.0	38.5	33.6	30.0	26.5	23.5	21.6	
12	94.4	79.0	64.3	53.5	45.0	38.5	33.6	30.0	26.5	23.5	21.6	

- 0.0000 - 0.0625 - 0
- 0.0625 - 0.1875 - 1/8
- 0.1875 - 0.3125 - 1/4
- 0.3125 - 0.4375 - 3/8
- 0.4375 - 0.5625 - 1/2
- 0.5625 - 0.6875 - 5/8
- 0.6875 - 0.8125 - 3/4
- 0.8125 - 0.9375 - 7/8
- 0.9375 - 1.0000 - 1

Pellet Mill 2 Cooler Run 2

Air Control Techniques EPA Method 2 Data Sheet			ACT Job Number	1911
Client	Enviva		ACT Run Number	8
Plant	Wiggins		Date	10/11/2013
City/State	Mississippi		Gauge ID	909033
Location	Pellet Mill 2 Cooler		Pitot ID	4PEXT
Averages	2.102	143.2	Thermocouple ID	4PEXT
Point No.	Delta P In Water	Temp Deg F		
A-1	2.400	147	Oxygen %	20.9
2	2.300	143	Carbon Dioxide %	0
3	2.200	144	Moisture %	4.64
4	2.000	144	Stack Area sq.in.	346.360595
5	1.800	142	Pbar	29.80
6	1.800	139	Static Pressure	-1.2
7	1.800	140	Pitot Coef.	0.84
8	1.700	140	Start Time	1450
B-1	1.800	142	Stop Time	1458
2	2.050	144		
3	2.250	143	Absolute Gas Pressure inches water	Ps = 29.71
4	2.200	144	Dry Mole Fraction of Gas	Mfd = 0.95361
5	2.300	144	Dry Molecular Weight of Gas lb/lb Mole	Md = 28.84
6	2.350	145	Wet Molecular Weight of Gas lb/lb Mole	Ms = 28.33
7	2.400	145	Average Gas Velocity ft/sec	vs = 88.13
8	2.400	145	Dry Volumetric Gas Flow Rate at Standard Conditions SCFM	Qsd = 10543
0			Wet Volumetric Flue Gas Flow Rate at Stack Conditions ACFM	Qaw = 12718
0			Wet Volumetric Gas Flow Rate at Standard Conditions WSCFH	WSCFH = 663328
0			LKCH	
0			Pre	3-4 good
0			Post	5-3 good
#REF!				
#REF!				

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/10/13
8/4/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVVA	Umbilical ID	200
City, State	Wiggins, MS	Meterbox ID	909033
Test Location	Green Hammer Mill	$\Delta H @$	1.917
Personnel	TJB JBG	Gamma (y)	0.9828

Run Identification <u>1741</u>				Pre Leak Check			Post Leak Check		
				Actual	Req'd	Vac			
				0.000	< 0.02 or 4%	10			
				0.000	< 0.02 or 4%	10			
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
9:17	0	470.000	65	1.0	N/A	N/A	55	5	
9:32	15	477.71	66	1.0	↓	↓	55	5	
9:47	30	487.5	66	1.0	↓	↓	56	5	
10:02	45	496.2	67	1.0	↓	↓	60	6	
10:17	60	504.468							

Run Identification <u>2</u>				Pre Leak Check			Post Leak Check		
				Actual	Req'd	Vac			
				0.000	< 0.02 or 4%	10			
				0.000	< 0.02 or 4%	9			
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
10:36	0	504.700	68	1.0	N/A	N/A	60	5	
10:51	15	513.10	70	↓	↓	↓	55	5	
11:06	30	521.9	72	↓	↓	↓	55	5	
11:21	45	530.0	73	↓	↓	↓	57	5	
11:36	60	538.681							

Run Identification <u>3</u>				Pre Leak Check			Post Leak Check		
				Actual	Req'd	Vac			
				0.000	< 0.02 or 4%	11			
				0.000	< 0.02 or 4%	9			
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
11:50	0	538.900	74	1.0	N/A	N/A	59	5	
12:05	15	549.0	75	↓	↓	↓	58	5	
12:20	30	557.8	76	↓	↓	↓	51	5	
12:35	45	563.4	77	↓	↓	↓	53	5	
12:50	60	572.056							

Method 4 - Air Control Techniques, P.C.

Date 10/14/13

Identification Information	
Client	ENLIVA
Plant Name	Wiggins
City	Wiggins
Job	191
Process	Green Green Hammer Mill
State	MS

Green Hammer Mill

Sampling Information	
Run Number	
Sampling Date	
Recovery Date	
Personnel	TJB JBG
Balance Number	100
Balance Type	Electronic
Balance Level	EVI-100
Recovery Area	<input checked="" type="checkbox"/>

Location Moisture Data			
Run Number	M4-1	M4-2	M4-3
<u>Impinger 1</u>			
Final Weight, grams/mls	809.3	743.0	822.7
Initial Weight, grams/mls	735.6	724.5	809.3
Condensed Water, grams	73.7	18.5	13.4
<u>Impinger 2</u>			
Final Weight, grams/mls	661.1	729.5	661.5
Initial Weight, grams/mls	719.0	728.8	661.1
Condensed Water, grams	-57.9	0.7	0.4
<u>Impinger 3</u>			
Final Weight, grams/mls	595.9	597.0	596.1
Initial Weight, grams/mls	594.4	595.6	595.9
Condensed Water, grams	1.5	1.4	0.2
Condensed Water, grams	17.3	20.6	
<u>Silica Gel</u>			
Final Weight, grams	815.3	797.7	817.9
Initial Weight, grams	807.5	791.1	815.3
Adsorbed Water, grams	7.8	6.6	2.6
Adsorbed Water, grams			
Total Water, grams	25.1	26.5	16.6

$V_m(\text{std}) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $V_m(\text{std}) = ((\text{Gamma} * 17.64 * V_m * (\text{Pbar} + (\Delta H / 13.6))) / (\text{Tm} + 460))$
 $V_{wc}(\text{std}) = \text{volume of water vapor at standard conditions (scf)}$
 $V_{wc}(\text{std}) = (0.04707) * (\text{volume of water collected (mls)})$
 $B_{ws} = \text{Mole fraction of water vapor}$
 $B_{ws} = V_{wc}(\text{std}) / (V_m(\text{std}) + V_{wc}(\text{std}))$
 $\text{Percent Moisture} = 100 * B_{ws}$

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 8/19/93
10/11/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENITVA	Umbilical ID	200
City, State	WAGONS, MS	Meterbox ID	909033
Test Location	DRYER #1	ΔH_{g}	1.917
Personnel	TJB, JBS	Gamma (γ)	0.9828

Run Identification									
				Actual	Req'd	Vac			
144				Pre Leak Check	0.000	< 0.02 or 4%	10		
				Post Leak Check	0.000	< 0.02 or 4%	9		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1739	0	572.300	80	1.0	N/A	N/A	58	3	
1753	15	580.90	81	↓	↓	↓	59	3	
1808	30	589.10	82	↓	↓	↓	56	3	
1823	45	597.2	82	↓	↓	↓	57	3	
1838	60	605.501		↓	↓	↓			

10/11/13

Run Identification									
				Actual	Req'd	Vac			
5				Pre Leak Check	0.000	< 0.02 or 4%	10		
				Post Leak Check	0.000	< 0.02 or 4%	10		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1000	0	605.700	70	1.0	N/A	N/A	59	3	
1015	15	614.00	74	↓	↓	↓	63	3	
1030	30	622.24	79	↓	↓	↓	66	3	
1045	45	630.61	83	↓	↓	↓	67	3	
1100	60	638.921		↓	↓	↓			

10/11/13

Run Identification									
				Actual	Req'd	Vac			
6				Pre Leak Check	0.000	< 0.02 or 4%	10		
				Post Leak Check	0.000	< 0.02 or 4%	10		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1137	0	639.100	86	1.0	N/A	N/A	56	3	
1152	15	647.5	87	↓	↓	↓	58	3	
1207	30	655.17	87	↓	↓	↓	59	3	
1222	45	663.24	88	↓	↓	↓	61	3	
1237	60	671.665		↓	↓	↓			

Method 4 - Air Control Techniques, P.C.

Date 10/10/2017

Identification Information

Client	Enviya	Job	1911
Plant Name	Wiggins	Process	DRYER #1
City	Wiggins	State	MS

Sampling Information

Run Number		Balance Number	V1000
Sampling Date		Balance Type	Electronic
Recovery Date		Balance Level	✓
Personnel	TTB JB6	Recovery Area	✓

Location Moisture Data

Run Number	4	5	6
<u>Impinger 1</u>			
Final Weight, grams/mls	858.1	943.8	826.7
Initial Weight, grams/mls	743.0	822.7	722.7
Condensed Water, grams	115.1	121.1	104.0
<u>Impinger 2</u>			
Final Weight, grams/mls	736.5	632.7	744.4
Initial Weight, grams/mls	729.5	661.5	736.5
Condensed Water, grams	7.0	-30.8	7.9
<u>Impinger 3</u>			
Final Weight, grams/mls	597.1	599.5	597.8
Initial Weight, grams/mls	597.0	596.1	597.1
Condensed Water, grams	0.1	3.4	0.7
Condensed Water, grams			
<u>Silica Gel</u>			
Final Weight, grams	805.0	824.0	809.9
Initial Weight, grams	797.7	817.9	805.0
Adsorbed Water, grams	7.3	6.1	4.9
Adsorbed Water, grams	129.5	99.8	—
Total Water, grams	↓	↓	117.5

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (\text{Pbar} + (\Delta H / 13.6))) / (\text{Tm} + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/11/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	Wiggins MS	Meterbox ID	909033
Test Location	PEPPER MILL COOLERS #2	ΔHe	1.917
Personnel	TPS JBB	Gamma (γ)	0.9828

Run Identification <u>M4-7</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%	10		10	
Post Leak Check				0.000	< 0.02 or 4%	8		8	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1343	0	672.000	85	1.0	N/A	N/A	57	3	
1358	15	680.60	86	↓	↓	↓	61	3	
1413	30	687.23	89	↓	↓	↓	61	3	
1428	45	698.1	89	↓	↓	↓	60	3	
1443	60	706.310							

Run Identification <u>M4-8</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%	10		10	
Post Leak Check				0.000	< 0.02 or 4%	4		4	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
1508	0	706.600	89	1.0	N/A	N/A	58	3	
1523	15	715.19	89	↓	↓	↓	57	3	
1538	30	723.95	89	↓	↓	↓	57	3	
1553	45	732.97	90	↓	↓	↓	61	3	
1608	60	741.023							

Run Identification <u>M4-9</u>				Actual			Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%	12		12	
Post Leak Check				0.000	< 0.02 or 4%	9		9	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)	
0	1629	741.300	85	1.0	N/A	N/A	57	3	
15	1644	749.90	84	↓	↓	↓	60	3	
30	1659	758.29	83	↓	↓	↓	59	3	
45	1714	766.65	83	↓	↓	↓	60	3	
60	1729	774.981							

Method.4 - Air Control Techniques, P.C.

Date

Identification Information

Client	ENVIVA	Job	1911
Plant Name	Wiggins, MS	Process	Elect M, II #2
City	Wiggins, MS	State	MS

codes

Sampling Information

Run Number				Balance Number	1620
Sampling Date				Balance Type	Electronic
Recovery Date				Balance Level	<input checked="" type="checkbox"/>
Personnel	TTB JBG			Recovery Area	<input checked="" type="checkbox"/>

Location Moisture Data

	Run Number	7	8	9
<u>Impinger 1</u>				
Final Weight, grams/mls		719.2	852.1	746.3
Initial Weight, grams/mls		695.2	826.7	719.2
Condensed Water, grams		24.0	25.4	27.1
<u>Impinger 2</u>				
Final Weight, grams/mls		715.4	747.4	717.5
Initial Weight, grams/mls		712.2	744.4	715.4
Condensed Water, grams		3.2	3.0	2.1
<u>Impinger 3</u>				
Final Weight, grams/mls		603.6	598.2	603.8
Initial Weight, grams/mls		599.5	597.8	603.6
Condensed Water, grams		4.1	0.4	0.2
Condensed Water, grams				
<u>Silica Gel</u>				
Final Weight, grams		827.9	814.6	830.9
Initial Weight, grams		824.0	809.9	827.9
Adsorbed Water, grams		3.9	4.7	3.0
Adsorbed Water, grams		—	—	—
Total Water, grams		35.2	33.5	32.4

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (\text{Pbar} + (\Delta H / 13.6))) / (\text{Tm} + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/11/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENUTVA	Umbilical ID	200
City, State	WISCONSIN, MS	Meterbox ID	900033
Test Location	DRY Hammer Mill #2	$\Delta H @$	197
Personnel	Tim JBF	Gamma (γ)	0.9828

Run Identification M4-10				Actual Req'd Vac				
Pre Leak Check				0.000	< 0.02 or 4%	10		
Post Leak Check				0.000	< 0.02 or 4%	10		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1811	0	775.300	80	1.0	N/A	N/A	55	3
1826	15	784.200	80				54	3
1841	30	793.100	80				54	3
1846	45	800.71	81				55	3
1861	60	808.79						
		795,100						

1856
~~1841~~
 1911

Run Identification M4-11				Actual Req'd Vac				
Pre Leak Check				0.000	< 0.02 or 4%	10		
Post Leak Check				0.000	< 0.02 or 4%	10		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1935	0 0	809.400	79	1.0	N/A	N/A	57	3
1950	15 15	817.9	78				55	3
2005	30 30	826.5	79				56	3
2020	45 45	835.3	79				56	3
2035	60 60	843.09						

Run Identification M4-12				Actual Req'd Vac				
Pre Leak Check				0.000	< 0.02 or 4%	12		
Post Leak Check				0.000	< 0.02 or 4%	11		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
2048	0	843.560	78	1.0	N/A	N/A	57	3
2103	15	852.17	78				57	3
2118	30	860.25	79				57	3
2133	45	868.22	78				56	3
2148	60	877.76						

32.4
~~34.5~~

Method 4 - Air Control Techniques, P.C.

Date

Identification Information			
Client	ENVIVA	Job	1911
Plant Name	Wiggins	Process	KY Hammer Mill #2
City	Wiggins	State	MS

Sampling Information			
Run Number		Balance Number	V1200
Sampling Date		Balance Type	Electronic
Recovery Date		Balance Level	<input checked="" type="checkbox"/>
Personnel	TJB JBG	Recovery Area	<input checked="" type="checkbox"/>

Location Moisture Data			
Run Number	10	11	12
<u>Impinger 1</u>			
Final Weight, grams/mls	875.7	770.2	898.8
Initial Weight, grams/mls	852.1	746.3	875.7
Condensed Water, grams	23.6	23.9	23.1
<u>Impinger 2</u>			
Final Weight, grams/mls	749.9	720.5	752.8
Initial Weight, grams/mls	747.4	717.5	749.9
Condensed Water, grams	2.5	3.0	2.9
<u>Impinger 3</u>			
Final Weight, grams/mls	598.4	604.4	598.8
Initial Weight, grams/mls	598.2	603.8	598.4
Condensed Water, grams	0.2	0.6	0.4
Condensed Water, grams			
<u>Silica Gel</u>			
Final Weight, grams	818.5	833.4	822.3
Initial Weight, grams	814.6	830.9	818.5
Adsorbed Water, grams	3.9	2.5	3.8
Adsorbed Water, grams	—	—	—
Total Water, grams	30.2	30.0	30.2

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (\text{Pbar} + (\Delta H / 13.6))) / (\text{Tm} + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/18/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	200
City, State	Wiggins MS	Meterbox ID	99033
Test Location	Pellet Mill #1 Cooler	$\Delta H @$	1.917
Personnel	TIA JBB	Gamma (γ)	0.9808

Run Identification		Actual		Req'd		Vac	
M4-13		Pre Leak Check	0.000	< 0.02 or 4%	12		
		Post Leak Check	0.000	< 0.02 or 4%	8		

Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
8:58	0	877.400	67	1.0	N/A	N/A	52	3
9:13	15	886.03	70	↓	↓	↓	55	3
9:28	30	895.1	73	↓	↓	↓	56	3
9:43	45	903.1	77	↓	↓	↓	58	3
9:58	60	911.368		↓	↓	↓		

Run Identification		Actual		Req'd		Vac	
M4-14		Pre Leak Check	0.000	< 0.02 or 4%	10		
		Post Leak Check	0.000	< 0.02 or 4%	10		

Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
10:22	0	911.500	74	1.0	N/A	N/A	59	3
10:37	15	920.39	82	↓	↓	↓	60	3
10:52	30	929.10	86	↓	↓	↓	54	3
11:07	45	938.32	88	↓	↓	↓	55	3
11:22	60	947.345		↓	↓	↓		

Run Identification		Actual		Req'd		Vac	
M4-15		Pre Leak Check	0.000	< 0.02 or 4%	4		
		Post Leak Check	0.000	< 0.02 or 4%	4		

Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
11:41	0	947.600	89	1.0	N/A	N/A	56	3
11:56	15	956.32	89	↓	↓	↓	60	3
12:11	30	964.92	89	↓	↓	↓	60	3
12:26	45	973.55	89	↓	↓	↓	61	3
12:41	60	982.167		↓	↓	↓		

Method 4 - Air Control Techniques, P.C.

Date

Identification Information

Client	Envira	Job	1411
Plant Name	Wiggins	Process	Relet Cools # 1
City	Wiggins	State	MS

Sampling Information

Run Number		Balance Number	
Sampling Date		Balance Type	
Recovery Date		Balance Level	
Personnel	TTB JBG	Recovery Area	

Location Moisture Data

Run Number	13	14	15
<u>Impinger 1</u>			
Final Weight, grams/mls	748.2	787.3	765.0
Initial Weight, grams/mls	728.1	763.4	748.2
Condensed Water, grams	20.1	23.9	16.8
<u>Impinger 2</u>			
Final Weight, grams/mls	722.1	754.0	722.9
Initial Weight, grams/mls	720.5	752.8	722.1
Condensed Water, grams	1.6	1.2	0.8
<u>Impinger 3</u>			
Final Weight, grams/mls	604.4	598.6	604.9
Initial Weight, grams/mls	604.4	598.8	604.4
Condensed Water, grams	0.0	-0.2	0.5
Condensed Water, grams			
<u>Silica Gel</u>			
Final Weight, grams	838.0	825.2	837.9
Initial Weight, grams	833.4	822.3	836.0
Adsorbed Water, grams	2.6	2.9	1.9
Adsorbed Water, grams	—	—	—
Total Water, grams	24.3	27.8	19.9

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (\text{Pbar} + (\Delta H / 13.6))) / (\text{Tm} + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

Method 4 - Air Control Techniques, P.C.

Date

Identification Information			
Client	ENVIVA	Job	1911
Plant Name	Wiggins	Process	ASPIRATOR
City	Wiggins	State	MS

Sampling Information			
Run Number		Balance Number	
Sampling Date		Balance Type	
Recovery Date		Balance Level	
Personnel	TJB JBG	Recovery Area	

Location Moisture Data			
Run Number	16	17	18
<u>Impinger 1</u>			
Final Weight, grams/mls	914.9	958.8	946.7
Initial Weight, grams/mls	787.3	760.0	743.8
Condensed Water, grams	127.6	198.8	202.9
<u>Impinger 2</u>			
Final Weight, grams/mls	877.1	790.3	814.9
Initial Weight, grams/mls	754.0	722.9	746.0
Condensed Water, grams	123.1	67.4	68.9
<u>Impinger 3</u>			
Final Weight, grams/mls	599.7	605.0	600.3
Initial Weight, grams/mls	598.6	604.9	599.7
Condensed Water, grams	1.1	0.1	0.6
Condensed Water, grams			
<u>Silica Gel</u>			
Final Weight, grams	830.2	841.2	832.2
Initial Weight, grams	825.2	837.9	830.2
Adsorbed Water, grams	5.0	3.3	2.0
Adsorbed Water, grams	—	—	—
Total Water, grams	256.8	269.6	271.4

$Vm(std) = \text{Volume of gas sampled at standard conditions (dscf)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

24.7
1016

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/12/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	ENVIVA	Umbilical ID	30
City, State	Wiggins, MS	Meterbox ID	98933
Test Location	Relief Mill Aspirator	ΔH_{ϕ}	1.917
Personnel	T13 JBG	Gamma (γ)	0.9828

Run Identification M4-16				Actual		Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%			12
Post Leak Check				0.000	< 0.02 or 4%			9
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1509	0	982.400	83	1.0	N/A	N/A	54	3
1524	15	989.81	85				60	3
1539	30	998.62	86	↓	↓	↓	60	3
1554	45	1007.31	86	↓	↓	↓	65	3
1609	60	1015.64						

Run Identification M4-17				Actual		Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%			10
Post Leak Check				0.000	< 0.02 or 4%			11
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1626	0	16.000	85	1.0	N/A	N/A	56	3
1651	15	24.81	84				65	3
1706	30	32.27	85	↓	↓	↓	57	3
1721	45	40.18	85	↓	↓	↓	61	3
1736	60	48.149						

Run Identification M4-18				Actual		Req'd		Vac
Pre Leak Check				0.000	< 0.02 or 4%			12
Post Leak Check				0.000	< 0.02 or 4%			8
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
1800	0	48.300	84	1.0	N/A	N/A	57	3
1816	15	57.41	82				61	3
1832	30	66.20	81	↓	↓	↓	62	3
1848	45	74.55	80	↓	↓	↓	62	3
1900	60	82.708						

Air Control Techniques, P.C.
Moisture Sampling Train Field Data Sheet

Date 10/13/13

SOURCE IDENTIFICATION		EQUIPMENT IDENTIFICATION	
Facility	AVIVA	Umbilical ID	200
City, State	Wiggins, MS	Meterbox ID	981033
Test Location	TRIPER #2	ΔH@	1.917
Personnel	115 JBG	Gamma (γ)	0.9828

Run Identification				Actual		Req'd		Vac
M4-19				Pre Leak Check	0.000	< 0.02 or 4%	5	
				Post Leak Check	0.000	< 0.02 or 4%	10	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
9:21	0	82.900	72	1.0	N/A	N/A	56	3
9:36	15	90.93	76	↓	↓	↓	58	3
9:51	30	99.15	79	↓	↓	↓	59	3
10:06	45	106.85	83	↓	↓	↓	60	3
10:21	60	114.788		↓	↓	↓		

Run Identification				Actual		Req'd		Vac
M4-20				Pre Leak Check	0.000	< 0.02 or 4%	2	
				Post Leak Check	0.000	< 0.02 or 4%	2	
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
11:04	0	115.000	88	1.0	N/A	N/A	57	3
11:19	15	123.65	89	↓	↓	↓	61	3
11:34	30	131.96	90	↓	↓	↓	61	3
11:49	45	140.32	91	↓	↓	↓	56	3
12:04	60	148.650		↓	↓	↓		

Run Identification				Actual		Req'd		Vac
M4-21				Pre Leak Check	0.000	< 0.02 or 4%	10	
				Post Leak Check		< 0.02 or 4%		
Clock Time	Elapsed Time (min)	Volume Metered (ft ³)	Meter Temp. (°F)	ΔH (in. W.C.)	Probe Temp. (°F)	Filter Temp. (°F)	Impinger Temp. (°F)	Vacuum (in. Hg)
12:31	0	149.200	89	1.0	N/A	N/A	51	3
12:46	15	157.72	90	↓	↓	↓	58	4
13:01	30	166.39	91	↓	↓	↓	60	7
13:16	45	172.82	91	↓	↓	↓	59	10
13:31	60	179.996		↓	↓	↓		

1346

off 1238 upset condition
 ON 1252

29.85
15224

Method 4 - Air Control Techniques, P.C.

Date 10/13/13

Identification Information			
Client	ENDIYA	Job	1911
Plant Name	Wiggins	Process	DRYER #2
City	Wiggins	State	MS

Sampling Information			
Run Number		Balance Number	V1200
Sampling Date		Balance Type	Electronic
Recovery Date		Balance Level	✓
Personnel		Recovery Area	✓

Location Moisture Data			
Run Number	19	20	21
<u>Impinger 1</u>			
Final Weight, grams/mls	970.0	908.2	922.2
Initial Weight, grams/mls	749.2	748.2	681.2
Condensed Water, grams	220.8	160	241.0
<u>Impinger 2</u>			
Final Weight, grams/mls	829.0	800.3	687.8
Initial Weight, grams/mls	790.3	680.0	674.0
Condensed Water, grams	38.7	120.3	13.8
<u>Impinger 3</u>			
Final Weight, grams/mls	609.3	603.1	612.5
Initial Weight, grams/mls	605.0	600.4	609.3
Condensed Water, grams	4.3	2.7	3.2
Condensed Water, grams			
<u>Silica Gel</u>			
Final Weight, grams	845.1	835.7	847.1
Initial Weight, grams	841.2	832.2	845.3
Adsorbed Water, grams	3.9	3.5	2.0
Adsorbed Water, grams			
Total Water, grams	267.7	286.5	260.0

$Vm(std) = \text{Volume of gas sampled at standard conditions (dsfc)}$
 $Vm(std) = ((\text{Gamma} * 17.64 * Vm * (Pbar + (\Delta H / 13.6))) / (Tm + 460))$
 $Vwc(std) = \text{volume of water vapor at standard conditions (scf)}$
 $Vwc(std) = (0.04707) * (\text{volume of water collected (mls)})$
 $Bws = \text{Mole fraction of water vapor}$
 $Bws = Vwc(std) / (Vm(std) + Vwc(std))$
 $\text{Percent Moisture} = 100 * Bws$

APPENDIX B

Method 25A Data

Test Run 1 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC
ppm

Start Averaging

10/10/2013	10:17:27	29.2
10/10/2013	10:18:26	29.1
10/10/2013	10:19:26	29.4
10/10/2013	10:20:26	28.5
10/10/2013	10:21:26	29.2
10/10/2013	10:22:27	29.8
10/10/2013	10:23:27	30.5
10/10/2013	10:24:27	31.5
10/10/2013	10:25:27	30.8
10/10/2013	10:26:26	29.3
10/10/2013	10:27:26	29.3
10/10/2013	10:28:26	28.9
10/10/2013	10:29:27	29.5
10/10/2013	10:30:27	31.4
10/10/2013	10:31:27	31.1
10/10/2013	10:32:26	31.3
10/10/2013	10:33:26	31.2
10/10/2013	10:34:26	30.4
10/10/2013	10:35:27	30.4
10/10/2013	10:36:27	30.1
10/10/2013	10:37:27	29.7
10/10/2013	10:38:27	30.2
10/10/2013	10:39:26	29.2
10/10/2013	10:40:26	30.1
10/10/2013	10:41:26	30.3
10/10/2013	10:42:26	29.1
10/10/2013	10:43:27	29.5
10/10/2013	10:44:27	30.6
10/10/2013	10:45:27	29.7
10/10/2013	10:46:25	31
10/10/2013	10:47:26	30.1
10/10/2013	10:48:26	30.7
10/10/2013	10:49:26	31.6
10/10/2013	10:50:27	31.6
10/10/2013	10:51:27	32.3
10/10/2013	10:52:27	31.4
10/10/2013	10:53:27	30.4
10/10/2013	10:54:26	31.9
10/10/2013	10:55:26	31.8
10/10/2013	10:56:26	33.1
10/10/2013	10:57:26	32.8
10/10/2013	10:58:27	31.8
10/10/2013	10:59:27	32.5
10/10/2013	11:00:27	32.8
10/10/2013	11:01:26	30.2

10/10/2013	11:02:26	31.2
10/10/2013	11:03:26	30.7
10/10/2013	11:04:26	31.2
10/10/2013	11:05:27	32.7
10/10/2013	11:06:27	31.6
10/10/2013	11:07:27	31.2
10/10/2013	11:08:25	32.5
10/10/2013	11:09:26	31
10/10/2013	11:10:26	30.8
10/10/2013	11:11:26	28.9
10/10/2013	11:12:26	30.9
10/10/2013	11:13:27	31.9
10/10/2013	11:14:27	32.1
10/10/2013	11:15:27	32.6
10/10/2013	11:16:26	34
Average	1807 sampl	30.8
Test Run 1 End		

Test Run 2 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	10:37:12	33.22
10/10/2013	10:38:13	32.73
10/10/2013	10:39:13	33.22
10/10/2013	10:40:13	33.21
10/10/2013	10:41:13	31.78
10/10/2013	10:42:14	29.83
10/10/2013	10:43:14	31.37
10/10/2013	10:44:12	31.5
10/10/2013	10:45:13	33.24
10/10/2013	10:46:13	32.96
10/10/2013	10:47:13	32.52
10/10/2013	10:48:13	32.17
10/10/2013	10:49:14	31.8
10/10/2013	10:50:14	30.68
10/10/2013	10:51:12	29.76
10/10/2013	10:52:12	31.03
10/10/2013	10:53:13	31.9
10/10/2013	10:54:13	32.57
10/10/2013	10:55:13	32.4
10/10/2013	10:56:14	32.68
10/10/2013	10:57:14	33.18
10/10/2013	10:58:12	33.26
10/10/2013	10:59:12	32.76
10/10/2013	11:00:13	31.1
10/10/2013	11:01:12	30.85
10/10/2013	11:02:14	30.84
10/10/2013	11:03:13	30.27
10/10/2013	11:04:12	30.6
10/10/2013	11:05:14	32.18
10/10/2013	11:06:13	30.96
10/10/2013	11:07:12	31.41
10/10/2013	11:08:12	30.82
10/10/2013	11:09:13	31.24
10/10/2013	11:10:13	31.94
10/10/2013	11:11:14	31.25
10/10/2013	11:12:13	30.81
10/10/2013	11:13:12	32.84
10/10/2013	11:14:12	32.11
10/10/2013	11:15:14	32.71
10/10/2013	11:16:13	32.57
10/10/2013	11:17:12	33.7
10/10/2013	11:18:14	33.87
10/10/2013	11:19:13	32.8
10/10/2013	11:20:13	31.93
10/10/2013	11:21:14	33.89

10/10/2013	11:22:13	33.12
10/10/2013	11:23:13	32.56
10/10/2013	11:24:14	32.31
10/10/2013	11:25:13	33.49
10/10/2013	11:26:12	34.83
10/10/2013	11:27:14	34.8
10/10/2013	11:28:13	33.96
10/10/2013	11:29:13	33.5
10/10/2013	11:30:14	34.21
10/10/2013	11:31:13	32.7
10/10/2013	11:32:13	31.67
10/10/2013	11:33:12	31.32
10/10/2013	11:34:13	31.95
10/10/2013	11:35:13	31.59
10/10/2013	11:36:14	31.24
10/10/2013	11:37:13	32.88

Test Run 3 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/10/2013	11:51:37	27.47
10/10/2013	11:52:37	25.81
10/10/2013	11:53:37	25.62
10/10/2013	11:54:38	26.13
10/10/2013	11:55:36	27.21
10/10/2013	11:56:36	27.54
10/10/2013	11:57:36	27.06
10/10/2013	11:58:37	27.89
10/10/2013	11:59:37	27.66
10/10/2013	12:00:37	26.76
10/10/2013	12:01:38	26.92
10/10/2013	12:02:38	26.42
10/10/2013	12:03:36	25.01
10/10/2013	12:04:36	25.47
10/10/2013	12:05:37	25.98
10/10/2013	12:06:37	26.95
10/10/2013	12:07:37	27.79
10/10/2013	12:08:37	26.71
10/10/2013	12:09:38	27.38
10/10/2013	12:10:38	27.84
10/10/2013	12:11:36	25.99
10/10/2013	12:12:36	25.7
10/10/2013	12:13:37	24.64
10/10/2013	12:14:37	25.2
10/10/2013	12:15:37	25.22
10/10/2013	12:16:37	24.65
10/10/2013	12:17:38	24.05
10/10/2013	12:18:36	23.8
10/10/2013	12:19:36	22.94
10/10/2013	12:20:36	23.17
10/10/2013	12:21:37	24.1
10/10/2013	12:22:37	25.63
10/10/2013	12:23:37	26.37
10/10/2013	12:24:37	26.85
10/10/2013	12:25:38	26.02
10/10/2013	12:26:36	25.65
10/10/2013	12:27:36	25.72
10/10/2013	12:28:37	27.03
10/10/2013	12:29:37	26.23
10/10/2013	12:30:37	25.87
10/10/2013	12:31:37	25.97
10/10/2013	12:32:38	25.53
10/10/2013	12:33:38	25.25
10/10/2013	12:34:36	26.76
10/10/2013	12:35:36	27.16

10/10/2013	12:36:37	27.29
10/10/2013	12:37:37	27.02
10/10/2013	12:38:37	27.31
10/10/2013	12:39:37	28.11
10/10/2013	12:40:38	28.86
10/10/2013	12:41:36	28.19
10/10/2013	12:42:36	27.22
10/10/2013	12:43:37	27.74
10/10/2013	12:44:37	28.08
10/10/2013	12:45:37	26.91
10/10/2013	12:46:38	26.97
10/10/2013	12:47:38	27.99
10/10/2013	12:48:36	27.63
10/10/2013	12:49:36	26.3
10/10/2013	12:50:37	25.95
Average	1802 sampl	26.38
Test Run 3 End		

Test Run 4 Begin. STRATA Version 3.2

Operator: DGG
Plant Name: Enviva Wiggins
THC
ppm

Start Averaging		
10/10/2013	17:39:30	73.6
10/10/2013	17:40:31	73.7
10/10/2013	17:41:31	74.2
10/10/2013	17:42:31	74.3
10/10/2013	17:43:31	74.4
10/10/2013	17:44:32	74.6
10/10/2013	17:45:32	75.3
10/10/2013	17:46:32	75.7
10/10/2013	17:47:30	75.7
10/10/2013	17:48:31	75.6
10/10/2013	17:49:31	75
10/10/2013	17:50:31	74.2
10/10/2013	17:51:31	72.5
10/10/2013	17:52:32	71.5
10/10/2013	17:53:32	70.7
10/10/2013	17:54:30	70
10/10/2013	17:55:30	69.3
10/10/2013	17:56:31	68.6
10/10/2013	17:57:31	68
10/10/2013	17:58:31	67.7
10/10/2013	17:59:32	67.1
10/10/2013	18:00:32	66.8
10/10/2013	18:01:30	66.4
10/10/2013	18:02:30	66
10/10/2013	18:03:31	65
10/10/2013	18:04:31	64.5
10/10/2013	18:05:31	64.3
10/10/2013	18:06:31	64.1
10/10/2013	18:07:32	64.8
10/10/2013	18:08:32	65.5
10/10/2013	18:09:30	65.6
10/10/2013	18:10:31	65.7
10/10/2013	18:11:31	65.8
10/10/2013	18:12:31	65.8
10/10/2013	18:13:31	66.6
10/10/2013	18:14:32	66.7
10/10/2013	18:15:32	67
10/10/2013	18:16:30	67
10/10/2013	18:17:30	66.2
10/10/2013	18:18:31	65.5
10/10/2013	18:19:31	65
10/10/2013	18:20:31	64.5
10/10/2013	18:21:32	63.4
10/10/2013	18:22:32	62.8
10/10/2013	18:23:30	62.2

10/10/2013	18:24:30	62
10/10/2013	18:25:31	62.2
10/10/2013	18:26:31	62.2
10/10/2013	18:27:31	62.6
10/10/2013	18:28:31	62.4
10/10/2013	18:29:32	61.7
10/10/2013	18:30:32	61.8
10/10/2013	18:31:30	61.4
10/10/2013	18:32:30	61.5
10/10/2013	18:33:31	61.3
10/10/2013	18:34:31	61.3
10/10/2013	18:35:31	61.1
10/10/2013	18:36:31	61.3
10/10/2013	18:37:32	60.8
10/10/2013	18:38:30	60.2
10/10/2013	18:39:30	60.4
Average	1837 sampl	66.7
Test Run 4 End		

Test Run 5 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	10:00:39	59.48
10/11/2013	10:01:40	59.35
10/11/2013	10:02:40	59.64
10/11/2013	10:03:40	59.19
10/11/2013	10:04:40	59.7
10/11/2013	10:05:41	60.45
10/11/2013	10:06:41	60.54
10/11/2013	10:07:41	60.86
10/11/2013	10:08:40	61.28
10/11/2013	10:09:40	62.22
10/11/2013	10:10:40	62.62
10/11/2013	10:11:40	62.46
10/11/2013	10:12:40	62.22
10/11/2013	10:13:41	61.96
10/11/2013	10:14:41	61.71
10/11/2013	10:15:39	61.79
10/11/2013	10:16:40	61.65
10/11/2013	10:17:40	61.76
10/11/2013	10:18:40	61.82
10/11/2013	10:19:40	61.41
10/11/2013	10:20:41	60.91
10/11/2013	10:21:41	60.34
10/11/2013	10:22:41	60.35
10/11/2013	10:23:39	60.17
10/11/2013	10:24:40	60.48
10/11/2013	10:25:40	60.31
10/11/2013	10:26:40	60.03
10/11/2013	10:27:40	60.26
10/11/2013	10:28:41	60.17
10/11/2013	10:29:41	59.83
10/11/2013	10:30:41	59.58
10/11/2013	10:31:40	60.56
10/11/2013	10:32:40	60.96
10/11/2013	10:33:40	60.79
10/11/2013	10:34:40	61.26
10/11/2013	10:35:41	61.22
10/11/2013	10:36:41	61.09
10/11/2013	10:37:41	61.12
10/11/2013	10:38:39	61.86
10/11/2013	10:39:40	62.32
10/11/2013	10:40:40	62.49
10/11/2013	10:41:40	62.15
10/11/2013	10:42:41	62.22
10/11/2013	10:43:41	62.04
10/11/2013	10:44:41	61.73

10/11/2013	10:45:41	60.99
10/11/2013	10:46:40	61.3
10/11/2013	10:47:40	61.17
10/11/2013	10:48:40	62.35
10/11/2013	10:49:40	63.58
10/11/2013	10:50:41	63.57
10/11/2013	10:51:41	65.12
10/11/2013	10:52:41	67.32
10/11/2013	10:53:39	67.58
10/11/2013	10:54:40	67.4
10/11/2013	10:55:40	66.77
10/11/2013	10:56:40	66
10/11/2013	10:57:40	65.74
10/11/2013	10:58:41	64.85
10/11/2013	10:59:41	64.09
Average	1810 sampl	61.92
Test Run 5 End		

Test Run 6 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	11:37:39	62.85
10/11/2013	11:38:39	63.21
10/11/2013	11:39:40	63.49
10/11/2013	11:40:38	63.72
10/11/2013	11:41:38	64.5
10/11/2013	11:42:38	65.32
10/11/2013	11:43:39	66.16
10/11/2013	11:44:39	66.6
10/11/2013	11:45:39	66.81
10/11/2013	11:46:40	66.6
10/11/2013	11:47:38	64.85
10/11/2013	11:48:38	62.59
10/11/2013	11:49:38	60.21
10/11/2013	11:50:38	58.27
10/11/2013	11:51:39	56.95
10/11/2013	11:52:39	55.02
10/11/2013	11:53:39	53.86
10/11/2013	11:54:39	52.91
10/11/2013	11:55:40	52.4
10/11/2013	11:56:38	52.38
10/11/2013	11:57:38	52.86
10/11/2013	11:58:39	53.87
10/11/2013	11:59:39	54.56
10/11/2013	12:00:39	53.55
10/11/2013	12:01:39	52.72
10/11/2013	12:02:39	52.05
10/11/2013	12:03:40	51.53
10/11/2013	12:04:38	51.4
10/11/2013	12:05:38	52.07
10/11/2013	12:06:38	52.86
10/11/2013	12:07:39	53.12
10/11/2013	12:08:39	53.31
10/11/2013	12:09:39	52.77
10/11/2013	12:10:40	51.76
10/11/2013	12:11:40	51.02
10/11/2013	12:12:38	51.05
10/11/2013	12:13:38	52.13
10/11/2013	12:14:39	52.93
10/11/2013	12:15:39	53.34
10/11/2013	12:16:39	53.7
10/11/2013	12:17:39	53.91
10/11/2013	12:18:40	54.85
10/11/2013	12:19:38	55.39
10/11/2013	12:20:38	55.82
10/11/2013	12:21:38	55.66

10/11/2013	12:22:39	55.8
10/11/2013	12:23:39	56.58
10/11/2013	12:24:39	57.45
10/11/2013	12:25:40	58.57
10/11/2013	12:26:40	59.56
10/11/2013	12:27:38	60.26
10/11/2013	12:28:38	60.52
10/11/2013	12:29:39	60.23
10/11/2013	12:30:39	59.97
10/11/2013	12:31:39	59.98
10/11/2013	12:32:39	58.38
10/11/2013	12:33:40	57.52
10/11/2013	12:34:38	58.26
10/11/2013	12:35:38	59.53
10/11/2013	12:36:38	60.41
Average	1796 sampl	57.17
Test Run 6 End		

Test Run 7 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	13:43:41	29.28
10/11/2013	13:44:42	27.18
10/11/2013	13:45:42	25.85
10/11/2013	13:46:40	24.55
10/11/2013	13:47:40	23.31
10/11/2013	13:48:41	22.64
10/11/2013	13:49:41	22.37
10/11/2013	13:50:41	22.49
10/11/2013	13:51:42	22.37
10/11/2013	13:52:42	22.04
10/11/2013	13:53:40	22.25
10/11/2013	13:54:40	22.98
10/11/2013	13:55:41	22.9
10/11/2013	13:56:41	22.72
10/11/2013	13:57:41	23.05
10/11/2013	13:58:42	23.38
10/11/2013	13:59:42	23.44
10/11/2013	14:00:40	24.2
10/11/2013	14:01:40	24.19
10/11/2013	14:02:41	23.32
10/11/2013	14:03:41	22.78
10/11/2013	14:04:41	22.4
10/11/2013	14:05:41	22.24
10/11/2013	14:06:42	22.53
10/11/2013	14:07:40	22.54
10/11/2013	14:08:40	22
10/11/2013	14:09:40	21.36
10/11/2013	14:10:41	20.81
10/11/2013	14:11:41	20.6
10/11/2013	14:12:41	20.52
10/11/2013	14:13:41	20.67
10/11/2013	14:14:42	21.18
10/11/2013	14:15:40	22.48
10/11/2013	14:16:40	23.46
10/11/2013	14:17:41	23.6
10/11/2013	14:18:41	24.02
10/11/2013	14:19:41	24.31
10/11/2013	14:20:41	24.25
10/11/2013	14:21:42	24.44
10/11/2013	14:22:42	24.59
10/11/2013	14:23:40	24.59
10/11/2013	14:24:40	25.03
10/11/2013	14:25:40	25.21
10/11/2013	14:26:41	25.16
10/11/2013	14:27:41	25.61

10/11/2013	14:28:41	25.91
10/11/2013	14:29:42	24.74
10/11/2013	14:30:42	24.82
10/11/2013	14:31:40	24.18
10/11/2013	14:32:40	23.94
10/11/2013	14:33:41	24.63
10/11/2013	14:34:41	25.19
10/11/2013	14:35:41	25.92
10/11/2013	14:36:41	26.43
10/11/2013	14:37:42	25.26
10/11/2013	14:38:42	24.93
10/11/2013	14:39:40	25.61
10/11/2013	14:40:40	25.25
10/11/2013	14:41:41	24.92
10/11/2013	14:42:41	24.81
Average	1795 sampl	23.8
Test Run 7 End		

Test Run 8 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	15:08:58	20.89
10/11/2013	15:09:58	21.18
10/11/2013	15:10:56	21.36
10/11/2013	15:11:57	21.39
10/11/2013	15:12:57	21.49
10/11/2013	15:13:57	21.51
10/11/2013	15:14:58	21.66
10/11/2013	15:15:58	21.02
10/11/2013	15:16:58	20.12
10/11/2013	15:17:56	19.71
10/11/2013	15:18:57	19.67
10/11/2013	15:19:57	19.07
10/11/2013	15:20:57	19.24
10/11/2013	15:21:57	19.85
10/11/2013	15:22:58	20.21
10/11/2013	15:23:58	20.9
10/11/2013	15:24:56	21.72
10/11/2013	15:25:57	22.45
10/11/2013	15:26:57	23.3
10/11/2013	15:27:57	23.07
10/11/2013	15:28:57	22.47
10/11/2013	15:29:58	22.24
10/11/2013	15:30:58	22.14
10/11/2013	15:31:58	21.87
10/11/2013	15:32:56	22.09
10/11/2013	15:33:57	22.17
10/11/2013	15:34:57	22.55
10/11/2013	15:35:57	22.32
10/11/2013	15:36:57	21.72
10/11/2013	15:37:58	21.14
10/11/2013	15:38:58	21.1
10/11/2013	15:39:58	21.29
10/11/2013	15:40:56	21.44
10/11/2013	15:41:57	21.58
10/11/2013	15:42:57	22.64
10/11/2013	15:43:57	22.48
10/11/2013	15:44:57	22.65
10/11/2013	15:45:58	22.37
10/11/2013	15:46:58	22.73
10/11/2013	15:47:56	22.8
10/11/2013	15:48:57	22.34
10/11/2013	15:49:57	21.76
10/11/2013	15:50:57	21.83
10/11/2013	15:51:57	22.04
10/11/2013	15:52:58	22.15

10/11/2013	15:53:58	22.07
10/11/2013	15:54:58	22.66
10/11/2013	15:55:58	22.99
10/11/2013	15:56:57	22.84
10/11/2013	15:57:57	22.83
10/11/2013	15:58:57	22.2
10/11/2013	15:59:58	21.03
10/11/2013	16:00:58	19.77
10/11/2013	16:01:58	18.88
10/11/2013	16:02:56	18.32
10/11/2013	16:03:57	17.86
10/11/2013	16:04:57	18.62
10/11/2013	16:05:57	18.41
10/11/2013	16:06:57	18.6
10/11/2013	16:07:58	19.1
Average	1796 sampl	21.29

Test Run 8 End

Test Run 9 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	16:29:59	22.84
10/11/2013	16:30:59	21.54
10/11/2013	16:31:59	21.11
10/11/2013	16:33:00	21.4
10/11/2013	16:34:00	21.21
10/11/2013	16:35:00	21.39
10/11/2013	16:36:00	21.79
10/11/2013	16:36:59	23.24
10/11/2013	16:37:59	23.79
10/11/2013	16:38:59	24.8
10/11/2013	16:39:59	25.11
10/11/2013	16:41:00	26.01
10/11/2013	16:42:00	28.05
10/11/2013	16:43:00	29.59
10/11/2013	16:44:00	29.65
10/11/2013	16:44:59	29.74
10/11/2013	16:45:59	29.86
10/11/2013	16:46:59	33.48
10/11/2013	16:48:00	32.59
10/11/2013	16:49:00	28.94
10/11/2013	16:49:59	26.37
10/11/2013	16:50:59	25.7
10/11/2013	16:51:59	24.69
10/11/2013	16:53:00	24.55
10/11/2013	16:54:00	24.78
10/11/2013	16:55:00	25.37
10/11/2013	16:55:59	26.6
10/11/2013	16:56:59	27.42
10/11/2013	16:57:59	26.35
10/11/2013	16:58:59	25.6
10/11/2013	17:00:00	25.52
10/11/2013	17:01:00	25.32
10/11/2013	17:02:00	24.67
10/11/2013	17:03:00	24.39
10/11/2013	17:04:01	24.2
10/11/2013	17:04:59	23.43
10/11/2013	17:05:59	22.29
10/11/2013	17:06:59	21.55
10/11/2013	17:08:00	21.18
10/11/2013	17:09:00	21.33
10/11/2013	17:10:00	21.67
10/11/2013	17:10:59	21.91
10/11/2013	17:11:59	22.59
10/11/2013	17:12:59	22.87
10/11/2013	17:14:00	23.27

10/11/2013	17:15:00	23.85
10/11/2013	17:16:00	23.83
10/11/2013	17:17:00	23.05
10/11/2013	17:17:59	23.11
10/11/2013	17:18:59	23.12
10/11/2013	17:19:59	24.45
10/11/2013	17:21:00	24.59
10/11/2013	17:22:00	24.41
10/11/2013	17:23:00	24.36
10/11/2013	17:24:00	25.25
10/11/2013	17:24:59	25.58
10/11/2013	17:25:59	26.03
10/11/2013	17:26:59	26.29
10/11/2013	17:27:59	26.55
10/11/2013	17:29:00	26.07
10/11/2013	17:30:00	25.36
10/11/2013	17:31:00	24.68
10/11/2013	17:32:00	24.5
10/11/2013	17:32:59	24.26
10/11/2013	17:33:59	24.15
Average	1951 sampl	24.82

Test Run 9 End

Test Run 10 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	18:11:17	29.88
10/11/2013	18:12:18	33.18
10/11/2013	18:13:18	31
10/11/2013	18:14:18	22.29
10/11/2013	18:15:18	19.06
10/11/2013	18:16:19	19
10/11/2013	18:17:19	21.06
10/11/2013	18:18:19	23.21
10/11/2013	18:19:17	22.71
10/11/2013	18:20:18	23.92
10/11/2013	18:21:18	23.38
10/11/2013	18:22:18	22.46
10/11/2013	18:23:19	23.73
10/11/2013	18:24:19	27.16
10/11/2013	18:25:19	28.89
10/11/2013	18:26:17	27.17
10/11/2013	18:27:18	22.65
10/11/2013	18:28:18	22.36
10/11/2013	18:29:18	23.07
10/11/2013	18:30:18	23.39
10/11/2013	18:31:19	21.74
10/11/2013	18:32:19	21
10/11/2013	18:33:19	21.29
10/11/2013	18:34:17	20.98
10/11/2013	18:35:18	18.39
10/11/2013	18:36:18	18.16
10/11/2013	18:37:18	18.91
10/11/2013	18:38:19	19.32
10/11/2013	18:39:19	21.57
10/11/2013	18:40:19	25.3
10/11/2013	18:41:17	31.9
10/11/2013	18:42:18	38.29
10/11/2013	18:43:18	33.17
10/11/2013	18:44:18	31.99
10/11/2013	18:45:19	25.13
10/11/2013	18:46:19	21.93
10/11/2013	18:47:19	19.45
10/11/2013	18:48:19	19.52
10/11/2013	18:49:18	18.88
10/11/2013	18:50:18	20.12
10/11/2013	18:51:18	20.89
10/11/2013	18:52:18	21.09
10/11/2013	18:53:19	21.01
10/11/2013	18:54:19	19.4
10/11/2013	18:55:17	19.85

10/11/2013	18:56:18	24.65
10/11/2013	18:57:18	24.98
10/11/2013	18:58:18	22.99
10/11/2013	18:59:18	23.31
10/11/2013	19:00:19	25.22
10/11/2013	19:01:19	25.84
10/11/2013	19:02:19	27.93
10/11/2013	19:03:17	30.86
10/11/2013	19:04:18	37.73
10/11/2013	19:05:18	41.49
10/11/2013	19:06:18	33.42
10/11/2013	19:07:19	28.12
10/11/2013	19:08:19	24.42
10/11/2013	19:09:19	28.47
10/11/2013	19:10:17	32.11
10/11/2013	19:11:18	35.91
10/11/2013	19:12:18	31.9
Average	1881 sampl	25.19
Test Run 10 End		

Test Run 11 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	19:35:45	16.3
10/11/2013	19:36:45	16.9
10/11/2013	19:37:45	19.2
10/11/2013	19:38:46	19.43
10/11/2013	19:39:46	20.92
10/11/2013	19:40:46	21.44
10/11/2013	19:41:45	23.07
10/11/2013	19:42:45	23.32
10/11/2013	19:43:45	24.41
10/11/2013	19:44:46	25.71
10/11/2013	19:45:46	30.06
10/11/2013	19:46:46	36.61
10/11/2013	19:47:46	35.99
10/11/2013	19:48:46	29.55
10/11/2013	19:49:45	23.62
10/11/2013	19:50:45	23.25
10/11/2013	19:51:45	22.61
10/11/2013	19:52:45	23.8
10/11/2013	19:53:46	21.47
10/11/2013	19:54:46	20.75
10/11/2013	19:55:46	21.14
10/11/2013	19:56:46	22.12
10/11/2013	19:57:45	23.08
10/11/2013	19:58:45	22.57
10/11/2013	19:59:46	25.43
10/11/2013	20:00:46	26.18
10/11/2013	20:01:46	27.36
10/11/2013	20:02:46	26.43
10/11/2013	20:03:45	32.28
10/11/2013	20:04:45	29.23
10/11/2013	20:05:45	34.45
10/11/2013	20:06:45	34.13
10/11/2013	20:07:46	30.96
10/11/2013	20:08:46	30.2
10/11/2013	20:09:46	32.75
10/11/2013	20:10:47	36.19
10/11/2013	20:11:45	38.78
10/11/2013	20:12:45	37.58
10/11/2013	20:13:45	34.83
10/11/2013	20:14:46	30.77
10/11/2013	20:15:46	30.88
10/11/2013	20:16:46	31.74
10/11/2013	20:17:46	34.53
10/11/2013	20:18:45	42.51
10/11/2013	20:19:45	44.65

10/11/2013	20:20:45	35.45
10/11/2013	20:21:46	25.21
10/11/2013	20:22:46	23.77
10/11/2013	20:23:46	28.87
10/11/2013	20:24:46	36.75
10/11/2013	20:25:45	45.05
10/11/2013	20:26:45	45.64
10/11/2013	20:27:45	41.52
10/11/2013	20:28:45	35.53
10/11/2013	20:29:46	33.91
10/11/2013	20:30:46	34.59
10/11/2013	20:31:46	29.84
10/11/2013	20:32:46	31.48
10/11/2013	20:33:45	39.63
10/11/2013	20:34:45	36.38
Average	1794 sampl	29.72
Test Run 11 End		

Test Run 12 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/11/2013	20:49:06	22.17
10/11/2013	20:50:04	21.67
10/11/2013	20:51:04	23.4
10/11/2013	20:52:05	24.29
10/11/2013	20:53:05	25.04
10/11/2013	20:54:05	26.33
10/11/2013	20:55:05	26.92
10/11/2013	20:56:06	25.87
10/11/2013	20:57:06	25.72
10/11/2013	20:58:04	25.14
10/11/2013	20:59:04	25.52
10/11/2013	21:00:05	25.37
10/11/2013	21:01:05	25.64
10/11/2013	21:02:05	26.15
10/11/2013	21:03:05	26.08
10/11/2013	21:04:06	24.52
10/11/2013	21:05:04	25.79
10/11/2013	21:06:04	26.55
10/11/2013	21:07:04	27.79
10/11/2013	21:08:05	28.72
10/11/2013	21:09:05	27.24
10/11/2013	21:10:05	30.06
10/11/2013	21:11:05	33.03
10/11/2013	21:12:06	28.99
10/11/2013	21:13:04	20.95
10/11/2013	21:14:04	19.34
10/11/2013	21:15:05	19.67
10/11/2013	21:16:05	21.55
10/11/2013	21:17:05	26.17
10/11/2013	21:18:05	34.11
10/11/2013	21:19:06	29.02
10/11/2013	21:20:06	23.47
10/11/2013	21:21:04	18.29
10/11/2013	21:22:04	20.47
10/11/2013	21:23:05	20.63
10/11/2013	21:24:05	18.82
10/11/2013	21:25:05	18.74
10/11/2013	21:26:06	17.07
10/11/2013	21:27:04	17.1
10/11/2013	21:28:04	18.57
10/11/2013	21:29:05	22.44
10/11/2013	21:30:05	23.51
10/11/2013	21:31:05	23.1
10/11/2013	21:32:05	23.66
10/11/2013	21:33:05	26.36

10/11/2013	21:34:06	29.16
10/11/2013	21:35:04	30.42
10/11/2013	21:36:04	24.58
10/11/2013	21:37:05	22.02
10/11/2013	21:38:05	21.27
10/11/2013	21:39:05	22.01
10/11/2013	21:40:05	21.7
10/11/2013	21:41:06	25.89
10/11/2013	21:42:06	27.16
10/11/2013	21:43:04	26.97
10/11/2013	21:44:04	27.62
10/11/2013	21:45:04	25.38
10/11/2013	21:46:05	22.73
10/11/2013	21:47:05	22.71
10/11/2013	21:48:05	24.06
Average	1802 samp	24.43
Test Run 12 End		

Test Run 13 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	8:58:20	33.01
10/12/2013	8:59:20	33.09
10/12/2013	9:00:21	33.69
10/12/2013	9:01:21	33.38
10/12/2013	9:02:19	34.58
10/12/2013	9:03:19	34.24
10/12/2013	9:04:20	32.82
10/12/2013	9:05:20	31.76
10/12/2013	9:06:20	31.56
10/12/2013	9:07:20	32.43
10/12/2013	9:08:21	32.07
10/12/2013	9:09:21	33.62
10/12/2013	9:10:21	35.22
10/12/2013	9:11:19	35.73
10/12/2013	9:12:20	36.7
10/12/2013	9:13:20	38.36
10/12/2013	9:14:20	39.65
10/12/2013	9:15:20	36.74
10/12/2013	9:16:21	34.73
10/12/2013	9:17:21	37.06
10/12/2013	9:18:19	39.31
10/12/2013	9:19:19	40.7
10/12/2013	9:20:20	41.32
10/12/2013	9:21:20	42.72
10/12/2013	9:22:20	44.45
10/12/2013	9:23:21	41.77
10/12/2013	9:24:21	41.75
10/12/2013	9:25:19	40.84
10/12/2013	9:26:19	40.01
10/12/2013	9:27:20	39.81
10/12/2013	9:28:20	38.16
10/12/2013	9:29:20	36.14
10/12/2013	9:30:20	33.8
10/12/2013	9:31:21	42.88
10/12/2013	9:32:21	44.68
10/12/2013	9:33:19	48.06
10/12/2013	9:34:19	48.98
10/12/2013	9:35:20	49.89
10/12/2013	9:36:20	50.59
10/12/2013	9:37:20	48.17
10/12/2013	9:38:20	42.62
10/12/2013	9:39:21	41.05
10/12/2013	9:40:21	40.93
10/12/2013	9:41:19	38.08
10/12/2013	9:42:19	36.88

10/12/2013	9:43:20	38.28
10/12/2013	9:44:20	37.83
10/12/2013	9:45:20	38.96
10/12/2013	9:46:20	39.74
10/12/2013	9:47:21	39.65
10/12/2013	9:48:21	38.16
10/12/2013	9:49:19	36.49
10/12/2013	9:50:19	37.79
10/12/2013	9:51:20	38.86
10/12/2013	9:52:20	38.2
10/12/2013	9:53:20	39.36
10/12/2013	9:54:21	42.28
10/12/2013	9:55:21	42.37
10/12/2013	9:56:19	42.48
10/12/2013	9:57:19	42.15
10/12/2013	9:58:20	42.58
Average	1843 sampl	39.05
Test Run 13 End		

Test Run 14 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	10:23:19	38.78
10/12/2013	10:24:19	38.95
10/12/2013	10:25:20	37.38
10/12/2013	10:26:20	35.26
10/12/2013	10:27:20	33.47
10/12/2013	10:28:21	33.54
10/12/2013	10:29:21	35.1
10/12/2013	10:30:19	36.39
10/12/2013	10:31:19	38.16
10/12/2013	10:32:20	37.83
10/12/2013	10:33:20	38.5
10/12/2013	10:34:20	39.8
10/12/2013	10:35:20	41.11
10/12/2013	10:36:20	43.31
10/12/2013	10:37:21	43.12
10/12/2013	10:38:19	41.6
10/12/2013	10:39:19	40.09
10/12/2013	10:40:20	41.76
10/12/2013	10:41:20	37.42
10/12/2013	10:42:20	35.32
10/12/2013	10:43:20	36.85
10/12/2013	10:44:21	37.03
10/12/2013	10:45:21	37.63
10/12/2013	10:46:19	37.23
10/12/2013	10:47:19	36.6
10/12/2013	10:48:20	36.58
10/12/2013	10:49:20	34.3
10/12/2013	10:50:20	32.95
10/12/2013	10:51:20	35.86
10/12/2013	10:52:21	40.36
10/12/2013	10:53:21	41.13
10/12/2013	10:54:19	40.92
10/12/2013	10:55:19	38.94
10/12/2013	10:56:20	35.9
10/12/2013	10:57:20	34.71
10/12/2013	10:58:20	35.12
10/12/2013	10:59:20	38.4
10/12/2013	11:00:21	38.46
10/12/2013	11:01:19	38.96
10/12/2013	11:02:19	39.11
10/12/2013	11:03:20	39.66
10/12/2013	11:04:20	37.43
10/12/2013	11:05:20	32.13
10/12/2013	11:06:20	25.88
10/12/2013	11:07:21	22.76

10/12/2013	11:08:19	20.44
10/12/2013	11:09:19	21.39
10/12/2013	11:10:20	19.1
10/12/2013	11:11:20	20.05
10/12/2013	11:12:20	19.67
10/12/2013	11:13:20	20.48
10/12/2013	11:14:21	23.27
10/12/2013	11:15:21	23.34
10/12/2013	11:16:19	22.56
10/12/2013	11:17:19	20.89
10/12/2013	11:18:20	21.23
10/12/2013	11:19:20	22.61
10/12/2013	11:20:20	24.32
10/12/2013	11:21:20	25.83
10/12/2013	11:22:21	25.38
Average	1802 sampl	33.29
Test Run 14 End		

Test Run 15 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC
ppm

Start Averaging

10/12/2013	11:41:41	42.04
10/12/2013	11:42:42	38.71
10/12/2013	11:43:42	37.78
10/12/2013	11:44:42	33.87
10/12/2013	11:45:42	33.86
10/12/2013	11:46:43	38.57
10/12/2013	11:47:43	38.29
10/12/2013	11:48:41	37.43
10/12/2013	11:49:41	35.42
10/12/2013	11:50:42	35.35
10/12/2013	11:51:42	36.29
10/12/2013	11:52:42	36.18
10/12/2013	11:53:42	39.17
10/12/2013	11:54:43	41.21
10/12/2013	11:55:43	45.09
10/12/2013	11:56:41	44.99
10/12/2013	11:57:42	42.66
10/12/2013	11:58:42	41.22
10/12/2013	11:59:42	40.64
10/12/2013	12:00:42	41.76
10/12/2013	12:01:43	41.25
10/12/2013	12:02:43	40.48
10/12/2013	12:03:41	40.5
10/12/2013	12:04:41	35.92
10/12/2013	12:05:42	39.32
10/12/2013	12:06:42	39.55
10/12/2013	12:07:42	37.98
10/12/2013	12:08:42	37.41
10/12/2013	12:09:43	34.56
10/12/2013	12:10:43	32.14
10/12/2013	12:11:41	30.17
10/12/2013	12:12:42	29.4
10/12/2013	12:13:42	31.84
10/12/2013	12:14:42	31.63
10/12/2013	12:15:42	30.68
10/12/2013	12:16:43	30.88
10/12/2013	12:17:43	31.21
10/12/2013	12:18:41	33.29
10/12/2013	12:19:41	35.08
10/12/2013	12:20:42	36.57
10/12/2013	12:21:42	34.06
10/12/2013	12:22:42	32.44
10/12/2013	12:23:43	31.77
10/12/2013	12:24:43	31.01
10/12/2013	12:25:41	31.56

10/12/2013	12:26:41	32.83
10/12/2013	12:27:42	31.92
10/12/2013	12:28:42	33.46
10/12/2013	12:29:42	33.76
10/12/2013	12:30:43	33.98
10/12/2013	12:31:43	33.51
10/12/2013	12:32:41	33.07
10/12/2013	12:33:41	32.11
10/12/2013	12:34:41	34.32
10/12/2013	12:35:42	32.87
10/12/2013	12:36:42	33.76
10/12/2013	12:37:42	35.71
10/12/2013	12:38:42	32.83
10/12/2013	12:39:43	31.48
10/12/2013	12:40:43	32.15
Average	1794 sampl	35.65
Test Run 15 End		

Test Run 1 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC
ppm

Start Averaging

10/12/2013	15:09:26	1001.1
10/12/2013	15:10:26	1022.4
10/12/2013	15:11:26	1009.4
10/12/2013	15:12:26	1027.4
10/12/2013	15:13:27	1045.1
10/12/2013	15:14:27	1073.3
10/12/2013	15:15:26	1039.6
10/12/2013	15:16:26	1038.3
10/12/2013	15:17:26	1049.6
10/12/2013	15:18:26	1074.6
10/12/2013	15:19:27	1072.1
10/12/2013	15:20:27	1010.8
10/12/2013	15:21:27	962.7
10/12/2013	15:22:25	922.6
10/12/2013	15:23:26	912.5
10/12/2013	15:24:26	885.5
10/12/2013	15:25:26	971
10/12/2013	15:26:27	1016
10/12/2013	15:27:27	1059.8
10/12/2013	15:28:27	1099.5
10/12/2013	15:29:25	1128.8
10/12/2013	15:30:26	1126.8
10/12/2013	15:31:26	1103.4
10/12/2013	15:32:26	1069.6
10/12/2013	15:33:27	1011.3
10/12/2013	15:34:27	1040.7
10/12/2013	15:35:27	1079.2
10/12/2013	15:36:25	1094
10/12/2013	15:37:26	1082.4
10/12/2013	15:38:26	1112.7
10/12/2013	15:39:26	1120.2
10/12/2013	15:40:26	1154.1
10/12/2013	15:41:27	1168.4
10/12/2013	15:42:27	1163.2
10/12/2013	15:43:27	1133.2
10/12/2013	15:44:26	1049.9
10/12/2013	15:45:26	1053.5
10/12/2013	15:46:26	1027
10/12/2013	15:47:26	1020.1
10/12/2013	15:48:27	1022.4
10/12/2013	15:49:27	1050
10/12/2013	15:50:27	1065.4
10/12/2013	15:51:25	1040.1
10/12/2013	15:52:26	1079.5
10/12/2013	15:53:26	1113.1

10/12/2013	15:54:26	1144
10/12/2013	15:55:26	1128.2
10/12/2013	15:56:27	1054
10/12/2013	15:57:27	993.8
10/12/2013	15:58:27	1039.7
10/12/2013	15:59:25	1073
10/12/2013	16:00:26	1061.5
10/12/2013	16:01:26	1101.2
10/12/2013	16:02:26	1085.7
10/12/2013	16:03:26	1125.9
10/12/2013	16:04:27	1169.1
10/12/2013	16:05:27	1190.6
10/12/2013	16:06:27	1218.4
10/12/2013	16:07:26	1252.7
10/12/2013	16:08:26	1293.9
Average	1811 sampl	1074.7
Test Run 1 End		

Test Run 2 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	16:36:23	989.3
10/12/2013	16:37:21	1058.5
10/12/2013	16:38:22	1059.2
10/12/2013	16:39:22	1090.3
10/12/2013	16:40:22	1113.4
10/12/2013	16:41:23	1157.2
10/12/2013	16:42:23	1148.6
10/12/2013	16:43:23	1105.5
10/12/2013	16:44:21	1046.7
10/12/2013	16:45:22	1012.7
10/12/2013	16:46:22	968.8
10/12/2013	16:47:22	963.1
10/12/2013	16:48:22	949.2
10/12/2013	16:49:23	960.6
10/12/2013	16:50:23	959
10/12/2013	16:51:21	942.5
10/12/2013	16:52:22	962.3
10/12/2013	16:53:22	925.5
10/12/2013	16:54:22	960.7
10/12/2013	16:55:23	971.3
10/12/2013	16:56:23	990.3
10/12/2013	16:57:23	949.2
10/12/2013	16:58:21	891.5
10/12/2013	16:59:22	905.3
10/12/2013	17:00:22	914.1
10/12/2013	17:01:22	914.2
10/12/2013	17:02:23	926.1
10/12/2013	17:03:23	930.9
10/12/2013	17:04:23	895.7
10/12/2013	17:05:21	943.1
10/12/2013	17:06:22	943.9
10/12/2013	17:07:22	978.3
10/12/2013	17:08:22	940.6
10/12/2013	17:09:23	993.2
10/12/2013	17:10:23	996.5
10/12/2013	17:11:23	986.9
10/12/2013	17:12:21	952
10/12/2013	17:13:22	875.5
10/12/2013	17:14:22	916.5
10/12/2013	17:15:22	939.4
10/12/2013	17:16:23	930.8
10/12/2013	17:17:23	919.8
10/12/2013	17:18:23	938.6
10/12/2013	17:19:21	999.3
10/12/2013	17:20:22	986.2

10/12/2013	17:21:22	963
10/12/2013	17:22:22	910.9
10/12/2013	17:23:23	886.5
10/12/2013	17:24:23	873.2
10/12/2013	17:25:21	870.2
10/12/2013	17:26:21	876.3
10/12/2013	17:27:22	925.8
10/12/2013	17:28:22	911.6
10/12/2013	17:29:22	865.7
10/12/2013	17:30:22	850
10/12/2013	17:31:23	893.9
10/12/2013	17:32:23	913.1
10/12/2013	17:33:21	915.1
10/12/2013	17:34:21	918.1
10/12/2013	17:35:22	960.6
10/12/2013	17:36:22	942.2
Average	1824 sampl	957
Test Run 2 End		

Test Run 3 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/12/2013	18:00:49	1126.2
10/12/2013	18:01:49	1091.3
10/12/2013	18:02:49	1034.6
10/12/2013	18:03:49	996.3
10/12/2013	18:04:50	1063.4
10/12/2013	18:05:50	1027.2
10/12/2013	18:06:50	995.6
10/12/2013	18:07:48	1085.5
10/12/2013	18:08:49	1133.7
10/12/2013	18:09:49	1177.7
10/12/2013	18:10:49	1174.3
10/12/2013	18:11:50	1169.6
10/12/2013	18:12:50	1112.9
10/12/2013	18:13:50	1135.7
10/12/2013	18:14:50	1102.2
10/12/2013	18:15:49	1176.6
10/12/2013	18:16:49	1201.9
10/12/2013	18:17:49	1217
10/12/2013	18:18:49	1248
10/12/2013	18:19:50	1297.6
10/12/2013	18:20:50	1351.7
10/12/2013	18:21:50	1412.8
10/12/2013	18:22:49	1417.9
10/12/2013	18:23:49	1368.5
10/12/2013	18:24:49	1287.4
10/12/2013	18:25:49	1173.7
10/12/2013	18:26:50	1198.4
10/12/2013	18:27:50	1205.2
10/12/2013	18:28:50	1198.8
10/12/2013	18:29:50	1194.9
10/12/2013	18:30:49	1174.8
10/12/2013	18:31:49	1184.2
10/12/2013	18:32:49	1161.6
10/12/2013	18:33:50	1200.8
10/12/2013	18:34:50	1239.5
10/12/2013	18:35:50	1260.8
10/12/2013	18:36:50	1242.4
10/12/2013	18:37:49	1230.9
10/12/2013	18:38:49	1200.6
10/12/2013	18:39:49	1159
10/12/2013	18:40:49	1156.6
10/12/2013	18:41:50	1183.6
10/12/2013	18:42:50	1112.7
10/12/2013	18:43:50	1146.3
10/12/2013	18:44:48	1178.5

10/12/2013	18:45:49	1184.8
10/12/2013	18:46:49	1190.2
10/12/2013	18:47:49	1236.3
10/12/2013	18:48:50	1229.3
10/12/2013	18:49:50	1299.9
10/12/2013	18:50:50	1314.9
10/12/2013	18:51:48	1303.2
10/12/2013	18:52:49	1305.8
10/12/2013	18:53:49	1308.6
10/12/2013	18:54:49	1314
10/12/2013	18:55:50	1277
10/12/2013	18:56:50	1203.3
10/12/2013	18:57:50	1144.9
10/12/2013	18:58:48	1242.6
10/12/2013	18:59:49	1242.4
Average	1796 sampl	1200

Test Run 3 End

Test Run 9 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/13/2013	9:22:03	71.7
10/13/2013	9:23:03	73.9
10/13/2013	9:24:04	76.1
10/13/2013	9:25:04	78.7
10/13/2013	9:26:04	80.4
10/13/2013	9:27:04	82.1
10/13/2013	9:28:05	83.8
10/13/2013	9:29:03	85.1
10/13/2013	9:30:03	85.8
10/13/2013	9:31:03	86.3
10/13/2013	9:32:04	86.9
10/13/2013	9:33:04	87.8
10/13/2013	9:34:04	88
10/13/2013	9:35:05	89.5
10/13/2013	9:36:03	87.7
10/13/2013	9:37:03	87
10/13/2013	9:38:03	86.1
10/13/2013	9:39:04	85.2
10/13/2013	9:40:04	84.8
10/13/2013	9:41:04	85.1
10/13/2013	9:42:04	85.9
10/13/2013	9:43:05	87.4
10/13/2013	9:44:03	88.9
10/13/2013	9:45:03	89.8
10/13/2013	9:46:03	90.7
10/13/2013	9:47:04	90.6
10/13/2013	9:48:04	90.8
10/13/2013	9:49:04	92.2
10/13/2013	9:50:05	93.7
10/13/2013	9:51:03	93.8
10/13/2013	9:52:03	94.6
10/13/2013	9:53:03	95.6
10/13/2013	9:54:04	96
10/13/2013	9:55:04	96.3
10/13/2013	9:56:04	97
10/13/2013	9:57:04	97.5
10/13/2013	9:58:05	98
10/13/2013	9:59:03	98.3
10/13/2013	10:00:03	99.7
10/13/2013	10:01:03	100.8
10/13/2013	10:02:04	101.7
10/13/2013	10:03:04	102.4
10/13/2013	10:04:04	103
10/13/2013	10:05:05	102.3
10/13/2013	10:06:03	101.1

10/13/2013	10:07:03	100
10/13/2013	10:08:03	98.6
10/13/2013	10:09:04	98.2
10/13/2013	10:10:04	98.4
10/13/2013	10:11:04	98.1
10/13/2013	10:12:04	97.6
10/13/2013	10:13:05	96.8
10/13/2013	10:14:03	95.4
10/13/2013	10:15:03	92.2
10/13/2013	10:16:03	91.5
10/13/2013	10:17:04	93.1
10/13/2013	10:18:04	94.6
10/13/2013	10:19:04	97.1
10/13/2013	10:20:04	97.7
10/13/2013	10:21:05	97.5
Average	1797 sampl	91.8
Test Run 9 End		

Test Run 10 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC
ppm

Start Averaging

10/13/2013	11:04:49	77.08
10/13/2013	11:05:50	78.11
10/13/2013	11:06:50	78.19
10/13/2013	11:07:50	77.63
10/13/2013	11:08:50	77.56
10/13/2013	11:09:51	77.71
10/13/2013	11:10:51	77.97
10/13/2013	11:11:49	77.89
10/13/2013	11:12:49	78.97
10/13/2013	11:13:50	79.14
10/13/2013	11:14:50	77.97
10/13/2013	11:15:51	76.86
10/13/2013	11:16:49	76.19
10/13/2013	11:17:49	76.58
10/13/2013	11:18:50	76.82
10/13/2013	11:19:50	77.53
10/13/2013	11:20:50	78.27
10/13/2013	11:21:50	79.01
10/13/2013	11:22:51	79.04
10/13/2013	11:23:51	78.95
10/13/2013	11:24:49	78.85
10/13/2013	11:25:50	78.45
10/13/2013	11:26:50	78.1
10/13/2013	11:27:50	78.55
10/13/2013	11:28:50	78.58
10/13/2013	11:29:51	78.39
10/13/2013	11:30:51	78.37
10/13/2013	11:31:49	79.42
10/13/2013	11:32:49	81.98
10/13/2013	11:33:50	84.04
10/13/2013	11:34:50	83.84
10/13/2013	11:35:50	83.55
10/13/2013	11:36:50	83.19
10/13/2013	11:37:51	82.62
10/13/2013	11:38:51	82.45
10/13/2013	11:39:49	82.09
10/13/2013	11:40:49	81.91
10/13/2013	11:41:50	81.54
10/13/2013	11:42:50	81.56
10/13/2013	11:43:50	82.21
10/13/2013	11:44:51	82.55
10/13/2013	11:45:51	82.6
10/13/2013	11:46:49	82.99
10/13/2013	11:47:49	83.33
10/13/2013	11:48:50	83.22

10/13/2013	11:49:50	83.17
10/13/2013	11:50:50	84.26
10/13/2013	11:51:50	86.33
10/13/2013	11:52:51	87.37
10/13/2013	11:53:51	85.99
10/13/2013	11:54:49	85.29
10/13/2013	11:55:49	85.22
10/13/2013	11:56:50	86.39
10/13/2013	11:57:50	86.43
10/13/2013	11:58:50	85.81
10/13/2013	11:59:50	86.1
10/13/2013	12:00:51	86.23
10/13/2013	12:01:51	84.93
10/13/2013	12:02:49	82.97
10/13/2013	12:03:50	82.23
10/13/2013	12:04:50	84.21
Average	1825 sampl	81.24
Test Run 10 End		

Test Run 11 Begin. STRATA Version 3.2

Operator: DGG

Plant Name: Enviva Wiggins

THC

ppm

Start Averaging

10/13/2013	12:31:14	107.99
10/13/2013	12:32:14	108.6
10/13/2013	12:33:15	109.57
10/13/2013	12:34:15	112.47
10/13/2013	12:35:15	115.91

Pause

10/13/2013	12:36:15	115.09
10/13/2013	12:37:14	112.39
10/13/2013	12:38:14	111.26
10/13/2013	12:39:14	112.42
10/13/2013	12:40:14	113.56
10/13/2013	12:41:15	114.42
10/13/2013	12:42:15	113.98
10/13/2013	12:43:15	112.12
10/13/2013	12:44:15	110.5
10/13/2013	12:45:14	109.3
10/13/2013	12:46:14	108.63
10/13/2013	12:47:14	110.13
10/13/2013	12:48:14	112.11
10/13/2013	12:49:15	112.2
10/13/2013	12:50:15	111.62
10/13/2013	12:51:15	111.91

End Pause

10/13/2013	12:52:15	111.76
10/13/2013	12:53:14	110.85
10/13/2013	12:54:14	109.25
10/13/2013	12:55:14	107.32
10/13/2013	12:56:15	105.6
10/13/2013	12:57:15	105.51
10/13/2013	12:58:15	105.13
10/13/2013	12:59:15	103.83
10/13/2013	13:00:15	101.32
10/13/2013	13:01:14	100.13
10/13/2013	13:02:14	99.2
10/13/2013	13:03:14	99
10/13/2013	13:04:14	99.6
10/13/2013	13:05:15	100.72
10/13/2013	13:06:15	100.21
10/13/2013	13:07:15	99.39
10/13/2013	13:08:15	99
10/13/2013	13:09:14	98.91
10/13/2013	13:10:14	98.55
10/13/2013	13:11:14	99.06
10/13/2013	13:12:15	99.18
10/13/2013	13:13:15	99.24

10/13/2013	13:14:15	100.67
10/13/2013	13:15:15	101.29
10/13/2013	13:16:14	100.86
10/13/2013	13:17:14	100.04
10/13/2013	13:18:14	99.03
10/13/2013	13:19:14	99.26
10/13/2013	13:20:15	100.68
10/13/2013	13:21:15	100.36
10/13/2013	13:22:15	99.65
10/13/2013	13:23:15	98.28
10/13/2013	13:24:14	96.42
10/13/2013	13:25:14	96.23
10/13/2013	13:26:14	96.14
10/13/2013	13:27:14	94.87
10/13/2013	13:28:15	95.34
10/13/2013	13:29:15	94.94
10/13/2013	13:30:15	94.01
10/13/2013	13:31:14	92.64
10/13/2013	13:32:14	91.56
10/13/2013	13:33:14	89.78
10/13/2013	13:34:14	87.93
10/13/2013	13:35:15	86.12
10/13/2013	13:36:15	85.57
10/13/2013	13:37:15	85.8
10/13/2013	13:38:14	85.88
10/13/2013	13:39:14	85.76
10/13/2013	13:40:14	85.56
10/13/2013	13:41:14	85.49
10/13/2013	13:42:15	84.8
10/13/2013	13:43:15	84.44
10/13/2013	13:44:15	83.05
10/13/2013	13:45:15	81.96
10/13/2013	13:46:14	81
10/13/2013	13:47:14	81.22
Average	1833 samp	97.19
Test Run 11 End		

Enviva - Wiggins
Run 1

Date: 10-Oct
Run Time: 0917-1017
(CEM Run Time Eastern)

Parameter	Symbol	Green Hammermill
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

0900

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	1.1
Mid-Level Gas	ACE_{mid}	1.6
High-Level Gas	ACE_{high}	0.4
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0
Final Zero	$C_{s, zero (post)}$	0.11
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.8
Final Upscale	$C_{v, up (post)}$	50.65

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	0.0
Upscale (post)	$SB_{final} (upscale)$	-0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	30.8
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	30.8

Enviva - Wiggins
Run 2

Date: 10-Oct
Run Time: 1036-1136

Parameter	Symbol	Green Hammermill
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	1.1
Mid-Level Gas	ACE_{mid}	1.6
High-Level Gas	ACE_{high}	0.4
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.11
Final Zero	$C_{s, zero (post)}$	0.05
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.65
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.1
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_{i (upscale)}$	-0.1
Upscale (post)	$SB_{final (upscale)}$	-0.7
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	-0.5
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	32.23
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	32.2

Enviva - Wiggins
Run 3

Date: 10-Oct
Run Time: 1150-1250

Parameter	Symbol	Green Hammermill
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	1.1
Mid-Level Gas	ACE_{mid}	1.6
High-Level Gas	ACE_{high}	0.4
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.05
Final Zero	$C_{s, zero (post)}$	0.1
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.1
Final Upscale	$C_{v, up (post)}$	49.8

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.1
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.7
Upscale (post)	$SB_{final} (upscale)$	-1.0
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.3
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	26.38
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	26.4

Enviva - Wiggins
Run #7

Date: 11-Oct
Run Time: 1343-1443

Parameter	Symbol	Pellet Cooler 2
		THC
		(as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.15

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.04
Final Zero	$C_{s, zero (post)}$	0.35
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.14
Final Upscale	$C_{v, up (post)}$	50.2

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.3
Upscale (pre)	$SB_i (upscale)$	-1.0
Upscale (post)	$SB_{final} (upscale)$	-0.9
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.3
Upscale	$D_{upscale}$	0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{avg}	23.80
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	23.8

Enviva - Wiggins
Run #8

Date: 11-Oct
Run Time: 1508-1608

Parameter	Symbol	Pellet Cooler 2
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.35
Final Zero	$C_{s, zero (post)}$	0.18
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.2
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.3
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.9
Upscale (post)	$SB_{final} (upscale)$	-1.0
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.2
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	21.29
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	21.3

Enviva - Wiggins
Run #9

Date: 11-Oct
Run Time: 29-1729

Parameter	Symbol	Pellet Cooler 2
		THC
		(as C ₃ H ₈)
ppm _w		

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.18
Final Zero	$C_{s, zero (post)}$	0.2
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.1
Final Upscale	$C_{v, up (post)}$	49.8

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.1
Zero (post)	$SB_{final} (zero)$	0.2
Upscale (pre)	$SB_i (upscale)$	-1.0
Upscale (post)	$SB_{final} (upscale)$	-1.3
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.0
Upscale	$D_{upscale}$	-0.3
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	24.84
Bias Average - Zero	C_0	NA
Bias Average - Upscale	C_M	NA
Corrected Run Average	C_{Gas}	24.8

Enviva - Wiggins
Run #4

Date: 10-Oct
Run Time: 1738-1838

Parameter	Symbol	Dryer 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.3
Mid-Level Gas	$C_{Dir, mid}$	50.8
High-Level Gas	$C_{Dir, high}$	86.5

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	1.1
Mid-Level Gas	ACE_{mid}	1.6
High-Level Gas	ACE_{high}	0.4
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0
Final Zero	$C_{s, zero (post)}$	0.85
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.8
Final Upscale	$C_{v, up (post)}$	50.9

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.0
Zero (post)	$SB_{final (zero)}$	0.9
Upscale (pre)	$SB_{i (upscale)}$	0.0
Upscale (post)	$SB_{final (upscale)}$	0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.9
Upscale	$D_{upscale}$	0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{avg}	66.70
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	66.7

Enviva - Wiggins
Run #5

Date: 11-Oct
Run Time: 1000-1100

Parameter	Symbol	Dryer 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	28.0
Mid-Level Gas	$C_{v, mid}$	50.0
High-Level Gas	$C_{v, high}$	86.1
Calibration Span	CS	100.0

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.85
Final Zero	$C_{s, zero (post)}$	0.15
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.9
Final Upscale	$C_{v, up (post)}$	50.5

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.8
Zero (post)	$SB_{final (zero)}$	0.1
Upscale (pre)	$SB_{i (upscale)}$	-0.2
Upscale (post)	$SB_{final (upscale)}$	-0.6
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.7
Upscale	$D_{upscale}$	-0.4
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	61.92
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Ges}	61.9

Enviva - Wiggins
Run #6

Date: 11-Oct
Run Time: 1137-1237

Parameter	Symbol	Dryer 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response

Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)

Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response

Initial Zero	$C_{s, zero (pre)}$	0.15
Final Zero	$C_{s, zero (post)}$	0.1
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.5
Final Upscale	$C_{v, up (post)}$	50.14

System Bias - Results (Percent)

Zero (pre)	$SB_i (zero)$	0.1
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.6
Upscale (post)	$SB_{final} (upscale)$	-1.0
Specification	SB_{spec}	NA

System Drift - Results (Percent)

Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	-0.4
Specification	D_{spec}	±3

Response Test - Results (seconds)

Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction

Raw Average	C_{ave}	57.17
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	57.2

Enviva - Wiggins
Run 10

Date: 11-Oct
Run Time: 1811-1911

Parameter	Symbol	Hammermill 2
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dr, zero}$	0.0
Low-Level Gas	$C_{Dr, low}$	28.1
Mid-Level Gas	$C_{Dr, mid}$	51.1
High-Level Gas	$C_{Dr, high}$	86.15

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.2
Final Zero	$C_{s, zero (post)}$	0.08
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	49.8
Final Upscale	$C_{v, up (post)}$	50

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.2
Zero (post)	$SB_{final} (zero)$	0.0
Upscale (pre)	$SB_i (upscale)$	-1.3
Upscale (post)	$SB_{final} (upscale)$	-1.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	0.2
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	25.19
Bias Average - Zero	C_0	NA
Bias Average - Upscale	C_M	NA
Corrected Run Average	C_{Gas}	25.2

Enviva - Wiggins
Run 11

Date: 11-Oct
Run Time: 1935-2035

Parameter	Symbol	Hammermill 2
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.08
Final Zero	$C_{s, zero (post)}$	0.21
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50
Final Upscale	$C_{v, up (post)}$	49.85

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.2
Upscale (pre)	$SB_i (upscale)$	-1.1
Upscale (post)	$SB_{final} (upscale)$	-1.3
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	29.72
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	29.7

Enviva - Wiggins
Run 12

Date: 10/11/2013
Run Time: 2048-2148

Parameter	Symbol	Hammermill 2
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.0
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	51.1
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.0
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	2.2
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.21
Final Zero	$C_{s, zero (post)}$	0.23
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	49.85
Final Upscale	$C_{v, up (post)}$	49.9

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.2
Zero (post)	$SB_{final} (zero)$	0.2
Upscale (pre)	$SB_i (upscale)$	-1.3
Upscale (post)	$SB_{final} (upscale)$	-1.2
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.0
Upscale	$D_{upscale}$	0.0
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	24.43
Bias Average - Zero	C_o	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	24.4

Enviva - Wiggins
Run 13

Date: 12-Oct
Run Time: 0858-0958

Parameter	Symbol	Pellet Cooler 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	27.99
Mid-Level Gas	$C_{v, mid}$	50
High-Level Gas	$C_{v, high}$	86.13
Calibration Span	CS	100

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.1
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, mid}$	50.4
High-Level Gas	$C_{Dir, high}$	86.15

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	0.8
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.1
Final Zero	$C_{s, zero (post)}$	0.35
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.4
Final Upscale	$C_{v, up (post)}$	50.3

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.0
Zero (post)	$SB_{final (zero)}$	0.3
Upscale (pre)	$SB_{i (upscale)}$	0.0
Upscale (post)	$SB_{final (upscale)}$	-0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.3
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{avg}	39.05
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	39.1

Enviva - Wiggins
Run 14

Date: 12-Oct
Run Time: 1022-1122

Parameter	Symbol	Pellet Cooler 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dr, zero}$	0.1
Low-Level Gas	$C_{Dr, low}$	28.1
Mid-Level Gas	$C_{Dr, mid}$	50.4
High-Level Gas	$C_{Dr, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{mid}	0.8
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.35
Final Zero	$C_{s, zero (post)}$	0.24
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.3
Final Upscale	$C_{v, up (post)}$	50.25

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.3
Zero (post)	$SB_{final} (zero)$	
Upscale (pre)	$SB_i (upscale)$	-0.1
Upscale (post)	$SB_{final} (upscale)$	
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	0.0
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	33.29
Bias Average - Zero	C_0	NA
Bias Average - Upscale	C_M	NA
Corrected Run Average	C_{Gas}	33.3

Enviva - Wiggins
Run 15

Date: 12-Oct
Run Time: 1141-124

Parameter	Symbol	Pellet Cooler 1
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	0.1
Low-Level Gas	$C_{Dir, low}$	28.1
Mid-Level Gas	$C_{Dir, md}$	50.4
High-Level Gas	$C_{Dir, high}$	86.2

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.4
Mid-Level Gas	ACE_{md}	0.8
High-Level Gas	ACE_{high}	0.0
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	0.24
Final Zero	$C_{s, zero (post)}$	0.33
Upscale Gas Standard	C_{MA}	50.0
Initial Upscale	$C_{v, up (pre)}$	50.25
Final Upscale	$C_{v, up (post)}$	50.1

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.2
Zero (post)	$SB_{final (zero)}$	0.3
Upscale (pre)	$SB_{i (upscale)}$	-0.1
Upscale (post)	$SB_{final (upscale)}$	-0.3
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	35.65
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	35.7

Enviva - Wiggins
Run 16

Date: 12-Oct
Run Time: 1509-1605

Parameter	Symbol	Aspirator
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	258.1
Mid-Level Gas	$C_{v, mid}$	507.1
High-Level Gas	$C_{v, high}$	836.9
Calibration Span	CS	1000

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	1.1
Low-Level Gas	$C_{Dir, low}$	260
Mid-Level Gas	$C_{Dir, mid}$	507
High-Level Gas	$C_{Dir, high}$	838.3

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.7
Mid-Level Gas	ACE_{mid}	0.0
High-Level Gas	ACE_{high}	0.1
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	1.1
Final Zero	$C_{s, zero (post)}$	2.4
Upscale Gas Standard	C_{MA}	836.9
Initial Upscale	$C_{v, up (pre)}$	838.3
Final Upscale	$C_{v, up (post)}$	837

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	0.0
Upscale (post)	$SB_{final} (upscale)$	-0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	1074.70
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	1074.7

Enviva - Wiggins
Run 17

Date: 12-Oct
Run Time: 1636-1736

Parameter	Symbol	Aspirator
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Calibration Standards		
Zero Gas	$C_{v, zero}$	0.0
Low-Level Gas	$C_{v, low}$	258.1
Mid-Level Gas	$C_{v, mid}$	507.1
High-Level Gas	$C_{v, high}$	836.9
Calibration Span	CS	1000.0

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	1.1
Low-Level Gas	$C_{Dir, low}$	260.0
Mid-Level Gas	$C_{Dir, mid}$	507.0
High-Level Gas	$C_{Dir, high}$	838.3

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.7
Mid-Level Gas	ACE_{mid}	0.0
High-Level Gas	ACE_{high}	0.1
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	2.40
Final Zero	$C_{s, zero (post)}$	1.4
Upscale Gas Standard	C_{MA}	836.9
Initial Upscale	$C_{v, up (pre)}$	837
Final Upscale	$C_{v, up (post)}$	837.5

System Bias - Results (Percent)		
Zero (pre)	$SB_{i (zero)}$	0.1
Zero (post)	$SB_{final (zero)}$	0.0
Upscale (pre)	$SB_{i (upscale)}$	-0.1
Upscale (post)	$SB_{final (upscale)}$	-0.1
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	-0.1
Upscale	$D_{upscale}$	0.1
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	957.00
Bias Average - Zero	C_0	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	957.0

Enviva - Wiggins
Run 18

Date: 12-Oct
Run Time: 1800-1900

Parameter	Symbol	Aspirator
		THC (as C ₃ H ₈)
		ppm _w

Analyzer Calibration Error - Instrument Response		
Zero Gas	$C_{Dir, zero}$	1.1
Low-Level Gas	$C_{Dir, low}$	260.0
Mid-Level Gas	$C_{Dir, mid}$	507.0
High-Level Gas	$C_{Dir, high}$	838.3

Analyzer Calibration Error - Results (Percent of Span)		
Zero Gas	ACE_{zero}	0.1
Low-Level Gas	ACE_{low}	0.7
Mid-Level Gas	ACE_{mid}	0.0
High-Level Gas	ACE_{high}	0.1
Specification	ACE_{spec}	±5

System Calibrations - Instrument Response		
Initial Zero	$C_{s, zero (pre)}$	1.40
Final Zero	$C_{s, zero (post)}$	2
Upscale Gas Standard	C_{MA}	836.9
Initial Upscale	$C_{v, up (pre)}$	837.5
Final Upscale	$C_{v, up (post)}$	835

System Bias - Results (Percent)		
Zero (pre)	$SB_i (zero)$	0.0
Zero (post)	$SB_{final} (zero)$	0.1
Upscale (pre)	$SB_i (upscale)$	-0.1
Upscale (post)	$SB_{final} (upscale)$	-0.3
Specification	SB_{spec}	NA

System Drift - Results (Percent)		
Zero	D_{zero}	0.1
Upscale	$D_{upscale}$	-0.3
Specification	D_{spec}	±3

Response Test - Results (seconds)		
Upscale Test		NA
Zero Test		NA
Response Time		28

Calibration Correction		
Raw Average	C_{ave}	1200.00
Bias Average - Zero	C_o	N/A
Bias Average - Upscale	C_M	N/A
Corrected Run Average	C_{Gas}	1200.0

Enviva - Wiggins
Run 19

Date: 13-Oct
Run Time: 0921-1021

Parameter	Symbol	Dryer 2	
		THC (as C ₃ H ₈)	
		ppm _w	

Analyzer Calibration Error - Calibration Standards			
Zero Gas	$C_{v, zero}$	0.0	0.0
Low-Level Gas	$C_{v, low}$	258.1	27.99
Mid-Level Gas	$C_{v, mid}$	507.1	50
High-Level Gas	$C_{v, high}$	836.9	86.13
Calibration Span	CS	1000	100

Analyzer Calibration Error - Instrument Response			
Zero Gas	$C_{Dir, zero}$	1.0	1.0
Low-Level Gas	$C_{Dir, low}$	259	28.4
Mid-Level Gas	$C_{Dir, mid}$	506.8	50.34
High-Level Gas	$C_{Dir, high}$	837.3	86.24

Analyzer Calibration Error - Results (Percent of Span)			
Zero Gas	ACE_{zero}	0.1	1.0
Low-Level Gas	ACE_{low}	0.3	1.5
Mid-Level Gas	ACE_{mid}	-0.1	0.7
High-Level Gas	ACE_{high}	0.0	0.1
Specification	ACE_{spec}	±5	±8

System Calibrations - Instrument Response			
Initial Zero	$C_{s, zero (pre)}$	1.0	1.0
Final Zero	$C_{s, zero (post)}$	1.6	1.6
Upscale Gas Standard	C_{MA}	507.1	50.0
Initial Upscale	$C_{v, up (pre)}$	506.8	50.34
Final Upscale	$C_{v, up (post)}$	504	50.6

System Bias - Results (Percent)			
Zero (pre)	$SB_i (zero)$	0.0	0.0
Zero (post)	$SB_{final} (zero)$	0.1	0.6
Upscale (pre)	$SB_i (upscale)$	0.0	0.0
Upscale (post)	$SB_{final} (upscale)$	-0.3	0.3
Specification	SB_{spec}	NA	NA

System Drift - Results (Percent)			
Zero	D_{zero}	0.1	0.6
Upscale	$D_{upscale}$	-0.3	0.3
Specification	D_{spec}	±3	±6

Response Test - Results (seconds)			
Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	28

Calibration Correction			
Raw Average	C_{ave}	91.8	91.8
Bias Average - Zero	C_o	NA	NA
Bias Average - Upscale	C_M	NA	NA
Corrected Run Average	C_{Gas}	91.8	91.8

Enviva - Wiggins
Run 20

Date: 13-Oct
Run Time: 1104-1204

Parameter	Symbol	Dryer 2	
		THC (as C ₃ H ₈) ppm _w	

Analyzer Calibration Error - Calibration Standards			
Zero Gas	$C_{v, zero}$	0.0	0.0
Low-Level Gas	$C_{v, low}$	258.1	28.0
Mid-Level Gas	$C_{v, mid}$	507.1	50.0
High-Level Gas	$C_{v, high}$	836.9	86.1
Calibration Span	CS	1000.0	100.0

Analyzer Calibration Error - Instrument Response			
Zero Gas	$C_{Dir, zero}$	1.0	1.0
Low-Level Gas	$C_{Dir, low}$	259.0	28.4
Mid-Level Gas	$C_{Dir, mid}$	506.8	50.3
High-Level Gas	$C_{Dir, high}$	837.3	86.2

Analyzer Calibration Error - Results (Percent of Span)			
Zero Gas	ACE_{zero}	0.1	1.0
Low-Level Gas	ACE_{low}	0.3	1.5
Mid-Level Gas	ACE_{mid}	-0.1	0.7
High-Level Gas	ACE_{high}	0.0	0.1
Specification	ACE_{spec}	±5	±8

System Calibrations - Instrument Response			
Initial Zero	$C_{s, zero (pre)}$	1.60	1.60
Final Zero	$C_{s, zero (post)}$	0.42	0.42
Upscale Gas Standard	C_{MA}	507.1	50.0
Initial Upscale	$C_{v, up (pre)}$	504	50.6
Final Upscale	$C_{v, up (post)}$	503	50.4

System Bias - Results (Percent)			
Zero (pre)	$SB_i (zero)$	0.1	0.6
Zero (post)	$SB_{final} (zero)$	-0.1	-0.6
Upscale (pre)	$SB_i (upscale)$	-0.3	0.3
Upscale (post)	$SB_{final} (upscale)$	-0.4	0.1
Specification	SB_{spec}	NA	NA

System Drift - Results (Percent)			
Zero	D_{zero}	-0.1	-1.2
Upscale	$D_{upscale}$	-0.1	-0.2
Specification	D_{spec}	±3	±3

Response Test - Results (seconds)			
Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	28

Calibration Correction			
Raw Average	C_{ave}	81.2	81.2
Bias Average - Zero	C_0	NA	NA
Bias Average - Upscale	C_M	NA	NA
Corrected Run Average	C_{Gas}	81.2	81.2

Enviva - Wiggins
Run 21

Date: 13-Oct
Run Time: 1231-1347
Paused (1236-1252)

Parameter	Symbol	Dryer 2	
		THC (as C ₂ H ₆) ppm _w	

Analyzer Calibration Error - Instrument Response			
Zero Gas	$C_{Dir, zero}$	1.0	1.00
Low-Level Gas	$C_{Dir, low}$	259.0	28.40
Mid-Level Gas	$C_{Dir, mid}$	506.8	50.34
High-Level Gas	$C_{Dir, high}$	837.3	86.24

Analyzer Calibration Error - Results (Percent of Span)			
Zero Gas	ACE_{zero}	0.1	1.0
Low-Level Gas	ACE_{low}	0.3	1.5
Mid-Level Gas	ACE_{mid}	-0.1	0.7
High-Level Gas	ACE_{high}	0.0	0.1
Specification	ACE_{spec}	±5	±8

System Calibrations - Instrument Response			
Initial Zero	$C_{s, zero (pre)}$	0.42	0.42
Final Zero	$C_{s, zero (post)}$	0.3	0.3
Upscale Gas Standard	C_{MA}	507.1	50.0
Initial Upscale	$C_{v, up (pre)}$	503	50.4
Final Upscale	$C_{v, up (post)}$	503.5	50.2

System Bias - Results (Percent)			
Zero (pre)	$SB_{i (zero)}$	-0.1	-0.6
Zero (post)	$SB_{final (zero)}$	-0.1	-0.7
Upscale (pre)	$SB_{i (upscale)}$	-0.4	0.1
Upscale (post)	$SB_{final (upscale)}$	-0.3	-0.1
Specification	SB_{spec}	NA	NA

System Drift - Results (Percent)			
Zero	D_{zero}	0.0	-0.1
Upscale	$D_{upscale}$	0.1	-0.2
Specification	D_{spec}	±3	±6

Response Test - Results (seconds)			
Upscale Test		NA	NA
Zero Test		NA	NA
Response Time		28	31

Calibration Correction			
Raw Average	C_{ave}	97.2	97.2
Bias Average - Zero	C_0	NA	NA
Bias Average - Upscale	C_M	NA	NA
Corrected Run Average	C_{Gas}	97.2	97.2

APPENDIX C

Method 320 Data

Company ACT
 Analyst Initials CJT
 Parameters EPA Method 320
 # Samples 21 Runs

Client # 1911
 Job # 0913-111
 PO # 3134 1911
 Report Date V0.62 13.10.18.12.58

Compound	Sample ID / Concentration (ppmv wet)												
	GMH Run 1			GMH Run 2			GMH Run 3			Data Runs			
Acrolein	1.13 J	1.20 J	1.15 J	1.79 J	1.72 ND	1.72 ND	1.72 ND	1.72 ND	1.72 ND	1.72 ND	1.72 ND	1.72 ND	1.72 ND
Formaldehyde	0.742	0.629	0.561	3.32	1.60	1.60	1.60	1.60	1.60	1.60	1.60	1.60	1.78
Methanol	0.508	0.460	0.376	2.52	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.59
Phenol	0.88 ND	0.88 ND	0.88 ND	2.04 ND	2.04 ND	2.04 ND	2.04 ND	2.04 ND	2.04 ND	2.04 ND	2.04 ND	2.04 ND	2.04 ND
Propionaldehyde	0.234 ND	0.234 ND	0.251 J	0.644 J	0.714 J	0.714 J	0.714 J	0.714 J	0.714 J	0.714 J	0.714 J	0.714 J	0.505 J
acetaldehyde	0.756 J	0.721 J	0.723 J	1.27 ND	1.27 ND	1.27 ND	1.27 ND	1.27 ND	1.27 ND	1.27 ND	1.27 ND	1.27 ND	1.27 ND
	Pellet Cooler 2 Run 1			Pellet Cooler 2 Run 2			Pellet Cooler 2 Run 3			Data Runs			
Acrolein	1.29 J	1.21 J	1.33 J	0.980 J	0.975 J	0.975 J	0.975 J	0.975 J	0.975 J	0.975 J	0.975 J	0.975 J	0.965 ND
Formaldehyde	1.07	0.663	1.84	1.04	1.14	1.14	1.14	1.14	1.14	1.14	1.14	1.14	1.11
Methanol	0.797	0.680 J	0.844	0.189 J	0.211 J	0.211 J	0.211 J	0.211 J	0.211 J	0.211 J	0.211 J	0.211 J	0.204 J
Phenol	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND	1.08 ND
Propionaldehyde	0.246 J	0.246 ND	0.359 J	0.233 J	0.243 J	0.243 J	0.243 J	0.243 J	0.243 J	0.243 J	0.243 J	0.243 J	0.263 J
acetaldehyde	0.864 J	0.825 J	0.786 J	0.715 J	0.710 J	0.710 J	0.710 J	0.710 J	0.710 J	0.710 J	0.710 J	0.710 J	0.707 ND
	Pellet Cooler 1 Run 1			Pellet Cooler 1 Run 2			Pellet Cooler 1 Run 3			Data Runs			
Acrolein	0.976 J	1.02 J	1.35 J	3.16	3.12	3.12	3.12	3.12	3.12	3.12	3.12	3.12	2.25 J
Formaldehyde	1.44	1.25	1.26	1.05 ND	1.58 J	1.58 J	1.58 J	1.58 J	1.58 J	1.58 J	1.58 J	1.58 J	1.06 J
Methanol	0.537	0.327	0.351	8.30	8.90	8.90	8.90	8.90	8.90	8.90	8.90	8.90	8.16
Phenol	1.00 J	0.98 ND	0.98 ND	2.73 ND	2.73 ND	2.73 ND	2.73 ND	2.73 ND	2.73 ND	2.73 ND	2.73 ND	2.73 ND	2.73 ND
Propionaldehyde	0.381 J	0.290 J	0.236 ND	3.00 ND	3.00 ND	3.00 ND	3.00 ND	3.00 ND	3.00 ND	3.00 ND	3.00 ND	3.00 ND	3.00 ND
acetaldehyde	0.691 J	0.695 J	0.769 J	4.65	3.92 J	3.92 J	3.92 J	3.92 J	3.92 J	3.92 J	3.92 J	3.92 J	3.75
	Dryer 2 Run 1			Dryer 2 Run 2			Dryer 2 Run 3			Data Runs			
Acrolein	1.90 J	2.59	2.49	2.49	2.49	2.49	2.49	2.49	2.49	2.49	2.49	2.49	2.49
Formaldehyde	6.40	6.58	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76	6.76
Methanol	18.8	10.2	10.8	10.8	10.8	10.8	10.8	10.8	10.8	10.8	10.8	10.8	10.8
Phenol	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND	2.78 ND
Propionaldehyde	2.37	1.38	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
acetaldehyde	0.967 J	3.28	1.02 J	1.02 J	1.02 J	1.02 J	1.02 J	1.02 J	1.02 J	1.02 J	1.02 J	1.02 J	1.02 J

Company ACT
 Analytical Methods EPA Method 320
 # Samples 21 Runs

Client # 1011
 Job # 0913-111
 PO # 3134-1911
 Report Date 06.02.13.10.18.12.58

Minimum Detectable Concentration - Default

GMH	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
Run 1	1.13	0.502	0.142	0.0718	0.51	0.02	0.88	0.44	0.24	0.120	0.75	0.371
Run 2	1.20	0.474	0.629	0.0894	0.68	0.653	0.88	0.44	0.24	0.118	0.721	0.351
Run 3	1.15	0.460	0.361	0.0677	0.38	0.0813	0.88	0.45	0.251	0.113	0.723	0.355
Average SEC(ppm):	0.465		0.0693		0.0920		0.44		0.117		0.359	
MDC(ppm):	0.971		0.139		0.184		0.88		0.234		0.718	
Dryer 1												
Run 1	1.75	0.917	3.32	0.131	2.52	0.298	2.04	1.00	0.844	0.239	1.270	0.679
Run 2	1.72	0.850	1.60	0.126	1.70	0.293	2.04	1.07	0.714	0.227	1.270	0.628
Run 3	1.72	0.812	1.78	0.120	1.59	0.287	2.04	0.99	0.595	0.213	1.270	0.598
Average SEC(ppm):	0.859		0.126		0.292		2.04		0.226		0.635	
MDC(ppm):	1.72		0.252		0.594		2.04		0.452		1.27	
Pellet Cooler 2												
Run 1	1.29	0.486	1.07	0.0711	0.60	0.0813	1.08	0.54	0.246	0.125	0.854	0.370
Run 2	1.21	0.487	0.653	0.0704	0.58	0.0823	1.08	0.54	0.246	0.120	0.825	0.376
Run 3	1.33	0.507	1.84	0.0732	0.84	0.0844	1.09	0.55	0.359	0.124	0.786	0.378
Average SEC(ppm):	0.500		0.0716		0.626		0.54		0.123		0.373	
MDC(ppm):	1.00		0.143		0.185		1.08		0.248		0.745	
Hammermill 2												
Run 1	0.88	0.460	1.04	0.0577	0.19	0.0808	1.08	0.54	0.233	0.113	0.715	0.353
Run 2	0.97	0.480	1.14	0.0682	0.21	0.0832	1.08	0.54	0.243	0.122	0.710	0.352
Run 3	0.97	0.488	1.11	0.0675	0.20	0.0839	1.08	0.55	0.263	0.113	0.707	0.356
Average SEC(ppm):	0.483		0.0578		0.0926		0.54		0.116		0.354	
MDC(ppm):	0.965		0.136		0.165		1.08		0.232		0.707	
Pellet Cooler 1												
Run 1	0.88	0.467	1.44	0.0646	0.54	0.0738	1.00	0.50	0.381	0.118	0.681	0.344
Run 2	1.02	0.463	1.25	0.0635	0.33	0.0723	0.88	0.50	0.260	0.119	0.685	0.341
Run 3	1.35	0.467	1.26	0.0647	0.35	0.0690	0.88	0.48	0.235	0.118	0.759	0.345
Average SEC(ppm):	0.466		0.0642		0.0717		0.48		0.118		0.343	
MDC(ppm):	0.931		0.128		0.143		0.88		0.236		0.686	
Aspirator												
Run 1	3.16	0.827	1.055	0.535	8.30	0.244	2.73	1.15	3.00	1.53	4.65	0.616
Run 2	3.12	0.858	1.56	0.467	8.90	0.256	2.73	1.60	3.00	1.35	3.92	0.602
Run 3	2.25	0.916	1.063	0.580	8.16	0.265	2.73	1.34	3.00	1.62	3.75	0.681
Average SEC(ppm):	0.850		0.527		0.255		1.38		1.50		0.633	
MDC(ppm):	1.70		1.05		0.510		2.73		3.00		1.27	
Dryer 2												
Run 1	1.90	0.631	6.40	0.108	16.8	0.539	2.78	1.29	2.37	0.222	0.967	0.472
Run 2	2.59	0.617	6.58	0.105	10.2	0.549	2.78	1.55	1.38	0.260	3.28	0.457
Run 3	2.49	0.633	6.75	0.112	10.8	0.631	2.78	1.33	1.70	0.283	1.02	0.473
Average SEC(ppm):	0.627		0.108		0.540		1.38		0.246		0.467	
MDC(ppm):	1.25		0.217		1.08		2.78		0.487		0.584	

Company ACT
 Analyst Initials
 Parameters, EPA Method 320
 # Samples 21 Runs

Client # 1011
 Job # 0913-111
 P-03 1/14 1911
 Report Date 10.6.13.10.16.12.58

GMH Run 1	Date	Method	Fluoranthene	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/10/2013 9:17	0913-111_A	13_10_10_0917_37_936	1.58	0.517	0.848	0.0700	0.424	0.0900	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 9:18	0913-111_A	13_10_10_0918_38_788	1.071	0.472	0.708	0.0680	0.457	0.0890	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 9:19	0913-111_A	13_10_10_0919_39_506	0.971	0.504	0.778	0.0720	0.443	0.0920	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 9:20	0913-111_A	13_10_10_0920_40_236	1.071	0.484	0.699	0.0680	0.487	0.0960	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:21	0913-111_A	13_10_10_0921_41_006	1.58	0.483	0.633	0.0700	0.454	0.0920	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 9:22	0913-111_A	13_10_10_0922_41_606	0.971	0.493	0.708	0.0680	0.457	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:23	0913-111_A	13_10_10_0923_42_538	0.971	0.464	0.814	0.0680	0.499	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:24	0913-111_A	13_10_10_0924_43_348	1.15	0.462	0.696	0.0630	0.481	0.0900	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:25	0913-111_A	13_10_10_0925_44_128	0.971	0.465	0.806	0.0680	0.477	0.0900	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 9:26	0913-111_A	13_10_10_0926_44_818	0.971	0.498	0.732	0.0680	0.407	0.0870	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:27	0913-111_A	13_10_10_0927_45_818	0.971	0.459	0.759	0.0680	0.481	0.0870	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:28	0913-111_A	13_10_10_0928_46_429	1.16	0.459	0.830	0.0680	0.481	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:29	0913-111_A	13_10_10_0929_47_159	1.61	0.471	0.784	0.0680	0.445	0.0870	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:30	0913-111_A	13_10_10_0930_47_989	0.971	0.454	0.903	0.0680	0.537	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:31	0913-111_A	13_10_10_0931_48_709	0.971	0.477	0.775	0.0700	0.442	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:32	0913-111_A	13_10_10_0932_49_219	0.971	0.480	0.746	0.0680	0.477	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:33	0913-111_A	13_10_10_0933_50_289	0.971	0.491	0.723	0.0730	0.473	0.0980	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:34	0913-111_A	13_10_10_0934_50_859	0.971	0.491	0.731	0.0680	0.458	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:35	0913-111_A	13_10_10_0935_51_689	0.971	0.489	0.739	0.0680	0.477	0.0870	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:36	0913-111_A	13_10_10_0936_52_439	0.971	0.483	0.803	0.0680	0.533	0.0890	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:37	0913-111_A	13_10_10_0937_53_149	1.32	0.497	0.751	0.0700	0.443	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:38	0913-111_A	13_10_10_0938_53_929	0.971	0.467	0.868	0.0680	0.487	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:39	0913-111_A	13_10_10_0939_54_729	0.971	0.482	0.800	0.0680	0.477	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:40	0913-111_A	13_10_10_0940_55_459	0.971	0.487	0.745	0.0700	0.416	0.0930	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:41	0913-111_A	13_10_10_0941_56_239	0.971	0.504	0.745	0.0710	0.435	0.0870	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:42	0913-111_A	13_10_10_0942_57_019	1.10	0.501	0.813	0.0700	0.470	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:43	0913-111_A	13_10_10_0943_57_749	0.971	0.489	0.773	0.0680	0.415	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:44	0913-111_A	13_10_10_0944_58_449	0.971	0.477	0.736	0.0700	0.407	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:45	0913-111_A	13_10_10_0945_59_209	0.971	0.482	0.534	0.0670	0.388	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:46	0913-111_A	13_10_10_0946_60_009	1.48	0.477	0.944	0.0690	0.459	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:47	0913-111_A	13_10_10_0947_60_729	0.971	0.477	0.859	0.0680	0.459	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:48	0913-111_A	13_10_10_0948_61_489	1.29	0.487	0.773	0.0680	0.501	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:49	0913-111_A	13_10_10_0949_62_249	0.971	0.483	0.721	0.0680	0.484	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:50	0913-111_A	13_10_10_0950_63_009	0.971	0.478	0.710	0.0700	0.437	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:51	0913-111_A	13_10_10_0951_63_769	0.971	0.489	0.863	0.0680	0.523	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:52	0913-111_A	13_10_10_0952_64_529	0.971	0.500	0.789	0.0680	0.523	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:53	0913-111_A	13_10_10_0953_65_289	0.971	0.455	0.737	0.0670	0.667	0.0900	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:54	0913-111_A	13_10_10_0954_66_049	1.41	0.489	0.889	0.0670	0.647	0.0860	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:55	0913-111_A	13_10_10_0955_66_809	0.971	0.513	0.980	0.0680	0.645	0.0870	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:56	0913-111_A	13_10_10_0956_67_569	0.971	0.482	0.870	0.0720	0.667	0.0880	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:57	0913-111_A	13_10_10_0957_68_329	0.971	0.488	0.920	0.0700	0.888	0.0950	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:58	0913-111_A	13_10_10_0958_69_089	1.42	0.497	0.986	0.0720	0.849	0.0950	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 9:59	0913-111_A	13_10_10_0959_70_079	0.971	0.492	0.821	0.0700	0.594	0.0900	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:00	0913-111_A	13_10_10_1000_09_811	1.62	0.494	0.597	0.0720	0.597	0.0630	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:01	0913-111_A	13_10_10_1001_10_511	0.971	0.487	0.850	0.0680	0.580	0.0820	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:02	0913-111_A	13_10_10_1002_11_291	0.971	0.487	0.843	0.0670	0.577	0.0830	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:03	0913-111_A	13_10_10_1003_12_091	1.07	0.496	0.745	0.0680	0.654	0.0920	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:04	0913-111_A	13_10_10_1004_12_832	0.978	0.474	0.794	0.0680	0.654	0.0920	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:05	0913-111_A	13_10_10_1005_13_542	1.21	0.489	0.819	0.0760	0.583	0.0890	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:06	0913-111_A	13_10_10_1006_14_322	0.971	0.478	0.718	0.0710	0.544	0.0830	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:07	0913-111_A	13_10_10_1007_15_182	1.07	0.487	0.789	0.0670	0.627	0.0810	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:08	0913-111_A	13_10_10_1008_15_892	1.28	0.512	0.804	0.0750	0.660	0.0950	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:09	0913-111_A	13_10_10_1009_16_712	1.61	0.591	0.828	0.0820	0.582	0.0910	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:10	0913-111_A	13_10_10_1010_17_422	0.986	0.559	0.706	0.0770	0.620	0.0940	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:11	0913-111_A	13_10_10_1011_18_172	1.39	0.517	0.867	0.0780	0.631	0.0940	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:12	0913-111_A	13_10_10_1012_18_922	0.971	0.535	0.703	0.0770	0.435	0.0950	0.88	0.44	0.234	0.114	0.718	0.353		
10/10/2013 10:13	0913-111_A	13_10_10_1013_19_722	1.46	0.582	0.825	0.0840	0.497	0.0970	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 10:14	0913-111_A	13_10_10_1014_20_522	0.971	0.582	0.594	0.0820	0.537	0.0950	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 10:15	0913-111_A	13_10_10_1015_21_272	1.71	0.581	0.563	0.0800	0.520	0.0910	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 10:16	0913-111_A	13_10_10_1016_22_022	0.971	0.705	0.431	0.0960	0.400	0.102	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 10:17	0913-111_A	13_10_10_1017_22_632	1.15	0.698	0.729	0.100	0.361	0.100	0.88	0.43	0.234	0.114	0.718	0.353		
Average Conc. (ppm): 1 1.18 0.622 0.742 0.0719 0.608 0.0912 0.88 0.44 0.234 0.120 0.758 0.371																

GMH Run 2	Date	Method	Fluoranthene	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/10/2013 10:26	0913-111_A	13_10_10_1026_37_174	1.30	0.438	0.768	0.0680	0.421	0.0890	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 10:27	0913-111_A	13_10_10_1027_37_934	1.05	0.483	0.596	0.0660	0.415	0.0900	0.88	0.43	0.234	0.114	0.718	0.353		
10/10/2013 10:28	0913-111_A	13_10_10_1028_38_924	1.88													

Company: JCT
 Analyst: Inialis C.T.
 Parameters: EPA Method 320
 # Samples: 21 Runs

Client # 1911
 Job # 0913-11
 PO # 3134 1911
 Report Date: V0.02 13.10.18.12.58

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionalsdehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/10/2013 11:50	0913-111_A	13_10_10_1150_33_060	1	0.971	0.485	0.541	0.0650	0.432	0.0370	0.88	0.44	0.234	0.109	0.718	0.348
10/10/2013 11:51	0913-111_A	13_10_10_1150_33_061	1	0.887	0.510	0.328	0.0700	0.457	0.0930	0.88	0.44	0.234	0.113	0.904	0.373
10/10/2013 11:52	0913-111_A	13_10_10_1152_34_081	1	0.871	0.513	0.488	0.0710	0.486	0.0940	0.88	0.44	0.234	0.116	0.718	0.374
10/10/2013 11:53	0913-111_A	13_10_10_1153_35_331	1	0.971	0.499	0.478	0.0690	0.418	0.0970	0.88	0.45	0.234	0.112	0.718	0.348
10/10/2013 11:54	0913-111_A	13_10_10_1154_36_151	1	1.30	0.457	0.511	0.0670	0.387	0.0950	0.88	0.45	0.234	0.112	0.718	0.348
10/10/2013 11:55	0913-111_A	13_10_10_1155_38_951	1	1.20	0.499	0.554	0.0710	0.438	0.0940	0.88	0.45	0.234	0.117	0.718	0.355
10/10/2013 11:56	0913-111_A	13_10_10_1156_37_891	1	0.971	0.481	0.425	0.0680	0.378	0.0910	0.88	0.45	0.234	0.112	0.718	0.355
10/10/2013 11:57	0913-111_A	13_10_10_1157_38_401	1	1.41	0.488	0.527	0.0690	0.458	0.0940	0.88	0.45	0.234	0.114	0.718	0.348
10/10/2013 11:58	0913-111_A	13_10_10_1158_39_211	1	1.13	0.498	0.472	0.0710	0.432	0.0940	0.88	0.45	0.234	0.113	0.718	0.351
10/10/2013 11:59	0913-111_A	13_10_10_1159_40_021	1	1.58	0.479	0.524	0.0680	0.324	0.0900	0.88	0.44	0.234	0.113	0.718	0.357
10/10/2013 12:00	0913-111_A	13_10_10_1200_40_731	1	0.971	0.485	0.472	0.0670	0.389	0.0950	0.88	0.45	0.234	0.112	0.718	0.359
10/10/2013 12:01	0913-111_A	13_10_10_1201_41_361	1	1.28	0.472	0.538	0.0700	0.357	0.0910	0.88	0.44	0.234	0.113	0.718	0.355
10/10/2013 12:02	0913-111_A	13_10_10_1202_42_302	1	0.971	0.473	0.512	0.0670	0.404	0.0910	0.88	0.44	0.234	0.114	0.718	0.349
10/10/2013 12:03	0913-111_A	13_10_10_1203_43_022	1	0.971	0.449	0.509	0.0630	0.398	0.0900	0.88	0.44	0.234	0.105	0.718	0.328
10/10/2013 12:04	0913-111_A	13_10_10_1204_43_872	1	1.01	0.489	0.509	0.0700	0.381	0.0930	0.88	0.45	0.234	0.116	0.718	0.359
10/10/2013 12:05	0913-111_A	13_10_10_1205_44_582	1	0.971	0.505	0.320	0.0700	0.401	0.0910	0.88	0.45	0.234	0.114	0.718	0.373
10/10/2013 12:06	0913-111_A	13_10_10_1206_45_332	1	1.86	0.478	0.582	0.0680	0.354	0.0930	0.88	0.44	0.234	0.112	0.718	0.376
10/10/2013 12:07	0913-111_A	13_10_10_1207_46_182	1	0.971	0.478	0.488	0.0640	0.379	0.0910	0.88	0.45	0.234	0.112	0.718	0.358
10/10/2013 12:08	0913-111_A	13_10_10_1208_46_912	1	1.00	0.500	0.522	0.0670	0.438	0.0910	0.88	0.45	0.234	0.112	0.718	0.368
10/10/2013 12:09	0913-111_A	13_10_10_1209_47_582	1	1.35	0.458	0.588	0.0670	0.406	0.0910	0.88	0.45	0.234	0.114	0.718	0.372
10/10/2013 12:10	0913-111_A	13_10_10_1210_48_492	1	0.971	0.533	0.475	0.0710	0.361	0.0910	0.88	0.47	0.234	0.117	0.718	0.391
10/10/2013 12:11	0913-111_A	13_10_10_1211_49_202	1	0.971	0.444	0.556	0.0680	0.338	0.0930	0.88	0.44	0.234	0.109	0.718	0.338
10/10/2013 12:12	0913-111_A	13_10_10_1212_50_012	1	0.971	0.500	0.555	0.0700	0.363	0.0910	0.88	0.45	0.234	0.116	0.718	0.376
10/10/2013 12:13	0913-111_A	13_10_10_1213_50_712	1	0.971	0.468	0.524	0.0660	0.410	0.0940	0.88	0.44	0.234	0.108	0.718	0.347
10/10/2013 12:14	0913-111_A	13_10_10_1214_51_513	1	1.38	0.450	0.604	0.0660	0.355	0.0920	0.88	0.45	0.234	0.108	0.718	0.334
10/10/2013 12:15	0913-111_A	13_10_10_1215_52_323	1	0.971	0.498	0.543	0.0720	0.420	0.0890	0.88	0.44	0.234	0.118	0.718	0.364
10/10/2013 12:16	0913-111_A	13_10_10_1216_53_003	1	1.00	0.485	0.565	0.0690	0.322	0.0900	0.88	0.44	0.234	0.114	0.718	0.341
10/10/2013 12:17	0913-111_A	13_10_10_1217_53_813	1	0.971	0.462	0.450	0.0670	0.311	0.0910	0.88	0.44	0.234	0.113	0.718	0.352
10/10/2013 12:18	0913-111_A	13_10_10_1218_54_503	1	0.980	0.474	0.507	0.0690	0.385	0.0890	0.88	0.44	0.234	0.113	0.718	0.368
10/10/2013 12:19	0913-111_A	13_10_10_1219_55_313	1	1.41	0.480	0.595	0.0680	0.409	0.0910	0.88	0.45	0.234	0.110	0.718	0.359
10/10/2013 12:20	0913-111_A	13_10_10_1220_55_973	1	0.971	0.469	0.563	0.0690	0.383	0.0900	0.88	0.44	0.234	0.116	0.718	0.365
10/10/2013 12:21	0913-111_A	13_10_10_1221_56_783	1	1.08	0.438	0.558	0.0680	0.413	0.0920	0.88	0.45	0.234	0.108	0.718	0.319
10/10/2013 12:22	0913-111_A	13_10_10_1222_57_533	1	1.29	0.501	0.511	0.0680	0.345	0.0930	0.88	0.45	0.234	0.117	0.718	0.345
10/10/2013 12:23	0913-111_A	13_10_10_1223_58_283	1	1.89	0.488	0.614	0.0690	0.278	0.0900	0.88	0.45	0.234	0.114	0.718	0.359
10/10/2013 12:24	0913-111_A	13_10_10_1223_59_033	1	0.971	0.487	0.561	0.0670	0.371	0.0900	0.88	0.45	0.234	0.109	0.718	0.345
10/10/2013 12:25	0913-111_A	13_10_10_1223_59_783	1	0.971	0.465	0.501	0.0670	0.410	0.0910	0.88	0.45	0.234	0.111	0.718	0.345
10/10/2013 12:26	0913-111_A	13_10_10_1224_00_544	1	0.971	0.493	0.580	0.0700	0.331	0.0920	0.88	0.45	0.234	0.114	0.718	0.359
10/10/2013 12:27	0913-111_A	13_10_10_1224_01_294	1	0.971	0.488	0.598	0.0680	0.349	0.0910	0.88	0.45	0.234	0.114	0.718	0.359
10/10/2013 12:28	0913-111_A	13_10_10_1224_02_044	1	1.27	0.485	0.520	0.0690	0.348	0.0900	0.88	0.45	0.234	0.112	0.718	0.359
10/10/2013 12:29	0913-111_A	13_10_10_1224_02_794	1	1.57	0.483	0.477	0.0670	0.323	0.0910	0.88	0.45	0.234	0.113	0.718	0.358
10/10/2013 12:30	0913-111_A	13_10_10_1224_03_544	1	0.971	0.467	0.589	0.0630	0.383	0.0920	0.88	0.45	0.234	0.107	0.718	0.338
10/10/2013 12:31	0913-111_A	13_10_10_1224_04_294	1	0.971	0.485	0.587	0.0660	0.353	0.0900	0.88	0.45	0.234	0.113	0.718	0.359
10/10/2013 12:32	0913-111_A	13_10_10_1224_05_044	1	0.971	0.485	0.587	0.0680	0.337	0.0900	0.88	0.45	0.234	0.116	0.718	0.368
10/10/2013 12:33	0913-111_A	13_10_10_1224_05_794	1	1.58	0.485	0.587	0.0660	0.353	0.0900	0.88	0.45	0.234	0.113	0.718	0.359
10/10/2013 12:34	0913-111_A	13_10_10_1224_06_544	1	1.02	0.480	0.648	0.0680	0.334	0.0910	0.88	0.45	0.234	0.116	0.718	0.365
10/10/2013 12:35	0913-111_A	13_10_10_1224_07_294	1	0.971	0.482	0.608	0.0660	0.357	0.0900	0.88	0.45	0.234	0.111	0.718	0.345
10/10/2013 12:36	0913-111_A	13_10_10_1224_08_044	1	0.971	0.487	0.608	0.0660	0.268	0.0900	0.88	0.45	0.234	0.113	0.718	0.345
10/10/2013 12:37	0913-111_A	13_10_10_1224_08_794	1	0.971	0.473	0.642	0.0650	0.403	0.0910	0.88	0.45	0.234	0.112	0.718	0.345
10/10/2013 12:38	0913-111_A	13_10_10_1224_09_544	1	0.971	0.463	0.701	0.0690	0.414	0.0900	0.88	0.45	0.234	0.117	0.718	0.355
10/10/2013 12:39	0913-111_A	13_10_10_1240_22_890	1	1.54	0.467	0.615	0.0670	0.370	0.0890	0.88	0.45	0.234	0.116	0.718	0.346
10/10/2013 12:40	0913-111_A	13_10_10_1240_23_640	1	1.50	0.503	0.599	0.0660	0.383	0.0880	0.88	0.45	0.234	0.115	0.718	0.346
10/10/2013 12:41	0913-111_A	13_10_10_1242_24_140	1	1.83	0.489	0.510	0.0690	0.323	0.0880	0.88	0.44	0.234	0.120	0.718	0.350
10/10/2013 12:42	0913-111_A	13_10_10_1242_24_890	1	1.81	0.487	0.520	0.0690	0.338	0.0910	0.88	0.44	0.234	0.119	0.718	0.354
10/10/2013 12:43	0913-111_A	13_10_10_1243_24_590	1	1.81	0.487	0.520	0.0690	0.338	0.0910	0.88	0.44	0.234	0.119	0.718	0.354
10/10/2013 12:44	0913-111_A	13_10_10_1244_25_340	1	1.08	0.481	0.560	0.0680	0.372	0.0910	0.88	0.45	0.234	0.115	0.718	0.346
10/10/2013 12:45	0913-111_A	13_10_10_1244_26_090	1	1.33	0.485	0.560	0.0680	0.332	0.0890	0.88	0.45	0.234	0.117	0.718	0.354
10/10/2013 12:46	0913-111_A	13_10_10_1244_27_150	1	0.971	0.479	0.592	0.0670	0.330	0.0900	0.88	0.44	0.234	0.113	0.718	0.343
10/10/2013 12:47	0913-111_A	13_10_10_1247_27_970	1	1.06	0.483	0.718	0.0640	0.390	0.0880	0.88	0.45	0.234	0.111	0.718	0.354
10/10/2013 12:48	0913-111_A	13_10_10_1248_28_700	1	0.971	0.489	0.599	0.0690	0.385	0.0900	0.88	0.45	0.234	0.119	0.718	0.368
10/10/2013 12:49	0913-111_A	13_10_10_1249_29_390	1	0.971	0.522	0.587	0.0710	0.345	0.0900	0.88	0.44	0.234	0.121	0.718	0.388
10/10/2013 12:50	0913-111_A	13_10_10_1250_30_290	1	1.08	0.475	0.612	0.0670	0.363	0.0880	0.88	0.45	0.234	0.114	0.718	0.390
Average Conc. (ppm): 1 1.16 0.480 0.561 0.0677 0.376 0.0815 0.88 0.45 0.251 0.113 0.723 0.356															

Date	Method	Filename	DF	Acroline (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionalsdehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/10/2013 17:36	0913-111_A	13_10_10_1738_19_855	1	0.995	0.911										

Company ACT
 Analyst Initials: CHT
 Parameters EPA Method 320
 # Samples: 21 Runs

Client #1911
 Job # 0913-11
 POC # 0314-1911
 Report Date: V0.02.13.10.18.12.58

Dryer 1 Run 2															
Date	Method	Filename	OF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 10:00	0913-111_A	13_10_11_1000_40_402	1	1.72	0.880	1.57	0.121	1.50	0.297	2.04	1.20	0.672	0.219	1.27	0.638
10/11/2013 10:01	0913-111_A	13_10_11_1001_41_122	1	1.72	0.811	1.50	0.116	1.53	0.301	2.04	1.18	0.500	0.215	1.27	0.595
10/11/2013 10:02	0913-111_A	13_10_11_1002_41_352	1	1.72	0.841	1.40	0.126	1.50	0.297	2.04	1.18	0.684	0.224	1.27	0.623
10/11/2013 10:03	0913-111_A	13_10_11_1003_42_642	1	1.72	0.846	1.51	0.128	1.64	0.306	2.04	1.13	0.624	0.224	1.27	0.623
10/11/2013 10:04	0913-111_A	13_10_11_1004_43_352	1	1.72	0.853	1.58	0.129	1.59	0.301	2.04	1.12	0.550	0.227	1.27	0.634
10/11/2013 10:05	0913-111_A	13_10_11_1005_44_132	1	1.72	0.825	1.53	0.123	1.52	0.297	2.04	1.10	0.513	0.219	1.27	0.603
10/11/2013 10:06	0913-111_A	13_10_11_1006_44_842	1	1.72	0.870	1.47	0.127	1.59	0.296	2.04	1.10	0.547	0.226	1.27	0.640
10/11/2013 10:07	0913-111_A	13_10_11_1007_45_852	1	1.72	0.847	1.43	0.123	1.58	0.300	2.04	1.10	0.492	0.223	1.27	0.624
10/11/2013 10:08	0913-111_A	13_10_11_1008_46_382	1	1.72	0.883	1.51	0.125	1.83	0.296	2.04	1.09	0.896	0.225	1.27	0.638
10/11/2013 10:09	0913-111_A	13_10_11_1009_47_132	1	1.72	0.883	1.42	0.127	1.83	0.292	2.04	1.08	0.888	0.225	1.27	0.648
10/11/2013 10:10	0913-111_A	13_10_11_1010_47_862	1	1.72	0.846	1.33	0.126	1.58	0.291	2.04	1.07	0.644	0.224	1.27	0.623
10/11/2013 10:11	0913-111_A	13_10_11_1011_48_803	1	1.72	0.850	1.50	0.124	1.66	0.290	2.04	1.06	0.644	0.224	1.27	0.623
10/11/2013 10:12	0913-111_A	13_10_11_1012_49_403	1	1.72	0.856	1.43	0.125	1.59	0.283	2.04	1.08	0.488	0.228	1.27	0.629
10/11/2013 10:13	0913-111_A	13_10_11_1013_50_133	1	1.72	0.854	1.48	0.126	1.81	0.291	2.04	1.09	0.613	0.228	1.27	0.632
10/11/2013 10:14	0913-111_A	13_10_11_1014_50_843	1	1.72	0.860	1.46	0.122	1.60	0.290	2.04	1.09	0.548	0.221	1.27	0.645
10/11/2013 10:16	0913-111_A	13_10_11_1015_51_833	1	1.72	0.869	1.44	0.128	1.81	0.285	2.04	1.09	0.578	0.228	1.27	0.642
10/11/2013 10:17	0913-111_A	13_10_11_1016_52_393	1	1.72	0.847	1.48	0.123	1.70	0.286	2.04	1.08	0.639	0.222	1.27	0.629
10/11/2013 10:18	0913-111_A	13_10_11_1017_53_133	1	1.72	0.852	1.52	0.127	1.84	0.282	2.04	1.09	0.640	0.227	1.27	0.633
10/11/2013 10:19	0913-111_A	13_10_11_1018_53_683	1	1.72	0.862	1.24	0.129	1.82	0.282	2.04	1.08	0.710	0.226	1.27	0.651
10/11/2013 10:20	0913-111_A	13_10_11_1019_54_983	1	1.72	0.814	1.44	0.125	1.61	0.280	2.04	1.07	0.697	0.222	1.27	0.636
10/11/2013 10:21	0913-111_A	13_10_11_1020_55_383	1	1.72	0.851	1.28	0.123	1.58	0.281	2.04	1.07	0.452	0.222	1.27	0.608
10/11/2013 10:22	0913-111_A	13_10_11_1021_56_083	1	1.72	0.843	1.35	0.128	1.50	0.281	2.04	1.07	0.537	0.227	1.27	0.627
10/11/2013 10:23	0913-111_A	13_10_11_1022_56_793	1	1.72	0.828	1.47	0.123	1.54	0.282	2.04	1.07	0.517	0.218	1.27	0.608
10/11/2013 10:24	0913-111_A	13_10_11_1023_57_334	1	1.72	0.887	1.48	0.126	1.53	0.293	2.04	1.08	0.581	0.223	1.27	0.640
10/11/2013 10:25	0913-111_A	13_10_11_1024_58_264	1	1.72	0.851	1.40	0.128	1.59	0.287	2.04	1.07	0.823	0.222	1.27	0.638
10/11/2013 10:26	0913-111_A	13_10_11_1025_58_974	1	1.72	0.867	1.50	0.122	1.81	0.286	2.04	1.08	0.599	0.226	1.27	0.635
10/11/2013 10:28	0913-111_A	13_10_11_1026_59_734	1	1.72	0.829	1.53	0.122	1.56	0.292	2.04	1.06	0.528	0.218	1.27	0.631
10/11/2013 10:29	0913-111_A	13_10_11_1027_60_474	1	1.72	0.844	1.58	0.129	1.89	0.286	2.04	1.05	0.636	0.222	1.27	0.631
10/11/2013 10:30	0913-111_A	13_10_11_1028_60_984	1	1.72	0.828	1.44	0.127	1.71	0.295	2.04	1.07	0.704	0.228	1.27	0.633
10/11/2013 10:31	0913-111_A	13_10_11_1029_61_734	1	1.72	0.822	1.48	0.124	1.51	0.282	2.04	1.08	0.749	0.219	1.27	0.610
10/11/2013 10:32	0913-111_A	13_10_11_1030_62_344	1	1.72	0.880	1.42	0.126	1.58	0.284	2.04	1.08	0.701	0.225	1.27	0.638
10/11/2013 10:33	0913-111_A	13_10_11_1031_63_044	1	1.72	0.853	1.47	0.127	1.81	0.286	2.04	1.08	0.721	0.224	1.27	0.628
10/11/2013 10:34	0913-111_A	13_10_11_1032_63_744	1	1.72	0.848	1.48	0.126	1.89	0.286	2.04	1.07	0.717	0.224	1.27	0.631
10/11/2013 10:35	0913-111_A	13_10_11_1033_64_044	1	1.72	0.859	1.62	0.130	1.80	0.289	2.04	1.08	0.719	0.231	1.27	0.633
10/11/2013 10:36	0913-111_A	13_10_11_1034_64_744	1	1.72	0.865	1.56	0.128	1.66	0.290	2.04	1.06	0.686	0.220	1.27	0.637
10/11/2013 10:37	0913-111_A	13_10_11_1035_65_264	1	1.72	0.841	1.47	0.127	1.57	0.295	2.04	1.06	0.740	0.227	1.27	0.631
10/11/2013 10:38	0913-111_A	13_10_11_1036_65_964	1	1.72	0.833	1.59	0.127	1.72	0.293	2.04	1.05	0.683	0.229	1.27	0.613
10/11/2013 10:39	0913-111_A	13_10_11_1037_66_674	1	1.72	0.842	1.59	0.127	1.67	0.294	2.04	1.06	0.712	0.228	1.27	0.624
10/11/2013 10:40	0913-111_A	13_10_11_1038_67_374	1	1.72	0.838	1.56	0.129	1.75	0.293	2.04	1.05	0.752	0.231	1.27	0.620
10/11/2013 10:41	0913-111_A	13_10_11_1039_68_074	1	1.72	0.858	1.59	0.129	1.83	0.294	2.04	1.05	0.773	0.225	1.27	0.631
10/11/2013 10:42	0913-111_A	13_10_11_1040_68_774	1	1.72	0.861	1.59	0.129	1.83	0.294	2.04	1.05	0.763	0.225	1.27	0.632
10/11/2013 10:43	0913-111_A	13_10_11_1041_69_474	1	1.72	0.849	1.59	0.129	1.74	0.293	2.04	1.05	0.796	0.228	1.27	0.637
10/11/2013 10:44	0913-111_A	13_10_11_1042_70_174	1	1.72	0.870	1.69	0.127	1.74	0.295	2.04	1.06	0.744	0.225	1.27	0.617
10/11/2013 10:45	0913-111_A	13_10_11_1043_70_874	1	1.72	0.843	1.52	0.123	1.63	0.297	2.04	1.05	0.754	0.224	1.27	0.614
10/11/2013 10:46	0913-111_A	13_10_11_1044_71_574	1	1.72	0.831	1.49	0.122	1.65	0.298	2.04	1.03	0.788	0.227	1.27	0.627
10/11/2013 10:47	0913-111_A	13_10_11_1045_72_274	1	1.72	0.838	1.57	0.129	1.83	0.297	2.04	1.05	0.744	0.225	1.27	0.617
10/11/2013 10:48	0913-111_A	13_10_11_1046_73_024	1	1.72	0.838	1.57	0.129	1.83	0.297	2.04	1.05	0.744	0.225	1.27	0.617
10/11/2013 10:49	0913-111_A	13_10_11_1047_73_724	1	1.72	0.849	1.54	0.127	1.70	0.295	2.04	1.04	0.706	0.231	1.27	0.624
10/11/2013 10:50	0913-111_A	13_10_11_1048_74_424	1	1.72	0.878	1.69	0.124	1.88	0.296	2.04	1.03	0.851	0.231	1.27	0.621
10/11/2013 10:51	0913-111_A	13_10_11_1049_75_124	1	1.72	0.890	1.59	0.129	1.91	0.291	2.04	1.03	0.940	0.237	1.27	0.650
10/11/2013 10:52	0913-111_A	13_10_11_1050_75_824	1	1.72	0.900	2.24	0.131	2.08	0.319	2.04	0.98	0.875	0.238	1.27	0.658
10/11/2013 10:53	0913-111_A	13_10_11_1051_76_524	1	1.72	0.900	2.70	0.131	2.33	0.320	2.04	0.97	1.12	0.241	1.27	0.666
10/11/2013 10:54	0913-111_A	13_10_11_1052_77_224	1	1.72	0.861	2.71	0.133	2.31	0.318	2.04	0.97	1.25	0.245	1.27	0.642
10/11/2013 10:55	0913-111_A	13_10_11_1053_77_924	1	1.72	0.863	2.31	0.132	2.15	0.315	2.04	0.98	1.30	0.241	1.27	0.637
10/11/2013 10:56	0913-111_A	13_10_11_1054_78_624	1	1.72	0.856	2.12	0.129	2.11	0.303	2.04	1.01	1.17	0.237	1.27	0.634
10/11/2013 10:57	0913-111_A	13_10_11_1055_79_324	1	1.72	0.871	1.93	0.127	2.00	0.299	2.04	1.03	1.10	0.235	1.27	0.641
10/11/2013 10:58	0913-111_A	13_10_11_1056_79_924	1	1.72	0.848	1.88	0.128	1.85	0.298	2.04	1.02	1.00	0.232	1.27	0.637
10/11/2013 10:59	0913-111_A	13_10_11_1057_80_624	1	1.72	0.848	1.81	0.131	1.87	0.299	2.04	1.02	0.984	0.232	1.27	0.637
10/11/2013 11:00	0913-111_A	13_10_11_1058_81_324	1	1.72	0.848	1.87	0.128	1.87	0.304	2.04	1.04	0.971	0.228	1.27	0.623
Average Conc. (ppm):	1	1.72	0.860	1.96	0.113	1.70	0.283	2.04	1.07	0.714	0.227	1.27	0.628		

Dryer 1 Run 3															
Date	Method	Filename	OF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 11:37	0913-111_A	13_10_11_1137_48_070	1	1.72	0.785	1.61	0.117	1.23	0.285	2.04	1.07	0.462	0.217	1.27	0.580
10/11/2013 11:38	0913-111_A	13_10_11_1138_49_370	1	1.72	0.778	1.61	0.119	1.23	0.285	2.04	1.05	0.462	0.211	1.27	0.572
10/11/2013 11:39	0913-111_A	13_10_11_1139_50_180	1	1.72	0.799	1.54	0.121	1.32	0.284	2.04	1.05	0.452	0.217	1.27	0.577
10/11/2013 11:40	0913-111_A	13_10_11_1140_50_990	1	1.72	0.811	1.95	0.125	1.36	0.282	2.					

Company ACT
 Analyst Initials CJT
 Parameters EPA Method 320
 # Samples: 21 Runs

Client # 1911
 Job # 0913-111
 PO # 3134 1911
 Report Date V0.82 13.10.18.12.58

Pellet Cooler 2 Run 1

Date	Method	Filename	DF	Aroclor (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/11/2013 13:44	0913-111_A	13_10_11_1346_00_484	1	1.00	0.514	1.48	0.0740	0.972	0.0810	1.08	0.54	0.246	0.127	1.07	0.368	
10/11/2013 13:45	0913-111_A	13_10_11_1346_01_204	1	1.21	0.477	1.41	0.0700	0.938	0.0810	1.08	0.53	0.246	0.128	1.10	0.382	
10/11/2013 13:46	0913-111_A	13_10_11_1346_02_004	1	1.38	0.509	1.09	0.0710	0.878	0.0810	1.08	0.53	0.249	0.124	1.10	0.384	
10/11/2013 13:47	0913-111_A	13_10_11_1347_02_754	1	1.00	0.492	1.15	0.0710	0.901	0.0790	1.08	0.53	0.246	0.122	0.812	0.367	
10/11/2013 13:48	0913-111_A	13_10_11_1348_00_464	1	1.39	0.518	1.02	0.0890	0.929	0.0820	1.08	0.53	0.246	0.123	0.745	0.381	
10/11/2013 13:49	0913-111_A	13_10_11_1349_04_244	1	1.06	0.483	1.02	0.0890	0.798	0.0790	1.08	0.54	0.248	0.117	0.878	0.338	
10/11/2013 13:50	0913-111_A	13_10_11_1350_05_064	1	1.47	0.480	1.00	0.0700	0.818	0.0820	1.08	0.54	0.248	0.119	0.745	0.356	
10/11/2013 13:51	0913-111_A	13_10_11_1351_05_795	1	1.89	0.503	1.06	0.0750	0.826	0.0830	1.08	0.54	0.248	0.128	0.745	0.381	
10/11/2013 13:52	0913-111_A	13_10_11_1352_06_946	1	2.23	0.484	0.984	0.0750	0.730	0.0800	1.08	0.53	0.248	0.124	1.12	0.383	
10/11/2013 13:53	0913-111_A	13_10_11_1353_07_335	1	1.00	0.521	1.10	0.0740	0.859	0.0800	1.08	0.53	0.248	0.128	0.819	0.398	
10/11/2013 13:54	0913-111_A	13_10_11_1354_08_045	1	1.00	0.498	1.02	0.0890	0.823	0.0830	1.08	0.54	0.248	0.121	0.884	0.362	
10/11/2013 13:55	0913-111_A	13_10_11_1355_08_815	1	2.04	0.513	1.06	0.0750	0.829	0.0800	1.08	0.54	0.248	0.128	0.857	0.392	
10/11/2013 13:56	0913-111_A	13_10_11_1356_09_516	1	1.85	0.514	1.06	0.0750	0.981	0.0800	1.08	0.53	0.246	0.127	0.874	0.384	
10/11/2013 13:57	0913-111_A	13_10_11_1357_10_335	1	1.12	0.488	1.15	0.0660	0.904	0.0840	1.08	0.54	0.246	0.116	0.784	0.380	
10/11/2013 13:58	0913-111_A	13_10_11_1358_11_105	1	1.00	0.487	1.12	0.0700	0.817	0.0820	1.08	0.54	0.246	0.122	1.02	0.380	
10/11/2013 13:59	0913-111_A	13_10_11_1359_11_825	1	1.00	0.480	1.11	0.0730	0.851	0.0830	1.08	0.53	0.246	0.124	1.23	0.358	
10/11/2013 14:00	0913-111_A	13_10_11_1400_12_475	1	1.18	0.488	1.01	0.0700	0.854	0.0830	1.08	0.54	0.246	0.124	1.19	0.383	
10/11/2013 14:01	0913-111_A	13_10_11_1401_13_185	1	1.00	0.514	1.08	0.0720	0.822	0.0770	1.08	0.53	0.248	0.124	0.745	0.381	
10/11/2013 14:02	0913-111_A	13_10_11_1402_13_945	1	1.42	0.492	1.05	0.0730	0.833	0.0800	1.08	0.53	0.246	0.122	0.745	0.381	
10/11/2013 14:03	0913-111_A	13_10_11_1403_14_706	1	1.36	0.500	1.03	0.0890	0.807	0.0790	1.08	0.53	0.246	0.122	0.745	0.377	
10/11/2013 14:04	0913-111_A	13_10_11_1404_15_458	1	1.18	0.484	1.18	0.0890	0.787	0.0810	1.08	0.54	0.246	0.124	0.869	0.366	
10/11/2013 14:05	0913-111_A	13_10_11_1405_16_186	1	1.00	0.488	1.11	0.0680	0.832	0.0810	1.08	0.54	0.246	0.121	0.745	0.368	
10/11/2013 14:06	0913-111_A	13_10_11_1406_16_946	1	1.11	0.527	1.01	0.0870	0.828	0.0800	1.08	0.54	0.246	0.124	0.869	0.366	
10/11/2013 14:07	0913-111_A	13_10_11_1407_17_746	1	1.00	0.488	1.11	0.0690	0.796	0.0810	1.08	0.53	0.248	0.121	0.917	0.387	
10/11/2013 14:08	0913-111_A	13_10_11_1408_18_506	1	1.28	0.491	1.10	0.0700	0.797	0.0790	1.08	0.53	0.246	0.122	0.875	0.365	
10/11/2013 14:09	0913-111_A	13_10_11_1409_19_206	1	1.00	0.488	1.06	0.0710	0.804	0.0790	1.08	0.53	0.246	0.123	0.745	0.368	
10/11/2013 14:10	0913-111_A	13_10_11_1410_20_016	1	1.06	0.496	1.05	0.0860	0.853	0.0780	1.08	0.53	0.246	0.122	1.05	0.377	
10/11/2013 14:11	0913-111_A	13_10_11_1411_20_816	1	2.4	0.504	1.04	0.0710	0.818	0.0790	1.08	0.53	0.246	0.125	1.25	0.376	
10/11/2013 14:12	0913-111_A	13_10_11_1412_21_506	1	1.11	0.489	1.10	0.0880	0.905	0.0770	1.08	0.53	0.246	0.123	1.06	0.363	
10/11/2013 14:13	0913-111_A	13_10_11_1413_22_276	1	1.23	0.489	1.06	0.0720	0.778	0.0790	1.08	0.53	0.246	0.121	0.888	0.367	
10/11/2013 14:14	0913-111_A	13_10_11_1414_23_277	1	1.14	0.487	1.17	0.0730	0.810	0.0810	1.08	0.54	0.246	0.123	0.745	0.361	
10/11/2013 14:15	0913-111_A	13_10_11_1415_23_897	1	1.13	0.488	0.926	0.0730	0.908	0.0800	1.08	0.54	0.246	0.125	0.367	0.371	
10/11/2013 14:16	0913-111_A	13_10_11_1416_24_517	1	1.50	0.503	1.06	0.0700	0.831	0.0830	1.08	0.54	0.246	0.127	0.947	0.370	
10/11/2013 14:17	0913-111_A	13_10_11_1417_25_297	1	1.00	0.504	1.14	0.0700	0.791	0.0790	1.08	0.54	0.246	0.122	0.887	0.371	
10/11/2013 14:18	0913-111_A	13_10_11_1418_26_097	1	1.00	0.488	1.09	0.0710	0.820	0.0810	1.08	0.54	0.246	0.126	0.745	0.380	
10/11/2013 14:19	0913-111_A	13_10_11_1419_26_887	1	1.72	0.500	1.07	0.0700	0.766	0.0810	1.08	0.54	0.246	0.126	0.745	0.371	
10/11/2013 14:20	0913-111_A	13_10_11_1420_27_457	1	1.45	0.488	1.11	0.0720	0.824	0.0820	1.08	0.54	0.248	0.125	1.13	0.350	
10/11/2013 14:21	0913-111_A	13_10_11_1421_28_207	1	1.09	0.486	1.04	0.0710	0.744	0.0800	1.08	0.54	0.246	0.124	0.745	0.363	
10/11/2013 14:22	0913-111_A	13_10_11_1422_28_987	1	1.40	0.490	1.03	0.0710	0.679	0.0800	1.08	0.54	0.252	0.128	0.745	0.369	
10/11/2013 14:23	0913-111_A	13_10_11_1423_29_697	1	1.80	0.513	1.12	0.0700	0.798	0.0820	1.08	0.54	0.246	0.125	0.905	0.382	
10/11/2013 14:24	0913-111_A	13_10_11_1424_30_467	1	1.48	0.492	1.11	0.0700	0.789	0.0820	1.08	0.54	0.246	0.124	0.828	0.368	
10/11/2013 14:25	0913-111_A	13_10_11_1425_31_177	1	1.00	0.488	1.09	0.0680	0.824	0.0800	1.08	0.54	0.246	0.124	0.901	0.381	
10/11/2013 14:26	0913-111_A	13_10_11_1426_31_987	1	1.62	0.517	1.12	0.0740	0.781	0.0820	1.08	0.54	0.246	0.129	0.846	0.380	
10/11/2013 14:27	0913-111_A	13_10_11_1427_32_718	1	1.00	0.482	1.07	0.0700	0.751	0.0820	1.08	0.54	0.248	0.122	0.745	0.349	
10/11/2013 14:28	0913-111_A	13_10_11_1428_33_468	1	1.94	0.483	1.07	0.0700	0.752	0.0810	1.08	0.54	0.246	0.125	0.745	0.380	
10/11/2013 14:29	0913-111_A	13_10_11_1429_34_178	1	1.00	0.488	1.09	0.0700	0.752	0.0810	1.08	0.54	0.246	0.125	0.745	0.380	
10/11/2013 14:30	0913-111_A	13_10_11_1430_35_028	1	1.00	0.518	0.988	0.0750	0.794	0.0830	1.08	0.54	0.248	0.129	0.988	0.380	
10/11/2013 14:31	0913-111_A	13_10_11_1431_35_796	1	1.50	0.499	1.04	0.0740	0.788	0.0830	1.08	0.54	0.248	0.126	0.762	0.376	
10/11/2013 14:32	0913-111_A	13_10_11_1432_36_488	1	1.19	0.506	1.04	0.0730	0.780	0.0820	1.08	0.54	0.246	0.128	0.745	0.379	
10/11/2013 14:33	0913-111_A	13_10_11_1433_37_208	1	1.00	0.487	1.06	0.0730	0.774	0.0800	1.08	0.54	0.246	0.127	0.760	0.368	
10/11/2013 14:34	0913-111_A	13_10_11_1434_37_918	1	1.06	0.498	1.14	0.0700	0.750	0.0830	1.08	0.54	0.248	0.126	0.374	0.378	
10/11/2013 14:35	0913-111_A	13_10_11_1435_38_748	1	1.00	0.487	1.08	0.0670	0.798	0.0840	1.08	0.54	0.248	0.122	0.745	0.349	
10/11/2013 14:36	0913-111_A	13_10_11_1436_39_408	1	2.12	0.483	1.08	0.0680	0.756	0.0840	1.08	0.55	0.248	0.124	0.760	0.370	
10/11/2013 14:37	0913-111_A	13_10_11_1437_40_168	1	1.00	0.488	1.06	0.0730	0.732	0.0850	1.08	0.55	0.248	0.128	0.745	0.374	
10/11/2013 14:38	0913-111_A	13_10_11_1438_40_989	1	1.55	0.494	0.950	0.0740	0.789	0.0840	1.08	0.55	0.248	0.128	0.745	0.372	
10/11/2013 14:39	0913-111_A	13_10_11_1439_41_689	1	1.00	0.513	1.05	0.0750	0.750	0.0860	1.08	0.55	0.249	0.131	0.745	0.379	
10/11/2013 14:40	0913-111_A	13_10_11_1440_42_448	1	1.96	0.487	1.12	0.0700	0.710	0.0860	1.08	0.55	0.246	0.125	0.745	0.362	
10/11/2013 14:41	0913-111_A	13_10_11_1441_43_188	1	1.17	0.522	1.12	0.0730	0.768	0.0860	1.08	0.55	0.246	0.132	0.745	0.386	
10/11/2013 14:42	0913-111_A	13_10_11_1442_43_779	1	1.00	0.517	0.993	0.0710	0.760	0.0860	1.08	0.55	0.248	0.127	0.745	0.381	
10/11/2013 14:43	0913-111_A	13_10_11_1443_44_509	1	1.44	0.475	0.983	0.0680	0.833	0.0860	1.08	0.58	0.246	0.153	0.745	0.389	
Average Conc (ppm):				1	1.29	0.496	1.07	0.0711	0.797	0.0813	1.08	0.54	0.246	0.125	0.864	0.370

Pellet Cooler 2 Run 2

Date	Method	Filename	DF	Aroclor (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 15:08	0913-111_A	13_10_11_1508_02_515	1	1.00	0.480	0.610	0.0650	0.802	0.0840	1.08	0.55	0.246	0.115	1.06	0.354
10/11/2013 15:09															

Company/ACT
 Analyst Initials/CT
 Parameters/EPA Method 320
 # Samples/21 Runs

Client # 1911
 Job # 0913-111
 PO # 0194 1911
 Report Date V0.62 13.10.16.12.58

Peiset Coaker 2 Run 3

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/2013 16:29	0913-111_A	13_10_11_1629_02_222	1	1.41	0.500	0.127	0.0730	0.793	0.0840	1.08	0.55	0.246	0.125	0.589	0.379
10/11/2013 16:30	0913-111_A	13_10_11_1630_02_272	1	1.08	0.500	1.12	0.0740	0.741	0.0840	1.08	0.55	0.246	0.125	0.589	0.379
10/11/2013 16:31	0913-111_A	13_10_11_1631_02_532	1	1.13	0.506	0.929	0.0710	0.715	0.0850	1.08	0.55	0.246	0.119	1.25	0.372
10/11/2013 16:32	0913-111_A	13_10_11_1632_04_402	1	1.00	0.521	1.10	0.0720	0.688	0.0820	1.08	0.55	0.249	0.123	1.18	0.385
10/11/2013 16:33	0913-111_A	13_10_11_1633_05_202	1	1.11	0.507	1.07	0.0730	0.760	0.0840	1.08	0.55	0.246	0.118	0.745	0.384
10/11/2013 16:34	0913-111_A	13_10_11_1634_05_962	1	1.25	0.512	1.11	0.0690	0.837	0.0860	1.08	0.55	0.246	0.117	1.02	0.379
10/11/2013 16:35	0913-111_A	13_10_11_1635_06_772	1	1.27	0.525	1.12	0.0730	0.837	0.0860	1.08	0.55	0.246	0.124	0.745	0.395
10/11/2013 16:36	0913-111_A	13_10_11_1636_07_512	1	1.00	0.524	1.20	0.0760	0.851	0.0840	1.08	0.58	0.246	0.127	0.745	0.393
10/11/2013 16:37	0913-111_A	13_10_11_1637_08_222	1	1.00	0.528	1.19	0.0780	0.887	0.0820	1.08	0.55	0.246	0.125	0.891	0.388
10/11/2013 16:38	0913-111_A	13_10_11_1638_09_063	1	1.67	0.504	1.20	0.0780	0.906	0.0860	1.08	0.58	0.246	0.129	1.16	0.377
10/11/2013 16:39	0913-111_A	13_10_11_1639_09_743	1	1.00	0.532	1.28	0.0740	0.832	0.0870	1.08	0.59	0.246	0.125	0.745	0.390
10/11/2013 16:40	0913-111_A	13_10_11_1640_10_483	1	1.00	0.538	1.34	0.0770	0.869	0.0870	1.08	0.59	0.246	0.122	0.745	0.372
10/11/2013 16:41	0913-111_A	13_10_11_1641_11_243	1	1.00	0.505	1.31	0.0720	0.840	0.0880	1.08	0.59	0.246	0.120	0.745	0.394
10/11/2013 16:42	0913-111_A	13_10_11_1642_12_003	1	1.05	0.482	1.31	0.0660	0.921	0.0880	1.08	0.58	0.248	0.121	0.922	0.362
10/11/2013 16:43	0913-111_A	13_10_11_1643_12_743	1	1.49	0.519	1.42	0.0730	0.948	0.0870	1.08	0.58	0.246	0.129	0.745	0.372
10/11/2013 16:44	0913-111_A	13_10_11_1644_13_493	1	1.52	0.519	1.30	0.0740	0.951	0.0850	1.08	0.58	0.246	0.149	0.403	0.378
10/11/2013 16:45	0913-111_A	13_10_11_1645_14_233	1	2.25	0.539	3.47	0.0800	1.075	0.0870	1.49	0.57	0.248	0.129	0.745	0.387
10/11/2013 16:46	0913-111_A	13_10_11_1646_15_003	1	2.60	0.502	3.49	0.0810	1.271	0.0870	1.14	0.58	0.246	0.129	0.745	0.372
10/11/2013 16:47	0913-111_A	13_10_11_1647_15_743	1	2.07	0.525	2.88	0.0850	1.050	0.0880	1.08	0.58	0.246	0.125	0.745	0.388
10/11/2013 16:48	0913-111_A	13_10_11_1648_16_503	1	1.17	0.504	2.40	0.0780	0.951	0.0850	1.08	0.58	0.246	0.124	0.745	0.384
10/11/2013 16:49	0913-111_A	13_10_11_1649_17_154	1	1.44	0.509	2.21	0.0760	0.739	0.0830	1.08	0.55	0.485	0.129	0.745	0.371
10/11/2013 16:50	0913-111_A	13_10_11_1650_17_954	1	1.22	0.521	2.09	0.0720	0.748	0.0850	1.08	0.58	0.404	0.124	0.745	0.384
10/11/2013 16:51	0913-111_A	13_10_11_1651_18_704	1	1.05	0.532	2.18	0.0770	0.833	0.0870	1.08	0.58	0.246	0.125	0.745	0.388
10/11/2013 16:52	0913-111_A	13_10_11_1652_19_514	1	1.67	0.519	2.13	0.0750	0.842	0.0860	1.08	0.58	0.246	0.125	0.745	0.379
10/11/2013 16:53	0913-111_A	13_10_11_1653_20_254	1	1.18	0.528	2.14	0.0770	0.888	0.0860	1.08	0.58	0.246	0.125	0.745	0.388
10/11/2013 16:54	0913-111_A	13_10_11_1654_21_014	1	1.00	0.498	2.22	0.0780	0.804	0.0840	1.08	0.58	0.338	0.127	0.745	0.380
10/11/2013 16:55	0913-111_A	13_10_11_1655_21_764	1	1.00	0.521	2.23	0.0760	0.784	0.0860	1.08	0.58	0.338	0.127	0.745	0.390
10/11/2013 16:56	0913-111_A	13_10_11_1656_22_494	1	1.79	0.517	2.23	0.0730	0.820	0.0840	1.08	0.618	0.128	0.745	0.385	0.379
10/11/2013 16:57	0913-111_A	13_10_11_1657_23_244	1	1.00	0.521	2.31	0.0750	0.857	0.0830	1.08	0.55	0.447	0.127	0.745	0.382
10/11/2013 16:58	0913-111_A	13_10_11_1658_24_014	1	1.43	0.484	2.09	0.0720	0.753	0.0870	1.08	0.56	0.384	0.125	0.745	0.370
10/11/2013 16:59	0913-111_A	13_10_11_1659_24_714	1	1.44	0.527	2.01	0.0740	0.783	0.0840	1.08	0.55	0.454	0.127	0.745	0.366
10/11/2013 17:00	0913-111_A	13_10_11_1700_25_504	1	1.00	0.521	2.05	0.0780	0.806	0.0840	1.08	0.55	0.454	0.127	0.745	0.366
10/11/2013 17:01	0913-111_A	13_10_11_1701_26_275	1	1.46	0.530	1.96	0.0740	0.722	0.0830	1.08	0.55	0.425	0.125	0.745	0.382
10/11/2013 17:02	0913-111_A	13_10_11_1702_26_915	1	1.52	0.496	1.90	0.0690	0.750	0.0840	1.08	0.55	0.454	0.127	0.745	0.366
10/11/2013 17:03	0913-111_A	13_10_11_1703_27_725	1	1.00	0.504	1.90	0.0740	0.764	0.0850	1.08	0.55	0.454	0.127	0.745	0.366
10/11/2013 17:04	0913-111_A	13_10_11_1704_28_495	1	1.37	0.488	1.78	0.0730	0.737	0.0850	1.08	0.55	0.380	0.126	0.745	0.371
10/11/2013 17:05	0913-111_A	13_10_11_1705_29_235	1	1.64	0.487	1.88	0.0720	0.809	0.0820	1.08	0.55	0.246	0.121	0.745	0.384
10/11/2013 17:06	0913-111_A	13_10_11_1706_30_015	1	1.24	0.491	1.92	0.0710	0.778	0.0820	1.08	0.56	0.313	0.119	0.761	0.370
10/11/2013 17:07	0913-111_A	13_10_11_1707_30_735	1	1.00	0.524	1.92	0.0730	0.809	0.0840	1.08	0.55	0.338	0.122	0.745	0.380
10/11/2013 17:08	0913-111_A	13_10_11_1708_31_465	1	1.00	0.502	1.92	0.0710	0.728	0.0830	1.08	0.55	0.301	0.122	0.745	0.380
10/11/2013 17:09	0913-111_A	13_10_11_1709_32_195	1	2.23	0.512	1.90	0.0720	0.804	0.0800	1.08	0.55	0.386	0.116	0.745	0.381
10/11/2013 17:10	0913-111_A	13_10_11_1710_33_005	1	1.31	0.488	1.91	0.0730	0.849	0.0840	1.08	0.54	0.413	0.120	0.745	0.367
10/11/2013 17:11	0913-111_A	13_10_11_1711_33_755	1	1.00	0.508	1.88	0.0710	0.831	0.0820	1.08	0.55	0.304	0.119	0.745	0.380
10/11/2013 17:12	0913-111_A	13_10_11_1712_34_485	1	1.00	0.505	1.96	0.0780	0.738	0.0840	1.08	0.55	0.312	0.127	0.745	0.386
10/11/2013 17:13	0913-111_A	13_10_11_1713_35_215	1	1.00	0.489	2.00	0.0710	0.907	0.0810	1.08	0.55	0.293	0.123	0.745	0.379
10/11/2013 17:14	0913-111_A	13_10_11_1714_36_988	1	1.38	0.473	1.83	0.0720	0.748	0.0850	1.08	0.55	0.246	0.121	0.745	0.385
10/11/2013 17:15	0913-111_A	13_10_11_1715_38_768	1	1.31	0.511	1.91	0.0710	0.731	0.0840	1.08	0.55	0.246	0.123	0.745	0.379
10/11/2013 17:16	0913-111_A	13_10_11_1716_39_496	1	1.54	0.489	1.88	0.0680	0.776	0.0800	1.08	0.55	0.246	0.122	0.745	0.350
10/11/2013 17:17	0913-111_A	13_10_11_1717_40_246	1	1.29	0.469	1.78	0.0710	0.830	0.0820	1.08	0.55	0.323	0.117	0.745	0.349
10/11/2013 17:18	0913-111_A	13_10_11_1718_41_016	1	1.51	0.474	1.81	0.0690	0.840	0.0850	1.08	0.55	0.248	0.123	0.745	0.361
10/11/2013 17:19	0913-111_A	13_10_11_1719_41_766	1	1.22	0.511	1.79	0.0700	0.870	0.0840	1.08	0.55	0.248	0.123	0.745	0.361
10/11/2013 17:20	0913-111_A	13_10_11_1720_42_506	1	1.17	0.497	1.92	0.0710	0.727	0.0820	1.08	0.55	0.281	0.116	0.745	0.369
10/11/2013 17:21	0913-111_A	13_10_11_1721_43_236	1	1.00	0.507	1.97	0.0690	0.785	0.0820	1.08	0.55	0.297	0.119	0.745	0.379
10/11/2013 17:22	0913-111_A	13_10_11_1722_44_066	1	1.00	0.519	1.95	0.0710	0.785	0.0820	1.08	0.55	0.297	0.119	0.745	0.379
10/11/2013 17:23	0913-111_A	13_10_11_1723_44_806	1	1.00	0.487	1.85	0.0700	0.879	0.0840	1.08	0.54	0.328	0.122	0.745	0.381
10/11/2013 17:24	0913-111_A	13_10_11_1724_45_527	1	1.00	0.492	1.98	0.0720	0.858	0.0840	1.08	0.56	0.246	0.123	0.745	0.367
10/11/2013 17:25	0913-111_A	13_10_11_1725_46_287	1	1.00	0.492	1.98	0.0720	0.858	0.0840	1.08	0.56	0.246	0.123	0.745	0.367
10/11/2013 17:26	0913-111_A	13_10_11_1726_46_987	1	2.21	0.487	2.04	0.0710	0.849	0.0830	1.08	0.55	0.403	0.121	0.758	0.373
10/11/2013 17:27	0913-111_A	13_10_11_1727_47_747	1	1.92	0.492	1.89	0.0720	0.869	0.0830	1.08	0.55	0.246	0.121	0.745	0.375
10/11/2013 17:28	0913-111_A	13_10_11_1728_48_477	1	1.23	0.490	1.80	0.0750	0.814	0.0820	1.08	0.55	0.246	0.122	0.745	0.367
10/11/2013 17:29	0913-111_A	13_10_11_1729_49_207	1	1.29	0.504	1.98	0.0720	0.843	0.0820	1.08	0.55	0.302	0.124	0.745	0.380
Average Conc. (ppm):			1	1.33	0.507	1.84	0.0732	0.844	0.0844	1.09	0.55	0.350	0.124	0.788	0.378

Hammermill 2 Run 1

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/11/201															

Company/ACT
 Analyst Initials CJT
 Parameters EPA Method 320
 # Samples/21 Runs

Client # 1911
 Job # 0913-111
 PO # 3134 1911
 Report Date V0.62 13.10.18.12.58

Hammermill 2 Run 2

Date	Method	Filename	DF	Acridin (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/1/2013 19:25	0913-111_A	13_10_11_1925_01_214	1.03	0.455	0.387	0.0692	0.165	0.0760	1.08	0.52	0.232	0.107	0.707	0.352	0.343
10/1/2013 19:26	0913-111_A	13_10_11_1926_02_534	1.03	0.455	0.478	0.0620	0.184	0.0770	1.08	0.52	0.232	0.104	0.707	0.343	0.343
10/1/2013 19:27	0913-111_A	13_10_11_1927_03_234	1.03	0.455	0.584	0.0660	0.155	0.0770	1.08	0.52	0.232	0.107	0.707	0.343	0.343
10/1/2013 19:28	0913-111_A	13_10_11_1928_03_994	1.03	0.455	0.470	0.0685	0.155	0.0690	1.08	0.53	0.232	0.110	0.707	0.348	0.348
10/1/2013 19:29	0913-111_A	13_10_11_1929_04_144	1.03	0.455	0.408	0.0620	0.165	0.0810	1.08	0.53	0.232	0.108	0.731	0.346	0.346
10/1/2013 19:40	0913-111_A	13_10_11_1940_05_514	1.03	0.455	0.569	0.0880	0.203	0.0800	1.08	0.54	0.232	0.109	0.707	0.360	0.360
10/1/2013 19:41	0913-111_A	13_10_11_1941_06_114	1.03	0.455	0.470	0.0705	0.188	0.0850	1.08	0.55	0.232	0.108	0.707	0.343	0.343
10/1/2013 19:42	0913-111_A	13_10_11_1942_06_324	1.03	0.455	0.504	0.0650	0.189	0.0830	1.08	0.55	0.232	0.114	0.707	0.369	0.369
10/1/2013 19:43	0913-111_A	13_10_11_1943_07_074	1.03	0.455	0.502	0.738	0.0700	0.180	0.0880	1.08	0.55	0.232	0.117	0.707	0.369
10/1/2013 19:44	0913-111_A	13_10_11_1944_08_285	1.03	0.455	0.467	0.818	0.0880	0.184	0.0850	1.08	0.55	0.232	0.114	0.707	0.355
10/1/2013 19:45	0913-111_A	13_10_11_1945_09_195	1.03	0.455	0.496	0.965	0.0730	0.189	0.0850	1.08	0.56	0.232	0.123	0.707	0.367
10/1/2013 19:46	0913-111_A	13_10_11_1946_09_395	1.03	0.455	0.512	1.22	0.0740	0.178	0.0800	1.08	0.57	0.232	0.127	0.707	0.375
10/1/2013 19:47	0913-111_A	13_10_11_1947_10_065	1.03	0.455	0.505	1.29	0.0720	0.175	0.0650	1.08	0.56	0.232	0.122	0.707	0.372
10/1/2013 19:48	0913-111_A	13_10_11_1948_11_485	1.03	0.455	0.487	1.11	0.0870	0.185	0.0830	1.08	0.55	0.232	0.113	0.707	0.367
10/1/2013 19:49	0913-111_A	13_10_11_1949_12_195	1.03	0.455	0.492	1.06	0.0700	0.185	0.0840	1.08	0.55	0.232	0.114	0.707	0.365
10/1/2013 19:50	0913-111_A	13_10_11_1950_12_345	1.03	0.455	0.460	1.14	0.0800	0.165	0.0640	1.08	0.55	0.232	0.114	0.707	0.365
10/1/2013 19:51	0913-111_A	13_10_11_1951_13_155	1.03	0.455	0.462	1.17	0.0850	0.165	0.0830	1.08	0.55	0.232	0.107	0.707	0.337
10/1/2013 19:52	0913-111_A	13_10_11_1952_14_475	1.03	0.455	0.501	1.09	0.0880	0.165	0.0840	1.08	0.55	0.232	0.114	0.707	0.359
10/1/2013 19:53	0913-111_A	13_10_11_1953_15_195	1.03	0.455	0.453	0.918	0.0860	0.165	0.0820	1.08	0.55	0.236	0.110	0.707	0.342
10/1/2013 19:54	0913-111_A	13_10_11_1954_16_315	1.03	0.455	0.468	0.986	0.0820	0.165	0.0840	1.08	0.55	0.232	0.109	0.707	0.338
10/1/2013 19:55	0913-111_A	13_10_11_1955_16_735	1.03	0.455	0.484	0.645	0.0870	0.168	0.0830	1.08	0.55	0.234	0.109	0.707	0.364
10/1/2013 19:56	0913-111_A	13_10_11_1956_17_548	1.03	0.455	0.477	0.739	0.0700	0.167	0.0870	1.08	0.55	0.232	0.114	0.707	0.366
10/1/2013 19:57	0913-111_A	13_10_11_1957_18_298	1.03	0.455	0.484	0.834	0.0700	0.165	0.0830	1.08	0.55	0.232	0.114	0.707	0.366
10/1/2013 19:58	0913-111_A	13_10_11_1958_19_168	1.03	0.455	0.497	0.781	0.0860	0.197	0.0800	1.08	0.56	0.230	0.114	0.707	0.361
10/1/2013 19:59	0913-111_A	13_10_11_1959_20_097	1.03	0.455	0.486	0.968	0.0700	0.165	0.0870	1.08	0.56	0.232	0.116	0.707	0.367
10/1/2013 20:00	0913-111_A	13_10_11_2000_20_526	1.03	0.455	0.485	1.18	0.0870	0.238	0.0840	1.08	0.55	0.232	0.116	0.707	0.367
10/1/2013 20:01	0913-111_A	13_10_11_2001_21_306	1.03	0.455	0.486	0.986	0.0860	0.232	0.0850	1.08	0.55	0.232	0.114	0.707	0.365
10/1/2013 20:02	0913-111_A	13_10_11_2002_22_068	1.03	0.455	0.470	1.20	0.0710	0.287	0.0870	1.08	0.58	0.232	0.117	0.707	0.366
10/1/2013 20:03	0913-111_A	13_10_11_2003_22_786	1.03	0.455	0.503	1.15	0.0730	0.286	0.0870	1.08	0.58	0.232	0.120	0.707	0.362
10/1/2013 20:04	0913-111_A	13_10_11_2004_23_566	1.03	0.455	0.490	1.52	0.0720	0.287	0.0860	1.08	0.58	0.232	0.121	0.707	0.366
10/1/2013 20:05	0913-111_A	13_10_11_2005_24_316	1.03	0.455	0.493	1.31	0.0720	0.287	0.0860	1.08	0.58	0.232	0.117	0.707	0.361
10/1/2013 20:06	0913-111_A	13_10_11_2006_25_026	1.03	0.455	0.479	1.24	0.0870	0.289	0.0850	1.08	0.55	0.232	0.116	0.707	0.361
10/1/2013 20:07	0913-111_A	13_10_11_2007_25_847	1.03	0.455	0.471	1.50	0.0880	0.281	0.0840	1.08	0.55	0.230	0.113	0.707	0.340
10/1/2013 20:08	0913-111_A	13_10_11_2008_26_547	1.03	0.455	0.496	1.77	0.0710	0.304	0.0840	1.08	0.55	0.232	0.121	0.707	0.363
10/1/2013 20:09	0913-111_A	13_10_11_2009_27_277	1.03	0.455	0.470	1.88	0.0920	0.323	0.0850	1.08	0.56	0.232	0.117	0.707	0.348
10/1/2013 20:10	0913-111_A	13_10_11_2010_28_067	1.03	0.455	0.516	2.01	0.0720	0.308	0.0880	1.08	0.56	0.232	0.127	0.707	0.373
10/1/2013 20:11	0913-111_A	13_10_11_2011_28_787	1.03	0.455	0.487	2.07	0.0880	0.316	0.0850	1.08	0.55	0.232	0.126	0.707	0.372
10/1/2013 20:12	0913-111_A	13_10_11_2012_29_547	1.03	0.455	0.517	1.95	0.0710	0.254	0.0850	1.08	0.54	0.232	0.119	0.707	0.358
10/1/2013 20:13	0913-111_A	13_10_11_2013_30_316	1.03	0.455	0.478	1.47	0.0700	0.284	0.0860	1.08	0.55	0.232	0.119	0.707	0.372
10/1/2013 20:14	0913-111_A	13_10_11_2014_31_027	1.03	0.455	0.488	1.48	0.0700	0.165	0.0830	1.08	0.55	0.234	0.117	0.707	0.352
10/1/2013 20:15	0913-111_A	13_10_11_2015_31_827	1.03	0.455	0.502	1.42	0.0710	0.200	0.0840	1.08	0.55	0.232	0.117	0.707	0.352
10/1/2013 20:16	0913-111_A	13_10_11_2016_32_537	1.03	0.455	0.474	1.60	0.0880	0.218	0.0860	1.08	0.55	0.232	0.115	0.707	0.349
10/1/2013 20:17	0913-111_A	13_10_11_2017_33_267	1.03	0.455	0.473	1.84	0.0950	0.244	0.0880	1.08	0.56	0.232	0.120	0.707	0.346
10/1/2013 20:18	0913-111_A	13_10_11_2018_34_067	1.03	0.455	0.483	1.79	0.0720	0.207	0.0840	1.08	0.55	0.232	0.118	0.707	0.363
10/1/2013 20:19	0913-111_A	13_10_11_2019_34_828	1.03	0.455	0.441	1.37	0.0870	0.231	0.0810	1.08	0.54	0.232	0.118	0.707	0.319
10/1/2013 20:20	0913-111_A	13_10_11_2020_35_678	1.03	0.455	0.483	0.833	0.227	0.0790	1.08	0.53	0.232	0.103	0.707	0.303	0.319
10/1/2013 20:21	0913-111_A	13_10_11_2021_36_418	1.03	0.455	0.433	0.987	0.0620	0.202	0.0750	1.08	0.53	0.232	0.103	0.707	0.310
10/1/2013 20:22	0913-111_A	13_10_11_2022_37_128	1.03	0.455	0.461	1.19	0.0820	0.237	0.0830	1.08	0.54	0.232	0.107	0.707	0.338
10/1/2013 20:23	0913-111_A	13_10_11_2023_37_728	1.03	0.455	0.479	1.39	0.0880	0.188	0.0860	1.08	0.55	0.232	0.119	0.707	0.359
10/1/2013 20:24	0913-111_A	13_10_11_2024_38_578	1.03	0.455	0.483	1.48	0.0950	0.184	0.0860	1.08	0.56	0.232	0.124	0.707	0.362
10/1/2013 20:25	0913-111_A	13_10_11_2025_39_308	1.03	0.455	0.491	1.36	0.0700	0.239	0.0850	1.08	0.56	0.232	0.121	0.707	0.360
10/1/2013 20:26	0913-111_A	13_10_11_2026_40_038	1.03	0.455	0.486	1.27	0.0880	0.182	0.0850	1.08	0.56	0.232	0.119	0.707	0.341
10/1/2013 20:27	0913-111_A	13_10_11_2027_40_768	1.03	0.455	0.484	1.15	0.0870	0.191	0.0860	1.08	0.55	0.232	0.119	0.707	0.356
10/1/2013 20:28	0913-111_A	13_10_11_2028_41_548	1.03	0.455	0.493	1.23	0.0950	0.243	0.0850	1.08	0.55	0.232	0.114	0.707	0.359
10/1/2013 20:29	0913-111_A	13_10_11_2029_42_348	1.03	0.455	0.477	0.973	0.0710	0.171	0.0840	1.08	0.55	0.232	0.113	0.707	0.350
10/1/2013 20:30	0913-111_A	13_10_11_2030_43_068	1.03	0.455	0.474	0.997	0.0860	0.165	0.0850	1.08	0.55	0.232	0.111	0.707	0.344
10/1/2013 20:31	0913-111_A	13_10_11_2031_43_869	1.03	0.455	0.483	1.65	0.0880	0.201	0.0860	1.08	0.55	0.232	0.114	0.707	0.356
10/1/2013 20:32	0913-111_A	13_10_11_2032_44_619	1.03	0.455	0.493	1.67	0.0710	0.253	0.0850	1.08	0.56	0.232	0.122	0.707	0.360
10/1/2013 20:33	0913-111_A	13_10_11_2033_45_369	1.03	0.455	0.463	1.44	0.0870	0.165	0.0840	1.08	0.55	0.232	0.111	0.707	0.342
10/1/2013 20:34	0913-111_A	13_10_11_2034_46_079	1.03	0.455	0.490	0.596	0.0870	0.165	0.0850	1.08	0.55	0.232	0.112	0.707	0.331
10/1/2013 20:35	0913-111_A	13_10_11_2035_46_799	1.03	0.455	0.516	0.136	0.102	0.168	0.0420	1.08	0.128	0.232	0.504	0.707	0.391
Average Conc. (ppm): 1 0.975 0.480 1.14 0.0682 0.211 0.0892 1.08 0.64 0.243 0.122 0.710 0.362															

Hammermill 2 Run 3

Date	Method	Filename	DF
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Company ACT
 Analytical Unit
 Parameters EPA Method 320
 # Samples 21 Runs

Client # 1911
 Job # 0913-111
 PO # 13-34 0911
 Report Date 10.02.13 10:18:12.58

Pellet Cooler 1 Run 1

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/12/2013 8:56	0913-111_A	13_10_12_0858_54_250	1	0.931	0.473	1.38	0.0630	0.373	0.0710	0.98	0.48	0.236	0.114	0.666	0.343	
10/12/2013 8:59	0913-111_A	13_10_12_0859_55_060	1	0.931	0.451	1.43	0.0630	0.416	0.0730	0.98	0.48	0.237	0.113	0.668	0.332	
10/12/2013 9:00	0913-111_A	13_10_12_0900_56_760	1	0.931	0.473	1.46	0.0630	0.440	0.0700	0.98	0.48	0.291	0.120	0.666	0.353	
10/12/2013 9:01	0913-111_A	13_10_12_0901_56_540	1	0.931	0.443	1.56	0.0630	0.412	0.0710	0.98	0.48	0.337	0.114	0.665	0.327	
10/12/2013 9:02	0913-111_A	13_10_12_0902_57_240	1	1.05	0.458	1.42	0.0670	0.487	0.0710	0.88	0.48	0.263	0.115	0.668	0.344	
10/12/2013 9:03	0913-111_A	13_10_12_0903_58_000	1	0.931	0.447	1.38	0.0610	0.431	0.0700	0.98	0.48	0.236	0.108	0.668	0.328	
10/12/2013 9:04	0913-111_A	13_10_12_0904_58_810	1	0.931	0.487	1.32	0.0680	0.495	0.0740	0.98	0.48	0.337	0.118	0.668	0.352	
10/12/2013 9:05	0913-111_A	13_10_12_0905_59_300	1	1.20	0.480	1.26	0.0660	0.496	0.0700	0.98	0.48	0.226	0.118	0.668	0.351	
10/12/2013 9:07	0913-111_A	13_10_12_0907_00_280	1	0.931	0.482	1.41	0.0670	0.483	0.0710	0.98	0.48	0.236	0.119	0.668	0.339	
10/12/2013 9:08	0913-111_A	13_10_12_0908_01_061	1	0.931	0.477	1.50	0.0680	0.496	0.0700	0.98	0.50	0.340	0.116	0.668	0.352	
10/12/2013 9:09	0913-111_A	13_10_12_0909_01_771	1	0.931	0.449	1.53	0.0590	0.483	0.0700	0.98	0.50	0.373	0.112	0.668	0.330	
10/12/2013 9:10	0913-111_A	13_10_12_0910_02_501	1	0.931	0.449	1.50	0.0510	0.450	0.0700	0.98	0.50	0.236	0.114	0.668	0.330	
10/12/2013 9:11	0913-111_A	13_10_12_0911_03_351	1	0.931	0.460	1.49	0.0630	0.502	0.0740	0.98	0.50	0.238	0.111	0.668	0.335	
10/12/2013 9:12	0913-111_A	13_10_12_0912_04_061	1	0.931	0.461	1.45	0.0640	0.553	0.0740	0.98	0.50	0.238	0.115	0.668	0.337	
10/12/2013 9:13	0913-111_A	13_10_12_0913_04_821	1	0.931	0.456	1.51	0.0650	0.543	0.0740	0.98	0.50	0.344	0.115	0.668	0.338	
10/12/2013 9:14	0913-111_A	13_10_12_0914_05_631	1	1.19	0.468	1.48	0.0630	0.513	0.0750	0.98	0.50	0.306	0.115	0.668	0.344	
10/12/2013 9:15	0913-111_A	13_10_12_0915_06_381	1	0.931	0.477	1.43	0.0640	0.522	0.0720	0.98	0.50	0.442	0.115	0.668	0.353	
10/12/2013 9:16	0913-111_A	13_10_12_0916_06_991	1	0.931	0.459	1.47	0.0640	0.484	0.0710	0.98	0.50	0.425	0.114	0.666	0.337	
10/12/2013 9:17	0913-111_A	13_10_12_0917_07_721	1	0.931	0.443	1.52	0.0700	0.524	0.0720	0.98	0.50	0.242	0.122	0.668	0.322	
10/12/2013 9:18	0913-111_A	13_10_12_0918_08_531	1	0.931	0.470	1.47	0.0680	0.515	0.0700	0.98	0.51	0.257	0.117	0.668	0.345	
10/12/2013 9:19	0913-111_A	13_10_12_0919_09_252	1	0.931	0.485	1.69	0.0640	0.581	0.0740	0.98	0.51	0.527	0.119	0.668	0.352	
10/12/2013 9:20	0913-111_A	13_10_12_0920_09_962	1	0.931	0.473	1.50	0.0650	0.348	0.0740	0.98	0.51	0.342	0.122	0.668	0.343	
10/12/2013 9:21	0913-111_A	13_10_12_0921_10_712	1	0.931	0.480	1.53	0.0620	0.634	0.0770	0.98	0.51	0.467	0.117	0.668	0.354	
10/12/2013 9:22	0913-111_A	13_10_12_0922_11_562	1	0.931	0.487	1.64	0.0700	0.574	0.0750	0.98	0.51	0.356	0.123	0.668	0.368	
10/12/2013 9:23	0913-111_A	13_10_12_0923_12_282	1	0.931	0.481	1.52	0.0810	0.620	0.0750	0.98	0.51	0.523	0.114	0.668	0.340	
10/12/2013 9:24	0913-111_A	13_10_12_0924_13_062	1	1.31	0.472	1.51	0.0640	0.608	0.0730	0.98	0.51	0.505	0.120	0.666	0.344	
10/12/2013 9:25	0913-111_A	13_10_12_0925_13_802	1	0.931	0.471	1.50	0.0610	0.611	0.0730	0.98	0.51	0.532	0.118	0.668	0.348	
10/12/2013 9:26	0913-111_A	13_10_12_0926_14_512	1	1.14	0.468	1.44	0.0680	0.681	0.0780	0.98	0.51	0.281	0.120	0.668	0.340	
10/12/2013 9:27	0913-111_A	13_10_12_0927_15_282	1	0.931	0.471	1.41	0.0640	0.518	0.0740	0.98	0.51	0.320	0.113	0.668	0.348	
10/12/2013 9:28	0913-111_A	13_10_12_0928_16_062	1	0.931	0.457	1.51	0.0630	0.548	0.0750	0.98	0.51	0.328	0.117	0.668	0.353	
10/12/2013 9:29	0913-111_A	13_10_12_0929_16_802	1	0.931	0.478	1.43	0.0660	0.568	0.0740	0.98	0.51	0.368	0.115	0.668	0.343	
10/12/2013 9:30	0913-111_A	13_10_12_0930_17_502	1	0.931	0.475	1.50	0.0670	0.570	0.0750	0.98	0.51	0.238	0.122	0.668	0.355	
10/12/2013 9:31	0913-111_A	13_10_12_0931_18_263	1	0.931	0.487	1.54	0.0680	0.600	0.0740	0.98	0.51	0.412	0.124	0.666	0.358	
10/12/2013 9:32	0913-111_A	13_10_12_0932_19_013	1	0.931	0.471	1.39	0.0650	0.511	0.0750	0.98	0.51	0.348	0.124	0.668	0.351	
10/12/2013 9:33	0913-111_A	13_10_12_0933_19_773	1	0.931	0.483	1.61	0.0650	0.626	0.0760	0.98	0.51	0.520	0.124	0.668	0.381	
10/12/2013 9:34	0913-111_A	13_10_12_0934_20_553	1	0.931	0.465	1.51	0.0660	0.570	0.0750	0.98	0.52	0.478	0.123	0.668	0.340	
10/12/2013 9:35	0913-111_A	13_10_12_0935_21_313	1	1.44	0.481	1.53	0.0690	0.660	0.0780	0.98	0.51	0.475	0.121	0.668	0.358	
10/12/2013 9:36	0913-111_A	13_10_12_0936_22_033	1	1.08	0.488	1.48	0.0630	0.588	0.0760	0.98	0.51	0.522	0.122	0.668	0.353	
10/12/2013 9:37	0913-111_A	13_10_12_0937_22_823	1	0.931	0.481	1.42	0.0700	0.585	0.0780	1.01	0.51	0.370	0.121	0.668	0.362	
10/12/2013 9:38	0913-111_A	13_10_12_0938_23_533	1	0.931	0.478	1.39	0.0630	0.543	0.0780	0.99	0.51	0.519	0.116	0.668	0.348	
10/12/2013 9:39	0913-111_A	13_10_12_0939_24_263	1	0.931	0.469	1.38	0.0680	0.609	0.0770	1.02	0.51	0.450	0.115	0.668	0.346	
10/12/2013 9:40	0913-111_A	13_10_12_0940_25_023	1	0.931	0.478	1.39	0.0630	0.548	0.0740	1.03	0.51	0.568	0.118	0.668	0.349	
10/12/2013 9:41	0913-111_A	13_10_12_0941_25_743	1	0.931	0.468	1.27	0.0630	0.612	0.0720	0.98	0.51	0.238	0.114	0.668	0.344	
10/12/2013 9:42	0913-111_A	13_10_12_0942_26_543	1	0.931	0.475	1.36	0.0640	0.510	0.0790	0.99	0.51	0.480	0.118	0.668	0.351	
10/12/2013 9:43	0913-111_A	13_10_12_0943_27_234	1	0.931	0.448	1.37	0.0660	0.502	0.0720	1.00	0.50	0.439	0.114	0.668	0.328	
10/12/2013 9:44	0913-111_A	13_10_12_0944_28_084	1	0.931	0.468	1.48	0.0610	0.517	0.0740	0.98	0.51	0.468	0.118	0.668	0.343	
10/12/2013 9:45	0913-111_A	13_10_12_0945_28_774	1	0.931	0.428	1.37	0.0610	0.502	0.0740	0.99	0.50	0.423	0.114	0.668	0.324	
10/12/2013 9:46	0913-111_A	13_10_12_0946_29_534	1	0.931	0.487	1.30	0.0680	0.518	0.0730	1.05	0.51	0.352	0.121	0.668	0.356	
10/12/2013 9:47	0913-111_A	13_10_12_0947_30_304	1	0.931	0.472	1.32	0.0650	0.497	0.0750	1.05	0.51	0.241	0.116	0.668	0.344	
10/12/2013 9:48	0913-111_A	13_10_12_0948_31_074	1	1.12	0.487	1.27	0.0640	0.492	0.0750	1.03	0.51	0.402	0.115	0.668	0.359	
10/12/2013 9:49	0913-111_A	13_10_12_0949_31_774	1	1.09	0.461	1.47	0.0600	0.528	0.0730	1.08	0.51	0.505	0.113	0.668	0.335	
10/12/2013 9:50	0913-111_A	13_10_12_0950_32_464	1	0.931	0.453	1.26	0.0650	0.505	0.0750	1.06	0.51	0.348	0.117	0.668	0.329	
10/12/2013 9:51	0913-111_A	13_10_12_0951_33_294	1	0.931	0.471	1.29	0.0630	0.571	0.0770	1.04	0.51	0.389	0.117	0.668	0.351	
10/12/2013 9:52	0913-111_A	13_10_12_0952_34_074	1	1.20	0.470	1.30	0.0610	0.563	0.0730	1.09	0.51	0.402	0.120	0.668	0.346	
10/12/2013 9:53	0913-111_A	13_10_12_0953_34_784	1	0.931	0.483	1.37	0.0630	0.527	0.0740	1.02	0.51	0.565	0.118	0.668	0.343	
10/12/2013 9:54	0913-111_A	13_10_12_0954_35_514	1	0.931	0.477	1.37	0.0690	0.563	0.0720	1.03	0.51	0.238	0.123	0.668	0.362	
10/12/2013 9:55	0913-111_A	13_10_12_0955_36_284	1	0.931	0.468	1.48	0.0630	0.497	0.0750	1.41	0.51	0.462	0.123	0.668	0.348	
10/12/2013 9:56	0913-111_A	13_10_12_0956_36_956	1	0.931	0.446	1.33	0.0620	0.388	0.0760	1.09	0.51	0.573	0.115	0.668	0.328	
10/12/2013 9:57	0913-111_A	13_10_12_0957_37_746	1	0.931	0.484	1.46	0.0640	0.523	0.0750	1.08	0.51	0.519	0.119	0.668	0.345	
10/12/2013 9:58	0913-111_A	13_10_12_0958_38_366	1	0.931	0.490	1.38	0.0650	0.534	0.0750	1.10	0.51	0.448	0.121	0.668	0.330	
Average Conc. (ppm):				1	0.976	0.467	1.44	0.0646	0.537	0.0738	1.00	0.60	0.381	0.118	0.681	0.344

Pellet Cooler 1 Run 2

Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 10:22	0913-111_A	13_10_12_1022_56_297	1	0.931	0.480	1.58	0.0660	0.307	0.0760	0.98	0.51	0.236	0.126	0.668	0.354
10/12/2013 10:23															

Company ACT
 Analyst Initials: JLT
 Parameters: EPA Method 320
 # Samples: 21 Runs

Client # 1911
 Job # 010111
 PO # 1314 1911
 Report Date: 10/02 13.10.18.12.58

Pellet Cooler 1 Run 3

Date	Method	Filename	DF	Aroclor (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/12/2013 11:41	0913-111_A	13_10_12_1141_54_484	1	0.967	0.469	1.43	0.940	0.316	0.0690	0.96	0.48	0.236	0.118	0.666	0.340	
10/12/2013 11:42	0913-111_A	13_10_12_1142_55_184	1	0.931	0.471	1.18	0.930	0.282	0.0710	0.98	0.48	0.236	0.114	0.905	0.345	
10/12/2013 11:43	0913-111_A	13_10_12_1143_56_874	1	1.57	0.480	1.16	0.900	0.327	0.0690	0.98	0.47	0.236	0.119	0.844	0.352	
10/12/2013 11:44	0913-111_A	13_10_12_1144_56_874	1	1.69	0.446	1.19	0.970	0.311	0.0700	0.98	0.48	0.236	0.120	0.905	0.329	
10/12/2013 11:45	0913-111_A	13_10_12_1145_57_474	1	1.18	0.455	1.20	0.930	0.402	0.0710	0.98	0.48	0.236	0.117	0.888	0.337	
10/12/2013 11:46	0913-111_A	13_10_12_1146_58_174	1	1.31	0.467	1.15	0.950	0.472	0.0720	0.98	0.48	0.236	0.119	0.888	0.348	
10/12/2013 11:47	0913-111_A	13_10_12_1147_58_954	1	1.52	0.463	1.23	0.930	0.368	0.0990	0.98	0.48	0.236	0.119	0.888	0.336	
10/12/2013 11:48	0913-111_A	13_10_12_1148_59_814	1	1.10	0.447	1.38	0.950	0.333	0.0710	0.98	0.48	0.236	0.118	0.888	0.333	
10/12/2013 11:50	0913-111_A	13_10_12_1150_00_524	1	1.41	0.478	1.43	0.920	0.400	0.0690	0.98	0.48	0.236	0.121	1.13	0.351	
10/12/2013 11:51	0913-111_A	13_10_12_1151_01_374	1	1.84	0.467	1.33	0.9870	0.385	0.0670	0.98	0.48	0.236	0.118	0.666	0.347	
10/12/2013 11:52	0913-111_A	13_10_12_1152_02_144	1	1.21	0.468	1.35	0.950	0.367	0.0590	0.98	0.48	0.236	0.119	0.888	0.344	
10/12/2013 11:53	0913-111_A	13_10_12_1153_02_904	1	1.13	0.475	1.40	0.990	0.294	0.0700	0.98	0.48	0.236	0.127	0.886	0.353	
10/12/2013 11:54	0913-111_A	13_10_12_1154_03_616	1	1.22	0.478	1.53	0.960	0.449	0.0710	0.98	0.49	0.236	0.129	0.978	0.348	
10/12/2013 11:55	0913-111_A	13_10_12_1155_04_416	1	1.43	0.472	1.51	0.990	0.356	0.0730	0.98	0.48	0.236	0.126	0.888	0.341	
10/12/2013 11:56	0913-111_A	13_10_12_1156_05_116	1	1.14	0.462	1.36	0.970	0.419	0.0700	0.98	0.48	0.236	0.122	0.886	0.348	
10/12/2013 11:57	0913-111_A	13_10_12_1157_05_822	1	0.932	0.444	1.41	0.950	0.344	0.0700	0.98	0.48	0.236	0.119	0.886	0.350	
10/12/2013 11:58	0913-111_A	13_10_12_1158_06_836	1	1.06	0.481	1.38	0.920	0.274	0.0680	0.98	0.48	0.236	0.123	0.688	0.351	
10/12/2013 11:59	0913-111_A	13_10_12_1159_07_346	1	0.931	0.461	1.37	0.980	0.336	0.0690	0.98	0.48	0.236	0.126	0.657	0.343	
10/12/2013 12:00	0913-111_A	13_10_12_1200_06_136	1	2.15	0.484	1.38	0.980	0.316	0.0680	0.98	0.48	0.236	0.124	0.665	0.356	
10/12/2013 12:01	0913-111_A	13_10_12_1201_08_906	1	1.29	0.452	1.45	0.940	0.327	0.0730	0.98	0.48	0.236	0.118	0.688	0.335	
10/12/2013 12:02	0913-111_A	13_10_12_1202_09_826	1	1.70	0.444	1.33	0.960	0.304	0.0680	0.98	0.48	0.236	0.117	0.688	0.327	
10/12/2013 12:03	0913-111_A	13_10_12_1203_10_386	1	1.24	0.434	1.22	0.900	0.353	0.0680	0.98	0.48	0.236	0.114	0.688	0.323	
10/12/2013 12:04	0913-111_A	13_10_12_1204_11_136	1	0.931	0.458	1.37	0.950	0.304	0.0700	0.98	0.48	0.236	0.117	0.709	0.328	
10/12/2013 12:05	0913-111_A	13_10_12_1205_11_766	1	2.02	0.471	1.33	0.950	0.376	0.0710	0.98	0.48	0.236	0.123	1.10	0.345	
10/12/2013 12:06	0913-111_A	13_10_12_1206_12_506	1	1.21	0.430	1.30	0.920	0.389	0.0690	0.98	0.48	0.236	0.114	0.888	0.321	
10/12/2013 12:07	0913-111_A	13_10_12_1207_13_246	1	0.931	0.485	1.44	0.980	0.308	0.0680	0.98	0.48	0.236	0.118	0.688	0.354	
10/12/2013 12:08	0913-111_A	13_10_12_1208_14_966	1	1.08	0.471	1.28	0.980	0.316	0.0680	0.98	0.48	0.236	0.117	0.709	0.328	
10/12/2013 12:09	0913-111_A	13_10_12_1209_14_766	1	1.21	0.447	1.21	0.9570	0.308	0.0680	0.98	0.48	0.236	0.114	0.780	0.331	
10/12/2013 12:10	0913-111_A	13_10_12_1210_15_476	1	2.17	0.465	1.12	0.930	0.315	0.0690	0.98	0.47	0.236	0.118	0.688	0.353	
10/12/2013 12:11	0913-111_A	13_10_12_1211_16_216	1	1.08	0.471	1.15	0.980	0.340	0.0670	0.98	0.47	0.236	0.115	0.888	0.350	
10/12/2013 12:12	0913-111_A	13_10_12_1212_16_976	1	0.931	0.437	1.05	0.920	0.366	0.0700	0.98	0.47	0.236	0.117	0.882	0.317	
10/12/2013 12:13	0913-111_A	13_10_12_1213_17_736	1	0.931	0.447	1.12	0.980	0.288	0.0670	0.98	0.47	0.236	0.118	0.874	0.331	
10/12/2013 12:14	0913-111_A	13_10_12_1214_18_466	1	2.48	0.475	1.17	0.980	0.253	0.0690	0.98	0.47	0.236	0.117	0.888	0.357	
10/12/2013 12:15	0913-111_A	13_10_12_1215_19_276	1	1.74	0.455	1.13	0.951	0.251	0.0680	0.98	0.47	0.236	0.121	0.888	0.356	
10/12/2013 12:16	0913-111_A	13_10_12_1216_19_986	1	1.72	0.479	1.21	0.970	0.294	0.0670	0.98	0.47	0.236	0.119	0.888	0.354	
10/12/2013 12:17	0913-111_A	13_10_12_1217_20_746	1	1.29	0.488	1.19	0.960	0.288	0.0700	0.98	0.47	0.236	0.118	1.06	0.349	
10/12/2013 12:18	0913-111_A	13_10_12_1218_21_467	1	0.931	0.483	1.29	0.930	0.375	0.0700	0.98	0.48	0.236	0.117	1.01	0.351	
10/12/2013 12:19	0913-111_A	13_10_12_1219_22_226	1	0.91	0.491	1.24	0.960	0.368	0.0670	0.98	0.48	0.236	0.118	0.688	0.353	
10/12/2013 12:20	0913-111_A	13_10_12_1220_23_037	1	1.58	0.461	1.21	0.950	0.408	0.0680	0.98	0.47	0.236	0.116	0.753	0.342	
10/12/2013 12:21	0913-111_A	13_10_12_1221_23_787	1	0.931	0.476	1.32	0.920	0.342	0.0670	0.98	0.47	0.236	0.114	0.778	0.336	
10/12/2013 12:22	0913-111_A	13_10_12_1222_24_527	1	1.59	0.481	1.24	0.980	0.333	0.0690	0.98	0.47	0.236	0.120	0.888	0.350	
10/12/2013 12:23	0913-111_A	13_10_12_1223_25_227	1	0.931	0.477	1.07	0.940	0.348	0.0680	0.98	0.47	0.236	0.119	0.743	0.348	
10/12/2013 12:24	0913-111_A	13_10_12_1224_25_967	1	1.50	0.467	1.21	0.930	0.463	0.0670	0.98	0.47	0.236	0.117	0.734	0.355	
10/12/2013 12:25	0913-111_A	13_10_12_1225_26_787	1	1.09	0.496	1.39	0.930	0.383	0.0690	0.98	0.47	0.236	0.116	0.688	0.341	
10/12/2013 12:26	0913-111_A	13_10_12_1226_27_507	1	1.74	0.476	1.23	0.980	0.360	0.0680	0.98	0.47	0.236	0.119	0.888	0.355	
10/12/2013 12:27	0913-111_A	13_10_12_1227_28_287	1	1.80	0.477	1.11	0.940	0.418	0.0680	0.98	0.47	0.236	0.118	0.759	0.350	
10/12/2013 12:28	0913-111_A	13_10_12_1228_29_047	1	1.83	0.475	1.18	0.960	0.458	0.0680	0.98	0.47	0.236	0.118	0.688	0.346	
10/12/2013 12:29	0913-111_A	13_10_12_1229_29_787	1	1.30	0.474	1.30	0.960	0.411	0.0690	0.98	0.47	0.236	0.115	0.790	0.350	
10/12/2013 12:30	0913-111_A	13_10_12_1230_30_487	1	1.42	0.468	1.22	0.940	0.370	0.0680	0.98	0.47	0.236	0.113	0.688	0.346	
10/12/2013 12:31	0913-111_A	13_10_12_1231_31_288	1	1.20	0.471	1.20	0.960	0.362	0.0680	0.98	0.47	0.236	0.119	0.765	0.355	
10/12/2013 12:32	0913-111_A	13_10_12_1232_31_988	1	1.31	0.464	1.17	0.960	0.328	0.0680	0.98	0.47	0.236	0.115	0.718	0.346	
10/12/2013 12:33	0913-111_A	13_10_12_1233_32_748	1	1.21	0.464	1.26	0.960	0.388	0.0680	0.98	0.47	0.236	0.113	0.688	0.338	
10/12/2013 12:34	0913-111_A	13_10_12_1234_33_488	1	1.45	0.468	1.13	0.970	0.327	0.0680	0.98	0.47	0.236	0.118	0.688	0.346	
10/12/2013 12:35	0913-111_A	13_10_12_1235_34_248	1	1.28	0.462	1.22	0.930	0.414	0.0700	0.98	0.47	0.236	0.117	1.07	0.344	
10/12/2013 12:36	0913-111_A	13_10_12_1236_35_008	1	1.59	0.462	1.28	0.950	0.370	0.0700	0.98	0.47	0.236	0.116	0.777	0.351	
10/12/2013 12:38	0913-111_A	13_10_12_1238_39_800	1	2.01	0.489	1.29	0.950	0.305	0.0680	0.98	0.47	0.236	0.118	0.688	0.346	
10/12/2013 12:39	0913-111_A	13_10_12_1239_40_540	1	1.63	0.485	1.18	0.940	0.248	0.0680	0.98	0.47	0.236	0.119	0.888	0.346	
10/12/2013 12:40	0913-111_A	13_10_12_1240_51_220	1	0.931	0.461	1.19	0.960	0.289	0.0680	0.98	0.47	0.236	0.116	0.688	0.346	
10/12/2013 12:41	0913-111_A	13_10_12_1241_51_930	1	1.45	0.462	1.03	0.970	0.350	0.0740	0.98	0.47	0.236	0.118	0.832	0.351	
Average Conc. (ppm):				1	1.35	0.467	1.28	0.9647	0.351	0.0690	0.88	0.48	0.236	0.118	0.769	0.345

Aspirator Run 1

Date	Method	Filename	DF	Aroclor (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 15:09	0913-111_A	13_10_12_1509_17_838	1	1.75	0.783	1.05	0.904	8.72	0.236	2.73	0.98	3.00	1.44	4.85	0.583
10/12/2013 15:10	0913-111_A	13_10_12_1510_18_588	1	3.53	0.815	1.05	0.990	8.01	0.233	2.73	1.02	3.00	1.43	4.37	0.609
10/12/2013 15:11	0913-111_A	13_10_12_1511_19_338	1	2.85											

Company ACT
Analyst Initials CJT
Parameters: EPA Method 320
Samples: 21 Runs

Client # 1911
Job # 0913411
PO # 3134 1911
Report Date V0.62 12.10.18.12.58

Aspirator Run 2		Client # 1911													
Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 18:36	0913-111_A	13_10_12_1638_22_016	1	2.99	0.831	1.26	0.505	8.21	0.237	1.31	3.00	1.47	4.99	0.821	
10/12/2013 18:37	0913-111_A	13_10_12_1637_22_786	1	3.74	0.820	1.54	0.511	8.34	0.282	2.73	1.64	3.00	1.46	4.01	0.514
10/12/2013 18:38	0913-111_A	13_10_12_1638_22_566	1	7.83	0.843	1.44	0.563	8.87	0.299	2.73	1.43	3.00	1.56	4.72	0.830
10/12/2013 18:39	0913-111_A	13_10_12_1639_24_388	1	3.46	0.860	1.49	0.557	8.84	0.303	2.73	1.50	3.00	1.57	4.58	0.636
10/12/2013 18:40	0913-111_A	13_10_12_1640_28_058	1	3.99	0.838	1.41	0.559	8.50	0.258	2.73	1.31	3.00	1.60	5.02	0.617
10/12/2013 18:41	0913-111_A	13_10_12_1641_28_868	1	3.44	0.843	1.29	0.538	8.46	0.270	2.73	1.31	3.00	1.55	5.08	0.832
10/12/2013 18:42	0913-111_A	13_10_12_1642_28_526	1	2.86	0.785	1.34	0.522	8.81	0.287	2.73	1.38	3.00	1.44	4.99	0.587
10/12/2013 18:43	0913-111_A	13_10_12_1643_27_336	1	2.73	0.797	1.45	0.494	8.65	0.270	2.73	1.81	3.00	1.38	4.46	0.937
10/12/2013 18:44	0913-111_A	13_10_12_1644_28_088	1	3.31	0.817	1.50	0.478	8.58	0.271	2.73	1.78	3.00	1.47	3.89	0.612
10/12/2013 18:45	0913-111_A	13_10_12_1645_28_828	1	2.82	0.785	1.68	0.489	8.67	0.272	2.73	1.68	3.00	1.35	4.60	0.582
10/12/2013 18:46	0913-111_A	13_10_12_1646_29_538	1	2.91	0.798	1.55	0.479	8.99	0.292	2.73	1.80	3.00	1.27	4.85	0.587
10/12/2013 18:47	0913-111_A	13_10_12_1647_30_358	1	3.94	0.795	1.64	0.471	8.81	0.285	2.73	1.54	3.00	1.30	4.70	0.591
10/12/2013 18:48	0913-111_A	13_10_12_1648_31_017	1	4.04	0.784	1.47	0.467	8.88	0.287	2.73	1.48	3.00	1.33	4.72	0.589
10/12/2013 18:49	0913-111_A	13_10_12_1649_31_837	1	2.86	0.770	1.43	0.465	8.94	0.282	2.73	1.47	3.00	1.30	4.44	0.587
10/12/2013 18:50	0913-111_A	13_10_12_1650_30_607	1	3.01	0.803	1.46	0.466	9.04	0.282	2.73	1.55	3.00	1.33	3.88	0.594
10/12/2013 18:51	0913-111_A	13_10_12_1651_33_377	1	2.63	0.782	1.61	0.458	8.98	0.250	2.73	2.12	3.00	1.31	3.80	0.591
10/12/2013 18:52	0913-111_A	13_10_12_1652_33_977	1	3.25	0.810	1.63	0.462	9.03	0.254	2.73	1.83	3.00	1.33	3.87	0.588
10/12/2013 18:53	0913-111_A	13_10_12_1653_34_787	1	3.78	0.796	1.59	0.468	8.20	0.266	2.73	1.83	3.00	1.33	4.16	0.591
10/12/2013 18:54	0913-111_A	13_10_12_1654_35_477	1	3.78	0.797	1.52	0.461	9.20	0.263	2.73	1.80	3.00	1.35	3.91	0.594
10/12/2013 18:55	0913-111_A	13_10_12_1655_36_207	1	3.31	0.775	1.87	0.458	8.96	0.254	2.73	1.82	3.00	1.30	3.30	0.577
10/12/2013 18:56	0913-111_A	13_10_12_1656_38_947	1	3.44	0.780	1.50	0.458	9.07	0.258	2.73	1.84	3.00	1.28	3.80	0.582
10/12/2013 18:57	0913-111_A	13_10_12_1657_31_757	1	2.86	0.770	1.40	0.447	9.14	0.261	2.73	1.42	3.00	1.28	4.10	0.571
10/12/2013 18:58	0913-111_A	13_10_12_1658_36_477	1	4.04	0.788	1.32	0.450	9.13	0.261	2.73	1.35	3.00	1.28	4.10	0.571
10/12/2013 18:59	0913-111_A	13_10_12_1659_38_217	1	3.22	0.792	1.32	0.441	9.08	0.270	2.73	1.28	3.00	1.28	4.55	0.595
10/12/2013 19:00	0913-111_A	13_10_12_1660_40_018	1	2.87	0.787	1.37	0.448	8.89	0.215	2.73	1.27	3.00	1.32	4.41	0.579
10/12/2013 19:01	0913-111_A	13_10_12_1661_40_728	1	3.25	0.821	1.49	0.451	9.28	0.259	2.73	1.49	3.00	1.29	4.13	0.614
10/12/2013 19:02	0913-111_A	13_10_12_1662_41_438	1	3.27	0.779	1.85	0.451	9.18	0.252	2.73	1.67	3.00	1.31	3.50	0.602
10/12/2013 19:03	0913-111_A	13_10_12_1663_42_208	1	3.09	0.814	1.71	0.459	9.05	0.257	2.73	1.89	3.00	1.29	4.19	0.607
10/12/2013 19:04	0913-111_A	13_10_12_1664_42_928	1	3.58	0.811	1.46	0.464	8.45	0.221	2.73	1.33	3.00	1.38	3.67	0.606
10/12/2013 19:05	0913-111_A	13_10_12_1665_43_758	1	2.79	0.814	1.41	0.471	8.13	0.268	2.73	1.37	3.00	1.36	4.20	0.588
10/12/2013 19:06	0913-111_A	13_10_12_1666_44_468	1	3.01	0.782	1.63	0.477	8.01	0.289	2.73	1.41	3.00	1.40	4.28	0.595
10/12/2013 19:07	0913-111_A	13_10_12_1667_45_238	1	3.91	0.800	1.57	0.489	8.57	0.230	2.73	1.48	3.00	1.36	4.01	0.604
10/12/2013 19:08	0913-111_A	13_10_12_1668_46_018	1	3.00	0.803	1.52	0.481	8.59	0.259	2.73	1.46	3.00	1.36	4.01	0.604
10/12/2013 19:09	0913-111_A	13_10_12_1669_46_708	1	2.61	0.787	1.68	0.468	8.99	0.267	2.73	1.87	3.00	1.33	4.46	0.606
10/12/2013 19:10	0913-111_A	13_10_12_1670_47_548	1	2.65	0.813	1.97	0.442	8.88	0.247	2.73	1.90	3.00	1.26	3.63	0.580
10/12/2013 19:11	0913-111_A	13_10_12_1671_48_248	1	3.22	0.776	1.67	0.441	9.04	0.255	2.73	1.67	3.00	1.27	3.31	0.589
10/12/2013 19:12	0913-111_A	13_10_12_1672_49_038	1	3.03	0.828	1.75	0.447	9.29	0.263	2.73	1.58	3.00	1.29	3.28	0.612
10/12/2013 19:13	0913-111_A	13_10_12_1673_49_798	1	3.28	0.802	1.78	0.451	9.21	0.259	2.73	1.59	3.00	1.30	3.77	0.597
10/12/2013 19:14	0913-111_A	13_10_12_1674_50_538	1	3.39	0.772	1.72	0.450	8.88	0.282	2.73	1.46	3.00	1.31	3.84	0.576
10/12/2013 19:15	0913-111_A	13_10_12_1675_51_278	1	2.99	0.794	1.88	0.464	8.99	0.285	2.73	1.47	3.00	1.33	4.39	0.587
10/12/2013 19:16	0913-111_A	13_10_12_1676_52_038	1	3.58	0.820	1.52	0.472	8.83	0.267	2.73	1.44	3.00	1.34	4.59	0.606
10/12/2013 19:17	0913-111_A	13_10_12_1677_52_748	1	2.91	0.839	1.78	0.460	8.84	0.270	2.73	1.58	3.00	1.36	4.61	0.621
10/12/2013 19:18	0913-111_A	13_10_12_1678_53_548	1	3.25	0.828	1.78	0.481	8.89	0.247	2.73	2.10	3.00	1.27	3.25	0.617
10/12/2013 19:19	0913-111_A	13_10_12_1679_54_258	1	2.16	0.804	2.08	0.455	8.72	0.240	2.73	2.10	3.00	1.28	3.28	0.604
10/12/2013 19:20	0913-111_A	13_10_12_1680_55_018	1	2.67	0.829	2.13	0.454	8.69	0.255	2.73	1.89	3.00	1.29	3.57	0.620
10/12/2013 19:21	0913-111_A	13_10_12_1681_55_908	1	2.49	0.800	1.80	0.427	8.19	0.287	2.73	1.80	3.00	1.26	3.85	0.594
10/12/2013 19:22	0913-111_A	13_10_12_1682_56_868	1	2.88	0.787	1.57	0.433	9.28	0.258	2.73	1.45	3.00	1.26	3.74	0.582
10/12/2013 19:23	0913-111_A	13_10_12_1683_57_728	1	2.15	0.763	1.68	0.417	9.16	0.251	2.73	1.38	3.00	1.21	3.44	0.567
10/12/2013 19:24	0913-111_A	13_10_12_1684_58_588	1	2.76	0.784	1.64	0.445	8.76	0.265	2.73	1.59	3.00	1.27	3.15	0.583
10/12/2013 19:25	0913-111_A	13_10_12_1685_59_448	1	2.16	0.785	1.71	0.444	9.38	0.251	2.73	1.54	3.00	1.27	3.27	0.572
10/12/2013 19:26	0913-111_A	13_10_12_1686_60_308	1	3.25	0.779	1.79	0.428	8.54	0.228	2.73	1.92	3.00	1.24	3.22	0.578
10/12/2013 19:27	0913-111_A	13_10_12_1687_61_168	1	2.88	0.759	2.03	0.424	8.98	0.256	2.73	2.41	3.00	1.18	2.94	0.570
10/12/2013 19:28	0913-111_A	13_10_12_1688_62_028	1	2.64	0.822	1.84	0.434	8.68	0.244	2.73	1.81	3.00	1.24	2.82	0.578
10/12/2013 19:29	0913-111_A	13_10_12_1689_62_888	1	1.92	0.786	1.45	0.447	9.18	0.257	2.73	1.20	3.00	1.30	3.78	0.592
10/12/2013 19:30	0913-111_A	13_10_12_1690_63_748	1	2.86	0.812	1.29	0.455	8.76	0.213	2.73	1.39	3.00	1.33	4.28	0.587
10/12/2013 19:31	0913-111_A	13_10_12_1691_64_608	1	3.12	0.788	1.43	0.462	8.13	0.259	2.73	1.44	3.00	1.32	3.79	0.599
10/12/2013 19:32	0913-111_A	13_10_12_1692_65_468	1	3.74	0.798	1.49	0.459	8.68	0.256	2.73	1.42	3.00	1.32	3.90	0.602
10/12/2013 19:33	0913-111_A	13_10_12_1693_66_328	1	3.29	0.835	1.53	0.457	8.52	0.254	2.73	1.62	3.00	1.31	3.72	0.595
10/12/2013 19:34	0913-111_A	13_10_12_1694_67_188	1	2.96	0.815	1.88	0.448	8.75	0.232	2.73	2.24	3.00	1.25	2.83	0.606
10/12/2013 19:35	0913-111_A	13_10_12_1695_68_048	1	3.24	1.19	1.65	0.523	8.25	0.181	2.73	1.31	3.00	1.27	1.27	0.919
Average Conc. (ppm):			1	3.12	0.808	1.58	0.467	8.90	0.256	2.73	1.60	3.00	1.36	3.92	0.602

Aspirator Run 3		Client # 1911													
Date	Method	Filename	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/12/2013 18:00	0913-111_A	13_10_12_1800_35_741	1	2.53	0.845	1.06	0.520	7.94	0.225	2.73	1.17	3.00	1.48	3.73	0.627
10/12/2013 18:01	0913-111_A	13_10_12_1801_37_551	1	2.68	0.859	1.05	0.504	8.15	0.224	2.73	1.04	3.00	1.45	3.52	0.631
10/12/2013 18:02	0913-111_A	13_10_12_1802_38_261	1	2.74	0.806	1.05	0.500	8.25	0.225	2.73	1.07	3.00	1.43	3.68	0.636
10/12/2013 18:03	0913-111_A	13_10_12_1803_													

Company/ACT
Analyte Initials/CIT
Parameters/EPA Method 320
Samples/21 Runs

Client # 1811
Job # 0913-111
PO # 3134-1811
Report Date 10.02.13.10.18.18.18.58

Dryer 2 Run 1																
Date	Method	File Name	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)	
10/13/2013 9:21	0913-111_A	13_10_13_0921_40_932	1	2.53	0.630	5.62	0.101	17.3	0.524	2.78	0.07	1.37	0.203	1.48	0.474	
10/13/2013 9:22	0913-111_A	13_10_13_0922_41_872	1	1.61	0.616	6.08	0.103	16.4	0.551	2.78	0.08	1.70	0.199	0.985	0.456	
10/13/2013 9:23	0913-111_A	13_10_13_0923_41_382	1	2.02	0.641	6.63	0.108	16.6	0.561	2.78	0.08	1.89	0.207	1.39	0.480	
10/13/2013 9:24	0913-111_A	13_10_13_0924_42_103	1	1.25	0.624	6.81	0.106	19.9	0.556	2.78	0.07	1.88	0.213	1.17	0.472	
10/13/2013 9:25	0913-111_A	13_10_13_0925_42_893	1	1.84	0.630	7.02	0.104	19.1	0.559	2.78	0.08	1.97	0.210	0.934	0.466	
10/13/2013 9:26	0913-111_A	13_10_13_0926_43_553	1	2.09	0.648	7.27	0.109	19.3	0.565	2.78	0.07	2.02	0.216	1.24	0.486	
10/13/2013 9:27	0913-111_A	13_10_13_0927_44_353	1	1.99	0.652	7.18	0.111	19.5	0.566	2.78	0.08	2.04	0.218	0.934	0.484	
10/13/2013 9:28	0913-111_A	13_10_13_0928_45_093	1	1.92	0.648	7.07	0.108	19.8	0.550	2.78	0.08	2.23	0.214	0.934	0.485	
10/13/2013 9:29	0913-111_A	13_10_13_0929_45_813	1	2.06	0.610	8.71	0.104	19.9	0.545	2.78	0.07	2.22	0.208	1.13	0.453	
10/13/2013 9:30	0913-111_A	13_10_13_0930_46_563	1	1.25	0.620	8.61	0.108	20.0	0.544	2.78	0.08	2.28	0.210	0.934	0.481	
10/13/2013 9:31	0913-111_A	13_10_13_0931_47_433	1	1.25	0.622	6.61	0.107	20.2	0.542	2.78	0.08	2.27	0.213	0.934	0.468	
10/13/2013 9:32	0913-111_A	13_10_13_0932_48_143	1	1.54	0.631	6.32	0.105	20.2	0.544	2.78	0.07	1.92	0.211	0.945	0.472	
10/13/2013 9:33	0913-111_A	13_10_13_0933_48_883	1	1.93	0.638	6.25	0.106	20.2	0.539	2.78	0.08	1.93	0.212	0.934	0.478	
10/13/2013 9:34	0913-111_A	13_10_13_0934_49_573	1	1.25	0.625	5.96	0.109	20.5	0.547	2.78	0.07	1.81	0.238	0.934	0.465	
10/13/2013 9:35	0913-111_A	13_10_13_0935_50_283	1	1.96	0.617	5.68	0.104	20.3	0.529	2.78	0.07	2.12	0.207	0.934	0.457	
10/13/2013 9:36	0913-111_A	13_10_13_0936_51_104	1	2.84	0.624	5.68	0.107	19.9	0.523	2.78	0.07	2.23	0.211	0.934	0.467	
10/13/2013 9:37	0913-111_A	13_10_13_0937_51_824	1	1.88	0.617	5.55	0.101	19.1	0.516	2.78	0.08	2.16	0.207	0.934	0.480	
10/13/2013 9:38	0913-111_A	13_10_13_0938_52_534	1	1.98	0.614	5.38	0.104	18.8	0.513	2.78	0.07	1.62	0.211	0.934	0.462	
10/13/2013 9:39	0913-111_A	13_10_13_0939_53_284	1	1.45	0.624	5.48	0.101	19.1	0.516	2.78	0.08	2.26	0.209	0.934	0.482	
10/13/2013 9:40	0913-111_A	13_10_13_0940_54_084	1	1.93	0.644	5.40	0.104	19.9	0.517	2.78	0.08	2.30	0.216	0.934	0.479	
10/13/2013 9:41	0913-111_A	13_10_13_0941_54_884	1	2.02	0.611	5.47	0.108	20.4	0.517	2.78	0.08	2.20	0.216	0.934	0.465	
10/13/2013 9:42	0913-111_A	13_10_13_0942_55_594	1	1.97	0.624	5.40	0.107	20.9	0.511	2.78	0.07	2.25	0.213	0.934	0.465	
10/13/2013 9:43	0913-111_A	13_10_13_0943_56_314	1	2.27	0.601	5.23	0.104	21.1	0.513	2.78	0.07	2.09	0.213	0.934	0.448	
10/13/2013 9:44	0913-111_A	13_10_13_0944_57_124	1	1.89	0.614	5.28	0.111	21.2	0.507	2.78	0.08	2.15	0.219	0.934	0.484	
10/13/2013 9:45	0913-111_A	13_10_13_0945_57_884	1	1.87	0.627	5.10	0.105	21.1	0.509	2.78	0.07	1.55	0.213	0.934	0.486	
10/13/2013 9:46	0913-111_A	13_10_13_0946_58_594	1	1.91	0.621	5.13	0.108	21.4	0.514	2.78	0.08	2.32	0.215	0.934	0.464	
10/13/2013 9:47	0913-111_A	13_10_13_0947_59_304	1	1.42	0.595	5.45	0.108	21.7	0.521	2.78	0.08	2.19	0.218	0.934	0.448	
10/13/2013 9:48	0913-111_A	13_10_13_0948_60_105	1	1.88	0.641	5.48	0.110	21.5	0.510	2.78	0.07	2.23	0.220	0.934	0.479	
10/13/2013 9:49	0913-111_A	13_10_13_0949_60_815	1	1.25	0.630	5.56	0.107	21.4	0.517	2.78	0.08	2.22	0.216	0.934	0.465	
10/13/2013 9:50	0913-111_A	13_10_13_0950_61_525	1	1.89	0.645	5.63	0.109	21.6	0.538	2.78	0.08	2.28	0.218	0.934	0.465	
10/13/2013 9:51	0913-111_A	13_10_13_0951_62_235	1	1.82	0.635	6.10	0.109	21.9	0.541	2.78	0.08	2.48	0.225	0.934	0.471	
10/13/2013 9:52	0913-111_A	13_10_13_0952_63_045	1	1.86	0.625	5.99	0.109	21.6	0.539	2.78	0.08	2.37	0.220	0.934	0.466	
10/13/2013 9:53	0913-111_A	13_10_13_0953_63_755	1	1.93	0.623	5.88	0.110	21.9	0.541	2.78	0.07	1.51	0.224	0.934	0.474	
10/13/2013 9:54	0913-111_A	13_10_13_0954_64_465	1	2.47	0.633	6.09	0.110	21.8	0.540	2.78	0.08	2.52	0.222	0.934	0.474	
10/13/2013 9:55	0913-111_A	13_10_13_0955_65_175	1	2.13	0.622	6.19	0.111	21.9	0.539	2.78	0.08	2.58	0.221	0.934	0.467	
10/13/2013 9:56	0913-111_A	13_10_13_0956_65_885	1	1.81	0.614	6.23	0.112	21.9	0.543	2.78	0.08	2.37	0.228	0.934	0.480	
10/13/2013 9:57	0913-111_A	13_10_13_0957_66_595	1	1.40	0.600	6.62	0.113	22.1	0.556	2.78	0.08	2.70	0.229	0.934	0.483	
10/13/2013 9:58	0913-111_A	13_10_13_0958_67_305	1	1.79	0.610	6.83	0.113	22.1	0.555	2.78	0.08	2.62	0.230	0.934	0.487	
10/13/2013 9:59	0913-111_A	13_10_13_0959_68_015	1	1.25	0.640	6.83	0.109	22.1	0.581	2.78	0.08	2.62	0.224	0.934	0.482	
10/13/2013 10:00	0913-111_A	13_10_13_1000_68_725	1	1.28	0.649	7.05	0.110	21.8	0.556	2.78	0.07	2.67	0.234	0.934	0.481	
10/13/2013 10:01	0913-111_A	13_10_13_1001_69_435	1	2.18	0.629	6.96	0.115	21.4	0.546	2.78	0.08	2.63	0.232	0.934	0.473	
10/13/2013 10:02	0913-111_A	13_10_13_1002_70_145	1	2.08	0.678	6.91	0.112	21.2	0.543	2.78	0.08	2.87	0.239	0.934	0.480	
10/13/2013 10:03	0913-111_A	13_10_13_1003_70_855	1	2.56	0.638	6.24	0.114	20.9	0.528	2.78	0.08	2.62	0.231	0.934	0.482	
10/13/2013 10:04	0913-111_A	13_10_13_1004_71_565	1	1.61	0.623	6.90	0.107	20.5	0.525	2.78	0.08	2.66	0.228	0.934	0.486	
10/13/2013 10:05	0913-111_A	13_10_13_1005_72_275	1	2.39	0.625	6.04	0.109	20.8	0.533	2.78	0.08	2.54	0.235	0.934	0.488	
10/13/2013 10:06	0913-111_A	13_10_13_1006_73_085	1	1.78	0.625	6.36	0.111	18.8	0.542	2.78	0.08	2.53	0.228	0.934	0.472	
10/13/2013 10:07	0913-111_A	13_10_13_1007_73_795	1	2.53	0.642	6.82	0.106	18.8	0.540	2.78	0.08	2.58	0.229	0.934	0.480	
10/13/2013 10:08	0913-111_A	13_10_13_1008_74_505	1	2.29	0.634	7.03	0.111	18.5	0.550	2.78	0.08	2.51	0.235	0.934	0.480	
10/13/2013 10:09	0913-111_A	13_10_13_1009_75_215	1	1.44	0.650	7.05	0.111	18.5	0.550	2.78	0.08	2.72	0.231	0.934	0.479	
10/13/2013 10:10	0913-111_A	13_10_13_1010_76_025	1	2.51	0.631	7.06	0.109	14.0	0.549	2.78	0.06	2.44	0.228	0.934	0.484	
10/13/2013 10:11	0913-111_A	13_10_13_1011_76_735	1	1.51	0.631	7.03	0.109	14.0	0.549	2.78	0.06	2.54	0.228	0.934	0.476	
10/13/2013 10:12	0913-111_A	13_10_13_1012_77_445	1	1.46	0.650	7.48	0.107	12.8	0.543	2.78	0.07	2.63	0.225	0.934	0.483	
10/13/2013 10:13	0913-111_A	13_10_13_1013_78_155	1	2.24	0.680	7.25	0.108	11.8	0.536	2.78	0.08	2.71	0.226	0.934	0.480	
10/13/2013 10:14	0913-111_A	13_10_13_1014_78_865	1	2.42	0.677	8.54	0.110	11.0	0.555	2.78	0.08	2.81	0.242	0.934	0.470	
10/13/2013 10:15	0913-111_A	13_10_13_1015_79_575	1	2.16	0.619	7.71	0.106	11.0	0.543	2.78	0.08	2.71	0.225	0.934	0.470	
10/13/2013 10:16	0913-111_A	13_10_13_1016_80_285	1	2.13	0.616	7.44	0.109	11.7	0.549	2.78	0.08	2.42	0.233	0.934	0.486	
10/13/2013 10:17	0913-111_A	13_10_13_1017_81_095	1	1.37	0.621	7.20	0.113	12.8	0.558	2.78	0.08	2.61	0.242	0.934	0.480	
10/13/2013 10:18	0913-111_A	13_10_13_1018_81_805	1	2.79	0.685	7.44	0.110	13.2	0.560	2.78	0.08	2.75	0.255	1.03	0.479	
10/13/2013 10:19	0913-111_A	13_10_13_1019_82_515	1	1.95	0.634	6.71	0.107	12.9	0.550	2.78	0.08	2.64	0.258	0.934	0.471	
10/13/2013 10:20	0913-111_A	13_10_13_1020_83_225	1	2.11	0.594	6.98	0.110	12.8	0.547	2.78	0.08	2.51	0.254	0.934	0.447	
10/13/2013 10:21	0913-111_A	13_10_13_1021_83_935	1	3.00	0.628	6.73	0.113	12.7	0.558	2.78	0.08	2.53	0.273	0.968	0.458	
Average Conc. (ppm):				1	1.90	0.631	6.40	0.108	18.8	0.539	2.78	1.25	2.37	0.222	0.967	0.472

Dryer 2 Run 2															
Date	Method	File Name	DF	Acrolein (ppm)	SEC (ppm)	Formaldehyde (ppm)	SEC (ppm)	Methanol (ppm)	SEC (ppm)	Phenol (ppm)	SEC (ppm)	Propionaldehyde (ppm)	SEC (ppm)	acetaldehyde (ppm)	SEC (ppm)
10/13/2013 11:04	0913-111_A	13_10_13_1104_59_401	1	2.45	0.615	6.06	0.106	10.4	0.532	2.78	1.31	1.47	0.260	3.09	0.457
10/13/2013 11:05	0913-111_A	13_10_13_1105_59_111	1	2.20	0.620	6.60	0.108	10.2	0.535	2.78	1.31	1.35	0.260	3.57	

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
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PO #	3134 1911
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Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_04_850	8.79	0.137
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_23_390	8.77	0.136
10/10/2013 8:12	0913-111_CTS	13_10_10_0812_42_040	8.78	0.137
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_00_420	8.80	0.136
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_18_930	8.82	0.137
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_37_540	8.81	0.138
10/10/2013 8:13	0913-111_CTS	13_10_10_0813_56_040	8.82	0.137
10/10/2013 8:14	0913-111_CTS	13_10_10_0814_14_670	8.80	0.138
Average (m)			8.80	0.137
10/10/2013 19:33	0913-111_CTS	13_10_10_1933_09_783	8.67	0.137
10/10/2013 19:33	0913-111_CTS	13_10_10_1933_28_313	8.69	0.137
10/10/2013 19:33	0913-111_CTS	13_10_10_1933_46_843	8.69	0.138
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_05_353	8.71	0.137
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_23_963	8.70	0.137
10/10/2013 19:34	0913-111_CTS	13_10_10_1934_42_473	8.71	0.138
10/10/2013 19:35	0913-111_CTS	13_10_10_1935_01_103	8.66	0.137
10/10/2013 19:35	0913-111_CTS	13_10_10_1935_19_513	8.67	0.139
Average (m)			8.69	0.138
Average Pathlength (m)			8.74	0.137
Max (m)			8.80	
Min (m)			8.69	
Max % Deviation			0.62%	

Company	ACT
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# Samples	21 Runs

Client #	1911
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Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/11/2013 9:38	0913-111_CTS	13_10_11_0938_33_970	8.13	0.130
10/11/2013 9:38	0913-111_CTS	13_10_11_0938_52_580	8.16	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_11_060	8.17	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_29_540	8.18	0.129
10/11/2013 9:39	0913-111_CTS	13_10_11_0939_48_180	8.19	0.130
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_06_710	8.18	0.129
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_25_190	8.20	0.129
10/11/2013 9:40	0913-111_CTS	13_10_11_0940_43_760	8.18	0.130
Average (m)			8.17	0.129
10/11/2013 11:22	0913-111_CTS	13_10_11_1122_55_958	8.63	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_14_479	8.66	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_32_989	8.68	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_51_519	8.71	0.133
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_10_019	8.70	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_28_559	8.73	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_47_159	8.74	0.134
10/11/2013 11:25	0913-111_CTS	13_10_11_1125_05_659	8.74	0.134
Average (m)			8.70	0.134
Average Pathlength (m)			8.44	0.131
Max (m)			8.70	
Min (m)			8.17	
Max % Deviation			3.10%	

Company	ACT
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Client #	1911
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Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/11/2013 11:22	0913-111_CTS	13_10_11_1122_55_958	8.63	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_14_479	8.66	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_32_989	8.68	0.133
10/11/2013 11:23	0913-111_CTS	13_10_11_1123_51_519	8.71	0.133
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_10_019	8.70	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_28_559	8.73	0.134
10/11/2013 11:24	0913-111_CTS	13_10_11_1124_47_159	8.74	0.134
10/11/2013 11:25	0913-111_CTS	13_10_11_1125_05_659	8.74	0.134
Average (m)			8.70	0.134
10/11/2013 13:02	0913-111_CTS	13_10_11_1302_32_762	8.73	0.133
10/11/2013 13:02	0913-111_CTS	13_10_11_1302_51_282	8.77	0.134
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_09_882	8.73	0.133
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_28_382	8.71	0.133
10/11/2013 13:03	0913-111_CTS	13_10_11_1303_46_792	8.74	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_05_402	8.75	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_23_922	8.74	0.133
10/11/2013 13:04	0913-111_CTS	13_10_11_1304_42_382	8.73	0.133
Average (m)			8.74	0.133
10/11/2013 17:56	0913-111_CTS	13_10_11_1756_33_272	8.44	0.129
10/11/2013 17:56	0913-111_CTS	13_10_11_1756_51_882	8.57	0.130
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_10_412	8.67	0.132
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_29_032	8.71	0.132
10/11/2013 17:57	0913-111_CTS	13_10_11_1757_47_542	8.75	0.132
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_06_042	8.76	0.132
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_24_642	8.79	0.133
10/11/2013 17:58	0913-111_CTS	13_10_11_1758_43_102	8.75	0.133
Average (m)			8.68	0.132
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_05_353	8.70	0.139
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_23_963	8.74	0.139
10/12/2013 7:59	0913-111_CTS	13_10_12_0759_42_473	8.71	0.137
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_01_103	8.70	0.136
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_19_593	8.69	0.137
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_38_103	8.75	0.136
10/12/2013 8:00	0913-111_CTS	13_10_12_0800_56_713	8.68	0.136
10/12/2013 8:01	0913-111_CTS	13_10_12_0801_15_143	8.68	0.136

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

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Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
		Average (m)	8.71	0.137
10/12/2013 8:15	0913-111_CTS	13_10_12_0815_33_684	8.60	0.134
10/12/2013 8:15	0913-111_CTS	13_10_12_0815_52_184	8.59	0.134
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_10_704	8.58	0.134
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_29_314	8.60	0.133
10/12/2013 8:16	0913-111_CTS	13_10_12_0816_47_804	8.60	0.133
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_06_244	8.61	0.134
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_24_834	8.62	0.133
10/12/2013 8:17	0913-111_CTS	13_10_12_0817_43_344	8.59	0.134
		Average (m)	8.60	0.134
10/12/2013 13:02	0913-111_CTS	13_10_12_1302_33_472	8.74	0.137
10/12/2013 13:02	0913-111_CTS	13_10_12_1302_52_082	8.76	0.137
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_10_582	8.79	0.137
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_29_082	8.79	0.138
10/12/2013 13:03	0913-111_CTS	13_10_12_1303_47_602	8.78	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_06_112	8.77	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_24_752	8.78	0.137
10/12/2013 13:04	0913-111_CTS	13_10_12_1304_43_242	8.78	0.138
		Average (m)	8.78	0.137
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_21_772	8.68	0.133
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_40_362	8.71	0.132
10/12/2013 19:42	0913-111_CTS	13_10_12_1942_58_862	8.77	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_17_462	8.77	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_35_992	8.80	0.134
10/12/2013 19:43	0913-111_CTS	13_10_12_1943_54_432	8.79	0.133
10/12/2013 19:44	0913-111_CTS	13_10_12_1944_13_082	8.82	0.135
10/12/2013 19:44	0913-111_CTS	13_10_12_1944_31_502	8.78	0.134
		Average (m)	8.76	0.134
10/13/2013 7:58	0913-111_CTS	13_10_13_0758_40_845	8.55	0.130
10/13/2013 7:58	0913-111_CTS	13_10_13_0758_59_345	8.50	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_17_835	8.49	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_36_445	8.50	0.129
10/13/2013 7:59	0913-111_CTS	13_10_13_0759_54_925	8.49	0.129
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_13_565	8.51	0.130
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_31_995	8.47	0.130

Company	ACT
Analyst Initials	CJT
Parameters	EPA Method 320
# Samples	21 Runs

Client #	1911
Job #	0913-111
PO #	3134 1911
Report Date	V0.62 13.10.18.12.58

Path Length - Path

Date	Method	FileName	ethylene (ppm)	SEC (ppm)
10/13/2013 8:00	0913-111_CTS	13_10_13_0800_50_506	8.52	0.130
Average (m)			8.50	0.130
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_09_687	8.73	0.133
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_28_197	8.69	0.133
10/13/2013 8:16	0913-111_CTS	13_10_13_0816_46_707	8.71	0.134
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_05_247	8.72	0.133
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_23_757	8.73	0.134
10/13/2013 8:17	0913-111_CTS	13_10_13_0817_42_347	8.77	0.134
10/13/2013 8:18	0913-111_CTS	13_10_13_0818_00_857	8.70	0.133
10/13/2013 8:18	0913-111_CTS	13_10_13_0818_19_377	8.74	0.134
Average (m)			8.72	0.134
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_10_233	8.70	0.135
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_28_743	8.73	0.135
10/13/2013 14:34	0913-111_CTS	13_10_13_1434_47_263	8.76	0.136
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_05_884	8.75	0.135
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_24_394	8.72	0.133
10/13/2013 14:35	0913-111_CTS	13_10_13_1435_42_804	8.74	0.135
10/13/2013 14:36	0913-111_CTS	13_10_13_1436_01_424	8.74	0.134
10/13/2013 14:36	0913-111_CTS	13_10_13_1436_19_934	8.72	0.134
Average (m)			8.73	0.135
Average Pathlength (m)			8.69	0.134
Max (m)			8.78	
Min (m)			8.50	
Max % Deviation			2.17%	

APPENDIX D

Method 320 Log Sheet

FTIR Log - Enviva Wiggins

Date	Time	Filename	Method	Pressure	Notes	Run ID
10-Oct	754	13.10.10.0753.42.969	CTS	14.7	Background	
	806	13.10.10.0806.08.036	CTS	14.7	CTS (pathlength = 8.78 m)	
	855	13.10.10.0855.00.744	0913-177A	14.6	Background	
	914	13.10.10.0914.12.674	0913-177A	13.5	Sampling GHM - Run 1 (0917-1017)	1
	1036	13.10.10.0914.12.674	0913-177A	13.3	Sampling GHM - Run 2 (1036-1136)	2
	1150	13.10.10.0914.12.674	0913-177A	13.5	Sampling GHM - Run 3 (1150-1250)	3
	1738	13.10.10.1429.45.242	0913-177A	13.9	Sampling Dryer 1 - Run 1 (1738-1838)	4
	1915	13.10.10.1915.03.541	0913-177A	14.6	Background	
	1923	13.10.10.1923.11.342	CTS	14.6	Background	
	1926	13.10.10.1926.54.274	CTS	14.7	CTS (pathlength = 8.78 m)	
	2005	13.10.10.2004.59.706	0913-177A	14.6	Water Spectra (Dryer 1 - Run 1)	
	2035	13.10.10.2034.59.394	0913-177A	14.6	Water Spectra (GHM)	
	11-Oct	933	13.10.11.0932.48.189	CTS	14.8	Background
936		13.10.11.0936.57.524	CTS	14.8	CTS (pathlength = 8.18 m)	
948		13.10.11.0948.41.630	0913-177A	14.8	Background	
955		13.10.11.0954.19.486	0913-177A	14.4	Sampling Dryer 1 - Run 2 (1000-1100)	5
1117		13.10.11.1117.32.588	CTS	14.8	Background	
1121		13.10.11.1121.00.310	CTS	14.8	CTS (pathlength = 8.73 m)	
1127		13.10.11.1127.34.199	0913-177A	14.7	Background	
1137		13.10.11.1134.41.951	0913-177A	14.2	Sampling Dryer 1 - Run 3 (1137-1237)	6
1257		13.10.11.1257.46.512	CTS	14.7	Background	
1301		13.10.11.1301.14.338	CTS	14.7	CTS (pathlength = 8.73 m)	
1308		13.10.11.1308.39.947	0913-177A	14.7	Background	
1342		13.10.11.1342.51.774	0913-177A	14.2	Sampling Pellet Cooler 2 - Run 1 (1343-1443)	7
1508		13.10.11.1342.51.774	0913-177A	14.1	Sampling Pellet Cooler 2 - Run 2 (1508-1608)	8
1650		13.10.11.1342.51.774	0913-177A	14.1	Sampling Pellet Cooler 2 - Run 3 (1629-1729)	9
1752		13.10.11.1752.08.661	CTS	14.6	Background	
1755		13.10.11.1755.37.781	CTS	14.6	CTS (pathlength = 8.7165 m)	
1802		13.10.11.1802.37.522	0913-177A	14.6	Background	
1342		13.10.11.1809.44.552	0913-177A	14.3	Sampling Hammermill 2 - Run 1 (1811-1911)	10
1935		13.10.11.1809.44.552	0913-177A	14.4	Sampling Hammermill 2 - Run 2 (1935-2035)	11
2048		13.10.11.1809.44.552	0913-177A	14.5	Sampling Hammermill 2 - Run 3 (2048-2148)	12
2200	13.10.11.2200.54.734	CTS	14.7	Background		
2204	13.10.11.2204.32.940	CTS	14.8	CTS (pathlength = 8.75475 m)		
2213	13.10.11.2213.44.875	0913-177A	14.8	Background		
2224	13.10.11.2224.53.772	0913-177A	14.7	Water Spectra (Dryer 1 - Run 2, 3)		
2240	13.10.11.2240.27.896	0913-177A	14.7	Water Spectra (Pellet Cooler 2, Hammermill 2)		
12-Oct	0805	13.10.12.0805.29.253	CTS	14.9	Background	
	0809	13.10.12.0809.22.964	CTS	14.9	CTS (pathlength = 8.59 m)	
	0822	13.10.12.08.22.17.097	0913-177A	14.8	Background	
	858	13.10.12.0857.28.740	0913-177A	14.4	Sampling Pellet Cooler 1- Run 1 (0858-0958)	13
	1022	13.10.12.0857.28.740	0913-177A	14.3	Sampling Pellet Cooler 1- Run 2 (1022-1122)	14
	1141	13.10.12.0857.28.740	0913-177A	14.2	Sampling Pellet Cooler 1- Run 1 (1141-1241)	15
	1257	13.10.12.1257.12.281	CTS	14.6	Background	
	1301	13.10.12.1300.55.794	CTS	14.6	CTS (pathlength = 8.77 m)	
	1308	13.10.12.1309.21.752	0913-177A	14.6	Background	
	1509	13.10.12.1347.50.707	0913-177A	13.8	Sampling Aspirator- Run 1 (1509-1609)	16
	1636	13.10.12.1347.50.707	0913-177A	13.8	Sampling Aspirator- Run 2 (1636-1736)	17
	1800	13.10.12.1347.50.707	0913-177A	13.9	Sampling Aspirator- Run 3 (1800-1900)	18
	1936	13.10.12.1936.27.563	CTS	14.91	Background	
	1940	13.10.12.1940.26.868	CTS	14.72	CTS (pathlength = 8.78 m)	
	1951	13.10.12.1951.39.443	0913-177A	14.75	Background	
2003	13.10.12.2003.07.633	0913-177A	14.59	Water Spectra (Aspirator)		
2023	13.10.12.2023.12.427	0913-177A	14.55	Water Spectra (Pellet Cooler 1)		
13-Oct	807	13.10.13.0807.16.306	0913-177A	14.77	Background	
	0810	13.10.13.0810.33.996	CTS	14.78	Background	
	0810	13.10.13.0813.37.211	CTS	14.85	CTS (pathlength = 8.71 m)	
	0921	13.10.13.0919.17.032	0913-177A	14.24	Sampling Dryer 2 - Run 1 (0921-1021)	19
	1104	13.10.13.0919.17.032	0913-177A	14.17	Sampling Dryer 2 - Run 2 (1104-1204)	20
	1231	13.10.13.0919.17.032	0913-177A	14.17	Sampling Dryer 2 - Run 3 (1231-1347); paused 1236-1252	21
	1420	13.10.13.1419.54.342	CTS	14.91	Background	
	1430	13.10.13.1425.31.173	CTS	14.85	CTS (pathlength = 8.73 m)	
	1447	13.10.13.1447.35.695	0913-177A	14.8	Background	
	1506	13.10.13.1506.31.082	0913-177A	14.71	Water Spectra (Dryer 2)	

Background interference

1130-1200 water condensation in

APPENDIX E

Example Calculations

EXAMPLE CALCULATIONS

Run Number: Dryer 1 – Run 1

Stack Gas Temperature, °R

$$T_s = 460 + t_s$$

$$T_s = 460 + 146.3 = 606.3 \text{ °R}$$

Volume of Dry Gas Sampled at Standard Conditions, Dry Standard Cubic Feet

$$V_{\text{mstd}} = [17.64] \gamma \left[V_m \left[\frac{\left(P_{\text{bar}} + \frac{\Delta H}{13.6} \right)}{T_m + 460} \right] \right]$$

$$V_{\text{mstd}} = [17.64] [0.9728] [33.201] \left[\frac{\left(29.90 + \frac{1.00}{13.6} \right)}{541.3} \right]$$

$$V_{\text{mstd}} = 31.564 \text{ ft}^3$$

Volume of Water Sampled, SCF

$$V_{\text{wstd}} = 0.04715 [\text{Weight of Condensed Moisture}]$$

$$V_{\text{wstd}} = 0.04715 [129.5]$$

$$V_{\text{wstd}} = 6.106 \text{ ft}^3$$

Fraction of Water Vapor in Sample Gas Stream

$$\% \text{H}_2\text{O} = \left[\frac{V_{\text{wstd}}}{V_{\text{mstd}} + V_{\text{wstd}}} \right] \times 100$$

$$\% \text{H}_2\text{O} = \left[\frac{6.106}{31.564 + 6.106} \right] \times 100$$

$$\% \text{H}_2\text{O} = 16.21$$

Dry Mole Fraction of Flue Gas

$$M_{fd} = 1 - \%H_2O/100$$

$$M_{fd} = 1 - [16.21/100]$$

$$M_{fd} = 0.838$$

Molecular Weight of Sample Gas, Dry

$$M_d = 0.44[\%CO_2] + 0.32[\%O_2] + 0.28[100 - \%O_2 - \%CO_2]$$

$$M_d = 0.44[2.0] + 0.32[19.0] + 0.28[100 - 19.0 - 2.0]$$

$$M_d = 29.08 \text{ pounds/pound-mole}$$

Molecular Weight of Sample Gas, Actual Conditions

$$M_s = [M_d \times M_{fd}] + [0.18 \times \%H_2O]$$

$$M_s = [29.08 \times 0.838] + [0.18 \times 16.21]$$

$$M_s = 27.28 \text{ pounds/pound-mole}$$

Average Stack Gas Velocity, Feet/second

$$v_s = K_p C_p (\sqrt{\Delta p})_{avg} \left[\sqrt{\frac{T_s + 460}{P_s M_s}} \right]$$

$$v_s = (85.49)(0.84)(\sqrt{0.1.283}) \left[\sqrt{\frac{606.3}{(29.84)(27.28)}} \right]$$

$$v_s = 70.18 \text{ feet/second}$$

Wet Volumetric Flue Gas Flow Rate at Stack Conditions, Cubic Feet per Minute

$$Q_{aw} = 60 \times v_s \times A$$

$$Q_{aw} = 60 \times 70.18 \times 10.56$$

$$Q_{aw} = 44,461 \text{ Actual Cubic Feet per Minute}$$

Dry Volumetric Flue Gas Flow Rate at Standard Conditions, Cubic Feet per Minute

$$Q_{sd} = 60 \times Mfd \times vs \times A \times \left[\frac{528}{ts + 460} \right] \left[\frac{Ps}{29.92} \right]$$

$$Q_{sd} = 60 \times 0.838 \times 70.18 \times 10.56 \left[\frac{528}{606.3} \right] \left[\frac{29.84}{29.92} \right]$$

$$Q_{sd} = 32,360 \text{ Dry Standard Cubic Feet per Minute}$$

Average THC Dry Basis Concentration as Propane

$$C_{THCD} = (C_{THCW}) / (M_{fd})$$

Where: C_{THCd} = dry basis concentration of THC in ppm
 M_{fd} = dry mole fraction from Method 4 concurrent run

$$C_{THCD} = 66.7 / 0.838 = 79.6 \text{ ppm THC as propane}$$

Average THC Dry Basis Concentration as Carbon

$$C_{THCD} = (C_{THCW}) \times (3) / (M_{fd})$$

Where: C_{THCd} = dry basis concentration of THC in ppm
 M_{fd} = dry mole fraction from Method 4 concurrent run

$$C_{THCD} = (66.7) \times (3) / 0.838 = 238.8 \text{ ppm THC as Carbon}$$

VOC Emission Rate in Pounds Per Hour

$$E_{VOC} = (C_{VOC}) (Q_{SD}) (60 \text{ min/hr}) (C_F)$$

Where: Q_{SD} = measured flow rate in stack in dscfm
 C_F = Conversion factor in lb/scf – ppm
 $C_F = 3.117 \times 10^{-8}$ for Carbon

$$E_{VOC} = (238.8) (32,360) (60 \text{ min/hr}) (3.117 \times 10^{-8}) = 14.5 \text{ lb/hr as Carbon}$$

APPENDIX F

Gas Cylinder Certification Sheets

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Part Number	E02AI99E15A00A6	Reference Number	122-124323950-1
Cylinder Number	CC410934	Cylinder Volume	146 Cu.Ft.
Laboratory	ASG - Durham - NC	Cylinder Pressure	2015 PSIG
PGVP Number	B22012	Valve Outlet	590
Gas Code	APPVD	Analysis Date	Jul 02, 2012

Expiration Date: Jul 02, 2015

Certification performed in accordance with "EPA Traceability Protocol (Sept. 1997)" using the assay procedures listed. Analytical Methodology does not require correction for analytical interferences. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.
 Do Not Use This Cylinder below 150 psig @ 1 Mega Pascal

ANALYTICAL RESULTS				
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty
PROPANE	28.00 PPM	27.99 PPM	G1	+/- 1% NIST Traceable
Air	Balance			

CALIBRATION STANDARDS				
Type	Lot ID	Cylinder No	Concentration	Expiration Date
NTRM	080610	CC263046	49.62PPM PROPANE/AIR	May 14, 2018

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 6700 AHR0801333 C3H8	FTIR	Jun 19, 2012

Triad Data Available Upon Request

Notes: ANW PN 781077



Approved for Release



Praxair Distribution Mid-Atlantic
 145 Shamersville Rd.
 Bethlehem, PA 18015
 Tel. (610) 317-1608 Fax: (610) 758 8382
 PGVP ID:

DocNumber: 000003740

CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

Customer & Order Information:

CHEROKEE INSTRUMENTS INC *
 901 BRIDGE ST
 FUQUAY VARINA NC 275260

Praxair Order Number: 13003732
 Customer P. O. Number: 10429
 Customer Reference Number:

Fill Date: 4/7/2010
 Part Number: EV AIPR60ME-A8
 Lot Number: 917009747
 Cylinder Style & Outlet: AS CGA 590
 Cylinder Pressure & Volume: 2000 psig 140 cu. ft.

Certified Concentration:

Expiration Date:	4/12/2018	NIST Traceable
Cylinder Number:	CC283143	Analytical Uncertainty:
50.0 ppm PROPANE		± 1 %
Balance AIR		

Certification Information: Certification Date: 4/12/2010 Term: 96 Months Expiration Date: 4/12/2018

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1. Do Not Use this Standard if Pressure is less than 150 PSIG.

Analytical Data:

(R=Reference Standard, Z=Zero Gas, C=Gas Candidate)

1. Component: PROPANE

Requested Concentration: 50 ppm
 Certified Concentration: 50.0 ppm
 Instrument Used: VARIAN 3300 INST 023 (PROPANE)
 Analytical Method: FID
 Last Multipoint Calibration: 3/16/2010

Reference Standard Type: GMS
 Ref. Std. Cylinder #: CC162336
 Ref. Std. Conc: 50.3 PPM
 Ref. Std. Traceable to SRM #: 1688b
 SRM Sample #: 82-J-49
 SRM Cylinder #: XF0037348

First Analysis Data:		Date: 4/12/2010	
Z: 0	R: 50.39	C: 49.84	Conc: 49.777
R: 50.38	Z: 0	C: 50.21	Conc: 50.147
Z: 0	C: 50.2	R: 50.34	Conc: 50.137
UOM: PPM	Mean Test Assay:		50.02 PPM

Second Analysis Data:		Date:	
Z: 0	R: 0	C: 0	Conc: 0
R: 0	Z: 0	C: 0	Conc: 0
Z: 0	C: 0	R: 0	Conc: 0
UOM: PPM	Mean Test Assay:		0 PPM

Analyzed by: *Megha Patel for*
 John Pishish

Certified by: *[Signature]*
 Robin Morgan

Information contained herein has been prepared at your request by qualified experts within Praxair Distribution, Inc. While we believe that the information is accurate within the limits of the analytical methods employed and is complete to the extent of the specific analyses performed, we make no warranty or representation as to the suitability of the use of the information for any purpose. The information is offered with the understanding that any use of the information is at the sole discretion and risk of the user. In no event shall the liability of Praxair Distribution, Inc., arising out of the use of the information contained herein exceed the fee established for providing such information.

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Part Number	E02AI99E15A3227	Reference Number	122-124370084-1
Cylinder Number	SG9164792BAL	Cylinder Volume	146.2 CF
Laboratory	ASG - Durham - NC	Cylinder Pressure	2015 PSIG
PGVP Number	B22013	Valve Outlet	590
Gas Code	PPN	Certification Date	Apr 17, 2013

Expiration Date: Apr 17, 2021

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 800-R-12-531 using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume:volume basis unless otherwise noted.

Do Not Use This Cylinder below 100 psig, i.e. 0.7 megapascals.

ANALYTICAL RESULTS					
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty	Assay Dates
PROPANE	86.00 PPM	86.13 PPM	G1	+/- 1% NIST Traceable	04/17/2013
AIR	Balance				

CALIBRATION STANDARDS					
Type	Lot ID	Cylinder No	Concentration	Uncertainty	Expiration Date
NTRM	09061735	CC304058	97.82 PPM PROPANE/AIR	+/- 0.5%	Oct 02, 2013

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 8700 AHR0801333 C3H8	FTIR	Mar 20, 2013

Triad Data Available Upon Request

Notes

Approved for Release



Praxair Distribution Mid-Atlantic
 145 Shiversville Rd
 Bethlehem, PA 18015
 Telephone (610) 317-1608
 Facsimile (610) 758-8382

DocNumber 000007981

CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

Customer & Order Information:

CHEROKEE INSTRUMENTS, INC *
 901 BRIDGE ST
 FUQUAY VARINA NC 275260

Praxair Order Number 15303079
 Customer P.O. Number 11036
 Customer Reference Number

Fill Date 12/20/10
 Part Number AI PR2602E AS
 Lot Number 917034206
 Cylinder Size & Outlet AS CGA 590
 Cylinder Pressure & Volume 2000 psig 146 cu ft

Certified Concentration:

Expiration Date	12/13/2013	NIST Traceable
Cylinder Number	CC109519	Analytical Uncertainty
258.1 ppm	PROPANE	± 1 %
Balance	AIR	

Certification Information: Certification Date 12/13/2010 Term 36 Months Expiration Date 12/13/2013

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1
 Do Not Use this Standard if Pressure is less than 150 PSIG

Analytical Data:

(R=Reference Standard, Z=Zero Gas, C=Gas Certificate)

1 Component: PROPANE

Requested Concentration 260 ppm
 Certified Concentration 258.1 ppm
 Instrument Used VARIAN 3300 INST 023 (PROPANE)
 Analytical Method FID
 Last Multipoint Calibration 11/19/2010

Reference Standard Type GMS
 Ref. Std. Cylinder # CC138736
 Ref. Std. Conc. 499.9 PPM
 Ref. Std. Traceable to SRM # 1669b
 SRM Sample # 81-H-14
 SRM Cylinder # XF004157h

First Analysis Data: Date: 12/13/2010
 Z: 0 R: 501.2 C: 258.6 Conc: 258.07
 R: 501.4 Z: 0 C: 258.5 Conc: 257.97
 Z: 0 C: 258.7 R: 500.2 Conc: 258.17
 UOM: PPM Mean Test Assay: 258.07 PPM

Second Analysis Data: Date:
 Z: 0 R: 0 C: 0 Conc: 0
 R: 0 Z: 0 C: 0 Conc: 0
 Z: 0 C: 0 R: 0 Conc: 0
 UOM: PPM Mean Test Assay: 0 PPM

Analyzed by 
 John Piobish 12/28/10

Certified by 
 Ashley Davila

Information contained herein has been prepared at your request by qualified experts within Praxair Distribution, Inc. While we believe that the information is accurate within the limits of the analytical methods employed and is complete to the extent of the specific analyses performed, we make no warranty or representation as to the suitability of the use of the information for any purpose. The information is offered with the understanding that any use of the information is at the sole discretion and risk of the user. In no event shall the liability of Praxair Distribution, Inc. arising out of the use of the information contained herein exceed the fee established for providing such information.



Praxair Distribution Mid-Atlantic
 145 Shinnetsville Rd
 Bethlehem, PA 18015
 Telephone: (610) 317-1608
 Facsimile: (610) 758-8182

DocNumber 000009995

CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

Customer & Order Information:

CHEROKEE INSTRUMENTS INC *
 901 BRIDGE ST
 FUQUAY VARINA NC 275260

Praxair Order Number 16230993
 Customer P. O. Number 11207
 Customer Reference Number

Exp Date 3/21/2011
 Part Number EV AIPR500ME-AS
 Lot Number 91211/568
 Cylinder Style & Outlet AS CGA 590
 Cylinder Pressure & Volume 2900 psig 140 cu ft

Certified Concentration:

Expiration Date	3/21/2014	NIST Traceable
Cylinder Number	SA20675	Analytical Uncertainty
507.1 ppm	PROPANE	± 1 %
Balance	AIR	

Certification Information: Certification Date 3/21/2011 Term 36 Months Expiration Date 3/21/2014

This cylinder was certified according to the 1997 EPA Traceability Protocol, Document #EPA-600/R-97/121, using Procedure G1
 Do Not Use this Standard if Pressure is less than 150 PSIG

Analytical Data:

(R=Reference Standard, Z=Zero Gas, C=Gas Candidate)

Component: PROPANE

Requested Concentration: 500 ppm
 Certified Concentration: 507.1 ppm
 Instrument Used: VARIAN 3300 INST 023 (PROPANE)
 Analytical Method: FILT
 Last Multiport Calibration: 3/16/2011

Reference Standard Type: GMIS
 Ref Std Cylinder #: CC103865
 Ref Std Conc: 749.3 PPM
 Ref Std Traceable to SRM #: 2646a
 SRM Sample #: 103 C-23
 SRM Cylinder #: XF0008208

First Analysis Date: Date 3/21/2011

Z: 0 R: 749.9 C: 508.2 Conc: 507.88
 R: 749.1 Z: 0 C: 507.2 Conc: 506.86
 Z: 0 C: 505.8 R: 750.4 Conc: 506.46

UOM: PPM Mean Test Assay: 507.06 PPM

Second Analysis Date: Date

Z: 0 R: 0 C: 0 Conc: 0
 R: 0 Z: 0 C: 0 Conc: 0
 Z: 0 C: 0 R: 0 Conc: 0

UOM: PPM Mean Test Assay: 0 PPM

Analyzed by


 John Pribish

Certified by


 Michelle Kostik

Information contained herein has been prepared at your request by qualified experts within Praxair Distribution, Inc. While we believe that the information is accurate within the limits of the analytical methods employed and is complete to the extent of the specific analyses performed, we make no warranty or representation as to the suitability of the use of the information for any purpose. The information is offered with the understanding that any use of the information is at the sole discretion and risk of the user. In no event shall the liability of Praxair Distribution, Inc. arising out of the use of the information contained herein exceed the fee established for providing such information.

CERTIFICATE OF ANALYSIS

Grade of Product: EPA Protocol

Airgas Specialty Gases

830 United Drive
 Durham, NC 27713
 919-544-3773 Fax: 919-544-3774
 www.airgas.com

Part Number	E02AI99E15A0333	Reference Number	122-124344171-1
Cylinder Number	CC148274	Cylinder Volume	146 Cu.Ft.
Laboratory	ASG - Durham - NC	Cylinder Pressure	2015 PSIG
PGVP Number	B22012	Valve Outlet	590
Gas Code	APPVD	Analysis Date	Nov 05, 2012

Expiration Date: Nov 05, 2020

Certification performed in accordance with "EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards (May 2012)" document EPA 800/R-12/531, using the assay procedures listed. Analytical Methodology does not require correction for analytical interference. This cylinder has a total analytical uncertainty as stated below with a confidence level of 95%. There are no significant impurities which affect the use of this calibration mixture. All concentrations are on a volume/volume basis unless otherwise noted.

Do Not Use This Cylin for pressures 140 psig, i.e. 9.7 megapascals.

ANALYTICAL RESULTS				
Component	Requested Concentration	Actual Concentration	Protocol Method	Total Relative Uncertainty
PROPANE	850.0 PPM	836.9 PPM	G1	+/- 1% NIST Traceable
Air	Balance			

CALIBRATION STANDARDS				
Type	Lot ID	Cylinder No	Concentration	Expiration Date
NTRM	110609	CC343416	1000.3PPM PROPANE/NITROGEN	Mar 04, 2017

ANALYTICAL EQUIPMENT		
Instrument/Make/Model	Analytical Principle	Last Multipoint Calibration
Nicolet 6700 AHR0801333 C3H8	FTIR	Oct 11, 2012

Triad Data Available Upon Request

Notes ANW PN 781018

Approved for Release



AIR LIQUIDE

DE

Air Liquide America
Specialty Gases LLC



CERTIFIED WORKING CLASS

Single-Certified Calibration Standard

6141 EASTON ROAD, BLDG 1, PLUMSTEADVILLE, PA 18949-0310

Phone: 800-331-4953 Fax: 215-766-7226

CERTIFICATE OF ACCURACY: Certified Working Class Calibration Standard

Product Information

Document # : 46628943-001
Item No.: MM301080-T-30AL
P.O. No.: 06081203

Cylinder Number: ALM018055
Cylinder Size: 30AL
Certification Date: 21Jun2012
Expiration Date: 21Jun2014
Lot Number: PLU0109851

Customer

ENTHALPY ANALYTICAL, INC.
06081203
800-1 CAPITOLA DRIVE
DURHAM, NC 27703
US

CERTIFIED CONCENTRATION

Component Name	Concentration (Moles)	Accuracy (+/-%)
METHANOL	105. PPM	5
SULFUR HEXAFLUORIDE	3.0 PPM	5
NITROGEN	BALANCE	

TRACEABILITY

Traceable To

Scott Reference Standard

APPROVED BY:

DAVID ASHNOFF

DATE:

6-21-2012

CERTIFICATE OF ANALYSIS

Grade of Product: **CERTIFIED STANDARD-SPEC**

Part Number:	X03NI99C15A1FX5	Reference Number:	83-124390037-1A
Cylinder Number:	CC90659	Cylinder Volume:	144.4 CF
Laboratory:	ASG - Port Allen - LA	Cylinder Pressure:	2015 PSIG
Analysis Date:	Sep 30, 2013	Valve Outlet:	350S
Lot Number:	83-124390037-1A		

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration (Mole %)	Analytical Uncertainty
SULFUR HEXAFLUORIDE	3.000 PPM	3.127 PPM	+/- 5%
METHANOL	100.0 PPM	91.71 PPM	+/- 2%
NITROGEN	Balance		

Notes:


Approved for Release

CERTIFICATE OF ANALYSIS

Grade of Product: CERTIFIED STANDARD-SPEC

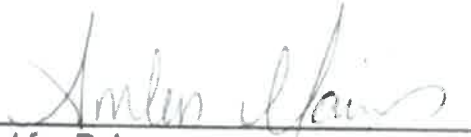
Part Number:	X02NI99C15A1268	Reference Number:	122-124373993-1
Cylinder Number:	CC432538	Cylinder Volume:	144.4 CF
Laboratory:	ASG - Durham - NC	Cylinder Pressure:	2015 PSIG
Analysis Date:	May 08, 2013	Valve Outlet:	350
Lot Number:	122-124373993-1		

Product composition verified by direct comparison to calibration standards traceable to N.I.S.T. weights and/or N.I.S.T. Gas Mixture reference materials.

ANALYTICAL RESULTS

Component	Requested Concentration	Actual Concentration (Mole %)	Analytical Uncertainty
ETHYLENE	100.0 PPM	99.88 PPM	+/- 2%
NITROGEN	Balance		

Notes:



Approved for Release

APPENDIX F
Equipment Calibration Sheets

**APEX INSTRUMENTS METHOD 5 POST-TEST CONSOLE CALIBRATION
USING CALIBRATED CRITICAL ORIFICES
3-POINT ENGLISH UNITS**

Meter Console Information	
Console Model Number	522
Console Serial Number	909033
DGM Model Number	RW 110
DGM Serial Number	961167

Calibration Conditions	
Date	10/23/13
Barometric Pressure	29.46 in Hg
Theoretical Critical Vacuum ¹	13.91 in Hg
Calibration Technician	TTB

Factors/Conversions	
Std Temp	528 °R
Std Press	29.92 in Hg
K ₁	17.647 or/in Hg

¹For valid test results, the Actual Vacuum should be 1 to 2 in. Hg greater than the Theoretical Critical Vacuum shown above.

²The Critical Orifice Coefficient, K', must be entered in English units, (ft³*R^{1/2})/(in.Hg*min).

Run Time	Metering Console				Calibration Data				Critical Orifice		
	DGM Orifice ΔH (P _m) in H ₂ O	Volume Initial (V _{mi}) cubic feet	Volume Final (V _{mf}) cubic feet	Volume (V _{net}) cubic feet	Outlet Temp Initial (t _{mi}) °F	Outlet Temp Final (t _{mf}) °F	Serial Number	Coefficient	Amb Temp Initial (t _{amb}) °F	Amb Temp Final (t _{amb}) °F	Actual Vacuum in Hg
16.0	1.20	637.000	646.659	646.659	62	63	FO55	0.4594	63	65	19.00
13.0	1.20	647.000	654.859	654.859	64	64	FO55	0.4594	65	65	19.00
13.0	1.20	655.100	662.965	662.965	64	65	FO55	0.4594	65	66	19.00

Standardized Data				Results			
Dry Gas Meter (V _{meas}) cubic feet	(Q _{meas}) cfm	Critical Orifice (V _{Cr(Std)}) cubic feet	(Q _{Cr(Std)}) cfm	Calibration Factor		Dry Gas Meter	
				Value (Y)	Variation (ΔY)	Flowrate Std & Corr (Q _{meas(corr)}) cfm	ΔH @ Variation (ΔH@) in H ₂ O
9.639	0.602	9.460	0.591	0.981	0.000	0.591	1.934
7.821	0.602	7.679	0.591	0.982	0.000	0.591	1.933
7.819	0.601	7.675	0.590	0.982	0.000	0.590	1.933
Pretest Gamma	0.9828	% Deviation	0.1	0.982	Y Average	1.933	ΔH@ Average

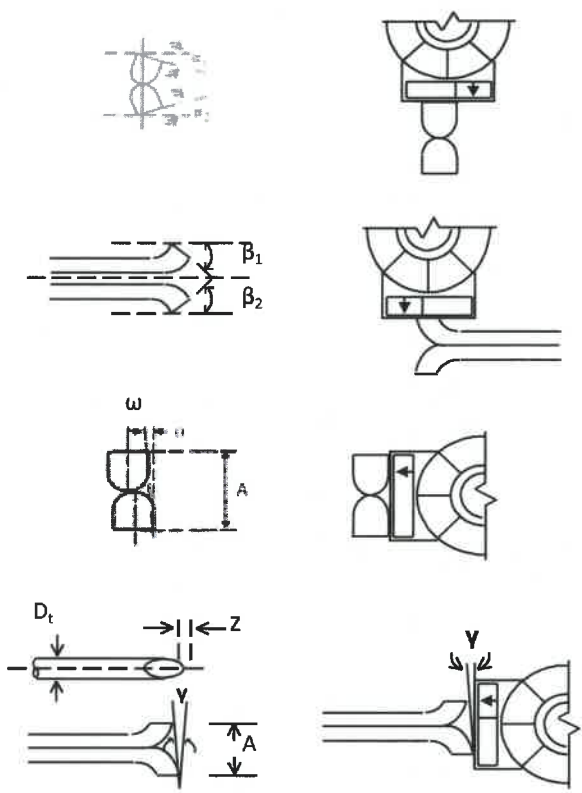
Note: For Calibration Factor Y, the ratio of the reading of the calibration meter to the dry gas meter, acceptable tolerance of individual values from the average is ±0.02.

I certify that the above Dry Gas Meter was calibrated in accordance with USEPA Methods, CFR Title 40, Part 60, Appendix A-3, Method 5, 16.2.3

Signature Todd Brozell

Date 10/23/2013

Type S Pitot Tube Inspection and
Stack Thermocouple Calibration

GENERAL INFORMATION																																													
Probe ID	<input type="text" value="4H"/>	Personnel	<input type="text" value="DLS"/>																																										
Date	<input type="text" value="9/21/2011"/>	Coefficient Value	<input type="text" value="0.84"/>																																										
PITOT TUBE INSPECTION																																													
Pitot Tube assembly level? (yes/no)	<input type="text" value="yes"/>																																												
Pitot Tube obstruction? (yes/no)	<input type="text" value="no"/>																																												
Pitot Tube openings damaged? (yes/no)	<input type="text" value="no"/>																																												
<div style="display: flex; justify-content: space-between;"> <div style="width: 30%;">  </div> <div style="width: 65%;"> <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="padding: 5px;">α_1</td> <td style="padding: 5px;"><input type="text" value="1.4"/></td> <td style="padding: 5px;">$\leq \pm 10^\circ$</td> </tr> <tr> <td style="padding: 5px;">α_2</td> <td style="padding: 5px;"><input type="text" value="0.4"/></td> <td style="padding: 5px;">$\leq \pm 10^\circ$</td> </tr> <tr> <td style="padding: 5px;">β_1</td> <td style="padding: 5px;"><input type="text" value="1.9"/></td> <td style="padding: 5px;">$\leq \pm 5^\circ$</td> </tr> <tr> <td style="padding: 5px;">β_2</td> <td style="padding: 5px;"><input type="text" value="1.2"/></td> <td style="padding: 5px;">$\leq \pm 5^\circ$</td> </tr> <tr> <td style="padding: 5px;">Ψ</td> <td style="padding: 5px;"><input type="text" value="2.9"/></td> <td></td> </tr> <tr> <td style="padding: 5px;">θ</td> <td style="padding: 5px;"><input type="text" value="0.2"/></td> <td></td> </tr> <tr> <td style="padding: 5px;">$z = A \tan(\Psi)$</td> <td style="padding: 5px;"><input type="text" value="0.049"/></td> <td style="padding: 5px;">$\leq \pm \frac{1}{8}''$</td> </tr> <tr> <td style="padding: 5px;">$\omega = A \tan(\theta)$</td> <td style="padding: 5px;"><input type="text" value="0.003"/></td> <td style="padding: 5px;">$\leq \pm \frac{1}{32}''$</td> </tr> <tr> <td style="padding: 5px;">D_t</td> <td style="padding: 5px;"><input type="text" value="0.375"/></td> <td></td> </tr> <tr> <td colspan="3" style="padding: 5px;"><small>($\frac{3}{16}'' < D_t < \frac{3}{8}''$ Recommended)</small></td> </tr> <tr> <td style="padding: 5px;">A</td> <td style="padding: 5px;"><input type="text" value="0.9375"/></td> <td></td> </tr> <tr> <td style="padding: 5px;">P_A</td> <td colspan="2" style="padding: 5px;"><input type="text" value="1.29"/></td> </tr> <tr> <td style="padding: 5px;">P_B</td> <td colspan="2" style="padding: 5px;"><input type="text" value="1.29"/></td> </tr> <tr> <td colspan="3" style="padding: 5px;"><small>($1.05 < P/D_t < 1.50$ Recommended)</small></td> </tr> </table> </div> </div>				α_1	<input type="text" value="1.4"/>	$\leq \pm 10^\circ$	α_2	<input type="text" value="0.4"/>	$\leq \pm 10^\circ$	β_1	<input type="text" value="1.9"/>	$\leq \pm 5^\circ$	β_2	<input type="text" value="1.2"/>	$\leq \pm 5^\circ$	Ψ	<input type="text" value="2.9"/>		θ	<input type="text" value="0.2"/>		$z = A \tan(\Psi)$	<input type="text" value="0.049"/>	$\leq \pm \frac{1}{8}''$	$\omega = A \tan(\theta)$	<input type="text" value="0.003"/>	$\leq \pm \frac{1}{32}''$	D_t	<input type="text" value="0.375"/>		<small>($\frac{3}{16}'' < D_t < \frac{3}{8}''$ Recommended)</small>			A	<input type="text" value="0.9375"/>		P_A	<input type="text" value="1.29"/>		P_B	<input type="text" value="1.29"/>		<small>($1.05 < P/D_t < 1.50$ Recommended)</small>		
α_1	<input type="text" value="1.4"/>	$\leq \pm 10^\circ$																																											
α_2	<input type="text" value="0.4"/>	$\leq \pm 10^\circ$																																											
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P_A	<input type="text" value="1.29"/>																																												
P_B	<input type="text" value="1.29"/>																																												
<small>($1.05 < P/D_t < 1.50$ Recommended)</small>																																													
STACK THERMOCUPLE CALIBRATION																																													
Ref. Type	<input type="text" value="Hg Thermometer"/>	Ref. ID	<input type="text" value="Hg-1"/>																																										
Source	Ref., °F	Stack TC, °F	Abs. Diff., °F																																										
Ice bath	43	45	2																																										
Ambient	75	75	0																																										
Hot water	193	194	1																																										
Maximum Temp. Difference, °F			2																																										

Type S Pitot Tube Inspection and
Stack Thermocouple Calibration

GENERAL INFORMATION

Probe ID
Date

Personnel
Coefficient Value

PITOT TUBE INSPECTION

Pitot Tube assembly level? (yes/no)
Pitot Tube obstruction? (yes/no)
Pitot Tube openings damaged? (yes/no)

α_1 $\leq \pm 10^\circ$
 α_2 $\leq \pm 10^\circ$

β_1 $\leq \pm 5^\circ$
 β_2 $\leq \pm 5^\circ$

γ
 θ

$z = A \tan(\gamma)$ $\leq \pm \frac{1}{16}''$
 $\omega = A \tan(\theta)$ $\leq \pm \frac{1}{32}''$

D_t
($\frac{3}{16}'' < D_t < \frac{3}{8}''$ Recommended)

A

P_A
 P_B
($1.05 < P/P_t < 1.50$ Recommended)

STACK THERMOCOUPLE CALIBRATION

Ref. Type

Ref. ID

Source	Ref., °F	Stack TC, °F	Abs. Diff., °F
Ice bath	43	45	2
Ambient	75	75	0
Hot water	193	192	1
Maximum Temp. Difference, °F			2

ATTACHMENT C

Air

Control Techniques, P.C.

301 East Durham Road
Cary, North Carolina 27513

Office (919) 460-7811
Fax (919) 460-7897

February 23, 2015

Sent via email: Mike.doniger@envivabiomass.com

Mr. Mike Doniger
Corporate Development
Enviva Biomass, L. P.
7200 Wisconsin Ave, Suite 1000
Bethesda, MD 20814 USA

Re: Benzene, Acrolein, and Phenol Emissions
Air Control Techniques, P.C. files 1909, 1912

Dear Mike,

I have prepared a summary of the technical basis for our conclusion that benzene, acrolein, and phenol are not present in the air emissions from dryers, dry hammermills, and pellet coolers of Enviva Biomass, L.P. facilities.

This conclusion is based on (1) our technical review of published literature concerning pellet production process air emissions, (2) our laboratory studies conducted to identify variables affecting emissions and types of organic compounds emitted, (3) our work with Dr. Grant Plummer of Enthalpy Analytical, Inc. concerning Method 320 data analyses, and (4) Method 320 testing at Enviva facilities. Work areas 1 through 3 were part of our pretest program to determine the most appropriate testing procedures for the pellet production industry. Work area 4 involved tests at two Enviva Biomass, L.P. facilities with quite different hardwood/softwood ratios.

1. Technical Review of Published Literature

Air Control Techniques, P.C. has obtained and reviewed peer-reviewed and internet-available technical articles concerning pellet production process air emissions. A list of the references that we reviewed is provided as an Attachment to this letter.

None of these articles listed benzene, acrolein, or phenol as significant components of the air emission streams. These articles published in the 2000 through 2010 period indicated that the air emissions consist primarily of mono-terpenes, di-terpenes and acetone. Organic hazardous air pollutants (HAPs) listed in these papers and articles indicate that methanol and formaldehyde are also present.

2. Laboratory Studies

Air Control Techniques, P.C. conducted a number of laboratory tests to evaluate the variables potentially affecting organic compound emissions and the specific compounds present in the air streams. We conducted these tests using equipment that simulated the conditions in Enviva wood dryers and pellet coolers.

We conducted more than 20 separate tests to evaluate the characteristics of emissions. These tests involved both U.S. EPA Reference Method 18 (gas canister, activated carbon tubes, and impinger solution) and NCASI Method 98.01 tests of the effluent gas stream. Benzene and phenol were not detected in any of these laboratory tests. Acrolein at very low concentrations was above the limit of quantification in one test; therefore, this compound was included as a possible compound in the effluent gas streams.

3. Method 320 Application to Pellet Production Facilities

One of the primary conclusions of the literature review and the laboratory study was that Method 25A was appropriate for measuring total VOCs and that Method 320 (FTIR) was appropriate for measuring organic HAP emissions.

The literature data and laboratory studies clearly indicated that the air emission streams from pellet production facilities were composed of a large number of mono- and di-terpenes, acetone, methanol, and formaldehyde. High concentrations of moisture and carbon dioxide, both major FTIR interferences, are in the dryer exhaust. Collectively, this mixture of compounds creates a complex matrix for conducting Method 320 analyses.

After the first test at the Enviva Northampton, LLC plant in the fall of 2013, Air Control Techniques, P.C. began an intensive data evaluation modeling program to identify the most accurate set of FTIR spectral analysis peaks to quantify organic HAPS, terpenes, acetone, and other compounds while minimizing interferences in this complex matrix. Air Control Techniques, P.C. consulted with Dr. Grant Plummer of Enthalpy, Inc. concerning this FTIR application. Dr. Plummer is co-developer of U.S. EPA Method 320 and is a recognized expert in this field. Based on work conducted by Dr. Plummer and by David Goshaw, P.E., QSTI (Air Control Techniques, P.C.'s FTIR expert), we developed an accurate FTIR model and data evaluation approach for each process emission source at Enviva. Based on these Method 320 procedures we analyzed the Northampton samples and laboratory samples. We did not observe benzene, acrolein, and phenol in these analyses after the evaluation program was refined to avoid interferences from terpene compounds, water, and carbon dioxide.

4. Northampton and Amory Test Programs

Air Control Techniques, P.C. has conducted Method 320 air emission testing at the Enviva Amory LLC facility using the Method 320 procedures developed after the tests at Northampton. Benzene, acrolein, and phenol were not detected in these tests.

If it is of interest to DENR, we can provide the FTIR files for these tests programs as a separate submission. Each test program generated over 1,500 separate files with a total size exceeding

400 megabytes for each test program. We can also supply the instrument specific data and quality assurance information relevant to these test programs.

5. Conclusions

I do not believe that benzene, acrolein, or phenol are present in significant concentrations in pellet production facility air emission streams. This conclusion is based on (1) the technical review of relevant literature, (2) a comprehensive set of laboratory studies, (3) guidance provided by Dr. Plummer on Method 320 data analyses, and (4) tests performed at Enviva facilities.

This conclusion is logical considering the specific characteristics and operating conditions of the Enviva processes. Specifically, the Enviva dryers operate at substantially lower temperatures and with high dryer-exit wood moisture levels. Both the literature data and laboratory data clearly indicated that both factors are related to substantially lower emissions than some other pellet processes.

Pellet production does not involve the use of resins similar to those used in particleboard and MDF processes. The thermal breakdown products of these additives are responsible for some, and perhaps all of the benzene from these quite different processes. Emission factors for particleboard and MDF processes are not relevant to Enviva pellet production facilities.

For the reasons stated in this letter, I believe that benzene, acrolein, and phenol are not present at significant concentrations in the air emission gas streams from Enviva facilities. If anyone at DENR has any questions, please have them contact David Goshaw or me.

Regards,



John Richards, Ph.D., P.E., QSTI
President, Air Control Techniques, P.C.

**ATTACHMENT
LITERATURE REFERENCES**

1. Beauchemin, P. and M. Tampier. "Emissions and Air Pollution Control for the Biomass Pellet Manufacturing Industry." Report submitted to the British Columbia Ministry of the Environment. May 12, 2010.
2. Granström, K. "Emissions of Volatile Organic Compounds from Wood." Dissertation, Karlstad University, Karlstad, Sweden. June 2005.
3. Granström, K, and B. Månsoon. "Volatile Organic Compounds Emitted from Hardwood Drying as a Function of Processing Parameters." *Journal of Environmental Science and Technology*, Volume 5, Number 2, Pages 141-148. 2008.
4. Milota, M.R. "Emissions from Wood Drying" *Forest Projects Journal*, Volume 50, Number 6, Pages 10-19, June 2000.
5. Milota, M. and P. Mosher. "Emissions of Hazardous Air Pollutants from Lumber Drying." *Forest Products Journal*, Volume 58, No. 7/8, Pages 50-55, July/August 2008.
6. Kung, X. T. et al. "Rate and Peak Concentrations of Off-Gas Emissions in Stored Wood Pellets—Sensitivities to Temperature, Relative Humidity, and Headspace Volume." *Annual of Occupational Hygiene*, Volume 53, No. 89, Pages 789-796, 2009.
7. Arshadi, M. P., Geladi, R. Gref, and P. Fjallstrom. "Emission of Volatile Aldehydes and Ketones from Wood Pellets Under Controlled Conditions." *Annals of Occupational Hygiene*, Vol. 53, No. 8, pp 797-805. 2009.

DIVISION OF AIR QUALITY
March 25, 2015

MEMORANDUM

To: Robert Fisher, Washington Regional Office

From: Shannon Vogel, Stationary Source Compliance Branch *Shannon Vogel*

Subject: Enviva Pellets Ahoskie, LLC
Ahoskie, Hertford County, North Carolina
Facility ID 4600107, Permit No. 10121R02
VOC Emissions Testing Performed by Air Control Techniques, Inc.
Tracking No. 2014-115st - Dry Hammermill ES-DHM-2 (6/25/14)
Tracking No. 2014-116st - Dryer ES-DRYER (7/2-3/14)
Tracking No. 2014-117st - Pellet Cooler ES-CLR2 (6/26/14)

Air Control Techniques, Inc. (ACT) performed EPA Method 25A on June 25-26 and July 2-3, 2014 in order to determine the VOC emissions from the wood pellet processes while operating at a higher softwood/hardwood ratio. The EPA Method 25A results are acceptable for VOC "emission factors" in pounds of alpha-pinene per oven dry tons pulp (lb/ODT).

ES-DRYER is a direct heat wood-fired dryer controlled by simple cyclone CD-DC and wet electrostatic precipitator CD-WESP. ES-CLR1, CLR2, CLR3, and CLR 4 are four pellet coolers controlled by two multicyclones CD-CLR-C1 and CD-CLR-C2. ES-DHM-1 through 4 are four dry wood hammermills controlled by four simple cyclones CD-DHM-C1 through C4 and two fabric filter CD-DHM-FF1 and CD-DHM-FF2.

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The test report included transcription errors in the results and reported production rates. The VOC as propane and VOC as alpha-pinene test results are acceptable only as tabulated below.

Source ID/Date	Softwood	Production	VOC as propane	VOC as α -pinene
Hammermill 6/25/14	33%	10.1 ODT/hr	1.01 lb/hr	0.94 lb/hr
			0.101 lb/ODT	0.093 lb/ODT
Pellet Cooler 6/26/14	45%	22.4 ODT/hr	11.02 lb/hr	10.24 lb/hr
			0.492 lb/ODT	0.457 lb/ODT
Dryer 7/2-3/14	30%	40.9 ODT/hr ¹	34.4 lb/hr	32.0 lb/hr
			0.844 lb/ODT	0.784 lb/ODT

1. Runs 1, 2, and 4 average from reported rates of 41.5, 41.9 and 39.3 ODT/hr, respectively.

If you have any questions regarding the results of this review, please contact me at (919) 707-8416 or Shannon.vogel@ncdenr.gov.

cc: Central Files, Hertford County
IBeam Documents 4600107

DIVISION OF AIR QUALITY
March 25, 2015

MEMORANDUM

To: Robert Fisher, Washington Regional Office

From: Shannon Vogel, Stationary Source Compliance Branch *Shannon Vogel*

Subject: Enviva Pellets Ahoskie, LLC
Ahoskie, Hertford County, North Carolina
Facility ID 4600107, Permit No. 10121R02
VOC Emissions Testing Performed by Air Control Techniques, Inc.
Tracking No. 2014-115st - Dry Hammermill ES-DHM-2 (6/25/14)
Tracking No. 2014-116st - Dryer ES-DRYER (7/2-3/14)
Tracking No. 2014-117st - Pellet Cooler ES-CLR2 (6/26/14)

Air Control Techniques, Inc. (ACT) performed EPA Method 25A on June 25-26 and July 2-3, 2014 in order to determine the VOC emissions from the wood pellet processes while operating at a higher softwood/hardwood ratio. The EPA Method 25A results are acceptable for VOC "emission factors" in pounds of alpha-pinene per oven dry tons pulp (lb/ODT).

ES-DRYER is a direct heat wood-fired dryer controlled by simple cyclone CD-DC and wet electrostatic precipitator CD-WESP. ES-CLR1, CLR2, CLR3, and CLR 4 are four pellet coolers controlled by two multicyclones CD-CLR-C1 and CD-CLR-C2. ES-DHM-1 through 4 are four dry wood hammermills controlled by four simple cyclones CD-DHM-C1 through C4 and two fabric filter CD-DHM-FF1 and CD-DHM-FF2.

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cc: **Central Files, Hertford County**
IBeam Documents 4600107

FROM AIR QUALITY MGMT
MAR 31 2015



North Carolina Department of Environment and Natural Resources

Pat McCrory
Governor

John E. Skvarla, III
Secretary

Hesterford
April 9, 2014

Alan H. McConnell
Council to Enviva Pellets, Ahoskie, LP
Kilpatrick Townsend & Stockton LLP
Suite 1400, 4208 Six Forks Road
Raleigh, NC 27609

RE: Request for Pine Trial, Enviva Pellets, Ahoskie, LP. AQ Permit #10121R01

Dear Mr. McConnell:

The Division is in receipt of your letter dated March 14, 2014 regarding the subject request to increase the percentage of softwood used as a raw material at the Ahoskie facility on a trial basis.

We understand that the Ahoskie facility will use the trial period to determine VOC emission factors resulting from higher softwood percentages in the raw material. While Enviva's permit does not limit the percentage of softwood in the raw material, the existing PSD avoidance limit is based on an emission factor derived from a 10% softwood content. At no time is the Ahoskie facility allowed to exceed any existing permitted limits related to emissions or throughput in order to conduct the trial.

Under the above conditions, the Division approves Enviva Pellets, Ahoskie, LP to conduct a 12-month trial to determine emission factors for the increased percentage of softwood in the raw material used at the facility. Prior to the use of such emission factors in future permitting decisions, Enviva shall submit a testing protocol and reference test method results to the Division for evaluation.

Please contact William Willets at 919-707-8726 with any questions.

Sincerely,

Mark Cuilla, CPM, Acting Chief, Permitting Section
Division of Air Quality, NCDENR

cc: Michael Pjetraj, Supervisor, Stationary Source Compliance Branch

REC'D AIR PERMITTING MGMT
FEB 13 15