

H.F. Lee Energy Complex Duke Energy Progress 1199 Black Jack Church Road Goldsboro, N.C. 27530

November 6, 2017

Mr. William Willets, Section Chief Division of Air Quality North Carolina Department of Environmental Quality 1641 Mail Service Center Raleigh, North Carolina 27699-1641

Reference: Construction Permit Application for STAR[®] Facility Duke Energy Progress, LLC H. F. Lee Steam Electric Plant Goldsboro, North Carolina; Wayne County Air Quality Permit No. 01812T; Facility ID: 9600017

Dear Mr. Willets:

Duke Energy Progress, LLC currently operates the H.F. Lee Steam Electric Plant under Air Quality Permit No. 01812T42 which will expire on June 30, 2020. Enclosed please find 3 copies of an air permit application including associated application forms and fee to construct an ash beneficiation facility at the H.F. Lee Plant. An additional copy has been sent to the attention of Robert Fisher at the Washington Regional Office.

If you have any questions concerning the contents of this submittal, please contact Erin Wallace at (919) 546-5797 or Mike Graham at (919) 722-6551.

Certification statement:

Based on information and belief formed after reasonable inquiry, the undersigned certifies under penalty of law that all information and statements provided in the enclosure are true, accurate, and complete.

Respectfully submitted,

flug Am

Jeffery Hines Station Manager

cc: Robert Fisher, Washington Regional Office Erin Wallace, Duke Energy Mike Graham, Duke Energy

PERMIT APPLICATION FOR MODIFICATION OF THE H.F. LEE STEAM ELECTRIC PLANT GOLDSBORO, NORTH CAROLINA

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Document Review

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1.0 INTRODUCTION

Duke Energy Progress, LLC (Duke Energy) is currently permitted (Air Permit No. 01812T42) to operate the H.F. Lee Steam Electric Plant (H.F. Lee Plant) located in Wayne County, North Carolina, which is currently attainment for all regulated pollutants. H.F. Lee Plant currently consists of five (5) combustion turbine generators (CTGs) operating in simple cycle mode. H.F. Lee Plant also consists of three (3) CTGs with supplemental duct firing operating in a 3x1 combined cycle mode and simple cycle mode.

Duke Energy is proposing to install and operate a fly ash processing facility consisting of a Staged Turbulent Air Reactor (STAR[®]) plant and associated ancillary activities. To support this project, Duke Energy is submitting this application for a minor source construction permit.

North Carolina Department of Environmental Quality (NC DEQ) application forms and tables are located in Appendix A. Supporting emission calculations are presented in Appendix B. Emission calculations support documentation is present in Appendix C. A site plan, plot plan and process flow diagrams for the proposed project can be found in Appendix D. The toxic air dispersion modeling files are presented in Appendix E. The non-hazardous secondary material (NHSM) determination is provided in Appendix F. A draft CAM Plan is provided in Appendix G and Appendix H contains Zoning Commission documentation.



1.1 GENERAL APPLICATION INFORMATION

Following is the applicant's primary point of contact and the address and telephone number where he/she can be reached:

Duke Energy Contact	Erin Wallace, Sr. Environmental Specialist Duke Energy Progress, LLC 410 S. Wilmington Street, Raleigh, North Carolina 27601 (919)-546-5797 (Office)
<u>ECT Contac</u> t	Thomas O. Pritcher, P.E. Environmental Consulting & Technology, Inc. 7208 Falls of Neuse Road, Suite 102 Raleigh, North Carolina 27615 (919) 861-8888 (Office) (919) 631-1537 (Mobile)

1.2 **PROJECT LOCATION**

The H.F. Lee STAR[®] facility will be located on the property associated with Duke Energy's H.F. Lee Plant, which is located at 1199 Black Jack Church Road, Goldsboro, NC 27530. Figure 1-1 provides a regional topographic map showing the site location.

1.3 **PROJECT OVERVIEW**

The STAR[®] system is a patented technology developed by The SEFA Group Inc. (SEFA) to process feedstock (of any carbon content) like fly ash (wet or dry) along with other ingredient materials into a variety of commercial products. These products are used, not only for application as a partial cement replacement, but for many other commercial and industrial applications. For example, there are several products that SEFA is currently capable of producing because of the flexibility embodied in the STAR[®] process, including STAR[®] RP, Ultrix[®], Spherix[®], Fortimix[®], and Permanix[™].





The associated sources of air emissions proposed to support the STAR[®] system includes the following:

- Ash Basin excavation.
- Ash Handling/Processing.
- Haul Roads.
- Screener.
- Crusher.
- Two diesel engines associated with a Screener and a Crusher.
- Wet ash receiving area and storage shed.
- Wet ash feed hopper.
- Wet ash unloading pile.
- Two External heat exchangers (EHE) (with baghouses).
- Transfer silo filling and unloading (with bin vent product capture device).
- Feed silo filling and unloading (with bin vent product capture device).
- Storage dome filling and unloading (with bin vent product capture device).
- Loadout silo (with bin vent product capture device).
- Loadout silo chute 1A (with bin vent product capture device).
- Loadout silo chute 1B (with bin vent product capture device).
- FGD Byproduct Silo (with bin vent product capture device).
- FGD Absorbent Silo (with bin vent product capture device).

The H.F. Lee STAR[®] facility will be designed to produce up to 400,000 tons of fly ash product annually. Figure 1-2 illustrates a general process flow diagram for proposed facility.

1.4 <u>CONTENTS OF THE MODIFICATION PERMIT APPLICATION</u>

Section 2.0 of this document provides a source description of the facility. Section 3.0 presents the projected air emissions. Section 4.0 discusses the regulatory applicability, and Section 5.0 presents the air toxic dispersion modeling methodology and results. The appendices are organized as follows:



- Appendix A—Required North Carolina permit application forms.
- Appendix B—Supporting emission calculations.
- Appendix C—Emission calculations support documentation.
- Appendix D— Facility Drawings.
- Appendix E— Electronic air dispersion modeling.
- Appendix F—NHSM Determination.
- Appendix G—CAM Plan.
- Appendix H—Zoning Commission Documentation.







2.0 PROCESS DESCRIPTION

2.1 PRE-REACTOR MATERIAL HANDLING EQUIPMENT

Excavation and processing of materials from the ash ponds to meet the STAR[®] system fly ash (ingredient) specifications will be under the control of Duke Energy. All fly ash reclaimed from an ash pond delivered for use as an ingredient in the STAR[®] system must first undergo processing by the owner to be:

- A. Free of all, but minimal contaminants (e.g., organic debris, slag);
- B. Finely-divided and free-flowing,
- C. Have consistent moisture content of $\leq 25\%$; and
- D. Have a consistent chemical composition, including organic content measured by loss on ignition.

The processing sequence of events will include fly ash being excavated and staged to allow for dewatering (ensures moisture content of $\leq 25\%$). Dewatered fly ash will then be screened to remove contaminants (organic debris, slag, etc.), to produce a consistent chemical composition and a finely divided free-flowing ingredient.

Wet fly ash, nominal 15 percent by weight moisture (water) is delivered via trucks. The wet fly ash can be unloaded from the trucks into the storage shed, unloaded from the trucks to a pile that is then transferred to a storage shed by a front-end loader, or unloaded from the trucks directly into the feed hopper. The wet fly ash in the shed is transferred via front-end loader to a hopper at up to 70 wet "short" tons per hour (tph) (one "short" ton = 2,000 lb), which then conveys the wet fly ash to the mechanical conveyance equipment. The material is discharged from the mechanical conveyance equipment into a material delumper unit to reduce the "overs" material. The material discharged from the delumper unit is then introduced into the EHE by gravity, where it is continually fluidized using preheated air.



The fluidized material is dried by two heat transfer means: (1) intimate contact of the wet, fluidized material with the heated fluidizing air and (2) direct contact of the wet material with hot water heat exchangers located in the EHE. By contact of the material with the outer surfaces of the heat exchanger tube, heating energy is transferred from the tube-side hot water (hot water that is a part of the facility's cooling loop at approximately 350 degrees Fahrenheit [°F] at 250 pounds per square inch gauge [psig]) to the material such that the material heats and, consequently, dries, while the supplied hot water temperature is reduced.

The material is discharged from the EHE units via two means. The primary method of material discharge from the unit is via the fixed-height overflow weir located at the discharge end of the unit. This overflow stream (comprising the majority of the material discharged from the unit) enters the integrally-constructed discharge box/chute of the unit. The second method of material discharge from the unit is via an integrally-constructed underflow discharge screw or rotary valve. The purpose of this underflow discharge stream is to discharge large or oversized material from the unit that, due to these particles' size, may not sufficiently fluidize to the point that they would reach the normal overflow weir height. The material is discharged from the unit at less than 2.0 percent by weight moisture and at a temperature range of 150 to 300°F to downstream material-handling equipment (transfer silos).

The exhaust air is discharged from each EHE through interconnecting ductwork to a highefficiency bag filter unit operation for feedstock recovery/exhaust air treatment. The moisture- and dust-laden exhaust air enters the unit, and, as the air passes through the filter media, dust is separated from the exhaust air stream with high fractional removal efficiency. The high-efficiency filter media used will be able to achieve a particulate matter (PM) exhaust rate of 0.025 grain per dry standard cubic foot (gr/dscf) of exhaust air (or less).



After the bag filter unit, the cleaned exhaust air stream passes through interconnecting ductwork to the exhaust air fan. The exhaust air volumetric rate is estimated at approximately 41,550 actual cubic feet per minute (acfm) at 10 inches in the water column (water gauge) static pressure (atmospheric pressure) and at approximately between 150-300°F (and at or below the dust loading rate of 0.025 gr/dscf).

2.2 <u>STAR® TECHNOLOGY</u>

As discussed previously, the STAR[®] process is a patented technology developed by SEFA to process feedstock (of any carbon content) like fly ash (wet or dry) along with other ingredient materials into a variety of commercial products. These products are used not only for application as a partial cement replacement but also as an ingredient in many other commercial and industrial applications.

The STAR[®] process is inherently flexible in that operating parameters can be varied and different ingredients can be added to produce a desired product. The primary component of the STAR[®] is a cylindrical refractory-lined vessel in which the majority of the process reactions take place. These reactions can include a range of both chemical and physical reactions. Air required for pneumatic uplift of the solids and for the process reactions enters through the floor of the STAR[®] system as well as through the walls at multiple locations. The raw feedstock and any other ingredients are introduced through the walls of the STAR[®]. All of the solids and gases exit together at the top of the reactor. The gas/solids mixture enters a hot cyclone, where the majority of solids are separated from the gas and recycled back to the STAR[®] system. The high rate of hot recycle solids increases the operating flexibility of the process. The process reactions can occur through this reactor/hot cyclone loop. Due to the high gas velocity, multiple injection points, and recycle solids, there is a significant amount of turbulence created that enhances the mixing of the ingredients and optimizes the reactions. The gas and remaining solids not collected by the hot cyclone are passed over a heat exchanger, which can be designed to preheat the process air, used in heat recovery or to simply cool the gas/solids mixture. Once cooled, the solids are separated from the gas in a fabric filter recovery device. The STAR[®] system's integral design allows for solids to be removed from the bottom of the reactor or from the recycle



loop ultimately to be combined with the solids/gas stream before the heat recovery equipment. By design the STAR[®] operates under a wide range of process parameters to produce a high-quality class F fly ash for beneficial use in ready mix concrete or other specialty products.

Fly ash entering the reactor is sprayed with water and it is assumed that 90% of the time the water used is recycled instead of raw water. Process wash-down water, Storm water and fly ash contact water may be recycled.

During startup, the process air is heated with a startup burner firing auxiliary fuel (i.e., natural gas or propane) until reactor temperatures reach auto-ignition. At this point, the residual carbon in the fly ash reacts and becomes the heat source for the self-sustaining process. Under certain conditions, auxiliary fuel may be co-fired with the residual carbon in the fly ash. Process controls meter additional raw fly ash through a feeder into the reactor as necessary. As additional material is added to the reactor, processed fly ash is entrained in the exhaust and exits the top of the reactor.

After exiting the reactor, the fly ash entrained in the flue gas passes through a hot cyclone where solids are returned to the reactor for temperature control. The fly ash and flue gas leaving the hot cyclone is conveyed to the air preheater then passes through a gas cooler. The cooled flue gas and fly ash passes through a fabric filter baghouse, which is an integral part of the process for product capture, and then exhausts to a Dry Flue Gas Desulfurization (FGD) system (using hydrated lime as a reagent and an additional fabric filter control device) to reduce sulfur dioxide (SO₂) emissions. The FGD exhaust is vented to the atmosphere through a stand-alone stack.

The Dry FGD system consist of a Circulating Dry Scrubbing System (CDS) and a Fabric Filter baghouse (FF). Flue gas, reagent (hydrated lime) and water are mixed homogenously in the CDS to absorb the acid gas, sulfur oxides, and is collected in the FF baghouse. The clean gas will then flow from the CDS-FF system to an Induced Draft (ID) fan which forces the clean exhaust gas up the stack where it discharges to atmosphere. The byproduct solids



are discharged from the FF baghouse into a byproduct storage silo. The system is comprised of a three (3) day storage silo with vent filter, fluidizing air stones and dry unloading chutes. Dry dust unloading chutes are telescoping chutes equipped with small ventilation fans that recirculate displaced air back to the top of the byproduct storage silo.

2.3 POST-REACTOR MATERIAL HANDLING EQUIPMENT

Once the fly ash leaves the reactor, it is collected in the product recovery baghouse and pneumatically transferred to either the storage dome or the loadout silo, each equipped with a bin vent. The truck loadout station uses telescoping chutes and a negative pressure ventilation system to reduce fugitive emissions.



3.0 EMISSIONS CALCULATIONS

For the emission sources to be added for the proposed Project, emission rates are based on process information developed and provided by SEFA, Duke Energy, manufacturers' data, and/or published emission factors such as those contained in the U.S. Environmental Protection Agency's (EPA) Compilation of Air Pollutant Emission Factors, AP-42. Unit design parameters and operational practices have been incorporated into the analysis to make the emission estimates conservative and representative of on-site conditions. Emission estimates are provided for criteria pollutants, hazardous air pollutants (HAP) and toxic air pollutants (TAP).

3.1 PROJECT EMISSIONS

3.1.1 STAR[®] SYSTEM

Emissions from the STAR[®] system, include PM/particulate matter with a diameter less than 10 microns (PM₁₀)/particulate matter with a diameter less than 2.5 microns (PM_{2.5}), SO₂, nitrogen dioxide (NO_x), carbon monoxide (CO), volatile organic compounds (VOC), and greenhouse gases (GHG) from the auxiliary fuels and residual carbon in the fly ash. Emissions from the auxiliary fuels were estimated using the most recent emissions factors for natural gas and propane-fired boilers contained in the EPA's Compilation of Air Pollutant Emissions Factors, AP-42. The auxiliary fuel burners are a low-NO_x design intended to comply with North Carolina NO_x control regulations.

Fly ash generated from the combustion of coal may contain trace quantities of heavy metals. Duke Energy performed site-specific ash analysis, data obtained was used to calculate the emission rates for each metal.

Emission factors of the heavy metals in the fly ash before entering the reactor are based on the site specific ash analysis data. Emission factors of the heavy metals in the fly ash after exiting from the reactor are based on the site specific ash analysis data with a contribution from the use of process water in the reactor.



Emissions of NO_x and CO from the processing of the residual carbon in the fly ash were estimated based on emissions estimates from other existing STAR[®] units. Particulate emissions for the STAR[®] are based on the baghouse manufacturer's data of 0.025 grain per actual cubic foot (gr/acf). The induced draft fan providing the motive force for the product transfer is rated at 77,500 acfm, at the expected process conditions of 350°F and nominal atmospheric pressure.

 SO_2 emissions are a function of the amount of fly ash processed through the reactor, the sulfur content of the fly ash, the amount of sulfur remaining in the product ash exiting the $STAR^{\ensuremath{\mathbb{R}}}$ reactor, and the SO_2 air pollution control equipment removal efficiency, in this case the dry scrubber. Assuming ash sulfur content of 0.15 percent and 100 percent oxidation of the sulfur, the dry scrubber will be designed to provide 100 percent capture and can be operated with an SO_2 control efficiency of 95 percent.

The STAR[®] system will normally fire auxiliary fuels during system startup and will cut back on auxiliary fuel feed as the reactor reaches self-sustaining conditions. However, emissions have been estimated conservatively by combining the total emissions associated with firing the worst-case auxiliary fuel at full capacity with the total emissions from fly ash processing.

GHG emissions were also calculated from the STAR[®] reactor. GHG emissions were based on the annual natural gas and propane usages and emissions factors from Table C-1 of Chapter 40, Part 98, Code of Federal Regulations (CFR), Subpart C, along with the loss of ignition of the fly ash. Appendix B provides detailed spreadsheets and example calculations.

3.1.2 MATERIAL HANDLING

The material handling system includes one wet ash raw feed unloading pile, one wet ash storage shed, one wet ash EHE feed hopper, two EHE's, raw feed silos, one loadout silo,



two loadout chutes, transfer silos, a product storage dome, FGD byproduct silo, FGD absorbent silo, screener, crusher, ash basin and handling and haul roads. The silos are each equipped with a bin vent product capture device to minimize product losses associated with the pneumatic transfer process. The truck loadout station uses telescoping chutes and a negative pressure ventilation system to reduce fugitive emissions.

Particulate emissions from the silos were estimated using the maximum short- and long-term transfer rates and appropriate emissions factors from previous STAR[®] facilities.

Trace metal concentration data discussed previously for the STAR[®] system were used in conjunction with the calculated PM emissions rates to estimate emissions of trace metal from the material handling activities. Appendix B contains detailed spreadsheets and example calculations.

3.1.3 FUGITIVE EMISSIONS

Additional particulate emissions were also calculated for the wet ash receiving process, ash handling process (including screening and crushing activities) and haul roads. Windblown fugitive dust emissions were also calculated from the unloading pile. The emissions were calculated using the appropriate emissions factors from AP-42. Appendix B contains detailed spreadsheets and example calculations.

3.1.4 PROJECT EMISSIONS

Table 3-1 presents a summary of the proposed project emissions.



-	Prop Project E	osed missions
Pollutant	lb/hr	tpy
PM	26.52	112.49
PM_{10}	23.50	99.43
PM _{2.5}	13.52	55.73
SO_2	24.94	98.53
NO _x	59.72	198.96
СО	25.01	92.26
VOC	3.21	9.54
Lead	5.30E-04	2.31E-03
GHG (mass basis)		116,599
GHG (CO ₂ e basis)*		116,604
Sulfuric acid mist	0.10	0.44

Table 3-1. Proposed Project Emissions

Note: lb/hr = pound per hour.

 PM_{10} = particulate matter less than or equal to 10 micrometers.

 $PM_{2.5}$ = particulate matter less than or equal to 2.5 micrometers.

 $CO_2e =$ carbon dioxide equivalent.

Source: ECT, 2017.



3.2 <u>MODIFIED PREVENTION OF SIGNIFICANT DETERIORATION AVOID-</u> <u>ANCE CONDITION</u>

Duke Energy will maintain emissions below the Prevention of Significant Deterioration (PSD) avoidance limits under conditions in Section 2.1.D.5.a of Air Permit No. 01812T42 for each PSD pollutant (PM/PM₁₀/PM_{2.5}, SO₂, NO_x, CO, VOCs, sulfuric acid and lead). Specifically, Duke Energy is requesting that the PSD avoidance condition will address each PSD pollutant emissions without any change to the respective avoidance limits indicated in Section 2.1.D.5.a Air Permit No. 01812T42 for the following units:

Existing units:

• Three natural gas/No. 2 fuel oil-fired simple/combined-cycle internal combustion turbines - Lee IC Unit 1A, Lee IC Unit 1B and Lee IC Unit 1C (Units 15, 16 and 17).

Proposed units:

STAR[®] unit (ES-31) and associated sources proposed to support the STAR[®] system as mentioned in Section 1.3.

The PSD Avoidance limits are shown in Table 3-2. Please note that GHG emissions are expected to increase by a value more than the Significant Emission Rate (SER) for GHG emissions. GHG emissions have been categorized as an "anyway" pollutant and require another PSD pollutant to be subject to PSD review before PSD review applies to GHG emissions. Therefore, GHG are not subject to PSD review for the proposed project. The emission calculation methodologies used to prepare the values are provided in Appendix B.



Pollutant	Limits (tpy)		
PM/ PM ₁₀ / PM _{2.5}	218.2		
SO_2	14,663.1		
NO _x	3,414.6		
СО	829.3		
VOC	65.1		
Lead	0.77		
Sulfuric acid mist	64.3		

Table 3-2. PSD Avoidance Limits

Source: Section 2.1.D.5.a of Air Permit No. 01812T42.



3.3 TOXIC EMISSIONS

The toxic permitting emission rate (TPER) analysis was performed using the procedures outlined in 15A NCAC 2Q.0706.

The first step of the TPER analysis is to determine if the modification results in "a net increase in emissions of any toxic air pollutant that the facility was emitting before the modification" or if the modification results in "emissions of any toxic air pollutant that the facility was not emitting before the modification if such emissions exceed the levels contained in Rule .0711." The proposed modification is the installation of the STAR[®] unit and associated equipment. Table 3-3 presents the potential emissions of the TAPs from the proposed modification at the H.F. Lee STAR[®] facility. Please note that the diesel engines (ES-39B and ES-40B) were not included in the TPER analysis per 15A NCAC 2Q.0702 (a)(27). Additional calculation information is provided in Appendix B.

Using the list of TAPs determined from the first step of the TPER analysis, the emissions from the H.F. Lee STAR[®] facility, including the proposed modifications (Table 3-3) and the existing equipment, were compared to the TPERs, presented in Table 3-4, to identify the compounds exceeding their respective TPERs. The emissions for the existing turbines and auxiliary equipment were taken from the Toxic Modeling Analysis Appendix A Table for Potential Emissions (April 2011). Once the compounds exceeding the TPERs were identified, an air dispersion modeling analysis was completed for the whole H.F. Lee STAR[®] facility including the STAR[®] unit, existing combined and simple cycle turbines and auxiliary equipment.

To maximize operational flexibility of the H.F. Lee STAR[®] facility, Duke Energy is requesting permit limits based on the optimization of the potential emissions from the STAR[®] unit and existing equipment, which are presented in Tables 3-5 through 3-7 for the shortterm and annual pollutants, respectively. Appendix B presents the calculations of the potential TAP emissions from the STAR[®] unit and from existing equipment. It also includes summary of the potential and optimized emissions for the H.F. Lee facility.



		Total Emissions	
Compound	lb/hr	lb/day	lb/yr
Sulfuric acid	1.00E-01	2.40	-
Benzene	-	-	3.34
Formaldehyde	7.64E-03	-	-
n-Hexane	-	2.54	-
Toluene	1.32E-03	3.17E-02	-
Arsenic	-	-	8.60
Beryllium	-	-	0.94
Cadmium	-	-	0.61
Chromium VI (Soluble Chromate)	-	4.05E-04	
Manganese	-	3.34E-02	-
Mercury	-	4.64E-04	-
Nickel	-	1.71E-02	-

Table 3-3. Net Emission Increases – Proposed STAR[®] Project



]	Total Emissions	5		TPER			Exceed TPI	ER
Compound	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr
									<u> </u>
Sulfuric acid	270.61	6,494.64		0.025	0.25		YES	YES	
Benzene			1,787.54			8.1			YES
Formaldehyde	11.61			0.04			YES		
n-Hexane		64.18			23.0			YES	
Toluene	4.42	106.11		14.4	98.0		NO	YES	
Arsenic			289.30			0.053			YES
Beryllium			8.86			0.28			YES
Cadmium			124.13			0.37			YES
Chromium VI (Sol- uble Chromate)		2.12			0.013			YES	
Manganese		302.91			0.630			YES	
Mercury		0.46			0.013			YES	
Nickel		1.79			0.013			YES	

Table 3-4. Summary of Potential TAP Emissions from the H.F. Lee facility and Comparison the TPERs



_	Potential	Optimized	Detic of Detertial to
Compound	Emissions (lb/hr)	Emissions (lb/hr)	Optimized Emissions
Formaldehyde	11.61	1,776.30	0.0065
Sulfuric acid	270.61	947.13	0.29
Toluene	4.42	961,534.32	0.0000046

Table 3-5. Comparison of Potential and Optimized 1-hr TAP Emissions from the H.F. Lee Facility



	Potential Optimized		Ratio of Potential	
Compound	Emissions (lb/day)	Emissions (lb/day)	sions	
Sulfuric acid	6,494.64	10,781.10	0.60	
n-Hexane	64.18	138,647.28	0.00046	
Toluene	106.11	11,593,642.41	0.0000092	
Chromic VI	2.12	616.41	0.0034	
Manganese	302.91	62,703.25	0.0048	
Mercury	0.46	1,204.33	0.00038	
Nickel	1.79	232.17	0.0077	

Table 3-6. Comparison of Potential and Optimized Daily TAP Emissions from the H.F. Lee Facility



	Potential	Optimized	Ratio of Potential
Compound	Emissions (lb/yr)	Emissions (lb/yr)	Emissions
Arsenic	289.30	387.55	0.75
Benzene	1,787.54	510,598.49	0.0035
Beryllium	8.86	212.67	0.042
Cadmium	124.13	14,274.49	0.0087

Table 3-7. Comparison of Potential and Optimized Annual TAP Emissions from the H.F. Lee Facility



4.0 REGULATORY ANALYSIS

Federal and state regulations were reviewed to determine their applicability to and implications for the various emissions sources at the H.F. Lee STAR[®] facility. The regulations that may apply only to the proposed emissions sources as a result of modification at the facility are discussed in the following subsections.

EPA promulgated regulations that set the national ambient air quality standards (NAAQS) for seven criteria compounds: SO₂, CO, NO_x, PM₁₀, PM_{2.5}, lead, and ozone (O₃). Two classes of ambient air quality standards have been established: (1) primary standards defining levels of air quality that the EPA has judged as necessary to protect public health; and (2) secondary standards defining levels for protecting soils, vegetation, wildlife, and other aspects of public welfare. Table 4-1 lists the national primary and secondary and state ambient air quality standards in micrograms per cubic meter (μ g/m³). The NC DEQ ambient air quality standards are also included in Table 4-1.

According to 40 CFR §81.334, the current attainment status for the project area, Wayne County, for each of the criteria pollutants is provided in Table 4-2. The proposed facility is located in an area that is in attainment of the NAAQS.

4.1 PSD (40 CFR 52.21)/ 15A NCAC 02D .0530

The determination of whether PSD regulations are applicable to a specific project is conducted in two parts: first dealing with the air quality status of the location of the project and second evaluating the type and quantity of PSD-regulated pollutants that will be emitted. For the regulations to apply to a given project, it must first be determined whether the proposed location is in an area that has been classified as attainment or as unclassifiable. The H.F. Lee facility is in Wayne County, which is designated as attainment or unclassifiable/attainment for all the criteria pollutants.



	Averaging	NAAQS	NAAQS (µg/m ³ †)		NC DEQ Regulation Standards (µg/m ³ †)	
Pollutant	Period*	Primary	Secondary	Primary	Secondary	
SO_2	Annual‡	80	—§	80	—§	
	24-hour‡	365	—§	365	—§	
	1-hour	196	—§	196	—§	
	3-hour	—§	1,300	—§	1,300	
PM_{10}	24-hour	150	150	150	150	
PM _{2.5}	Annual	12	15	12	15	
	24-hour	35	35	35	35	
CO	8-hour	10,000	—§	10,000	—§	
	1-hour	40,000	—§	40,000	—§	
Ozone	8-hour	0.070 ppm	0.070 ppm	0.075 ppm	0.075 ppm	
NO_2	Annual	100	100	100	100	
	1-hour	188	—-§	188	—§	
Lead	3-month£	0.15	0.15	0.15	0.15	

Table 4-1. Ambient Air Quality Standards

Note: ppm = part per million.

ppb = part per billion. $NO_2 = nitrogen dioxide$.

*National short-term ambient standards may be exceeded once per year; annual standards may never be exceeded. North Carolina short-term standards may be exceeded once per year, annual standards may never be exceeded. Ozone standard is attained when the expected number of days of an exceedance is equal to or less than one.

†Standards expressed in micrograms per cubic meter ($\mu g/m^3$) unless otherwise noted.

[‡]Final rule signed June 2, 2010. The 1971 annual and 24-hour SO₂ standards were revoked in this rulemaking. However, these standards remain in effect until one year after an area is designated for the 2010 standard, except in areas designated nonattainment for the 1971 standards, where the 1971 standards remain in effect until implementation plans to attain or maintain the 2010 standard are approved.

§No ambient standard for this pollutant and/or averaging period.

 \pounds The rule signed October 15, 2008, finalized a new lead standard. The 1978 lead standard of 1.5 µg/m³ as a quarterly average remains in effect until one year after an area is designated for the 2008 standard, except in areas designated nonattainment for the 1978 standard, where, the 1978 standard remains in effect until implementation plans to attain or maintain the 2008 standard are approved.

Sources: 40 CFR 50. 15A NCAC 2D .0400.



Pollutant	Attainment Status	
СО	Unclassifiable/attainment	
SO_2	Attainment	
NO_2	Unclassifiable/attainment	
PM_{10}	Unclassifiable/attainment	
PM _{2.5}	Unclassifiable/attainment	
Ozone (8-hour)	Unclassifiable/attainment	
Lead	Unclassifiable/attainment	

Table 4-2. Attainment Status for Wayne County, North Carolina

Source: 40 CFR 81.334.



The project's potential to emit (PTE) is then reviewed to determine whether it constitutes a major stationary source or major modification. A major stationary source is defined as either one of the sources identified in 40 CFR 52.21 and which has a PTE 100 tons or more per year of any regulated pollutant, or any other stationary source which has the PTE 250 tons or more per year of a regulated pollutant. A major modification is defined as a source having an increase in emissions above the PSD significant emission rates.

As explained in Section 3.2, Duke Energy will maintain emissions below the PSD avoidance limits under conditions in Section 2.1.D.5.a of Air Permit No. 01812T42 for each PSD pollutant. Again, GHG emissions are expected to increase by a value more than the Significant Emission Rate (SER) for GHG emissions. GHG emissions have been categorized as an "anyway" pollutant and require another PSD pollutant to be subject to PSD review before PSD review applies to GHG emissions. Therefore, GHG are not subject to PSD review for the proposed project.

4.2 NORTH CAROLINA AMBIENT AIR QUALITY STANDARDS

4.2.1 15A NCAC 2Q .0101 - REQUIRED AIR QUALITY PERMITS

This regulation requires the owner or operator of all sources for which there is an ambient air quality or emission control standard, which is not exempted from permit requirements, to apply for an air quality permit. The owner or operator of a source required to have a permit shall not begin construction or operation of the source without first obtaining a permit. The STAR[®] system and the material handling equipment listed in Section 1.3 are not categorically exempt from permitting. Thus, Duke Energy is submitting this air permit application to obtain a permit prior to any construction or change in method of operation of these sources. Duke Energy will submit a separate Title V permit application within 12 months after the initial start-up of the proposed project.

4.2.2 15A NCAC 2D .0400. AMBIENT AIR QUALITY STANDARDS

The purpose of the ambient air quality standards is to establish certain maximum limits on parameters of air quality considered desirable for the preservation and enhancement of the


quality of the State's air resources. The ambient air quality standards for North Carolina are the same as those promulgated by the EPA. All standards promulgated by the EPA as of June 22, 1988, have been adopted and incorporated by reference as the official ambient air quality standards of the State of North Carolina. Duke Energy expects that the proposed project will be in compliance with the applicable air quality standards.

4.2.3 15A NCAC 2D .0515 – PARTICULATES FROM MISCELLANEOUS INDUSTRIAL PROCESSES

Allowable emissions of particulate matter from any industrial process for which no other emission control standards are applicable shall not exceed the amounts calculated by the following equation:

 $E = 4.10 \text{ x P}^{0.67}$ for $P \le 30$ tons per hour

or

 $E = 55.0 \text{ x } P^{0.11}$ - 40 for P > 30 tons per hour

where: E = allowable emission rate in pounds per hour

P =process weight in tons per hour

Solid fuels charged are considered as part of the process weight, liquid and gaseous fuels and combustion air are not.

Table 4-3 presents the process weight rates and associated allowable emissions for the equipment onsite. Compliance with this requirement is expected and appropriate monitoring and recordkeeping will be performed to verify this expectation.



Emissions Source	Process Rate (tph)	Allowable PM (lb/hr)
EHE (Units1 and 2)	70	47.8
Feed silo filling	125	53.5
Feed silo unloading	75	48.4
FGD Byproduct Silo filling	1.75	5.97
FGD Byproduct Silo unloading	300	63
FGD Absorbent Silo filling	25	35.4
FGD Absorbent Silo unloading	1.5	5.4
STAR [®] Reactor	75	48.4
Storage dome filling	75	48.4
Storage dome unloading	275	62.02
Transfer silo filling	125	53.5
Transfer silo unloading	75	48.4
Loadout	300	63
Loadout chute 1A	100	51.3
Loadout chute 1B	100	51.3
Screener	165	56.4
Crusher	7	15.1

Table 4-3. 15A NCAC 2D .0515 Allowable Emissions

Note: lb/hr = pound per hour.

Source: 15A NCAC 2D .0515.



4.2.4 15A NCAC 02D .0516 – SULFUR DIOXIDE EMISSIONS FROM COMBUSTION SOURCES

Emission of sulfur dioxide from any source of combustion that is discharged from any vent, stack, or chimney shall not exceed 2.3 pounds of sulfur dioxide per million BTU input. Sulfur dioxide formed by the combustion of sulfur in fuels, wastes, ores, and other substances shall be included when determining compliance with this standard. Sulfur dioxide formed or reduced as a result of treating flue gases with sulfur trioxide or other materials shall also be accounted for when determining compliance with this standard.

A source subject to an emission standard for sulfur dioxide in Rules 2D .0524, .0527, .1110, .1111, .1205, .1206, .1210, or .1211 of 15A NCAC shall meet the standard in that particular rule instead of the standard in the above paragraph.

The STAR[®] unit is not subject to any sulfur dioxide standards; therefore, it is subject to the requirements in 2D .0516. Compliance with the emission standard of 2.3 lb/million Btu is expected based on the conceptual design of the SO₂ device. Appropriate monitoring and recordkeeping will be performed to verify this expectation.

4.2.5 15A NCAC 2D .0521 – CONTROL OF VISIBLE EMISSIONS

The intent of this Rule is to prevent, abate and control emissions generated from fuel burning operations and industrial processes where visible emissions can be reasonably expected to occur, except during startup, shutdowns, and malfunctions approved as such according to procedures approved under 15A NCAC 2D .0535.

This Rule shall apply to all fuel burning sources and to other processes that may have a visible emission. However, sources subject to a visible emission standard in Rules .0506, .0508, .0524, .0543, .0544, .1110, .1111, .1205, .1206, .1210, .1211, or .1212 of this Sub-chapter shall meet that standard instead of the standard contained in this Rule.



For sources manufactured after July 1, 1971, visible emissions shall not be more than 20 percent opacity when averaged over a six-minute period. However, except for sources required to install, operate, and maintain continuous opacity monitoring systems (COMS), compliance with the 20 percent opacity limit shall be determined as follows:

- i. No six-minute period exceeds 87 percent opacity;
- ii. No more than one six-minute period exceeds 20 percent opacity in any hour; and
- iii. No more than four six-minute periods exceed 20 percent opacity in any 24-hour period.

Duke Energy assumes the proposed STAR[®] unit and associated sources of air emissions will be subject to this rule. Compliance will be achieved through the use of the proposed emission control equipment.

4.2.6 15A NCAC 02D .0530 PREVENTION OF SIGNIFICANT DETERIORATION

As explained above in Section 4.1, the Project will maintain emissions below the PSD avoidance limits under conditions in Section 2.1.D.5.a of Air Permit No. 01812T42, therefore the PSD review provisions of this rule do not apply.

4.2.7 15A NCAC 2D .0535 - EXCESS EMISSIONS REPORTING AND MALFUNCTIONS

This regulation applies to all permitted facilities and outlines the procedures of reporting excess emissions as a result of malfunctions or operational upsets. The facility owner/operator must notify the appropriate regional office of any excess emissions that last for greater than four hours. This report must be made by 9:00 a.m. Eastern time of the Division's next business day of becoming aware of the occurrence. Notify the Director or designee immediately when the corrective measures have been accomplished. Submit a written report to the Director within 15 days after the request.



4.2.8 15A NCAC 02D .0540 - PARTICULATES FROM FUGITIVE DUST EMIS-SION SOURCES

This rule requires that fugitive dust emissions not cause or contribute to substantive complaints, excessive fugitive dust emissions at the property boundary, or NAAQS violations. Dust emissions from the Ash handling and Loading/Unloading sources are expected to be in compliance. Appropriate monitoring and recordkeeping will be performed to verify this expectation.

4.2.9 15A NCAC 02D .0544 - PREVENTION OF SIGNIFICANT DETERIORATION REQUIREMENTS FOR GREENHOUSE GASES

This rule indicates that a major stationary source or major modification shall not be required to obtain a PSD permit on the sole basis of its greenhouse gases emissions. Duke Energy will maintain emissions below the PSD avoidance limits under conditions in Section 2.1.D.5.a of Air Permit No. 01812T42 for each PSD pollutant, thus, PSD review for GHGs does not apply.

4.2.10 15A NCAC 02D .1100 - CONTROL OF TOXIC AIR POLLUTANTS

This rule applies to all facilities that emit a toxic air pollutant that are required to have a permit under 15A NCAC 2Q .0700. NC DEQ requires any facility that emits a regulated TAP at a rate greater than the TPER, as listed in the 15A NCAC 2Q .0711, demonstrate through air dispersion modeling that emissions from the facility are not resulting in the exceedance of the Acceptable Ambient Level (AAL) for that pollutant, as listed in 15A NCAC 2D .1104. Per 2Q.0700, The H.F. Lee facility has the potential to emit TAPs in excess of de minimis thresholds. Detailed explanation of toxic modeling analyses is presented in Section 5 of this application.

4.2.11 15A NCAC 02D .1200 - CONTROL OF EMISSIONS FROM INCINERATORS

Fly ash is not a waste material; instead, it is a feedstock (or an ingredient) for the H.F. Lee STAR[®] facility. The coal fly ash is a raw material for the proposed H.F. Lee STAR[®] facility. It is required to produce beneficiated product as per the standards of American Society for Testing and Materials (ASTM) Standard C618, and American Association of State



Highway and Transportation Officials (AASHTO) Standard M 295 for pozzolan-grade fly ash.

Based on the determination that fly ash, as proposed to be used, is not a waste material, the H.F. Lee STAR[®] facility is not subject to this requirement. NC DEQ's concurrence with this conclusion is supported by the documentation included in Appendix F.

4.2.12 15A NCAC 02D .1400 - NITROGEN OXIDES

Under this Section Rules .1407 through .1409(b) and .1413 applies to facilities with potential emissions of NO_x equal to or greater than 100 tons per year or 560 pounds per calendar day beginning May 1 through September 30 of any year in the following areas: (1) Cabarrus County; (2) Gaston County; (3) Lincoln County; (4) Mecklenburg County; (5) Rowan County; (6) Union County; and (7) Davidson Township and Coddle Creek Township in Iredell County. The H.F. Lee STAR[®] facility is in Wayne county which is not in the list provided above, hence this rule is not applicable.

Under the same Section Rules .1416 through .1423 apply statewide and Rule .1409(c) applies to Gas Pipeline Stations. Rule .2400 has expired and is no longer valid, Rules .1416, .1417, .1419, .1420, .1421 and .1422 are being repealed and H.F. Lee STAR[®] facility does not fall under the category of a Gas Pipeline Station, hence this section is not applicable. Rule .1418 applies to any fossil fuel-fired stationary boiler, combustion turbine, or combined cycle system having a maximum design heat input greater than 250 million Btu per hour and large reciprocating internal combustion (IC) engines rated at equal to or greater than 2,400 brake horsepower. The H.F. Lee STAR[®] facility is not proposing any boiler or turbine or large IC engine which will meet the definition above, hence Rule .1418 is not applicable.

Under this standard, Rule .1400 is not applicable to incinerator or thermal or catalytic oxidizer used primarily for the control of air pollution, emergency generator, emergency use internal combustion engine and stationary internal combustion engine less than 2400 brake



horsepower that operates no more than the following hours between May 1 and September 30:

- (A) for diesel engines:
 - t = 833,333 / ES
- (B) for natural gas-fired engines:

t= 700,280 / ES

where t equals time in hours and ES equals engine size in horsepower.

There are two stationary internal combustion diesel engines proposed at the site:

- Screener Engine 91 hp, 2,600 hr/yr
- Crusher Engine 300 hp; 365 hr/yr.

Based on the equation provide above the diesel engines will be exempt if they operate less than the following hours:

- Screener Engine 9,157 hours
- Crusher Engine 2,777 hours

The diesel engines will operate less than the allowable hours; therefore, they are exempt.

The STAR[®] process does not meet the definition of a fuel-burning operation or meet the definition of any such unit mentioned previously. The combustion of natural gas or propane during startup is direct-fired with all of the STAR[®] ingredients, including fly ash. As described above, rule .1400 is not applicable to the STAR[®] unit or any other units of the H.F. Lee STAR[®] facility.

4.3 **FEDERAL REGULATIONS**

Federal regulations were reviewed to determine their applicability to the proposed H.F. Lee STAR[®] facility. The federal regulations that were found to be potentially applicable only to the proposed STAR[®] are discussed as follows:



4.3.1 NEW SOURCE PERFORMANCE STANDARDS (NSPS)

NSPS are technology-based standards applicable to new and modified stationary sources. The standards relevant to the proposed H.F. Lee STAR[®] facility are discussed in this subsection.

4.3.1.1 <u>NSPS for Commercial and Industrial Solid Waste Incineration Units</u> (40 CFR 60, Subpart CCCC)

Unless exempt, combustion of a NHSM as defined in 40 C.F.R. Part 241 would subject an emissions unit to 40 CFR 60 Subpart CCCC-Standards Of Performance For Commercial And Industrial Solid Waste Incineration Units (CISWI). In accordance with 40 CFR 241.3(b)(3), "non-hazardous secondary materials used as an ingredient in a combustion unit that meet the legitimacy criteria..." are not solid wastes. Additionally, in accordance with 40 CFR 241.3(b)(4), "...ingredient products that are used in a combustion unit and are produced from the processing of discarded non-hazardous secondary materials and that meet the legitimacy criteria" are not solid wastes. Based on this it is determined that use of fly ash is not a waste but an ingredient. Therefore, the H.F. Lee STAR[®] unit is not subject to CISWI.

4.3.1.2 NSPS for Large Municipal Waste Combustors (40 CFR 60, Subpart Eb)

These standards apply to large municipal waste combustor units with a combustion capacity greater than 250 tons per day of municipal solid waste that initiated construction after September 20, 1994. According to 40 CFR 60.51b, a municipal waste combustor means "any equipment that combusts solid, liquid, or gasified municipal solid waste." Municipal solid waste means household, commercial, retail, or institutional waste and specifically excludes "industrial process or manufacturing wastes." Even if the raw fly ash were considered a solid waste, it does not meet the definition of municipal solid waste. The proposed H.F. Lee STAR[®] unit, therefore, is not subject to the NSPS codified under 40 CFR 60, Subpart Eb.



4.3.1.3 <u>NSPS Subpart IIII—Standards of Performance for Stationary</u> <u>Compression Ignition Internal Combustion Engines</u>

Per 40 CFR 60.4200(a)(2), the provisions of this subpart are applicable to, "Owners and operators of stationary compression ignition internal combustion engines that commence construction after July 11, 2005, where the stationary compression ignition internal combustion engines are:

- (i) Manufactured after April 1, 2006, and are not fire pump engines, or
- (ii) Manufactured as a certified National Fire Protection Association fire pump engine after July 1, 2006."

The diesel-fired engines will commence construction (be ordered) after July 11, 2005, and be manufactured after April 1, 2006; therefore, are subject to 40 CFR 60, Subpart IIII, Standards of Performance for Stationary Compression Ignition Internal Combustion Engines. Per 40 CFR 60.4201(a), Stationary CI internal combustion engine manufacturers must certify their 2007 model year and later non-emergency stationary CI ICE with a maximum engine power less than or equal to 2,237 kilowatt (KW) (3,000 horsepower (HP)) and a displacement of less than 10 liters per cylinder to the certification emission standards for new nonroad CI engines in 40 CFR 89.112, 40 CFR 89.113, 40 CFR 1039.101, 40 CFR 1039.102, 40 CFR 1039.104, 40 CFR 1039.105, 40 CFR 1039.107, and 40 CFR 1039.115, as applicable, for all pollutants, for the same model year and maximum engine power. Proposed diesel engines (ES-39B and ES-40B) have displacement less than 10 liters per cylinder to the certification this rule are applicable. Duke Energy will comply with all applicable Subpart IIII emissions limitation, monitoring, recordkeeping, and reporting requirements.

4.3.2 NATIONAL EMISSION STANDARD FOR HAZARDOUS AIR POLLU-TANT (NESHAP)

NESHAP are standards for HAPs from stationary sources. In general, the 40 CFR 63 NESHAP are only applicable to major HAP sources (i.e., facilities that have potential emissions of an individual HAP of 10 tpy or more and potential emissions of total HAPs of 25 tpy or more). The H.F. Lee facility has potential HAP emissions above the NESHAP



standard. Therefore, the H.F. Lee facility is a major source of HAP emissions. The applicability of relevant NESHAP is discussed in the following subsections.

4.3.2.1 <u>NESHAP for Stationary Reciprocating Internal Combustion Engines (40</u> <u>CFR 63, Subpart ZZZZ)</u>

NESHAP Subpart ZZZZ applies to new and existing internal combustion engines located at major and area sources. The engines associated with the screening and crushing are subject to Subpart ZZZZ. Since the engines are new and located at a major source of HAP, the requirements of 40 CFR 60, Subpart IIII, must be met to meet the requirements of Subpart ZZZZ. The engines will meet applicable NSPS requirements.

4.3.2.2 <u>NESHAP for Industrial, Commercial and Institutional Boilers and Process</u> <u>Heaters (40 CFR 63, Subpart DDDDD)</u>

40 CFR 63 Subpart DDDDD, establishes national emission limitations and work practice standards for HAP emitted from industrial, commercial, and institutional boilers and process heaters located at major sources of HAP. None of the proposed units at the H.F Lee STAR[®] facility meet the definition of a boiler or a process heater under 40 CFR 63.7575. Therefore, the STAR[®] system is not subject to the NESHAP codified under 40 CFR 63, Subpart DDDDD.

4.3.2.3 <u>NESHAP for Industrial, Commercial and Institutional Boilers Area</u> <u>Sources (40 CFR 63, Subpart JJJJJJ)</u>

These standards apply to industrial, commercial, and institutional boilers at an area source of HAP. An area HAP source is defined as a facility that has the potential to emit less than 10 tpy of any individual HAP or less than 25 tpy of any combination of HAPs (40 CFR 63.2). The H.F. Lee facility is major source of HAPs. Therefore, no sources are subject to the NESHAP codified under 40 CFR 63, Subpart JJJJJJ. In addition, no proposed units for the project meet the definition of a boiler under 40 CFR 63.11237.



4.3.3 40 CFR 64 - COMPLIANCE ASSURANCE MONITORING REGULA-TIONS

On October 27, 1997, EPA promulgated the Compliance Assurance Monitoring (CAM) Rule, 40 CFR Part 64, which addresses monitoring for certain emission units at major sources, thereby assuring that facility owners and operators conduct effective monitoring of their air pollution control equipment. In order to be subject to CAM, the following criteria must be met:

- The unit is subject to an emissions limitation or standard for the pollutant of concern;
- An "active" control device is used to achieve compliance with the emission limit; and
- The emission unit's pre-control potential-to-emit is greater than the applicable major source threshold.

For emissions of SO₂ from the STAR® system (ES-31), Duke Energy is subject to CAM requirements for the state SO₂ standard, i.e., 2.3 lb/MMBtu per 15A NCAC 02D .0516. A preliminary draft of a CAM plan is included in Appendix G for the agency's review.



5.0 AIR QUALITY IMPACT ASSESSMENT

5.1 MODEL SELECTION

For this modeling analysis, the American Meteorological Society (AMS)/EPA Regulatory Model Improvement Committee (AERMIC) model (AERMOD) system components were used. These include the existing regulatory components (AERMOD, AERMOD meteorological preprocessor program [AERMET], AERMOD terrain preprocessor program [AER-MAP], and Building Profile Input Program [BPIP] for Plume Rise Model Enhancement [PRIME] [BPIPPRM]), AERSURFACE and AERMINUTE. AERMOD (Version 16216r) was used in the refined modeling analyses for flat, elevated, and complex terrain.

The procedures used in conducting the air quality modeling analyses followed the requirements outlined in the 40 CFR 51, Appendix W, Guidelines on Air Quality Models; NC DEQ Air Toxic Quality Modeling Guidelines, February 2014; and direction received from the NC DEQ Modeling Section. Supporting information for the air quality modeling study included building downwash analyses, meteorological data, and terrain data.

5.1.1 PHYSICAL SOURCE GEOMETRY/GOOD ENGINEERING PRACTICE STACK HEIGHT ANALYSIS

A good engineering practice (GEP) stack height/building wake effect analysis was conducted to identify which building structures influence plume dispersion from each emissions source. Based on the formula, GEP stack height and region of influence, the Building Profile Input Program (BPIP) PRIME program was run for the point source emissions points and related building structures. Figure 5-1 shows the H.F. Lee facility layout (including the modeled sources) and property lines. The BPIP PRIME (Version 04274 dated September 30, 2004) program was used to calculate the GEP height and wind directionspecific building dimensions for input to the air dispersion model.

The GEP analysis was used to identify critical buildings and to determine wind directionspecific building dimensions for use in the modeling analysis. GEP was also used to



demonstrate compliance with applicable state and federal stack height regulations. Following the Guideline for Determination of GEP Stack Height (Technical Document for the Stack Height Regulation), GEP height was calculated using the following equation:

```
Hg = H + 1.5 L
```

where: Hg = good engineering practice stack height.

- H = height of the structure or nearby structure.
- L = lesser dimension (height or projected width of the structure or nearby building).

In a situation where a nearby structure consists of multiple tiers or there are several structures nearby, the GEP height was calculated for each tier or structure, and the one resulting in the greatest calculated GEP height determined both the GEP height and the wind direction-specific building dimension used when modeling a stack that is lower than the GEP height.

The direction-specific building dimensions obtained from the BPIP PRIME analysis were put into the air dispersion model to simulate the effects of building-induced downwash. The BPIP files are included with the air dispersion modeling files on the DVD included in Appendix E.





5.1.2 LOCAL TOPOGRAPHY

Local topography played an important role in the selection of the appropriate dispersion model. Available dispersion models can be divided into two general categories: those applicable to terrain that is below stack top (simple terrain) and above stack top (complex terrain). The terrain near the H.F. Lee facility can be described as generally flat terrain. A model that simulated both simple and complex terrain was used.

5.2 AERMOD MODEL APPLICATION

The AERMOD modeling system consists of two preprocessors and the dispersion model. AERMET is the meteorological preprocessor component, and AERMAP is the terrain preprocessor component that characterizes the terrain and generates receptor elevations along with critical hill heights for those receptors.

AERMOD has the following capabilities applicable to this study:

- Handles all terrain features.
- Simulates PRIME aerodynamic building downwash.
- Simulates both short- and long-term averaging periods.
- Handles large numbers of receptors.
- Calculates concentrations within the building cavity and within 5L of the stack.

5.2.1 METEOROLOGICAL DATA

For this project, refined modeling analyses were conducted using a data set downloaded from the NC DEQ Website that consisted of 5 years (2012 through 2016) of hourly meteorological data from Rocky Mount-Wilson, North Carolina (surface), and Newport, North Carolina (upper air). This data set was processed by NC DEQ.

5.2.2 RECEPTORS AND TOPOGRAPHY FOR AERMOD

A single nested Cartesian receptor grid was generated for use in the AERMOD refined modeling. Receptors were spaced 100 meters apart along the property boundary, except where a source was within 100 meters, receptors were spaced 25 meters apart. Receptors



were spaced 100 meters apart extending from the property boundary out to 1,000 meters. Receptors were spaced 500 meters apart extending from 1,000 meters out to 10,000 meters. The receptor grid used in the modeling analysis was based on North American Datum of 1983 (NAD 83) and in Zone 17. The AERMAP (Version 11103) processor program was used to calculate terrain elevations and critical hill heights for the receptor grid (NAD 83 and Zone 17) using National Elevation Data (NED). The NED dataset was downloaded from the Multi-Resolution Land Characteristics Consortium (MRLC) website.

The base elevation for the buildings and emissions sources was also obtained from the NED. The base elevation for each building and emission source was then manually adjusted to be the lowest elevation for the buildings and sources in a particular area.

5.2.3 PHYSICAL SOURCE AND EMISSIONS DATA

The air dispersion modeling analysis was conducted with emissions rates and exhaust characteristics (flow rate and temperature) that are expected to represent the worst-case parameters for the proposed and existing sources.

Please note that this toxic analysis included the existing combustion turbines in combinedcycle mode at 100-percent load with duct burners and in simple-cycle mode at 100-percent load with evaporative cooler to account for the worst-case stack parameters. The annual emissions were modeled with four scenarios that are based on the following combinations:

- <u>Scenario #1</u>—Each combustion turbine operating in:
 - Combined-cycle mode for 6,760 hours per year (hr/yr) operating on natural gas.
 - Simple-cycle mode for 1,000 hr/yr operating on natural gas and 1,000 hr/yr operating on fuel oil.
- <u>Scenario #2</u>—Each combustion turbine operating in:
 - Combined-cycle mode for 5,760 hr/yr operating on natural gas and 1,000 hr/yr operating on fuel oil.
 - Simple-cycle mode for 2,000 hr/yr operating on natural gas.



- <u>Scenario #3</u>—Each combustion turbine operating in combined-cycle mode for 8,760 hr/yr operating on natural gas.
- <u>Scenario #4</u>—Each combustion turbine operating in combined-cycle mode for 7,760 hr/yr operating on natural gas and 1,000 hr/yr operating on fuel oil.

Tables 5-1 through 5-3 provide summaries of the exhaust data. Tables 5-4 through 5-6 present summaries of optimized emission rates for the air pollutants addressed in this modeling analysis.



Source ID and Description	Stack Height (ft)	Stack Diameter (ft)	Temperature (°F)	Exit Velocity (fps)€
Existing Units				
SC_FO10 & SC_FO11 – Unit 10 & 11*	100	20	962.01	129.10
SC_FO12 & SC_FO13 – Unit 12 & 13*	115	18	1,065.99	154.90
SC_FO14 – Unit 40	115	18	1,065.99	151.80
SC_NG10 & SC_NG11 – Unit 10 & 11*	100	20	973	129.80
SC_NG12 & SC_NG13 – Unit 12 & 13*	115	18	1,068.01	150.90
SC_NG14 – Unit 40	115	18	1,068.01	147.90
CC_NG15, CC_NG16 & CC_NG17 – Unit 15, 16 & 17 (100% w/ Evap Clr)*	175	18	171	65.28
CC_F015, CC_F016 & CC_F017 – Unit 15, 16&17 (Base Load w/ Evap Clr)*	175	18	260.01	76.09
SC_NG15, SC_NG16 & SC_NG17 – Unit 15, 16 & 17 (100% w/ Evap Clr)*	120	22	1,087	111.35
SC_F015, SC_F016 & SC_F017 – Unit 15, 16&17 (Base Load w/ Evap Clr)*	120	22	1,053	109.11
AUX_BLR – Auxiliary Boiler	55	3	570	47.50
FGH – Fuel Gas Heater	25	2	717.01	18.91
DPH15, DPH16 & DPH17 – Dew Point Heater for Unit 15, 16 & 17*	45	1.30	70	6.30
FWP – Fire Water Pump	20	0.50	840	119.18
EXST_FGH – Fuel Gas Heater at Wayne site	25	2	717.01	18.91
Proposed Units				
EP30 (ES-30A&B) – Feed Silo	111	1.5	70	0.003281
EP31 (ES-31) – STAR [®] Reactor (Exhaust Stack)	110	4	155	102.79
EP34 (ES-34) – EHE – 1 (Dust Collector)	51	4	187	55.11
EP35 (ES-35) – EHE – 2 (Dust Collector)	51	4	187	55.11
EP36 (ES-36A&B) – Transfer Silo	100	0.667	70	0.003281
EP37 (ES-37A&B) – Storage Dome (Ash)	125	1.5	70	0.003281
EP38 (ES-38) – Loadout Silo (1500 Ton)	111	1.5	70	0.003281
EP38A (ES-38A) – Loadout Silo Chute 1A	111	1.5	70	0.003281
EP38B (ES-38B) – Loadout Silo Chute 1B	111	1.5	70	0.003281

Table 5-1. Source Parameters—Existing and Proposed Point Sources

Note: ${}^{\circ}F =$ degree Fahrenheit. fps = foot per second. ft = foot.

 ${\ensuremath{\in}}$ Horizontal exhaust orientation is represented as 0.003281 fps.

* Stack parameters for individual stack units.



Source ID and Description	Release Height (ft)	Initial Horizontal Dimension (ft)	Initial Vertical (ft)
FEP1 (F-1) - wet ash receiving, transfer to storage shed FEP2 (F-2) - wet ash receiving, transfer to hopper	5	29.76	13.94
	10	6.99	6.99

Table 5-2. Source Parameters—Proposed Volume Sources

Note: ft = foot.



Source ID and Description	Release Height (ft)	Easterly Length (ft)	Northerly Length (ft)	Angle from North (degree)
FEP3 (F-3) – Unloading Pile FEP4A/4B/4C (F-4/F-5/EP39A/EP-40A) – Ash Basin/Ash Handling/Screener/Crusher	4 10	119.75 660.0	Default Default	Default Default

Note: ft = foot.



								Emi	ssions Rates (I	b/hr)						
Pollutant	Averag- ing Pe- riod	SC_FO10 &11*	SC_FO12 &13*	SC_FO14	SC_NG10 &11*	SC_NG12 &13*	SC_NG14	CC_NG1 5,16&17*	CC_FO15 ,16&17*	SC_NG15 ,16&17*	SC_FO15 ,16&17*	AUX_BL R	FGH	DPH15,1 6&17*	FWP	EXST_F GH
Formaldehyde	1-HR	8.25E+01	7.79E+01	8.71E-01	2.10E+02	1.97E+02	2.11E+02	2.49E+02	9.23E+01	2.42E+02	9.23E+01	9.56E-01	5.06E-02	4.50E-02	7.68E-01	6.18E-02
Sulfuric Acid Mist	1-HR	2.84E+01	2.83E+01	2.80E+01	3.19E+00	2.91E+00	2.91E+00	3.61E+00	2.68E+02	6.65E-01	5.84E-01					
Toluene	1-HR	1.55E+05	1.47E+05	1.64E+05	5.44E+04	5.13E+04	5.48E+04	6.39E+04		6.29E+04		3.81E+01	3.26E+00	2.89E+00	3.78E+02	3.98E+00
Sulfuric Acid Mist	24-HR	1.35E+01	1.34E+01	1.33E+01	1.51E+00	1.38E+00	1.38E+00	1.71E+00	1.27E+02	3.15E-01	2.77E+01					
Hexane	24-HR							1.81E+03				3.39E+02	1.80E+01	1.60E+01		2.20E+01
Toluene	24-HR	7.81E+04	7.39E+04	8.24E+04	2.73E+04	2.58E+04	2.75E+04	3.21E+04		3.16E+04		1.91E+01	1.64E+00	1.45E+00	1.90E+02	2.00E+00
Chromium VI (Sol-																
uble Chromate)	24-HR	1.00E+00	9.46E-01	1.06E+00				1.81E-01	6.90E+00		6.90E+00	3.40E-02	1.80E-03	1.60E-03		2.20E-03
Manganese	24-HR	3.15E+02	2.98E+02	3.31E+02				3.50E-02	3.52E+02		3.52E+02	6.56E-03	3.48E-04	3.08E-04		4.24E-04
Mercury	24-HR	6.04E+00	5.70E+00	6.38E+00				3.00E-01	6.74E+00		6.74E+00	5.67E-02	3.00E-03	2.67E-03		3.66E-03
Nickel	24-HR	1.15E+00	1.09E+00	1.21E+00				1.21E-01	1.29E+00		1.29E+00	2.28E-02	1.20E-03	1.07E-03		1.47E-03
Arsenic	Annual‡	6.53E-03	6.17E-03	6.89E-03				1.20E-04	3.65E-03		3.65E-03	2.25E-05	1.19E-06	3.17E-06		
Benzene	Annual‡	7.26E+00	6.84E+00	7.65E+00	1.58E+00	1.49E+00	1.60E+00	7.39E+00	3.71E+00	1.67E+00	4.05E+00	5.25E-02	2.78E-03	7.41E-03	6.78E-02	7.77E-04
Beryllium	Annual‡	3.26E-03	3.10E-03	3.46E-03				1.28E-04	1.83E-03		1.83E-03	2.40E-05	1.27E-06	3.38E-06		3.55E-07
Cadmium	Annual‡	2.43E-01	2.29E-01	2.56E-01				5.62E-02	1.32E-01		1.36E-01	1.05E-02	5.58E-04	1.48E-03		1.55E-04

Table 5-4. Modeled (Optimized) Emission Rates-Existing Units Point Sources

* Stack emission rates are for individual stacks.

‡ Emission rate is the overall maximum emission rate considered over the four operating scenarios.



	Averaging					Emissions Ra	ates (lb/hr)			
Pollutant	Period	EP30	EP31	EP34	EP35	EP36	EP37	EP38	EP38A	EP38B
Formaldehyde	1-HR		6.75E-01							
Sulfuric Acid Mist	1-HR		3.50E-01							
Toluene	1-HR		4.35E+01							
Sulfuric Acid Mist	24-HR		1.66E-01							
Hexane	24-HR		2.40E+02							
Toluene	24-HR		2.19E+01							
Chromium VI (Soluble										
Chromate)	24-HR	1.90E-06	3.23E-03	1.34E-03	1.34E-03	1.90E-06	3.32E-06	2.85E-06	9.49E-07	9.49E-07
Manganese	24-HR	1.10E-04	1.91E-01	7.70E-02	7.70E-02	1.10E-04	1.92E-04	1.64E-04	5.46E-05	5.46E-05
Mercury	24-HR	4.08E-06	4.70E-02	2.87E-03	2.87E-03	4.08E-06	7.13E-06	6.11E-06	2.04E-06	2.04E-06
Nickel	24-HR	2.95E-05	6.64E-02	2.08E-02	2.08E-02	2.95E-05	5.17E-05	4.43E-05	1.48E-05	1.48E-05
Arsenic	Annual‡	2.31E-07	8.82E-04	3.58E-04	3.58E-04	2.31E-07	2.32E-07	1.16E-07	5.79E-08	5.79E-08
Benzene	Annual‡		3.71E-02							
Beryllium	Annual‡	4.54E-07	1.71E-03	7.01E-04	7.01E-04	4.54E-07	4.54E-07	2.27E-07	1.13E-07	1.13E-07
Cadmium	Annual‡	9.22E-08	7.80E-03	1.42E-04	1.42E-04	9.22E-08	9.22E-08	4.62E-08	2.31E-08	2.31E-08

Table 5-5. Modeled (Optimized) Emission Rates—Proposed Units Point Sources

	Averaging		Emissions F	Rates (lb/hr)	
Pollutant	Period	FEP1	FEP2	FEP3	FEP4A/4B/4C
Formaldehyde	1-HR				
Sulfuric Acid Mist	1-HR				
Toluene	1-HR				
Sulfuric Acid Mist	24-HR				
Hexane	24-HR				
Toluene	24-HR				
Chromium VI (Soluble Chromate)	24-HR	2.91E-07	5.85E-07	6.11E-07	3.26E-04
Manganese	24-HR	1.68E-05	3.37E-05	3.52E-05	1.87E-02
Mercury	24-HR	6.27E-07	1.25E-06	1.31E-06	6.98E-04
Nickel	24-HR	4.55E-6	9.10E-06	9.52E-06	5.06E-03
Arsenic	Annual‡	5.09E-08	1.02E-07	1.63E-07	8.75E-05
Benzene	Annual‡				
Beryllium	Annual‡	9.97E-08	1.99E-07	3.20E-07	1.68E-04
Cadmium	Annual‡	2.02E-08	4.04E-08	6.49E-08	3.41E-05

Table 5-6. Modeled (Optimized) Emission Rates-Proposed Volume and Area Sources

‡ Emission rate is the overall maximum emission rate considered over the four operating scenarios.

5.3 MODELING RESULTS

This section presents the results of the air quality impact analyses performed for the H.F. Lee STAR[®] facility. The air quality analyses were conducted using the inputs and methodologies described previously. Methodologies and protocols adhere to the EPA and NC DEQ Guidelines. In accordance with NC DEQ requirements, Appendix E contains a DVD containing the modeling input and output files.

Optimized emissions from the equipment were modeled with AERMOD to estimate the maximum concentrations for the pollutants and corresponding averaging period for each year of meteorological data. Table 5-7 provides a summary of the AERMOD modeling results for each pollutant with the optimized emission rates and averaging period for the Cartesian grid and fenceline receptors discussed in Section 5.2.2.

Based on the results, the H.F. Lee STAR[®] facility demonstrates compliance with 15A NCAC 02Q .0700.



	Averaging			Mode	eled Impact (µ	g/m ³)		Maximum Impact	Maximum Allowable Concentration	Percent of AAL	Complies
Chemical	Period	Rank	2012	2013	2014	2015	2016	$(\mu g/m^3)$	$(\mu g/m^3)$	(%)	(Yes/No)
Formaldehyde	1-HR	Н	107.58	131.19	140.91	106.71	98.47	140.91	150	93.9	Yes
Sulfuric Acid Mist	1-HR	Н	76.02	91.01	91.61	68.44	71.39	91.61	100	91.6	Yes
Toluene	1-HR	Н	46,702.41	46,920.21	53,600.71	39,975.63	47,744.78	53,600.71	56,000	95.7	Yes
Sulfuric Acid Mist	24-HR	Н	5.90	10.51	7.62	7.80	8.68	10.51	12.00	87.6	Yes
Hexane	24-HR	Н	1,039.88	807.94	933.07	1063.46	961.91	1,063.46	1,100	96.7	Yes
Toluene	24-HR	Н	4,327.50	4,244.73	4,502.69	3,435.96	3,309.75	4,502.69	4,700	95.8	Yes
Chromium VI (Soluble Chromate)	24-HR	Н	0.33	0.58	0.43	0.44	0.48	0.58	0.62	93.5	Yes
Manganese	24-HR	Н	26.12	29.13	27.13	21.64	24.13	29.13	31	94.0	Yes
Mercury	24-HR	Н	0.50	0.57	0.52	0.44	0.48	0.57	0.60	95.4	Yes
Nickel	24-HR	Н	0.55	0.53	0.44	0.59	0.42	0.59	0.60	98.4	Yes
Arsenic	Annual‡	Н	2.02E-03	1.93E-03	1.64E-03	1.84E-03	1.61E-03	2.02E-03	2.10E-03	96.2	Yes
Benzene	Annual‡	Н	8.65E-02	1.15E-01	7.48E-02	7.99E-02	9.08E-02	1.15E-01	1.20E-01	95.9	Yes
Beryllium	Annual‡	Н	3.94E-03	3.77E-03	3.21E-03	3.60E-03	3.16E-03	3.94E-03	4.10E-03	96.1	Yes
Cadmium	Annual‡	Н	5.15E-03	5.04E-03	5.37E-03	5.21E-03	4.69E-03	5.37E-03	5.50E-03	97.6	Yes

Table 5-7. Results for AERMOD Dispersion Modeling using Optimized Emission Rates

Note: $\mu g/m^3 =$ microgram per cubic meter. H = highest.

\$Maximum concentration is the overall maximum ground level impact considered over the four operating scenarios.

APPENDIX A

AIR PERMIT APPLICATION FORMS



FORM A GENERAL FACILITY INFORMATION

VISED 09	/22/16	NCDEQ/Division of /	Air Quality - Ap	Opplication for Air Permit to Construct/Operate					
	Local Zoning Consistency Determi	nation (new or	LNOIBER	PROCESSED WITHOUT THE FOLLOWING:					
	modification only)			ate Number of Copies of Application					
Ø	Responsible Official/Authorized Co	ntact Signature	2 P	P.E. Seal (if required)					
12.33			GENERAL	INFORMATION					
gal Corpo	rate/Owner Name: Duke En	ergy Progress, LLC							
e Name:	H.F. Lee Steam Electric Plant								
e Address	(911 Address) Line 1: 1199 Bla	ck Jack Church Road							
e Address	Line 2.								
ly:	Goldsboro			State: NC					
Code	27530			County. Wayne					
-			CONTACT	INFORMATION					
sponsible	Official/Authorized Contact:			Invoice Contact:					
me/Title:	Jeffery D. Hines / General Manage	r II, H.F. Lee Steam Electric F	Plant	Name/Title: Cynthia Winston/ Manager, Permitting & Compliance, Carolinas					
illing Addre	ess Line 1: 1199 Black Jack Church R	pad		Mailing Address Line 1: 410 S. Wilmington Street					
iling Addre	ess Line 2.		-	Mailing Address Line 2:					
y: Golds	sboro State NC	Zip Code: 2753	30	City: Raleigh State NC Zip Code 27601					
mary Phor	ne No.: 919-722-6450	Fax No.		Primary Phone No.: (919)-546-5538 Fax No.:					
condary P	hone No.:			Secondary Phone No.					
iall Addres	s. jeitery ninesi@duke-energy.com	a		Email Address: Cynthia Winston@duke-energy.com					
cility/Insp	ection Contact:			Permit/Technical Contact:					
me/Title	Mike Graham, Sr. EHS Profession	al		Name/Title: Erin Wallace, Sr. Environmental Specialist					
ung Addre	ess Line 1. 1199 Black Jack Church R	oad		Mailing Address Line 1: 410 S. Wilmington Street					
ung Addre	ess Line 2.			Mailing Address Line 2					
y Golds	Sboro State NC	Zip Code: 275	30	City Raleigh State NC Zip Code: 27601					
mary Phor	10 No.: 919-722-6551	Fax No.		Primary Phone No.: 919-546-5797 Fax No.:					
ondary P	none No	· · · · · · · · · · · · · · · · · · ·		Secondary Phone No.					
nai Auures	a. Intergrandinz@duke-energy.com	ADI	LICATION	Email Address: erin.wallace@duke-energy.com					
New	Non-nermitted Facility/Greenfield	Modification of East	by (permitted)						
Nam	e Change Ownership Change	e Administrative Amor	ndment						
		FACILITY CLASSIFI	CATION AF	TER APPLICATION (Check Only One)					
	General	Small		Prohibitory Small Synthetic Minor Title V					
100		FAC	LITY (Plan	It Site) INFORMATION					
		olium Elevin, Piant - Ger	TER BILLIN UT BIEC	Facility ID No. 9600017					
rimary SIC/	NAICS Code: 4911			Current/Previous Air Permit No. 01812T42 Expiration Date: 06/30/2020					
acility Coord	dinates	Latitude: 764252.694		Longitude: 3919730.81					
oes this ap onfidential	oplication contain 🛛 🗍	YES 🗹 NO	•	***If yes, please contact the DAQ Regional Office prior to submitting this application.*** (See Instructions)					
and the second		PERSON O	R FIRM THA	AT PREPARED APPLICATION					
erson Nam	e: Thomas O. Pritcher			Firm Name: Environmental Consulting & Technology, Inc.					
ailing Addr	ess Line 1: 7208 Falls of Neuse Road,	Suite 102		Mailing Address Line 2:					
ty: Raleigh		State: NC		Zip Code: 27615 County: Wake					
hone No.:	(919) 861-8888	Fax No.:		Email Address: tpritcher@ectinc.com					
		SIGNATURE OF RE	SPONSIBL	E OFFICIAL/AUTHORIZED CONTACT					
ame (typed	i): Jeffery D. Hines			Title: General Manager II, H.F. Lee Steam Electric Plant					
Signature	(Blue Ink)	in		Date: 11/6/2017					
	117	Attach Add	ditional Sh	neets As Necessary Page					

FORM A (continued, page 2 of 2) GENERAL FACILITY INFORMATION

REVISED 09/	/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate	Α
	SECTION AA1 - APPLICATION FOR NON-TITLE V PERMIT RENEWAL	
	(Company Name) hereby formally requests renewal of Air Permit No.	
There have be	een no modifications to the originally permitted facility or the operations therein that would require an air permit since the last permit was issued.	-
Is your facility	subject to 40 CFR Part 68 "Prevnetion of Accidental Releases" - Section 112(r) of the Clean Air Act?	
If yes, have ye	ou already submitted a Risk Manage Plan (RMP) to EPA?	-
If no, did you	n a current emissions inventory?	
		_
In accordance	a with the provisions of Title 15A 20, 0512, the responsible official of	
hereby formal	llv requests renewal of Air Permit No. (Air Permit No.) and further certifies that:	
(1)	The current air quality permit identifies and describes all emissions units at the above subject facility, except where such units are exempted under the	
	North Carolina Title V regulations at 15A NCAC 2Q .0500;	
(2)	The current air quality permit cits all applicable requirements and provides the method or methods for determing compliance with the applicable requirements;	
(3)	The facility is currently in compliance, and shall continue to comply, with all applicable requiremetns. (Note: As provided under 15A NCAC 2Q .0512	
	compliance with the conditions of the permit shall be deemed compliance with the applicable requirements specifically identified in the permit);	
(4)	For applicable requirements that become effective during the term of the renewed permit that the facility shall comply on a timely basis;	
(5)	The facility shall fulfill applicable enhanced monitoring requirements and submit a compliance certification as required by 40 CFR Part 64.	
The responsit	ble official (signature on page 1) certifies under the penalty of law that all information and statements provided above, based on information and belief	
	SECTION AA3- APPLICATION FOR NAME CHANGE	
New Facility N	Name:	
Former Facilit	ty Name:	
An official faci	ility name change is requested as described above for the air permit mentioned on page 1 of this form. Complete the other sections if there have been	
modifications	to the originally premitted facility that would requie an air quality permit since the last permit was issued and if ther has been an ownership change	
associated wi	ith this name change.	
	SECTION AA4- APPLICATION FOR AN OWNERSHIP CHANGE	
By this applica	ation we hereby request transfer of Air Quality Permit No. from the former owner to the new owner as described below.	
The transfer o	of permit responsibility, coverage and liability shall be effective (immediately or insert date.) The legal ownership of the	
facility describ	bed on page 1 of this form has been or will be transferred on (date). There have been no modifications to the originally	
permitted faci	lity that would require an air quality permit since the last permit was issued.	
Signature of N	New (Buyer) Responsible Official/Authorized Contact (as typed on page 1):	
X Signature (E	Blue Ink):	
Date:		
New Facility N	Name:	
Former Facilit	ty Name:	
Signature of F	Former (Seller) Responsible Official/Authorized Contact:	
Name (typed	or print):	
Title:		
X Signature (E	Blue Ink):	
Date:		
Former Legal	Corporate/Owner Name:	
	In lieu of the seller's signature on this form, a letter may be submitted with the seller's signature indicating the ownership change	
	SECTION AA5- APPLICATION FOR ADMINISTRATIVE AMENDMENT	
Describe the I	requested administrative amendment here (attach additional documents as necessary):	

FORMs A2, A3 EMISSION SOURCE LISTING FOR THIS APPLICATION - A2

112r APPLICABILITY INFORMATION - A3

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate					
	EMISSION SOURCE LISTING: New, Modified	, Previously Unpe	ermitted, Replaced, Deleted		
EMISSION SOURCE	EMISSION SOURCE	CONTROL DEVICE	CONTROL DEVICE		
ID NO.	DESCRIPTION	ID NO.	DESCRIPTION		
	Equipment To Be ADDED By This Application	(New, Previously	Unpermitted, or Replacement)		
ES-30A	Eeed Silo Filling	CD-30	Bin Vent		
ES-30B	Feed Silo Unloading	CD-30	Bin Vent		
ES-31	STAR® Reactor	CD-31A & CD-31B	Scrubber and Bagbouse		
ES-32	EGD Byproduct Silo	CD-32	Bin Vent		
ES-33	FGD Absorbent Silo	CD-33	Bin Vent		
ES-34	EHE- External Heat Exchanger 1	CD-34	Baghouse		
ES-35	EHE- External Heat Exchanger 2	CD-35	Baghouse		
ES-36A	Transfer Silo Filling	CD-36	Bin Vent		
ES-36B	Transfer Silo Unloading	CD-36	Bin Vent		
ES-37A	Storage Dome Filling	CD-37	Bin Vent		
ES-37B	Storage Dome Unloading	CD-37	Bin Vent		
ES-38		CD-38	Bin Vent		
ES-38A	Loadout Silo Chute 1A	CD-38A	Bin Vent		
ES-38B	Loadout Silo Chute 1A	CD-38B	Bin Vent		
ES-39A	Screener	N/A	N/A		
ES-30B	Screener-Diesel Engine	N/A	N/A		
ES-40A	Crusher	N/A	N/A		
ES 40R	Crusher Dissel Engine	N/A	N/A		
E3-40B	Wet Ach Respiring Transfer to Shed	N/A			
r-1	Wet Ash Receiving-Transfer to Shed	IN/A			
F-2	Wet Ash Receiving-Transfer to Hopper	N/A	N/A		
F-3	Wet Ash Receiving-Onloading Pile	N/A	N/A		
F-4	Ash Basin	N/A	N/A		
F-5	Asn Handling	N/A	N/A		
F-6	Haul Roads		N/A		
	Existing Permitted Equipment To E		/ This Application		
	Equipment To Be DELE	TED By This App	lication		
1					

112(r) APPLICABILITY INFORMATION										
Is your facility subject to 40 CFR Part 68 "Prevention of Accidental Releases" - Section 112(r) of the Federal Clean Air Act? 🛛 Yes 🗹 No										
If No, please specify in detail how your facility avoided applicabilit	Facility does not use, store or handles any of the regulated substances listed unde this rule above their respective threshold quantity.									
If your facility is Subject to 112(r), please complete the following:	If your facility is Subject to 112(r), please complete the following:									
A. Have you already submitted a Risk Management Plan (RMP) to EPA Pursuant to 40 CFR Part 68.10 or Part 68.150?										
□ Yes □ No Specify required RMP submittal date: If submitted, RMP submittal date:										
B. Are you using administrative controls to subject your facility	y to a lesser 112(r) pr	ogram standard?								
Yes No If yes, please specify:										
C. List the processes subject to 112(r) at your facility:										
PROCESS DESCRIPTION	PROCESS LEVEL (1, 2, or 3)	HAZARDOUS CHEMICAL	MAXIMUM INVENTC	INTENDED DRY (LBS)						

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCDE	Q/Division of A	Air Quality - Applic	ation for A	ir Permit to	Construct/	Operate		В
EMISSION SOURCE DESCRIPTION: F	eed Silo Filling	I		EMISSION	SOURCE I	D NO: ES-3	80A	
				CONTROL		NO(S): CE	-30	
OPERATING SCENARIO1_	OF _	1		EMISSION	POINT (ST	ACK) ID NO	D(S): EP-30	
DESCRIBE IN DETAILTHE EMISSION Ash feed silo filled pneumatically at the f	SOURCE PRO illing rate of 12	CESS (ATTACH F 5 ton/hr and equipp	LOW DIAG	RAM): vent produc	t capture de	evice.		
TYPE OF EMISSION SOUR	CE (CHECK A	ND COMPLETE AF	PROPRIA	TE FORM B	1-B9 ON TH	E FOLLOV	VING PAGE	S):
Coal,wood,oil, gas, other burner (Fo	rm B1)		(Form B4)		🗆 Man	uf. of chemi	cals/coating	gs/inks (Form E
Int.combustion engine/generator (Fc	orm B2)	Coating/finishi	ng/printing	(Form B5)	🗌 Incin	eration (For	m B8)	
Liquid storage tanks (Form B3)		Storage silos/	oins (Form I	36)	□ Othe	er (Form B9)	1	
START CONSTRUCTION DATE: TBD			DATE MA	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBD			EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	2 WK/YR
IS THIS SOURCE SUBJECT 🛛 NS	SPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGHPU	JT (%): DEC-F	EB 25 MAF	R-MAY 25	5 JL	JN-AUG	25	SEP-NO	/ 25
CRITERIA AI	R POLLUTA	ANT EMISSION	IS INFOF	RMATION	FOR TH	SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA		DNS
		EMISSION	AFTER CON	ROLS / LIMITS	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS (PM ₁₀)			1				
PARTICULATE MATTER<2.5 MICRONS	(PM _{2.5})							
SULFUR DIOXIDE (SO2)	(* 2.0)							
NITROGEN OXIDES (NOx)			SEE		B. Table 5			
CARBON MONOXIDE (CO)			-	1	_,			
VOLATILE ORGANIC COMPOUNDS (V								
	00,							
			1					
HAZARDOUS	AIR POLLU	TANT EMISSIO	ONS INFO	ORMATIO	N FOR T	HIS SOU	RCE	
	<u>т. с</u> Т					POTENTIA		MIC
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE	APPENDIX	B, Table 5			
	T							
TOXIC AIR	POLLUTAN	IT EMISSIONS	INFORM	IATION F	OR THIS	SOURC	Ξ	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lt	o/hr	lb/e	day		lb/yr
			SEE A	PPENDIX B,	Table 5			
	1							
Attachments: (1) emissions calculations and s	supporting docum	entation: (2) indicate :	all requested	state and fed	eral enforceal	ole permit lim	its (e.a. hour	s of operation

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

 MPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOU

 Attach Additional Sheets As Necessary

EMISSION SOURCE (STORAGE SILO/BINS)

REVISED 09/22/16	NCDEQ/Divis	ion of Air Quality - Ap	plicatior	n for Air Permit to Co	nstruct/Operate		B6	
EMISSION SOURCE DESCRIPT	MISSION SOURCE DESCRIPTION: Feed Silo Filling EMISSION SOURCE ID NO: ES-30A							
				CONTROL DEVICE ID NO(S): CD-30				
OPERATING SCENARIO:	1	OF1		EMISSION PC	DINT(STACK) ID N	O(S): EP-30		
DESCRIBE IN DETAIL THE PRC Ash feed silo filled pneumatically	CESS (ATTACH FLC at the filling rate of 12	W DIAGRAM): 25 ton/hr and equipped v	vith bin v	vent product capture de	evice.			
MATERIAL STORED: Fly Ash				DENSITY OF MATER	RIAL (LB/FT3): 60 t	oulk, 90 structural		
CAPACITY	CUBIC FEET: 76,000)		TONS:				
DIMENSIONS (FEET)	HEIGHT: 97	DIAMETER: 41	(OR)	LENGTH:	WIDTH:	HEIGHT:		
ANNUAL PRODUCT THRO	UGHPUT (TONS)	ACTUAL: 400,000		MAXIMUM DE	SIGN CAPACITY	400,000		
PNEUMATICALLY FIL	LED	MECHANIC	ALLY FI	LLED		FILLED FROM		
BLOWER		SCREW CONVEYOR				R		
		BELT CONVEYOR						
OTHER:		BUCKET ELEVATOR				GE PILE		
		OTHER:			□ OTHER	:		
NO. FILL TUBES: 3								
MAXIMUM ACFM: 6600								
MATERIAL IS UNLOADED TO:								
N/A								
N/A								
MAXIMUM DESIGN FILLING RA	TE OF MATERIAL (T	ONS/HR): 125						
MAXIMUM DESIGN UNLOADING	G RATE OF MATERIA	AL (TONS/HR): N/A						
COMMENTS: This form is for Feed Silo Filling.	Unloading data is prov	vided in Form B6 for ES	-30B.					

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCI	DEQ/Division of A	Air Quality - Applic	ation for Ai	r Permit to	Construct/	Operate		В	
EMISSION SOURCE DESCRIPTION:	Feed Silo Unloa	ding		EMISSION	SOURCE	ID NO: ES-	30B		
				CONTROL		D NO(S): CE	0-30		
OPERATING SCENARIO	1 OF	1		EMISSION	POINT (ST	TACK) ID N	O(S): EP-30)	
DESCRIBE IN DETAILTHE EMISSIO Ash feed silo unloaded at the rate of 7	N SOURCE PRO	CESS (ATTACH FL	OW DIAGR	AM): ure device.					
TYPE OF EMISSION SO	URCE (CHECK A	ND COMPLETE AF	PROPRIAT	E FORM B	1-B9 ON TH	IE FOLLOV	VING PAGE	:S):	
Coal,wood,oil, gas, other burner (Form B1)	Woodworking	Form B4)		🗆 Man	uf. of chem	icals/coatin	gs/inks (Form E	
Int.combustion engine/generator ((Form B2)	Coating/finishi	ng/printing (Form B5)	🗌 Incir	neration (Fo	rm B8)		
Liquid storage tanks (Form B3)		Storage silos/b	ins (Form B	6)	□ Othe	er (Form B9)		
START CONSTRUCTION DATE: TBI	0		DATE MA	NUFACTUR	RED: TBD				
MANUFACTURER / MODEL NO.: TB	D		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK \$	52 WK/YR	
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	ΓS?):			SHAP (SUB	PARTS?):_			
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-FI	EB 25 MAR	-MAY 25	JU	N-AUG	25	SEP-NOV	25	
CRITERIA	AIR POLLUT	ANT EMISSION	IS INFOR	MATION	FOR TH	IS SOUR	CE		
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	AL EMISSIO	SSIONS	
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CON	TROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)	
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr	
PARTICULATE MATTER (PM)									
PARTICULATE MATTER<10 MICRON	S (PM ₁₀)								
PARTICULATE MATTER<2.5 MICRON	IS (PM _{2.5})								
SULFUR DIOXIDE (SO2)									
NITROGEN OXIDES (NOx)			SEE	APPENDIX	B, Table 5				
CARBON MONOXIDE (CO)									
VOLATILE ORGANIC COMPOUNDS	(VOC)								
LEAD									
OTHER									
HAZARDOUS	S AIR POLLU	TANT EMISSIC	ONS INFC	RMATIO	N FOR T	'HIS SOU	RCE		
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	AL EMISSIC	DNS	
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CON	TROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)	
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr	
			SEE	APPENDIX	B, Table 5				
TOXIC AI	R POLLUTA	NT EMISSIONS	INFORM	ATION F	OR THIS	SOURCE	5		
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION	
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lt)/hr	lb/	day		lb/yr	
				SEE AF	PPENDIX B	, Table 5			

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

 MPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOUL

 Attach Additional Sheets As Necessary

EMISSION SOURCE (STORAGE SILO/BINS)

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate							B6		
- EMISSION SOURCE DESCRIPTION: Feed Silo Unloading					EMISSION SOURCE ID NO: ES-30B				
				CONTROL DEVICE ID NO(S): CD-30				30	
OPERATING SCENARIO:	1	OF1			EMISSION POI	NT(STA	ACK) ID NO(S): EP-30	
DESCRIBE IN DETAIL THE PRC Ash feed silo unloaded at the rate	CESS (ATTACH FLO e of 75 ton/hr and equi	W DIAGRAM): ipped with bin vent proc	duct capt	ture dev	ice.				
MATERIAL STORED: Flv Ash				DENS	ITY OF MATERIA	AL (LB/I	FT3): 60 bull	k. 90 structural	
CAPACITY	CUBIC FEET: 76,000)		TONS	:	(,	10). 00 24		
DIMENSIONS (FEET)	HEIGHT: 97	DIAMETER: 41	(OR)	LENG	TH:	WIDTH	l: F	HEIGHT:	
ANNUAL PRODUCT THRO	UGHPUT (TONS)	ACTUAL: 400,000			MAXIMUM DES	SIGN CA	APACITY: 4	00,000	
PNEUMATICALLY FIL	LED	MECHANIC	ALLY FI	ILLED				FILLED FROM	
BLOWER		SCREW CONVEYOR	2				RAILCAR		
		BELT CONVEYOR					TRUCK		
OTHER:		BUCKET ELEVATOR					STORAGE	PILE	
		OTHER:					OTHER:		
NO. FILL TUBES: N/A									
MAXIMUM ACFM: 6600									
MATERIAL IS UNLOADED TO:									
STAR® Reactor									
N/A MAXIMUM DESIGN FILLING RA		ONS/HR): N/A							
COMMENTS: This form is for Feed Silo Unload	ling. Filling data is prov	/ided in Form B6 for ES	3-30A.						

FORM C1 CONTROL DEVICE (FABRIC FILTER)

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate C								C1	
CONTROL DEVICE ID NO: CD-30	CONTROLS EMISSIONS FROM WHICH EMISSION SOURCE ID NO(S): ES-30A & ES-30B								
EMISSION POINT (STACK) ID NO(S): EP-30	POSITION IN SERIE	POSITION IN SERIES OF CONTROLS NO. 1 OF 1 UN							
OPERATING SCENARIO:									
1OF1		P.E. SEAL REQUIR	ED (PE	ER 2q .0112)?		7	YES		NO
DESCRIBE CONTROL SYSTEM: A bin vent for particulate o	ontrol on the feed silo.								
POLLUTANTS COLLECTED:		PM (Filling)		PM10/PM2.5 (Filling)		PM (Unloading)		PM10/PM2.5 (Unloading)	
BEFORE CONTROL EMISSION RATE (LB/HR):		0.0061		0.00288		0.00365		0.00173	
CAPTURE EFFICIENCY:		<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%
CONTROL DEVICE EFFICIENCY:		N/A	%	N/A	%	N/A	%	N/A g	%
CORRESPONDING OVERALL EFFICIENCY:		N/A	%	N/A	%	N/A	%	N/A ^d	%
EFFICIENCY DETERMINATION CODE:		2		2		2		2	
TOTAL AFTER CONTROL EMISSION RATE (LB/HR):		0.0061		0.00288		0.00365		0.00173	
PRESSURE DROP (IN H ₂ 0): MIN: MAX: Avg: 10-15 wg	GAUGE?	YES] NO					
BULK PARTICLE DENSITY (LB/FT ³): 25		INLET TEMPERATU	JRE (°F	F): Contract	MIN		MAX		
POLLUTANT LOADING RATE: N/A 🛛 LB/HR 🛛] GR/FT ³	OUTLET TEMPERA	TURE	(°F) Contract	MIN		MAX		
INLET AIR FLOW RATE (ACFM): 1300		FILTER OPERATIN	G TEM	P (°F): Contract					
NO OF COMPARTMENTS: 1 NO OF BAGS F	PER COMPARTMENT	Contract			LENG	TH OF BAG (IN)	20-30		
		PIDGE (ET ²): Contrac	4				. 5-15		
TOTAL EILTER SUPEACE AREA (ET ²): Contract		(DO: 1 to 4 : 1					. 0 10		
		10. 1104.1			م مناسبة ما مر م	Chula II	MOVE		
	FORCED/POSITIVE			FILTER MATERIAL: G	annoge	s Style 🗹	WOVE		FELIED
DESCRIBE CLEANING PROCEDURES:				F			PARTIC	LE SIZE DISTRIBUTION	
AIR PULSE	SONIC					SIZE		WEIGHT %	CUMULATIVE
REVERSE FLOW	SIMPLE BAG COLLA	APSE				(MICRONS)		OF TOTAL	%
□ MECHANICAL/SHAKER □	RING BAG COLLAPS	SE				0-1			
OTHER:				•		1-10			
DESCRIBE INCOMING AIR STREAM: Air stream will contain	fly ash.					10-25			
				-		25-50			
				•		50-100			
				•		>100			
				•			1	TOTAL - 100	
				r	Suppli	er specific. 94% na	ssina 3	25 mesh	
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHOWING	THE RELATIONSHIP	OF THE CONTROL D	DEVICE	TO ITS EMISSION SO	URCE((S):			
COMMENTS:									

Attach Additional Sheets As Necessary

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCDE	U/Division of A	ar Quality - App	Discrition fo	r Aır Permit	to Constru	ict/Operate		Ď
EMISSION SOURCE DESCRIPTION:	STAR® Reactor			EMISSION	SOURCE I	D NO: ES-31		
				CONTROL	DEVICE ID	NO(S): CD-3	1	
OPERATING SCENARIO	1 OF	1		EMISSION	POINT (ST	ACK) ID NO(S): EP-31	
DESCRIBE IN DETAILTHE EMISSIO The STAR® Reactor will process feed variety of commercial products.	N SOURCE PRO stock (of any car	DCESS (ATTAC bon content) like	H FLOW Di e flyash (we	AGRAM): et or dry) alor	ng with othe	er ingredient m	aterials into	а
TYPE OF EMISSION SOU	RCE (CHECK A	ND COMPLETE	APPROPR		B1-B9 ON	THE FOLLO	WING PAG	ES):
Coal,wood,oil, gas, other burner (I	Form B1)	□ Woodwork	ing (Form E	34)	🗆 Man	uf. of chemica	als/coatings/	inks (Form B
Int.combustion engine/generator (Form B2)	Coating/fin	ishing/printi	ing (Form B5	🗌 Incir	neration (Form	B8)	
Liquid storage tanks (Form B3)		Storage sil	os/bins (Fo	rm B6)	🔽 Othe	er (Form B9)		
START CONSTRUCTION DATE: TBD)		DATE MAI	NUFACTUR	D: TBD			
MANUFACTURER / MODEL NO.: TBI	D		EXPECTE	D OP. SCHE	DULE: 24	HR/DAY 7 DA	AY/WK 52 W	VK/YR
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	TS?):			HAP (SUB	PARTS?):		
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 N	MAR-MAY	25	JUN-AUG	25	SEP-NC)V 25
CRITERIA A	IR POLLUTA	ANT EMISSIO	ONS INF	ORMATIC	N FOR T	THIS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSION	IS
		EMISSION	(AFTER CONT	ROLS / LIMITS)	BEFORE CO	NTROLS / LIMITS)	(AFTER CON	ITROLS / LIMITS
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	6 (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})							
SULFUR DIOXIDE (SO2)	(,	1						
				SEE APPENDIX B. Table 3A & 3B				
					,			
	(VOC)							
	(100)	1						
OTHER								
HAZARDOUS	AIR POLLU	TANT EMISS	SIONS IN	FORMAT	ION FOR	THIS SOU	IRCE	
		SOURCE OF	EXPECTE			POTENTIAI		IS
		EMISSION						
HAZARDOUS AIR POLI UTANT	CAS NO	FACTOR	lb/hr	tons/vr	lh/hr	tons/vr	lh/hr	tons/vr
		Therefu	10/111	torio/yi	10/11	torio/ yr	10/11	tonio/yi
		1						
		1						
		1						
		1		SEE APP		able 3A & 3B		
		1		1		<u> </u>		
		1		1	L	1		
TOXIC AI		IT EMISSION	VS INFO		FOR TH	IS SOURC	E	
10/10/11								
		SOURCE OF	EXPECT	ED ACTUAL	EMISSION	IS AFTER CO	NTROLS / I	IMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lt	o/hr	lt	o/dav		b/vr
								, j.
SEE APPENDIX B, Table 3A & 3B								
		4						
		4	ļ				ļ	
		1					I	

Attachments: (1) emissions calculations and supporting documentation; (2) indicate all requested state and federal enforceable permit limits (e.g. hours of operation emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

IPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOU Attach Additional Sheets As Necessary

FORM B9 EMISSION SOURCE (OTHER)

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate							
EMISSION SOURCE DESCRIPTION: STAR® Reactor		EMISSION SOURCE ID NO: ES-31					
	CONTROL DEVICE ID NO(S): CD-31						
OPERATING SCENARIO:1 OF1		EMISSION POINT (STACK) ID NO	O(S): EP-31				
DESCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIAGRAM): The STAR ingredient materials into a variety of commercial products. The fly ash is not a fuel to maintain temperature in the reactor should the fly ash not contain enough carbor British thermal units per hour and are low-NOx burners.	Reactor will p and does not un n to be self-sust n to be self-sust	rocess feedstock (of any carbon cor ndergo combustion. The natural gas taining. These startup burners have	ntent) like flyash (wet o /propane burners are o a combined heating ca	r dry) along with other only used for startup or apacity of 60 million			
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS		MAX. DESIGN	REQUEST	ED CAPACITY			
ТҮРЕ	UNITS	CAPACITY (UNIT/HR)	LIMITATIO	N(UNIT/HR)			
Reactor- Feed Ash	MMBtu	140		140			
MATERIALS ENTERING PROCESS - BATCH OPERATION		MAX. DESIGN	REQUEST	REQUESTED CAPACITY			
ТҮРЕ	UNITS	CAPACITY (UNIT/BATCH)	LIMITATION	(UNIT/BATCH)			
MAXIMUM DESIGN (BATCHES / HOUR):		·					
REQUESTED LIMITATION (BATCHES / HOUR):	(BATCHES/Y	′R):					
FUEL USED: Natural Gas/Propane	TOTAL MAXI	MUM FIRING RATE (MILLION BTU	J/HR): 140				
MAX. CAPACITY HOURLY FUEL USE: NG-58,824 scf/hr & Propane- 663 gal/hr	REQUESTED	CAPACITY ANNUAL FUEL USE:	NG-58,824 scf/hr & Pr	opane- 663 gal/hr			
COMMENTS:							
FORM C9 CONTROL DEVICE (OTHER)

REVISED 09/22/16	NCDEQ/Divisi	on of Air Qualit	y - Applica	tion for Air Perm	it to Construct/Opera	ate	C9	
CONTROL DEVICE ID NO: CD-31A	۱.	CON	TROLS EN	ISSIONS FROM	WHICH EMISSION SC	OURCE ID NO(S): E	S-31	
EMISSION POINT (STACK) ID NO(S): EP-31	POSI	ITION IN S	ERIES OF CONT	ROLS: NO. 1	OF 2 UNI	rs	
CONTROL DEVICE ID NO: CD-31A CONTROLS EMISSIONS FROM WHICH EMISSION SOURCE ID NO(S): ES-31 EMISSION POINT (STACK) ID NO(S): EP-31 POSITION IN SERIES OF CONTROLS: NO. 1 OF 2 UNITS OPERATING SCENARIO: PIE. SEAL REQUIRED (PER 2Q.0112)? YES NO DESCRIBE CONTROL SYSTEM: Dry scrubber for SO2 removal. P.E. SEAL REQUIRED (PER 2Q.0112)? YES NO POLLUTANT(S) COLLECTED: SO2 Social and the second and the								
1_	OF1		F	P.E. SEAL REQUI	RED (PER 2Q .0112)?	✓ YES	□ NO	
DESCRIBE CONTROL SYSTEM: D	Dry scrubber for SO ₂	removal.						
POLLUTANT(S) COLLECTED:			SO_2					
BEFORE CONTROL EMISSION RA	TE (LB/HR):		482.79					
CAPTURE EFFICIENCY:			N/A	/₀	%	%	%	
CONTROL DEVICE EFFICIENCY:			95	%	%	%	%	
CORRESPONDING OVERALL EFF	ICIENCY:		N/A	/6	%	%	%	
EFFICIENCY DETERMINATION CO	DDE:		2					
TOTAL AFTER CONTROL EMISSIO	ON RATE (LB/HR):		24.14					
PRESSURE DROP (IN. H ₂ 0):	10 MIN	15 MAX	E	BULK PARTICLE	DENSITY (LB/FT ³) Use	e gypsum as surroga	ate.	
INLET TEMPERATURE (°F):	335MIN	_400MAX	(OUTLET TEMPER	ATURE (°F):	150 MIN	225N	1AX
INLET AIR FLOW RATE (ACFM): 6	 5000 operating/7750	0 maximum	(OUTLET AIR FLO	W RATE (ACFM): 77,5	500		
INLET AIR FLOW VELOCITY (FT/S	(OUTLET AIR FLO	W VELOCITY (FT/SEC	C):				
INLET MOISTURE CONTENT (%):	NLET MOISTURE CONTENT (%): 15-25% by volume					AIR		
COLLECTION SURFACE AREA (F	Γ ²): N/A		F	UEL USED: N/A		FUEL USAGE	RATE: N/A	
DESCRIBE MAINTENANCE PROC	ned as per	manufacturing gu	idelines.					
DESCRIBE ANY AUXILIARY MATE	RIALS INTRODUCE	D INTO THE CC	ONTROL S	YSTEM: None				
DESCRIBE ANY MONITORING DE	VICES, GAUGES, T	EST PORTS, ET	C: Typical	for this type of ins	tallations.			
			51					
ATTACH A DIAGRAM OF THE REL	ATIONSHIP OF TH	= CONTROL DE	VICE TO I	IS EMISSION SO	URCE(S):			
COMMENTS:								
Attach mar	ufacturor's enocifi	cations schome	atice and	all other drawing	s necessary to decor	ibe this control		
Allach mar	iulaciulei s specifi	cations, scheme	auco, and	an other urawing	a necessary to descr			

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate C									
CONTROL DEVICE ID NO: CD-31B	CONTROLS EMISS	IONS FROM WHICH EMISSION SO	URCE ID NO(S)	: ES-31					
EMISSION POINT (STACK) ID NO(S): EP-31	POSITION IN SERIE	S OF CONTROLS		NO.	2 OF 2	UNITS			
OPERATING SCENARIO:									
1OF1		P.E. SEAL REQUIRED (PER 2q.0)112)?	v	YES	□ NO			
DESCRIBE CONTROL SYSTEM: A baghouse for particula	te control on the STAR	reactor.	,						
POLLUTANTS COLLECTED:		PM	PM10	PM2.5					
						-			
BEFORE CONTROL EMISSION RATE (LB/HR):		16.61	15.28	8.8		_			
CAPTURE EFFICIENCY:		100 %	100	% 100	%	_%			
CONTROL DEVICE EFFICIENCY:		> 99.9 %	> 99.9	% > 99.9	%	%			
		·				-			
CORRESPONDING OVERALL EFFICIENCY:		> 99.9 %	> 99.9	% > 99.9	%	%			
				_					
EFFICIENCY DETERMINATION CODE:		2	2	2		-			
TOTAL AFTER CONTROL EMISSION RATE (LB/HR):		16.61	15.28	8.8					
	044050				-				
PRESSURE DROP (IN H ₂ 0): MIN: MAX: AVg: 4-12 Inch BUILK PARTICLE DENSITY (LB/ET ³): 25	GAUGE? L			MIN 170	MAX 350				
	GR/FT ³ 437	OUTLET TEMPERATURE (°F)		MIN 165	MAX 350				
INLET AIR FLOW BATE (ACFM): 77500		FILTER OPERATING TEMP (°F):	170						
	PER COMPARTMENT	· 169		I ENGTH OF BAG (IN): 315				
NO OF CARTRINGTON FOR STATE APEA OF A DED CARTRIDGE (ET ²), Der ban – 30.63. DIAMETER OF BAG (IN) - 6									
TOTAL FILTER SURFACE AREA (FT ²): 26.790	AIR TO CLOTH RAT	TIO: 2.18 : 1							
DRAFT TYPE: INDUCED/NEGATIVE	FORCED/POSITIVE	FILTER	R MATERIAL:		WOVEN 🗹	FELTED			
DESCRIBE CLEANING PROCEDURES:				PAR	TICLE SIZE DISTRIB	UTION			
	SONIC		ſ	SIZE	WEIGHT %				
	SIMPLE BAG COLL	APSE		(MICRONS)	OF TOTAL	%			
		сс СС	-	0.1		1			
	KING BAG COLLAP	5L	-	1-10					
DESCRIBE INCOMING AIR STREAM: The circulating dry s	crubber effluent flue gas	s, containing gypsum and unreacted	lime, passes	10-25					
through the baghouse for particulate control.				25-50					
			ŀ	50-100					
			ŀ	>100					
				100	τοται	- 100			
			•	See attached jpeg.	101/1	- 100			
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHOWING COMMENTS:	G THE RELATIONSHIP	OF THE CONTROL DEVICE TO ITS	S EMISSION SO	URCE(S):					





Size (µm)	Vol Under %	Size (µm)	Vol Under %	Size (um)	Vol Under %	Size (um)	Vol Under %	Size (µm)	Vol Under %	Size (µm)	Vol Under %
0.020	0.00	0.142	0.00	1.002	27.29	7.095	99.98	50.238	100.001	355.656	100.00
0.022	0.00	0.159	0.00	1.125	30.92	7,952	100.00	56,368	100.00	399.052	100.00
0.025	0.00	0.178	0.00	1.262	34.91	8.934	100.00	63.246	100.00	447.744	100.00
0.028	0.00	0.200	0.02	1.416	39.35	10.000	100.00	70.963	100.00	502.377	100.00
0.032	0,00	0.224	0.33	1.589	44.27	11.247	100.00	79.621	100.00	563.877	100.00
0.036	0,00	0.252	0.85	1.783	49.67	12.619	100.00	69.337	100.00	632.456	100.00
0,040	0.00	0.283	1.60	2.000	55.49	14,159	100.00	100,237	100.00	709.627	100.00
0,045	0.00	0.317	2.63	2.244	61.62	15,587	100.00	112.468	100.00	796.214	100.00
0,050	0.00	0,356	3,98	2.518	67.66	17.825	100.00	128,191	100.00	893.357	100.00
0,056	0.00	0,399	5.09	2.825	73,99	20,000	100.00	141,589	100.00	1002.374	100.00
0.063	0.00	0.445	7.72	3.170	79.75	22,440	100.00	158.866	100.00	1124.083	100.00
0.071	0.00	0.502	10.02	3.557	85.03	25,179	100.00	178,250	100.00	1261.915	100.00
0.080	0.00	0.564	12.51	3.001	89.55	28,251	100.00	200.000	100.00	1415.892	100.00
0.089	0.00	0.632	15.16	4,477	93.27	31.695	100.00	224,404	100.00	1588.656	100.00
0,100	0.00	0,710	17.94	5.024	95.16	35,586	100.00	251,785	100 00	1782.502	100.00
0.112	0.00	0.796	20.67	5.637	98,26	39.905	100.00	282,508	100.00	2000,000	100.00
0,126	0,00	0.893	23.97	8 325	99.55	44.774	100.00	318,979	100.00	100000	

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCDE	Q/Division of A	ir Quality - Applic	ation for A	ir Permit to	o Construc	t/Operate		В
EMISSION SOURCE DESCRIPTION:	FGD Byproduc	t Silo		32				
				CONTROL		D NO(S): CE	D-32	
OPERATING SCENARIO	1 OF	1		EMISSION	I POINT (S	TACK) ID N	O(S): EP-3	2
DESCRIBE IN DETAILTHE EMISSIO The byproduct solids from the dry FGI	N SOURCE PRO	OCESS (ATTACH charged from the I	FLOW DIA Fabric Filter	GRAM): baghouse i	nto a bypro	duct storage	e silo.	
TYPE OF EMISSION SOUR	RCE (CHECK A		PPROPRIA	TE FORM E	31-B9 ON T	HE FOLLO	WING PAG	ES):
Coal,wood,oil, gas, other burner (F	Form B1)	U Woodworking	g (Form B4)		🗆 Man	uf. of chemi	cals/coating	gs/inks (Form
□ Int.combustion engine/generator (Form B2)	Coating/finish	ning/printing	(Form B5)	🗌 Incir	eration (For	rm B8)	
Liquid storage tanks (Form B3)		Storage silos	/bins (Form	B6)	□ ^{Othe}	er (Form B9))	
START CONSTRUCTION DATE: TBD)		DATE MA	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBI	C		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK	52 WK/YR
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	TS?):			SHAP (SUE	PARTS?):_		
PERCENTAGE ANNUAL THROUGHE	PUT (%): DEC-F	EB 25 MA	R-MAY	25	JUN-AUG	25	SEP-N	OV 25
CRITERIA A	IR POLLUTA	ANT EMISSION	NS INFOR	RMATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	ONS
		EMISSION	AFTER CONT	ROLS / LIMITS)	BEFORE CON	TROLS / LIMITS	(AFTER COM	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	6 (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE	APPENDIX	B, Table 7			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD								
OTHER								
HAZARDOUS	AIR POLLU	TANT EMISSIC	ONS INFO	ORMATIO	N FOR T	'HIS SOU	RCE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	NS
		EMISSION	AFTER CONT	ROLS / LIMITS)	BEFORE CON	TROLS / LIMITS	(AFTER CON	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
N/A								
TOXIC AIF	R POLLUTAN	IT EMISSIONS	S INFORM	IATION F	OR THIS	SOURC	E	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lb	/hr	lb/	dav		lb/vr
			-			,		,
			1					
	1							
N/A								
			1					
	1							

REVISED 09/22/16	NCDEQ/Divis	sion of Air Quality - A	oplication	n for Air	r Permit to Con	struct/O	perate		B6
EMISSION SOURCE DESCRIP	TION: FGD Byproduct	Silo			EMISSION SOL	JRCE ID	NO: ES-3	32	
					CONTROL DEV	/ICE ID N	NO(S): CD	-32	
OPERATING SCENARIO:	1	OF1			EMISSION POI	NT(STAC	CK) ID NO	9(S): EP-32	
DESCRIBE IN DETAIL THE PRO	OCESS (ATTACH FLC y FGD system are dis	OW DIAGRAM): charged from the Fabri	c Filter ba	aghouse	into a byproduc	t storage	e silo.		
MATERIAL STORED: Byproduct	ts from FGD			DENSI	TY OF MATERI	AL (LB/F	T3): 30		
CAPACITY	CUBIC FEET: 3120			TONS:	47	X	-,		
DIMENSIONS (FEET)	HEIGHT: 65	DIAMETER: 13	(OR)	LENGT	TH:	WIDTH:		HEIGHT:	
ANNUAL PRODUCT THRO	DUGHPUT (TONS)	ACTUAL: 5694	MAXIMUM DESIGN CAPACITY: 15,100					5,100	
PNEUMATICALLY FI	LLED	MECHANIC	MECHANICALLY FILLED					FILLED FROM	
BLOWER		SCREW CONVEYOR	2				RAILCAR		
		BELT CONVEYOR					TRUCK		
OTHER:		BUCKET ELEVATOR STORAGE PILE						E PILE	
		OTHER: OTHER: Dry Scrubber							
NO. FILL TUBES: 1									
MAXIMUM ACFM: 1300									
MATERIAL IS UNLOADED TO:									
BY WHAT METHOD IS MATER Gravity unloading to trucks.	IAL UNLOADED FROI	M SILO?							
MAXIMUM DESIGN FILLING RA	ATE OF MATERIAL (T	ONS/HR): 1.75							
MAXIMUM DESIGN UNLOADIN	G RATE OF MATERIA	AL (TONS/HR): 300							
COMMENTS:									

REVISED 09/22/16		NCDEQ/Division of	of Air Quality - Appli	cation f	or Air Permit to Cons	truct/O	perate			C1
CONTROL DEVICE ID NO: CD-32		CONTROLS EMISSI	ONS FROM WHICH	EMISSI	ON SOURCE ID NO(S): ES-3	32			
EMISSION POINT (STACK) ID NO(S): EP-32		POSITION IN SERIE	S OF CONTROLS				NO.		1 OF 1	UNITS
OPERATING SCENARIO	:									
1 OF1			P.E. SEAL REQUIR	ED (PE	R 2q .0112)?		V	YES		□ NO
DESCRIBE CONTROL SYSTEM: A bin vent for partie	culate	control on the FGD By	product Silo.							
POLLUTANTS COLLECTED:			PM		PM10		PM2.5			
				-		-				
BEFORE CONTROL EMISSION RATE (LB/HR):			0.06	_	0.05	_	0.03			
CAPTURE EFFICIENCY:			<= 0.005 gr/dscf	%	<= 0.005 gr/dscl	%	<= 0.005 gr/dscf	%	·	%
			N/A	%	N/A	%	N/A	%		%
			107		107			/0		70
CORRESPONDING OVERALL EFFICIENCY:			N/A	%	N/A	%	N/A	%		%
				_		_				
EFFICIENCY DETERMINATION CODE:			2	-	2	_	2		·	
TOTAL AFTER CONTROL EMISSION RATE (LB/HR)		0.06		0.05		0.03				
		0411052		-	NO	-				
PRESSURE DROP (IN H ₂ 0): MIN: MAX: AVg: 10-1 BULK PARTICLE DENSITY (LB/ET ³): 25	5 wg	GAUGE? L): Contract	MIN		ΜΔΥ		
	- 1	□ GR/FT ³			(°F) Contract	MIN		MAX		
INLET AIR FLOW BATE (ACFM): 1300		_	FILTER OPERATIN	G TEM	P (°F): Contract					
NO. OF COMPARTMENTS: 1 NO. OF F	BAGS	PER COMPARTMENT	Contract		(.).	LENG	TH OF BAG (IN.): 20)-30		
NO_OF_CARTRIDGES: Contract FILTERS	SURF/	CE AREA PER CART	RIDGE (FT ²): Contra	ct		DIAME	TER OF BAG (IN):	5-15		
TOTAL FILTER SUBFACE AREA (FT ²): Contract		AIR TO CLOTH RAT	IO: 1 to 4 · 1			0.0 0010		0.0		
	~	FORCED/POSITIVE			FILTER MATERIAL: (Cartrido	e Style 🔽	wov	EN 🔽	FELTED
DESCRIBE CLEANING PROCEDURES:							PARTIC	LESI)N
		SONIC					SIZE		WEIGHT %	
		SIMPLE BAG COLL	APSE				(MICRONS)			%
			SE				0.1		OF TOTAL	,,,
		KING BAG COLLAP	3E				1 10			
DESCRIBE INCOMING AIR STREAM:							10-25			
							25-50			
							50-100			
							>100			
							100		τοται	- 100
						Suppli	er specific, 94% pass	sing 3	25 mesh	- 100
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHC	WING	THE RELATIONSHIP	OF THE CONTROL	DEVICE	E TO ITS EMISSION S	SOURCI	E(S):			
COMMENTS.										

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCDEC)/Division of Ai	r Quality - Appli	cation for A	Air Permit te	o Construc	t/Operate		В
EMISSION SOURCE DESCRIPTION:	FGD Absorber	nt Silo		EMISSION	SOURCE	ID NO: ES-	33	
				CONTROL) NO(S): C	D-33	
OPERATING SCENARIO1	OF	1		EMISSION	POINT (S	FACK) ID N	O(S): EP-3	3
DESCRIBE IN DETAILTHE EMISSION Storage of absorbent (hydrated lime)	N SOURCE PRO	DCESS (ATTACH FGD system.	FLOW DIA	AGRAM):				
TYPE OF EMISSION SOUR	CE (CHECK AN	ID COMPLETE A	PPROPRIA	TE FORM	B1-B9 ON 1		WING PAC	GES):
Coal,wood,oil, gas, other burner (F	orm B1)	U Woodworkir	ng (Form B4	.)	🗆 Man	uf. of chemi	icals/coating	gs/inks (Form I
□ Int.combustion engine/generator (I	Form B2)	Coating/finis	shing/printin	g (Form B5)	🗌 Incin	eration (Fo	rm B8)	
Liquid storage tanks (Form B3)		Storage silo	s/bins (Forn	n B6)	□ ^{Othe}	er (Form B9))	
START CONSTRUCTION DATE: TBD			DATE MAI	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBE)		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK	52 WK/YR
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	:TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGHP	UT (%): DEC-F	EB 25 N	IAR-MAY	25	JUN-AUG	25	SEP-	NOV 25
CRITERIA AI	R POLLUTA	NT EMISSIO	NS INFOI	RMATION	I FOR TH	IIS SOUR	RCE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	ONS
		EMISSION	AFTER CONT	ROLS / LIMITS)	BEFORE CON	ROLS / LIMITS	(AFTER CON	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	(PM ₁₀)							
PARTICULATE MATTER<2.5 MICRONS	6 (PM _{2.5})	-						
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE		B, Table 7			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
HAZARDOUS	AIR FULLUI					DOTENTIA		
		SOURCE OF						
HAZARDOUS AIR POLLUTANT	CAS NO	FACTOR	Ih/hr	tons/vr	lh/hr	tons/vr	Ih/hr	tons/vr
			10/11	tonio, yr	16/111	torio, yr	10/111	torio, yr
N/A								
TOXIC AIR	POLLUTAN	T EMISSION	S INFORM	MATION F	OR THIS	SOURC	E	
		SOURCE OF	EXPECTE		EMISSION	S AFTER C		
		EMISSION						
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lb	/hr	lb/	day		lb/yr
N/A								
N/A								
N/A								

NCDEQ/Divis	ion of Air Quality - Ap	plicatior	n for Air Permit to C	Construct/Operate	B6
ION: FGD Absorbent	Silo		EMISSION	SOURCE ID NO: ES-33	
			CONTROL	DEVICE ID NO(S): CD-33	
1	OF1		EMISSION	POINT(STACK) ID NO(S): EP-33	
CESS (ATTACH FLO ime) used in the dry F	W DIAGRAM): GD system.				
orbent			DENSITY OF MAT	ERIAL (LB/FT3): 25	
CUBIC FEET: 10000			TONS: 125		
HEIGHT: 100	DIAMETER: 14	(OR)	LENGTH:	WIDTH: HEIGHT:	
UGHPUT (TONS)	ACTUAL: 3723	DESIGN CAPACITY: 13,140			
.LED	MECHANIC	FILLED FROM			
	SCREW CONVEYOR				
	BELT CONVEYOR			TRUCK	
	BUCKET ELEVATOR			STORAGE PILE	
	OTHER:			OTHER:	
	0119/1401/- 25				
	(TONS/HR): 23				
J RATE OF MATERIA	L (TONS/HR). 1.5				
	NCDEQ/Divis	NCDEQ/Division of Air Quality - App TON: FGD Absorbent Silo OF1	NCDEQ/Division of Air Quality - Application ION: FGD Absorbent Silo	NCDEQ/Division of Air Quality - Application for Air Permit to (ION: FGD Absorbent SiloOFEMISSIONOTTONOFEMISSIONOFEMISSION DCESS (ATTACH FLOW DIAGRAM): ime) used in the dry FGD system. rbent CUBIC FEET: 10000 TONS: 125 HEIGHT: 100 DIAMETER: 14 (0R) LENGTH: UGHPUT (TONS) ACTUAL: 3723 ACTUAL: 3723 MAXIMUM LEDMAXIMUM LOADED FROM SILO? TE OF MATERIAL (TONS/HR): 25 3 RATE OF MATERIAL (TONS/HR): 1.5	NODEQDivision of Air Quality - Application for Air Permit to Construct/Operate ION: FGD Absorbent Silo EMISSION SOURCE ID NO: ES:33 CONTROL DEVICE ID NO(S): CD:33 OF OF OF OF OF OF OF Mont DENSITY OF MATERIAL (LB/FT3): 25 CUBIC FEET: 10000 TONS: 125 HEIGHT: 100 DIAMETER: 14 (OR) LENGTH: WIDTH: HEIGHT: 13,140 LED MACHANICALLY FILLED FILLED FROM OFTROL DEVICE

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate C1									
CONTROL DEVICE ID NO: CD-33	CONTROLS EMISSI	ONS FROM WHICH	EMISSIC	ON SOURCE ID NO(S): ES-3	3			
EMISSION POINT (STACK) ID NO(S): EP-33	POSITION IN SERIE	S OF CONTROLS				NO.	1	OF 1	UNITS
OPERATING SCENARIO:									
1OF1		P.E. SEAL REQUIR	ED (PEF	R 2q .0112)?		7	YES		□ NO
DESCRIBE CONTROL SYSTEM: A bin vent for particula	ate control on the FGD Ab	sorbent Silo.							
POLLUTANTS COLLECTED:		РМ		PM10		PM2.5			
			_				-		
BEFORE CONTROL EMISSION RATE (LB/HR):		0.06	_	0.05		0.03	_		
CAPTURE EFFICIENCY:		<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%		%
		N/A	0/_	N/A	0/_	NI/A	0/_		0/
		107	<i>,</i> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1071			-		/0
CORRESPONDING OVERALL EFFICIENCY:		N/A	%	N/A	%	N/A	%		%
						-			
EFFICIENCY DETERMINATION CODE:		2	_	2		2	-		
	0.06		0.05		0.03				
				0.00		0.00			
PRESSURE DROP (IN H ₂ 0): MIN: MAX: Avg: 10-15 v	vg GAUGE? L	YES		NO					
	GR/FT ³				MIN		MAX		
			C TEMP		IVIIIN		IVIAA		
NO OF COMPARTMENTS: 1		Contract	GIEWF	(F). Contract			20		
NO. OF COMPARTMENTS. 1 NO. OF BAC		DIDCE (ET ²): Contro	at			TED OF DAG (IN.). 20	5.45		
TOTAL EILTER SURFACE AREA (ET ²): Contract		10: 1 to 4 : 1	u		DIAIVIE	TER OF BAG (IN.).	5-15		
		10. 1104.1			ortriday	Stulo II	WOVE	N D	
			1	IETER WATERIAL C	annuge				N
					_				
						SIZE	vv	EIGHT %	CUMULATIVE
		APSE				(MICRONS)	0	FIUTAL	%
	J RING BAG COLLAP	SE				0-1			
						1-10			
						10-25			
						25-50			
						50-100			
						>100			
					Suppli	erspecific 94% pass	sing 325	TOTAL 5 mesh	= 100
					ouppin		5111g 020	mean	
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHOWI	NG THE RELATIONSHIP	OF THE CONTROL	DEVICE	TO ITS EMISSION S	OURCE	E(S):			
COMMENTS:									
1									

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCDE	Q/Division of A	Air Quality - Applic	ation for A	ir Permit to	Construct/	Operate		В	
EMISSION SOURCE DESCRIPTION: E	HE- External H	leat Exchanger 1 &	2	EMISSION SOURCE ID NO: ES-34 and ES-35					
				CONTROL		NO(S): CE	0-34 and CI)-35	
OPERATING SCENARIO1_	OF	1		EMISSION	POINT (ST	ACK) ID N	O(S): EP-34	and EP-35	
DESCRIBE IN DETAILTHE EMISSION Process heat exchanger. Maximum ann	SOURCE PRO ual emissions a	DCESS (ATTACH F are based on the lb	LOW DIAG	RAM): Jle unit * 876	0 hours per	year.			
TYPE OF EMISSION SOUR	CE (CHECK A	ND COMPLETE A	PPROPRIA	TE FORM B	1-B9 ON TH	HE FOLLO	WING PAGI	ES):	
Coal,wood,oil, gas, other burner (Fo	orm B1)	U Woodworking	(Form B4)		🗆 Man	uf. of chemi	icals/coating	gs/inks (Form E	
Int.combustion engine/generator (Fe	orm B2)	Coating/finish	ing/printing	(Form B5)	🗌 Incin	eration (Fo	rm B8)		
Liquid storage tanks (Form B3)		Storage silos/	bins (Form	B6)	🔽 Othe	er (Form B9))		
START CONSTRUCTION DATE: TBD			DATE MA	NUFACTUR	ED: TBD				
MANUFACTURER / MODEL NO.: TBD			EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	62 WK/YR	
IS THIS SOURCE SUBJECT	SPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_			
PERCENTAGE ANNUAL THROUGHPU	JT (%): DEC-F	EB 25 MAI	R-MAY 2	5 JI	JN-AUG	25	SEP-NO	/ 25	
CRITERIA AI	R POLLUT	ANT EMISSION	IS INFOR	RMATION	FOR TH	IS SOUR	CE		
		SOURCE OF	EXPECTE	ED ACTUAL		POTENTIA	AL EMISSIC	ONS	
		EMISSION	AFTER CON	ROLS / LIMITS	BEFORE CONT	ROLS / LIMITS	(AFTER COI	NTROLS / LIMITS)	
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr	
PARTICULATE MATTER (PM)									
PARTICULATE MATTER<10 MICRONS	(PM ₁₀)								
PARTICULATE MATTER<2.5 MICRONS	(PM _{2.5})								
SULFUR DIOXIDE (SO2)									
NITROGEN OXIDES (NOx)			SEE	APPENDIX	B, Table 4				
CARBON MONOXIDE (CO)									
VOLATILE ORGANIC COMPOUNDS (V	/OC)								
LEAD									
OTHER									
HAZARDOUS	AIR POLLU	TANT EMISSIO	ONS INFO	ORMATIO	N FOR T	'HIS SOU	IRCE		
		SOURCE OF	EXPECTE	ED ACTUAL		POTENTIA	AL EMISSIC	NS	
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CONT	ROLS / LIMITS	(AFTER COI	NTROLS / LIMITS)	
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr	
			SEE		R Table 4				
			ULL		D, Table 4				
TOXIC AIR	POLLUTA	T EMISSIONS		ATION F	OR THIS	SOURC	E		
		EMISSION	OF EXPECTED ACTUAL E			JAFIER U	UNI RULS		
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lk	o/hr	lb/e	day		lb/yr	
	+		1		ļ				
			SEE A	PPENDIX B,	Table 4				
				,					
		1	1						
Attachments: (1) emissions calculations and s	supporting docum	nentation; (2) indicate	all requested	state and fed	eral enforcea	ble permit lin	nits (e.g. hou	rs of operation,	

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

FORM B9 EMISSION SOURCE (OTHER)

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate								
EMISSION SOURCE DESCRIPTION: EHE- Extern	nal Heat Exchanger 1 & 2		EMISSION SOURCE ID NO: ES-3	34 and ES-35				
			CONTROL DEVICE ID NO(S): CD	0-34 and CD-35				
OPERATING SCENARIO:1 O	F1		EMISSION POINT (STACK) ID NO	O(S): EP-34 and EP-3	5			
DESCRIBE IN DETAIL THE PROCESS (ATTACH	FLOW DIAGRAM): Proces	s neat exch	anger					
MATERIALS ENTERING PROCESS -	CONTINUOUS PROCESS		MAX DESIGN	REQUESTED				
ТҮРЕ		UNITS	CAPACITY (UNIT/HR)		UNIT/HR)			
Heat Exchanger	Тс	ons	70	X				
¥								
MATERIALS ENTERING PROCESS	- BATCH OPERATION		MAX. DESIGN	REQUESTED	CAPACITY			
ТҮРЕ		UNITS	CAPACITY (UNIT/BATCH)	LIMITATION (U	NIT/BATCH)			
MAXIMUM DESIGN (BATCHES / HOUR):								
REQUESTED LIMITATION (BATCHES / HOUR):	(B	ATCHES/YI	R):					
FUEL USED: N/A	тс	TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A						
MAX. CAPACITY HOURLY FUEL USE: N/A	RI	EQUESTED	CAPACITY ANNUAL FUEL USE:	N/A				
COMMENTS:								

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate C1									
CONTROL DEVICE ID NO: CD-34 & CD-35	CONTROLS EMISSI	ONS FROM WHICH	EMIS	SION SOURCE ID NO(S): ES-3	4 & ES-35			
EMISSION POINT (STACK) ID NO(S): EP-34 & EP-35	POSITION IN SERIE	S OF CONTROLS		· · · · ·		NO.	1 OF	1	UNITS
OPERATING SCENARIO:									
1 OF 1		P.F. SEAL REQUIR	ED (P	FR 2g (0112)?			YES		
DESCRIBE CONTROL SYSTEM: A bagbouse for particulate c	ontrol on the EHE- Ext	ternal Heat Exchange	er 1 &	2. Emissions below are f	for one	unit.	120		
POLLUTANTS COLLECTED:		PM		PM10	-	PM2.5			
BEFORE CONTROL EMISSION RATE (LB/HR):		6.86		6.31	-	3.63			
CAPTURE EFFICIENCY:		99.95	%	99.95	%	99.95	%		%
CONTROL DEVICE EFFICIENCY:		N/A	%	N/A	%	N/A	%		%
CORRESPONDING OVERALL EFFICIENCY:		N/A	%	N/A	%	N/A	%		%
EFFICIENCY DETERMINATION CODE:		2		2	-	2			
TOTAL AFTER CONTROL EMISSION RATE (LB/HR):	6.86		6.31	-	3.63				
PRESSURE DROP (IN H ₂ 0): MIN: MAX: Avg: 10"	GAUGE?	YES] NO					
BULK PARTICLE DENSITY (LB/FT ³): 60		INLET TEMPERATI	URE (°	F):	MIN 18	30	MAX 325		
POLLUTANT LOADING RATE: 🛛 LB/HR	GR/FT ³	OUTLET TEMPERA	TURE	(°F)	MIN 15	50	MAX 300		
INLET AIR FLOW RATE (ACFM): 48,000	FILTER OPERATIN	G TEN	1P (°F): 250 (excursions	s to 325	i)				
NO. OF COMPARTMENTS: 1 NO. OF BAGS PER			LENGT	H OF BAG	(IN.): N/A				
NO. OF CARTRIDGES: N/A FILTER SURFACE	AREA PER CARTRI	DGE (FT ²): N/A			DIAME	TER OF BA	G (IN.): 6		
TOTAL FILTER SURFACE AREA (FT ²): N/A	AIR TO CLOTH RAT	IO: 3:1							
DRAFT TYPE: 🗹 INDUCED/NEGATIVE 🗌	FORCED/POSITIVE			FILTER MATERIAL:			WOVEN	V	FELTED
DESCRIBE CLEANING PROCEDURES:						PAR	TICLE SIZI		UTION
☑ AIR PULSE	SONIC					SIZE	WEIG	iHT %	CUMULATIVE
REVERSE FLOW	SIMPLE BAG COLLA	APSE			(MIC	CRONS)	OF T	OTAL	%
	RING BAG COLLAPS	SE		=		0-1			
OTHER:				-		1-10			
DESCRIBE INCOMING AIR STREAM: Air stream will contain fly	/ ash.				1	0-25			
				-	2	25-50			
				Ī	5	0-100			
					:	>100			
								TOTAL	= 100
					Particle	Size Distrib	oution 0-100	micron wit	h an average of 20
			E) // 0 =		005/				
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHOWING TH	IE RELATIONSHIP OI	F THE CONTROL D	EVICE	TO ITS EMISSION SOL	JRCE(S	5):			

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

	EQ/DIVISION OF A	ation for A		В				
EMISSION SOURCE DESCRIPTION:	Transfer Silo Fi	lling		EMISSION	SOURCE I	D NO: ES-3	86A	
				CONTROL	DEVICE ID	NO(S): CD	-36	
OPERATING SCENARIO	1OF	1		EMISSION	POINT (ST	ACK) ID NO	D(S): EP-36	
DESCRIBE IN DETAILTHE EMISSIO Transfer silo is filled at the rate of 125	N SOURCE PRC ton/hr and equip	DCESS (ATTACH F ped with bin vent p	LOW DIAG product capt	RAM): ure device.				
TYPE OF EMISSION SOU	RCE (CHECK A	ND COMPLETE A	PPROPRIA	TE FORM B	1-B9 ON TH	HE FOLLOW		ES):
Coal,wood,oil, gas, other burner (F	Form B1)	U Woodworking	(Form B4)		🗆 Man	uf. of chemi	cals/coating	gs/inks (Form
 Int.combustion engine/generator (Liquid storage tanks (Form B3) 	Form B2)	Coating/finish	ing/printing /bins (Form	(Form B5) B6)	☐ Incin ☐ Othe	eration (For r (Form B9)	m B8)	
START CONSTRUCTION DATE: TBE)		DATE MA	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBI	D		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 MA	R-MAY 2	5 JI	JN-AUG	25	SEP-NO	V 25
CRITERIA A	AIR POLLUT	ANT EMISSION	IS INFOR	RMATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA		NS
		EMISSION	AFTER CON	ROLS / LIMITS	BEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	S (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE	APPENDIX	B, Table 5			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD								
OTHER HAZAPOOUS						HIS SOL	PCF	
TIAZAND003		SOURCE OF	EXPECTED ACTUAL POTENTIAL EMISSION					NS
		EMISSION	AFTER CON	ROLS / LIMITS	BEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE	APPENDIX	B, Table 5			
TOXIC AI	R POLLUTAN	NT EMISSIONS	INFORM	IATION F	OR THIS	SOURC	Ε	
		SOURCE OF EMISSION	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lt	o/hr	lb/d	day		lb/yr
			SEE A	PPENDIX B	Table 5			

EMISSION SOURCE DESCRIPTION: T OPERATING SCENARIO: DESCRIBE IN DETAIL THE PROCESS Transfer silo is filled at the rate of 125 to MATERIAL STORED: Fly Ash CAPACITY CUBIC DIMENSIONS (FEET) HEIGH ANNUAL PRODUCT THROUGHPL PNEUMATICALLY FILLED	Transfer Silo Fill1 S (ATTACH FLO on/hr and equip	ing OF1 W DIAGRAM): ped with bin vent produ	ct captur	EMISSION SC CONTROL DE EMISSION PC	DURCE ID NO: ES EVICE ID NO(S): (DINT(STACK) ID N	5-36A 2D-36 VO(S): EP-36	
OPERATING SCENARIO: DESCRIBE IN DETAIL THE PROCESS Transfer silo is filled at the rate of 125 to MATERIAL STORED: Fly Ash CAPACITY CUBIC DIMENSIONS (FEET) HEIGH ANNUAL PRODUCT THROUGHPL PNEUMATICALLY FILLED	1 S (ATTACH FLO ron/hr and equip	OF1 W DIAGRAM): ped with bin vent produ	ct captur	CONTROL DE EMISSION PC	EVICE ID NO(S): (DINT(STACK) ID N	CD-36 VO(S): EP-36	
OPERATING SCENARIO: DESCRIBE IN DETAIL THE PROCESS Transfer silo is filled at the rate of 125 tc MATERIAL STORED: Fly Ash CAPACITY CUBIC DIMENSIONS (FEET) HEIGH ANNUAL PRODUCT THROUGHPL PNEUMATICALLY FILLED	1 S (ATTACH FLO on/hr and equip	OF1 W DIAGRAM): ped with bin vent produ	ct captur	EMISSION PC	DINT(STACK) ID N	NO(S): EP-36	
DESCRIBE IN DETAIL THE PROCESS Transfer silo is filled at the rate of 125 to MATERIAL STORED: Fly Ash CAPACITY CUBIC DIMENSIONS (FEET) HEIGH ANNUAL PRODUCT THROUGHPL PNEUMATICALLY FILLED	S (ATTACH FLO con/hr and equip,	W DIAGRAM): ped with bin vent produ	ict captur	e device.			
MATERIAL STORED: Fly Ash CAPACITY CUBIC DIMENSIONS (FEET) HEIGH ANNUAL PRODUCT THROUGHPL PNEUMATICALLY FILLED							
CAPACITY CUBIC DIMENSIONS (FEET) HEIGH ANNUAL PRODUCT THROUGHPU PNEUMATICALLY FILLED				DENSITY OF MATER	RIAL (LB/FT3): 60	bulk, 90 structural	
DIMENSIONS (FEET) HEIGH ANNUAL PRODUCT THROUGHPU PNEUMATICALLY FILLED	C FEET: N/A			TONS: 300			
ANNUAL PRODUCT THROUGHPU PNEUMATICALLY FILLED	HT: 100	DIAMETER: 41	(OR)	LENGTH:	WIDTH:	HEIGHT:	
PNEUMATICALLY FILLED	UT (TONS)	ACTUAL: 400,000		MAXIMUM DE	SIGN CAPACITY	: 400,000	
		MECHANIC	ALLY FI	LLED		FILLED FROM	
BLOWER		SCREW CONVEYOR				١R	
		BELT CONVEYOR				•	
☐ OTHER:		BUCKET ELEVATOR				GE PILE	
		OTHER:				<u>t:</u>	
NO. FILL TUBES: 3							
MAXIMUM ACFM: 9000							
MATERIAL IS UNLOADED TO:							
BY WHAT METHOD IS MATERIAL UNL N/A	LOADED FROM	I SILO?					
MAXIMUM DESIGN FILLING RATE OF	- MATERIAL (T(ONS/HR): 125					
MAXIMUM DESIGN UNLOADING RATE	E OF MATERIA	L (TONS/HR): N/A					
COMMENTS: This form is for Transfer Silo Filling. Unlo	loading data is p	rovided in Form B6 for	ES-36B.				

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCI	DEQ/Division of	Air Quality - Applic	ation for Air	Permit to	Construct/C	Operate		В		
EMISSION SOURCE DESCRIPTION:	Transfer Silo Un	loading		EMISSION SOURCE ID NO: ES-36B						
				CONTROL		NO(S): CE	0-36			
OPERATING SCENARIO	1OF_	11		EMISSION	N POINT (ST	ACK) ID N	D(S): EP-36	3		
DESCRIBE IN DETAILTHE EMISSIO Transfer silo unloaded at the rate of 7	N SOURCE PRO 5 ton/hr and equip	CESS (ATTACH FL oped with bin vent pr	OW DIAGRA	AM): re device.	X					
TYPE OF EMISSION SO	URCE (CHECK A	ND COMPLETE AP	PROPRIAT	E FORM B	1-B9 ON TH	E FOLLOW	ING PAGE	S):		
Coal,wood,oil, gas, other burner (Form B1)	Woodworking (Form B4)		🗆 Man	uf. of chemi	cals/coating	gs/inks (Form		
Int.combustion engine/generator ((Form B2)	Coating/finishin	g/printing (F	orm B5)	🗌 Incin	eration (Fo	rm B8)			
Liquid storage tanks (Form B3)		Storage silos/bi	ins (Form B6	6)	□ Othe	er (Form B9))			
START CONSTRUCTION DATE: TBI	D		DATE MA	NUFACTUF	RED: TBD					
MANUFACTURER / MODEL NO.: TB	D		EXPECTE	D OP. SCH	IEDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR		
IS THIS SOURCE SUBJECT	NSPS (SUBPART	rs?):			SHAP (SUB	PARTS?):_				
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-FI	EB 25 MAR-	-MAY 25	JUI	N-AUG	25	SEP-NOV	25		
CRITERIA	AIR POLLUT	ANT EMISSION	S INFORI	MATION	FOR THI	s sourd	CE			
		SOURCE OF	EXPECTE	D ACTUAL	-	POTENTIA	L EMISSIC	ONS		
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CONT	FROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)		
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr		
PARTICULATE MATTER (PM)										
PARTICULATE MATTER<10 MICRON	S (PM ₁₀)									
PARTICULATE MATTER<2.5 MICRON	IS (PM _{2.5})							1		
SULFUR DIOXIDE (SO2)			SEE	APPENDIX	B, Table 5			1		
NITROGEN OXIDES (NOx)										
CARBON MONOXIDE (CO)								1		
VOLATILE ORGANIC COMPOUNDS	(VOC)							1		
LEAD										
OTHER										
HAZARDOU	S AIR POLLU	TANT EMISSIC	NS INFO	RMATIO	N FOR TI	HIS SOU	RCE			
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA		DNS		
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CONT	FROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)		
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr		
						-				
								1		
								1		
								1		
			SEE	APPENDIX	B, Table 5			1		
								1		
								1		
				İ						
				l				1		
				[[
TOXIC A	IR POLLUTA	NT EMISSIONS	INFORM	ATION F	OR THIS	SOURCE				
			EVDEOTE							
		EMISSION	EXPECTE	DACTUAL	EMISSION	S AFTER C	UNTROLS	/ LIMITATION		
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lb	/hr	lb/	day		lb/yr		
			SEE AF	PENDIX B	, Table 5					
Attachments: (1) emissions calculations an	d supporting docum	entation: (2) indicate a	I requested st	ate and fede	ral enforceable	e permit limit	s (e.a. hours	of operation.		

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

REVISED 09/22/16	NCDEQ/Divis	sion of Air Quality - Ap	plicatior	n for Air Permit to Con	struct/Oper	rate	B6
EMISSION SOURCE DESCRIPT	FION: Transfer Silo Ur	nloading		EMISSION SO	URCE ID NO	D: ES-36B	
				CONTROL DE	VICE ID NO	(S): CD-36	
OPERATING SCENARIO:	1	OF1		EMISSION PO	INT(STACK)) ID NO(S): EP-36	
DESCRIBE IN DETAIL THE PRO	DCESS (ATTACH FLC	DW DIAGRAM): ipped with bin vent prod	uct captu	ire device.			
MATERIAL STORED: Fly Ash				DENSITY OF MATERI	AL (LB/FT3)): 60 bulk, 90 structural	
CAPACITY	CUBIC FEET: N/A			TONS: 300			
DIMENSIONS (FEET)	HEIGHT: 100	DIAMETER: 41	(OR)	LENGTH:	WIDTH:	HEIGHT:	
ANNUAL PRODUCT THRO	UGHPUT (TONS)	ACTUAL: 400,000		MAXIMUM DES	SIGN CAPA	CITY: 400,000	
PNEUMATICALLY FIL	LED	MECHANIC	ALLY FI	LLED		FILLED FROM	
□ BLOWER		SCREW CONVEYOR			🗆 RA	AILCAR	
		BELT CONVEYOR				RUCK	
OTHER:		BUCKET ELEVATOR			□ st	ORAGE PILE	
		OTHER:			П от	THER:	
NO. FILL TUBES: N/A							
MAXIMUM ACFM: 9000							
MATERIAL IS UNLOADED TO:							
Gravity							
MAXIMUM DESIGN FILLING RA	ATE OF MATERIAL (I	ONS/HR): N/A					
MAXIMUM DESIGN UNLOADIN	G RATE OF MATERI	AL (TONS/HR): 75					
COMMENTS: This form is for Transfer Silo Unle	oading. Filling data is	provided in Form B6 for	ES-36A				

REVISED 09/22/16	REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate C1								
CONTROL DEVICE ID NO: CD-36	CONTROLS EMISSI	ONS FROM WHICH	EMISS	ION SOURCE ID NO(S)	: ES-36	6A & ES-36B			
EMISSION POINT (STACK) ID NO(S): EP-36	POSITION IN SERIE	S OF CONTROLS				NO.	1	OF 1	UNITS
OPERATING SCENARIO:									
1OF1		P.E. SEAL REQUIR	ED (PE	ER 2q .0112)?		7	YES		NO
DESCRIBE CONTROL SYSTEM: A bin vent for particulate c	ontrol on the transfer s	ilo.							
POLLUTANTS COLLECTED:		PM (Filling)		PM10/PM2.5 (Filling)		PM (Unloading)	-	PM10/PM2.5 (Unloading)	
BEFORE CONTROL EMISSION RATE (LB/HR):		0.0061		0.0029		0.0037		0.0017	
CAPTURE EFFICIENCY:		<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%
CONTROL DEVICE EFFICIENCY:		N/A	%	N/A	%	N/A	%	N/A	%
CORRESPONDING OVERALL EFFICIENCY:		N/A	%	N/A	%	N/A	%	N/A	%
EFFICIENCY DETERMINATION CODE:		2		2		2	•	2	
TOTAL AFTER CONTROL EMISSION RATE (LB/HR):		0.0061		0.0029		0.0037		0.0017	
PRESSURE DROP (IN H ₂ 0): MIN: MAX: Avg: 10-15 wg	GAUGE?] YES] NO					
BULK PARTICLE DENSITY (LB/FT ³): 25		INLET TEMPERATU	JRE (°F	F): Contract	MIN		MAX		
POLLUTANT LOADING RATE: N/A 🛛 LB/HR 🛛	GR/FT ³	OUTLET TEMPERA	TURE	(°F) Contract	MIN		MAX		
INLET AIR FLOW RATE (ACFM): 1300		FILTER OPERATIN	G TEM	P (°F): Contract					
NO. OF COMPARTMENTS: 1 NO. OF BAGS F	PER COMPARTMENT:	Contract			LENG	TH OF BAG (IN.):	20-30		
NO_OF_CARTRIDGES: Contract FILTER_SUBEA	CE AREA PER CARTE	RIDGE (ET ²): Contrac	t.		DIAME	TER OF BAG (IN	5-15		
TOTAL FILTER SURFACE AREA (FT ²): Contract	AIR TO CLOTH RAT	IO: 1 to 4 · 1			20,000				
		0. 104.1			artridad	Style 2	WOVE		
	TORCED/TOSHIVE			TIETER WATERIAL G	artriuge	sotyle 🖸	ABTIC		
DESCRIBE CLEANING PROCEDURES.				r i			AKTIC	LE SIZE DISTRIBUTION	
☑ AIR PULSE □	SONIC					SIZE		WEIGHT %	CUMULATIVE
REVERSE FLOW	SIMPLE BAG COLLA	APSE				(MICRONS)		OF TOTAL	%
□ MECHANICAL/SHAKER □	RING BAG COLLAPS	SE				0-1			
OTHER:						1-10			
DESCRIBE INCOMING AIR STREAM: Air stream will contain	fly ash.					10-25			
						25-50			
						50-100			
						>100			
								TOTAL = 100	
					Suppli	er specific, 94% pa	ssing 32	25 mesh	
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHOWING	THE RELATIONSHIP	OF THE CONTROL [DEVICE	TO ITS EMISSION SO	URCE((S):			
COMMENTS:									

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCD	EQ/Division of	Air Quality - Applic	ation for A	ir Permit to	Construct/	Operate		В
EMISSION SOURCE DESCRIPTION:	Storage Dome	Filling		EMISSION	37A			
				CONTROL) NO(S): CE	D-37	
OPERATING SCENARIO	1OF	1		EMISSION	I POINT (ST	ACK) ID N	O(S): EP-37	7
DESCRIBE IN DETAILTHE EMISSIO Storage Dome silo is filled at the rate of	N SOURCE PRO of 75 ton/hr and o	DCESS (ATTACH F equipped with bin v	LOW DIAG ent product	RAM): capture dev	rice.			
TYPE OF EMISSION SOU	RCE (CHECK A		PPROPRIA	TE FORM B	1-B9 ON TH	HE FOLLO	WING PAG	ES):
Coal,wood,oil, gas, other burner (I	Form B1)		(Form B4)		🗆 Man	uf. of chem	icals/coating	gs/inks (Form E
Int.combustion engine/generator (Form B2)	Coating/finish	ing/printing	(Form B5)	🗌 Incin	eration (Fo	rm B8)	
Liquid storage tanks (Form B3)		Storage silos/	bins (Form	B6)		er (Form B9)	
START CONSTRUCTION DATE: TBE)		DATE MA	NUFACTUR	RED: TBD			
MANUFACTURER / MODEL NO.: TBI	D		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGHE	PUT (%): DEC-F	EB 25 MAI	R-MAY 2	5 JI	UN-AUG	25	SEP-NO	V 25
CRITERIA A	AIR POLLUT	ANT EMISSION	IS INFOR	RMATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	AL EMISSIO	ONS
		EMISSION	AFTER CON	ROLS / LIMITS	BEFORE CONT	FROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)				 			ļ	
PARTICULATE MATTER -10 MICRONS	S (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})							
			055					
			SEE	APPENDIX	B, Table 6			
	(1 (0 0)							
VOLATILE ORGANIC COMPOUNDS	(VUC)							
							IPCE	
MAZANDOUS						DOTENTI		2010
		SOURCE OF						
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE		B Tablo 6			
			JLL					
		1		1				
TOXIC AI	R POLLUTAI	NT EMISSIONS	INFORM	ATION F	OR THIS	SOURC	E	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lt	o/hr	lb/e	day		lb/yr
			SEE A	PPENDIX B	, Table 6			
		1	1				1	
	-	1	1		1		1	

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

REVISED 09/22/16	NCDEQ/Divis	ion of Air Quality - Ap	plicatior	n for Aiı	r Permit to Con	struct/C	Operate		B6
EMISSION SOURCE DESCRIPT	FION: Storage Dome F	filling			EMISSION SOL	JRCE II	D NO: ES-	37A	
					CONTROL DEV	/ICE ID	NO(S): CI	D-37	
OPERATING SCENARIO:	1	OF1			EMISSION POI	NT(STA	ACK) ID NO	D(S): EP-37	
DESCRIBE IN DETAIL THE PRC Storage Dome is filled at the rate	CESS (ATTACH FLO → of 75 ton/hr and equip	W DIAGRAM): oped with bin vent prod	uct captu	ure devic	ce.				
MATERIAL STORED: Fly Ash				DENSI	TY OF MATERIA	AL (LB/I	FT3): 60 b	ulk, 90 structural	
CAPACITY	CUBIC FEET: N/A			TONS:	30,000				
DIMENSIONS (FEET)	HEIGHT: 125	DIAMETER: 41	: 41 (OR) LENGTH:			WIDTH		HEIGHT:	
ANNUAL PRODUCT THRO	UGHPUT (TONS)	ACTUAL: 400,000			MAXIMUM DES	SIGN CA	APACITY:	400,000	
PNEUMATICALLY FIL	LED	MECHANIC	ALLY FI	LLED				FILLED FROM	
BLOWER		SCREW CONVEYOR	,				RAILCAF	२	
		BELT CONVEYOR					TRUCK		
OTHER:		BUCKET ELEVATOR					STORAG	GE PILE	
		OTHER:					OTHER:		
NO. FILL TUBES: 1									
MAXIMUM ACFM: 7600									
MATERIAL IS UNLOADED TO:									
BY WHAT METHOD IS MATERI N/A	AL UNLOADED FROM	/ SILO?							
MAXIMUM DESIGN FILLING RA	TE OF MATERIAL (TO	ONS/HR): 75							
MAXIMUM DESIGN UNLOADIN	G RATE OF MATERIA	L (TONS/HR): N/A							
COMMENTS: This form is for Storage Dome Fi	lling. Unloading data is	s provided in Form B6 f	or ES-37	В.					

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCD	EQ/Division of A	Air Quality - Applic	ation for A		В						
EMISSION SOURCE DESCRIPTION:	Storage Dome	Unloading		EMISSION	I SOURCE I	D NO: ES-3	37B				
				CONTROL		0 NO(S): CE	0-37				
OPERATING SCENARIO	1OF	1		EMISSION	I POINT (ST	Introduction Image: Control of the second secon					
DESCRIBE IN DETAILTHE EMISSIO Storage Dome is unloaded at the rate	N SOURCE PRO of 275 ton/hr and	ICESS (ATTACH F	LOW DIAG	RAM): ct capture de	evice.						
TYPE OF EMISSION SOU	RCE (CHECK A		PPROPRIA	TE FORM B	1-B9 ON TH	HE FOLLO	WING PAG	ES):			
Coal,wood,oil, gas, other burner (I	Form B1)) (Form B4)		🗌 Man	uf. of chemi	cals/coating	js∕inks (Form I			
Int.combustion engine/generator (Form B2)	Coating/finish	ning/printing	(Form B5)		eration (Fo	rm B8)				
Liquid storage tanks (Form B3)		Storage silos/	/bins (Form	B6)	□ Othe	er (Form B9))				
START CONSTRUCTION DATE: TBE)		DATE MA	NUFACTUR	RED: TBD						
MANUFACTURER / MODEL NO.: TBI	D		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR			
	NSPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_					
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 MA	R-MAY 2	5 JI	UN-AUG	25	SEP-NO	V 25			
CRITERIA A	VIR POLLUTA	ANT EMISSION	VS INFOR	RMATION	FOR TH	IS SOUR	CE				
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	NS			
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CONT	ROLS / LIMITS	(AFTER CO	VTROLS / LIMITS)			
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr			
PARTICULATE MATTER (PM)											
PARTICULATE MATTER<10 MICRONS	S (PM ₁₀)	ļ									
PARTICULATE MATTER<2.5 MICRON	IS (PM _{2.5})	ļ	ļ					ļ			
SULFUR DIOXIDE (SO2)		ļ	ļ					ļ			
NITROGEN OXIDES (NOx)			SEE	APPENDIX	B, Table 6			ļ			
CARBON MONOXIDE (CO)				───							
VOLATILE ORGANIC COMPOUNDS	(VOC)	ļ	ļ					ļ			
LEAD		<u> </u>						 			
OTHER							1205				
HAZARDOUS	AIR POLLO	TANT EMISSIC	JNS INFO	DRMATIO	N FOR I	HIS SOU	IRCE				
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	AL EMISSIC	NS			
HAZARDOUS AIR POLLUTANT	CAS NO.	EMISSION FACTOR	AFTER CONT lb/hr	TROLS / LIMITS	BEFORE CONT Ib/hr	tons/yr	(AFTER COI lb/hr	ITROLS / LIMITS)			
	<u> </u>			<u> </u>							
			SEE		B, Table 6						
	_		<u> </u>								
				<u> </u>							
TOXIC AII	R POLLUTAN	IT EMISSIONS	INFORI	ATION F	OR THIS	SOURC	E				
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION			
TOXIC AIR POLLUTANT	CAS NO.	EMISSION FACTOR	l	o/hr	lb/e	dav		lb/vr			
			+			,					
			SEE A	PPENDIX B,	, Table 6						
			1								
Attachments: (1) emissions calculations and	d supporting docum	nentation; (2) indicate	all requester	d state and fec	deral enforcea	able permit lir	nits (e.g. hou	rs of operation,			

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

NCDEQ/Divi	sion of Air Quality	y - Applicatior	for Air Permit to C	onstruct/Operate		B6
ION: Storage Dome	Unloading		EMISSION S	SOURCE ID NO: E	S-37B	
			CONTROL D	EVICE ID NO(S):	CD-37	
1	OF	1	EMISSION F	OINT(STACK) ID	NO(S): EP-37	
DCESS (ATTACH FL e rate of 275 ton/hr ar	OW DIAGRAM): nd equipped with bir	n vent product	capture device.			
			DENSITY OF MATE	RIAL (LB/FT3): 60) bulk, 90 structural	
CUBIC FEET: N/A			TONS: 30,000		,	
HEIGHT: 125	DIAMETER: 41	(OR)	LENGTH:	WIDTH:	HEIGHT:	
UGHPUT (TONS)	ACTUAL: 400,0	00	MAXIMUM D	ESIGN CAPACIT	Y: 400,000	
LED	MECH	IANICALLY FI	LLED		FILLED FROM	
	SCREW CONVE	EYOR		RAILC	AR	
	BELT CONVEYO	OR			к	
	BUCKET ELEVA	ATOR			AGE PILE	
	OTHER:				R:	
TE OF MATERIAL (TONS/HR): N/A					
G RATE OF MATERI	AL (TONS/HR): 27	5				
nloading. Filling data	is provided in Form	n B6 for ES-37	Α.			
	NCDEQ/Divi ION: Storage Dome 1 DCESS (ATTACH FLI rate of 275 ton/hr ar CUBIC FEET: N/A HEIGHT: 125 UGHPUT (TONS) LED AL UNLOADED FRC TE OF MATERIAL (COMMATERIAL (COMMATER	NCDEQ/Division of Air Quality ION: Storage Dome Unloading	NCDEQ/Division of Air Quality - Application ION: Storage Dome Unloading	NCDEQ/Division of Air Quality - Application for Air Permit to C ION: Storage Dome Unloading EMISSION E	NODEQ/Division of Air Quality - Application for Air Permit to Construct/Operate ION: Storage Dome Unloading EMISSION SOURCE ID NO: E	WDEEQDivision of Air Quality - Application for Air Permit to Construct/Operate ION: Storage Dome Unloading EMISSION SOURCE ID NO(S): ED-37 CONTROL DEVICE ID NO(S): CD-37 EMISSION DOINT(STACK) ID NO(S): EP-37 ION: Storage Dome Unloading DENSITY OF MATERIAL (LB/FT3): 60 bulk, 90 structural CUBIC FEET: N/A DENSITY OF MATERIAL (LB/FT3): 60 bulk, 90 structural CUBIC FEET: N/A DENSITY OF MATERIAL (LB/FT3): 60 bulk, 90 structural CUBIC FEET: N/A DENSITY OF MATERIAL (LB/FT3): 60 bulk, 90 structural CUBIC FEET: N/A DENSITY OF MATERIAL (LB/FT3): 60 bulk, 90 structural CUBIC FEET: N/A DIAMETER: 41 (OR) MARTERIAL (LB/FT3): 60 bulk, 90 structural CUBIC FEET: N/A OPMONE ONE ONE TO NO.0000 MARTERIAL (LB/FT3): 60 bulk, 90 structural CUBIC FEET: N/A SCREW CONVEYOR RAILCAR BUL CONVEYOR RAILCAR BUL CONVEYOR STORAGE PILE

REVISED 09/22/16	REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate C1								
CONTROL DEVICE ID NO: CD-37	CONTROLS EMISSI	ONS FROM WHICH	EMISS	ION SOURCE ID NO(S)	: ES-37	'A & ES-37B			
EMISSION POINT (STACK) ID NO(S): EP-37	POSITION IN SERIE	S OF CONTROLS				NO.	1	OF 1	UNITS
OPERATING SCENARIO:									
1OF1		P.E. SEAL REQUIR	ED (PE	ER 2q .0112)?		7	YES		NO
DESCRIBE CONTROL SYSTEM: A bin vent for particulate c	control on the storage d	lome.							
POLLUTANTS COLLECTED:		PM (Filling)		PM10/PM2.5 (Filling)		PM (Unloading)		PM10/PM2.5 (Unloading)	
BEFORE CONTROL EMISSION RATE (LB/HR):		0.0037		0.0017		0.0134		0.0063	
CAPTURE EFFICIENCY:		<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%
CONTROL DEVICE EFFICIENCY:		N/A	%	N/A	%	N/A	%	N/A	%
CORRESPONDING OVERALL EFFICIENCY:		N/A	%	N/A	%	N/A	%	N/A	%
EFFICIENCY DETERMINATION CODE:		2		2		2		2	
TOTAL AFTER CONTROL EMISSION RATE (LB/HR):		0.0037		0.0017		0.0134		0.0063	
PRESSURE DROP (IN H ₂ 0): MIN: MAX: Avg: 10-15 wg	GAUGE?	YES] NO					
BULK PARTICLE DENSITY (LB/FT ³): 25		INLET TEMPERATU	JRE (°F	F): Contract	MIN		MAX		
POLLUTANT LOADING RATE: N/A 🛛 LB/HR 🛛	GR/FT ³	OUTLET TEMPERA	TURE	(°F) Contract	MIN		MAX		
INLET AIR FLOW RATE (ACFM): 1300		FILTER OPERATIN	G TEM	P (°F): Contract					
NO. OF COMPARTMENTS: 1 NO. OF BAGS F	PER COMPARTMENT:	Contract			LENG	TH OF BAG (IN.):	20-30		
NO. OF CARTRIDGES: Contract FILTER SURFA	CE AREA PER CARTI	RIDGE (FT ²): Contrac	:t		DIAME	TER OF BAG (IN.)	: 5-15		
TOTAL FILTER SURFACE AREA (FT ²): Contract	AIR TO CLOTH RAT	IQ: 1 to 4 : 1							
	FORCED/POSITIVE			FILTER MATERIAL · C:	artridae	Style 🔽	WOVE	N D	FELTED
	TOROLD/TOOTIVE			THETER MULTERINE. O	annage	i otyle 🖂	APTIC		
				F			ARTIO		
M AIR POLSE	SONIC					SIZE		WEIGHT %	CUMULATIVE
REVERSE FLOW	SIMPLE BAG COLLA	APSE				(MICRONS)		OF TOTAL	%
MECHANICAL/SHAKER	RING BAG COLLAPS	SE				0-1	-		
OTHER:						1-10	-		
DESCRIBE INCOMING AIR STREAM: Air stream will contain	i fly ash.					10-25			
						25-50			
						50-100			
						>100			
								TOTAL = 100	
					Suppli	er specific, 94% pa	ssing 3	25 mesh	
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHOWING	THE RELATIONSHIP	OF THE CONTROL [DEVICE	TO ITS EMISSION SO	URCE(S):			
COMMENTS:									

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NC	DEQ/Division of	Air Quality - Applic	ation for Ai	r Permit to	Construct/	Operate		В
EMISSION SOURCE DESCRIPTION:	Loadout Silo			EMISSION	SOURCE	ID NO: ES-3	38	
				CONTROL)-38	
OPERATING SCENARIO	1 OF	1		EMISSION			D(S): EP-38	3
DESCRIBE IN DETAILTHE EMISSIO Loadout silo is unloaded at the rate of	N SOURCE PRO 300 ton/hr and e	CESS (ATTACH FL quipped with bin ver	.OW DIAGR	AM): apture devic	:е.		<u> (), 1, 0,</u>	<u>, </u>
TYPE OF EMISSION SO	URCE (CHECK A	ND COMPLETE AF	PROPRIAT	E FORM B	1-B9 ON TH	IE FOLLOV	VING PAGE	S):
Coal,wood,oil, gas, other burner (Form B1)	□ Woodworking (Form B4)		🗆 Man	uf. of chemi	icals/coatin	gs/inks (Form I
Int.combustion engine/generator ((Form B2)	Coating/finishir	ng/printing (I	Form B5)	🗌 Incir	neration (Fo	rm B8)	
Liquid storage tanks (Form B3)		Storage silos/b	ins (Form B	6)	☐ Othe	er (Form B9)	
START CONSTRUCTION DATE: TB	C		DATE MA	NUFACTUF	RED: TBD			
MANUFACTURER / MODEL NO.: TB	D		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK :	52 WK/YR
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	TS?):	•		SHAP (SUB	PARTS?):		
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 MAR	-MAY 25	JU	N-AUG	25	SEP-NOV	25
CRITERIA	AIR POLLUT	ANT EMISSION	IS INFOR	MATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA		
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CON	TROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/vr	lb/hr	tons/vr	lb/hr	tons/vr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRON	S (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	IS (PM _{2.5})							
SULFUR DIOXIDE (SO2)	- (2.3)							
NITROGEN OXIDES (NOx)			SEE	APPENDIX	B, Table 6			
CARBON MONOXIDE (CO)					,			
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD	(100)							
OTHER								
HAZARDOUS	S AIR POLLU	TANT EMISSIC	NS INFO	RMATIO	N FOR T	HIS SOU	RCE	
		SOURCE OF	EXPECTE			POTENTIA		
		EMISSION	AFTER CONT				(AFTER CO	
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/vr	lb/hr	tons/vr	lb/hr	tons/vr
				, j.				
			SEE	APPENDIX	B, Table 6			
					,			
			1		1	1		1
			1	1	1	1	1	1
			1		1	1		1
ΤΟΧΙΟ ΑΙ	R POLLUTA	NT EMISSIONS	INFORM	ATION F	OR THIS	SOURCE	Ē	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION
	CAS NO		ll-)/hr	lh/	dav		lb/vr
			1.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		uuy		10/ 91
			SEE AF	PPENDIX B	, Table 6			
			1					
Attachments: (1) emissions calculations an	d supporting docum	entation; (2) indicate a	Il requested s	state and fede	eral enforceat	ole permit limi	ts (e.g. hours	s of operation,

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

REVISED 09/22/16	NCDEQ/Divis	ion of Air Quality - Ap	plicatior	n for Air Permit to Cor	nstruct/Operate		B6
EMISSION SOURCE DESCRIPT	FION: Loadout Silo			EMISSION SO	URCE ID NO: ES-38		
				CONTROL DE	VICE ID NO(S): CD-3	38	
OPERATING SCENARIO:	1	OF1		EMISSION PO	INT(STACK) ID NO(S): EP-38	
DESCRIBE IN DETAIL THE PRO	CESS (ATTACH FLO ate of 300 ton/hr and e	W DIAGRAM): quipped with bin vent p	roduct ca	apture device.			
MATERIAL STORED: Fly Ash				DENSITY OF MATER	IAL (LB/FT3): N/A		
	CUBIC FEET: N/A			TONS: 50.000			
DIMENSIONS (FEET)	HEIGHT: 111	DIAMETER: 41	(OR)	LENGTH:	WIDTH: H	IEIGHT:	
ANNUAL PRODUCT THRO	UGHPUT (TONS)	ACTUAL: 400,000		MAXIMUM DE	SIGN CAPACITY: 40	00,000	
PNEUMATICALLY FIL	LED	MECHANIC	ALLY FI	LLED		FILLED FROM	
BLOWER		SCREW CONVEYOR			□ RAILCAR		
		BELT CONVEYOR					
OTHER:		BUCKET ELEVATOR				PILE	
		OTHER:			OTHER:		
NO. FILL TUBES: 1							
MAXIMUM ACFM: 6000							
MATERIAL IS UNLOADED TO:							
BY WHAT METHOD IS MATERI Gravity	AL UNLOADED FROM	1 SILO?					
MAXIMUM DESIGN FILLING RA	ATE OF MATERIAL (TO	ONS/HR): N/A					
MAXIMUM DESIGN UNLOADIN	G RATE OF MATERIA	L (TONS/HR): 300					
COMMENTS: This silo only unloads.							

REVISED 09/22/16 N	CDEQ/Division of Air	Quality - Applicatio	on for <i>l</i>	Air Permit to Construct	/Operate			C1
CONTROL DEVICE ID NO: CD-38	CONTROLS EMISSIC	ONS FROM WHICH	EMISS	SION SOURCE ID NO(S)): ES-38			
EMISSION POINT (STACK) ID NO(S): EP-38	POSITION IN SERIES	S OF CONTROLS			NC). 1 C)F 1	UNITS
OPERATING SCENARIO:								
1 OF 1		P.E. SEAL REQUIR	ED (PI	ER 2g .0112)?	v	YES	[□ NO
DESCRIBE CONTROL SYSTEM: A bin vent for particulate co	ontrol on the Loadout s	ilo.						
POLLUTANTS COLLECTED:	-	PM		PM10/PM2.5				
BEFORE CONTROL EMISSION RATE (LB/HR):	-	0.0146		0.0069				
CAPTURE EFFICIENCY:	-	<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	_%		%
CONTROL DEVICE EFFICIENCY:		N/A	%	N/A	%	_%		%
CORRESPONDING OVERALL EFFICIENCY:	-	N/A	%	N/A	%	%		%
EFFICIENCY DETERMINATION CODE:	-	2		2				
TOTAL AFTER CONTROL EMISSION RATE (LB/HR):		0.0146		0.0069				
PRESSURE DROP (IN H ₂ 0): MIN: MAX: Avg: 10-15 wg	GAUGE?] YES] NO				
BULK PARTICLE DENSITY (LB/FT ³): 25		INLET TEMPERATU	JRE (°I	F): Contract	MIN	MAX		
POLLUTANT LOADING RATE: N/A 🛛 LB/HR 🗌] GR/FT ³	OUTLET TEMPERA	TURE	(°F) Contract	MIN	MAX		
INLET AIR FLOW RATE (ACFM): 1300		FILTER OPERATING	G TEM	P (°F): Contract				
NO. OF COMPARTMENTS: 1 NO. OF BAGS P	ER COMPARTMENT:	Contract			LENGTH OF BAG	(IN.): 20-3	30	
NO. OF CARTRIDGES: Contract FILTER SURFAC	CE AREA PER CARTR	RIDGE (FT ²): Contrac	zt		DIAMETER OF BA	G (IN.): 5-	-15	
TOTAL FILTER SURFACE AREA (FT ²): Contract	AIR TO CLOTH RATION	O: 1 to 4 : 1						
DRAFT TYPE: INDUCED/NEGATIVE	FORCED/POSITIVE			FILTER MATERIAL: C	artridge Style <	WOVEN		FELTED
DESCRIBE CLEANING PROCEDURES:					PA	RTICLE SIZ	ZE DISTRIBL	JTION
AIR PULSE	SONIC				SIZE	WE	IGHT %	CUMULATIVE
REVERSE FLOW	SIMPLE BAG COLLA	PSE			(MICRONS)	OF	TOTAL	%
MECHANICAL/SHAKER	RING BAG COLLAPS	SE			0-1			
OTHER:					1-10			
DESCRIBE INCOMING AIR STREAM: Air stream will contain	fly ash.				10-25			
					25-50			
					50-100			
					>100			
							TOTAL	. = 100
					Supplier specific, §	4% passin	g 325 mesh	
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHOWING	THE RELATIONSHIP C	OF THE CONTROL D	DEVICI	E TO ITS EMISSION SO	URCE(S):			
COMMENTS:								

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCDE	Q/Division of A	Air Quality - Applic	ation for A	ir Permit to	Construct/	Operate		В
EMISSION SOURCE DESCRIPTION: L	oadout Silo Ch	ute 1A		EMISSION	SOURCE I	D NO: ES-3	38A	
				CONTROL		NO(S): CE)-38A	
OPERATING SCENARIO1_	OF	11		EMISSION	POINT (ST	ACK) ID N	D(S): EP-38	8A
DESCRIBE IN DETAILTHE EMISSION Loadout silo chute 1A is unloaded at the	SOURCE PRO a rate of 100 tor	CESS (ATTACH F n/hr and equipped v	LOW DIAG with bin ven	RAM): t product cap	oture device			
TYPE OF EMISSION SOUR	CE (CHECK A		PPROPRIA	TE FORM B	1-B9 ON TH	HE FOLLOW	VING PAGE	ES):
Coal,wood,oil, gas, other burner (Fo	orm B1)		(Form B4)		∐ Man	uf. of chemi	cals/coating	gs/inks (Form E
Int.combustion engine/generator (Fo	orm B2)	Coating/finish	ing/printing	(Form B5)	🗌 Incin	eration (Fo	rm B8)	
Liquid storage tanks (Form B3)		Storage silos/	bins (Form	B6)		er (Form B9)		
START CONSTRUCTION DATE: TBD			DATE MA	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBD			EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT UNS	SPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGHPL	JT (%): DEC-F	EB 25 MAR	R-MAY 2	5 Jl	JN-AUG	25	SEP-NO	/ 25
CRITERIA AI	R POLLUTA	ANT EMISSION	IS INFOR	RMATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECTE	ED ACTUAL		POTENTIA	L EMISSIC	ONS
		EMISSION	AFTER CON	ROLS / LIMITS	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS ((PM ₁₀)							
PARTICULATE MATTER<2.5 MICRONS	(PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE	APPENDIX	B, Table 6			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS (V	OC)							
LEAD								
OTHER								
HAZARDOUS	AIR POLLU	TANT EMISSIC	ONS INFO	ORMATIO	N FOR T	'HIS SOU	RCE	
		SOURCE OF	EXPECTE	ED ACTUAL		POTENTIA	L EMISSIC	DNS
		EMISSION	AFTER CON	ROLS / LIMITS	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE	APPENDIX	B, Table 6			
TOXIC AIR	POLLUTAN	IT EMISSIONS	INFORM	IATION F	OR THIS	SOURC	E	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lt	o/hr	lb/	day		lb/yr
			SEE A	PPENDIX B,	Table 6			
Attachments: (1) emissions calculations and s	supporting docum	entation: (2) indicate	all requested	state and fed	eral enforcea	ble permit lin	nits (e.a. hou	s of operation.

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

REVISED 09/22/16	NCDEQ/Divis	ion of Air Quality -	Applicatior	for Air Permit to Co	onstruct/Operate		B6
EMISSION SOURCE DESCRIPT	ION: Loadout Silo Ch	ute 1A		EMISSION S	OURCE ID NO: ES	-38A	
				CONTROL D	EVICE ID NO(S): C	D-38A	
OPERATING SCENARIO:	1	OF1		EMISSION P	OINT(STACK) ID N	O(S): EP-38A	
DESCRIBE IN DETAIL THE PRC Loadout silo chute 1A is unloade	DCESS (ATTACH FLO d at the rate of 100 tor	W DIAGRAM): n/hr and equipped wi	th bin vent p	product capture devic	e.		
				DENSITY OF MATER	RIAL (LB/F13): N/A		
		DIAMETER: 41	(OR)				
			(0.1)			200.000	
PNEUMATICALLY FIL	LED	MECHAN	ICALLY FI		ESIGN CAFACITT.	FILLED FROM	
			R			R	
			JR				
)R				
		OTHER.					
NO. FILL TUBES' N/A		Official.				·	
MAXIMUM ACFM: 6000							
MATERIAL IS UNLOADED TO:	l						
N/A							
BY WHAT METHOD IS MATERI. N/A	AL UNLOADED FROM	1 SILO?					
MAXIMUM DESIGN FILLING RA	TE OF MATERIAL (TO	ons/hr): N/A					
MAXIMUM DESIGN UNLOADING	G RATE OF MATERIA	L (TONS/HR): 100					
COMMENTS: This silo only unloads.							

REVISED 09/22/16	N	ICDEQ/Division of Air	r Quality - Applicatio	on for	Air Permit to Construct	t/Operate			C1
CONTROL DEVICE ID NO: CD-38A		CONTROLS EMISSI	ONS FROM WHICH	EMIS	SION SOURCE ID NO(S): ES-38A			-
EMISSION POINT (STACK) ID NO(S): EP-	-38A	POSITION IN SERIE	S OF CONTROLS			NC	. 1	OF 1	UNITS
OPERATING SCEN	IARIO:								
10F1	1		P.E. SEAL REQUIR	ED (F	PER 2q .0112)?	\checkmark	YES		□ NO
DESCRIBE CONTROL SYSTEM: A bin vent for	particulate c	ontrol on the Loadout	silo chute 1A.						
POLLUTANTS COLLECTED:			PM		PM10/PM2.5				
BEFORE CONTROL EMISSION RATE (LB/HR):	:		0.005		0.002				
CAPTURE EFFICIENCY:			<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	_%		%
CONTROL DEVICE EFFICIENCY:			N/A	%	N/A	%	_%		%
CORRESPONDING OVERALL EFFICIENCY:			N/A	%	N/A	%	_%		%
EFFICIENCY DETERMINATION CODE:			2		2				
TOTAL AFTER CONTROL EMISSION RATE (LE	3/HR):		0.005		0.002				<u>. </u>
PRESSURE DROP (IN H ₂ 0): MIN: MAX: Avg	j: 10-15 wg	GAUGE?	YES	[NO				
BULK PARTICLE DENSITY (LB/FT ³): 25			INLET TEMPERATU	JRE (F): Contract	MIN	MAX		
POLLUTANT LOADING RATE: N/A	_B/HR [GR/FT°	OUTLET TEMPERA	TURE	E (°F) Contract	MIN	MAX		
INLET AIR FLOW RATE (ACFM): 1300			FILTER OPERATIN	G TEN	MP (^o F): Contract				
NO. OF COMPARTMENTS: 1 NO	· OF BAGS F	PER COMPARTMENT	Contract			LENGTH OF BAG	(IN.): 20-	30	-
NO. OF CARTRIDGES: Contract FIL	TER SURFA		RIDGE (FI ⁻): Contrac	t		DIAMETER OF BA	G (IN.): 5	-15	
	<u>x</u> r D		10: 1 to 4:1			antrida a Otuda 🖂			
	E	FORCED/POSITIVE			FILTER MATERIAL: C	artridge Style			
		CONIC							
			ADSE				VVE		COMOLATIVE
		SIMPLE BAG COLLAR					0	TOTAL	/8
		RING BAG COLLAP	SE			0-1			
DESCRIBE INCOMING AIR STREAM: Air stream	m will contain	fly ash.				10.25			
						25-50			
						50-100			
						>100			
								ΤΟΤΑΙ	L = 100
						Supplier specific, 9	4% passi	ng 325 mesh	
ON A SEPARATE PAGE, ATTACH A DIAGRAM	I SHOWING		OF THE CONTROL D	DEVIC	E TO ITS EMISSION SO	URCE(S):			
COMMENTS:									

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCI	DEQ/Division of	Air Quality - Applica	ation for Air	Permit to 0	Construct/C)perate		В
EMISSION SOURCE DESCRIPTION:	Loadout Silo Ch	ute 1B		EMISSION			18B	
							200	
		1					-30D	
					IPUINT (ST	ACK) ID N	J(3). EP-30	D
Loadout silo chute 1B is unloaded at ti	he rate of 100 tor	/hr and equipped wit	th bin vent p	roduct captu	ure device.			
TYPE OF EMISSION SO	URCE (CHECK A	ND COMPLETE AP	PROPRIAT	E FORM B1	-B9 ON TH	E FOLLOW	ING PAGE	S):
Coal,wood,oil, gas, other burner (F	Form B1)	Woodworking (I	Form B4)		🗆 Man	uf. of chemi	cals/coating	gs/inks (Form
□ Int.combustion engine/generator (Form B2)	Coating/finishin	g/printing (F	orm B5)	🗌 Incin	eration (For	m B8)	
Liquid storage tanks (Form B3)		Storage silos/bi	ns (Form B6	5)	□ Othe	er (Form B9)		
START CONSTRUCTION DATE: TBE)		DATE MA	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBI	D		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT 🛛 I	NSPS (SUBPAR	FS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGHF	PUT (%): DEC-F	EB 25 MAR-	MAY 25	JUN	I-AUG	25	SEP-NOV	25
CRITERIA	AIR POLLUT	ANT EMISSION	S INFOR	MATION	FOR THIS	s sourc	E	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	DNS
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	S (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE	APPENDIX	B, Table 6			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD								
OTHER								
HAZARDOU	S AIR POLLU	ITANT EMISSIC	ONS INFO	RMATIOI	N FOR TH	IIS SOUI	RCE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	DNS
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE	APPENDIX	B, Table 6			
TOXIC AI	IR POLLUTA	NT EMISSIONS	INFORM	ATION FO	OR THIS	SOURCE		
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION
		EMISSION						
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lk	o/hr	lb/e	day		lb/yr
			SEE A	PPENDIX B,	Table 6			

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

REVISED 09/22/16	NCDEQ/Divis	ion of Air Qualit	ty - Applicatior	n for Air Permit to Co	onstruct/Operate	B6
EMISSION SOURCE DESCRIPT	ION: Loadout Silo Chu	ute 1B		EMISSION S	OURCE ID NO: ES-38B	
				CONTROL D	EVICE ID NO(S): CD-38B	
OPERATING SCENARIO:	1	OF	1	EMISSION P	OINT(STACK) ID NO(S): EP-38B	
DESCRIBE IN DETAIL THE PRC Loadout silo chute 1B is unloader	CESS (ATTACH FLO	W DIAGRAM): ı/hr and equipped	d with bin vent p	product capture device	e.	
MATERIAL STORED [,] Fly Ash				DENSITY OF MATER	RIAL (LB/FT3): N/A	
	CUBIC FEET: N/A			TONS: 150 tph		
DIMENSIONS (FEET)	HEIGHT: 111	DIAMETER: 41	(OR)	LENGTH:	WIDTH: HEIGHT:	
ANNUAL PRODUCT THRO	UGHPUT (TONS)	ACTUAL: 200,(000	MAXIMUM DI	ESIGN CAPACITY: 200,000	
PNEUMATICALLY FIL	LED	MECI	HANICALLY FI	LLED	FILLED FROM	
BLOWER		SCREW CONV	EYOR		RAILCAR	
		BELT CONVEY	′OR			
OTHER:		BUCKET ELEV	ATOR		STORAGE PILE	
		OTHER:			OTHER:	
NO. FILL TUBES: N/A						
MAXIMUM ACFM: 6000						
MATERIAL IS UNLOADED TO:						
N/A						
N/A						
MAXIMUM DESIGN FILLING RA	TE OF MATERIAL (TO	ons/hr): N/A				
MAXIMUM DESIGN UNLOADING	3 RATE OF MATERIA	L (TONS/HR): 1(00			
COMMENTS: This silo only unloads.						

REVISED 09/22/16	N	CDEQ/Division of Ai	r Quality - Applicatio	on for	Air Permit to Construct	t/Operate		C1
CONTROL DEVICE ID NO: CD-38B		CONTROLS EMISSI	IONS FROM WHICH	EMIS	SION SOURCE ID NO(S): ES-38B		-
EMISSION POINT (STACK) ID NO(S): EP-	-38B	POSITION IN SERIE	S OF CONTROLS			NO	. 1 OF	1 UNITS
OPERATING SCEN	IARIO:							
1OF1	1		P.E. SEAL REQUIR	ED (F	PER 2q .0112)?	v	YES	□ NO
DESCRIBE CONTROL SYSTEM: A bin vent for	particulate c	ontrol on the Loadout	silo chute 1B.					
POLLUTANTS COLLECTED:			PM		PM10/PM2.5			
BEFORE CONTROL EMISSION RATE (LB/HR):	:		0.005		0.002			
CAPTURE EFFICIENCY:			<= 0.005 gr/dscf	%	<= 0.005 gr/dscf	%	%	%
CONTROL DEVICE EFFICIENCY:			N/A	%	N/A	%	%	%
CORRESPONDING OVERALL EFFICIENCY:			N/A	%	N/A	%	_%	%
			2		2			
TOTAL AFTER CONTROL EMISSION RATE (LE	3/HR):		0.005		0.002	<u> </u>		
PRESSURE DROP (IN H ₂ 0): MIN: MAX: Avg	j: 10-15 wg	GAUGE?	YES	[NO			
BULK PARTICLE DENSITY (LB/FT ³): 25			INLET TEMPERATU	JRE ('F): Contract	MIN	MAX	
POLLUTANT LOADING RATE: N/A	.B/HR	GR/FT	OUTLET TEMPERA		(°F) Contract	MIN	MAX	
INLETAIR FLOW RATE (ACFM): 1300			FILTER OPERATING	GIEN	AP ('F): Contract		(1)	
NO. OF COMPARIMENTS: 1 NO.			: Contract	*		LENGTH OF BAG	(IN.): 20-30	
TOTAL FILTER SURFACE AREA (FT ²): Contract	TER SURFA		RIDGE (FT). Contrac	il.		DIAIVIETER OF BA	3 (IN.). 5-15	
			10. 1104.1			artridae Style	WOVEN	
DESCRIBE CLEANING PROCEDURES		TOROED/TOSITIVE			TIETER MATERIAL O			RIBUTION
		SONIC				SIZE		
			ADSE					CONICEATIVE %
							OFTOTAL	70
		RING BAG COLLAP	'SE			0-1		
DESCRIBE INCOMING AIR STREAM:Air stream	n will contain	fly ash.				10.25		
						25-50		
						50-100		
						>100		
						100	ТС)TAL = 100
						Supplier specific, 9	4% passing 325 m	esh
ON A SEPARATE PAGE, ATTACH A DIAGRAM	I SHOWING	THE RELATIONSHIP	OF THE CONTROL D	DEVIC	E TO ITS EMISSION SC	URCE(S):		
COMMENTS:								

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCD	EQ/Division of A	Air Quality - Appli	cation for A	ir Permit to	Construct/	Operate		В
EMISSION SOURCE DESCRIPTION:	Screener			EMISSION	SOURCE II	D NO: ES-3	9A	
				CONTROL	DEVICE ID	NO(S): N/A		
OPERATING SCENARIO	1OF	1		EMISSION	POINT (ST	ACK) ID NC)(S): EP-39	
DESCRIBE IN DETAILTHE EMISSIO The screening process will occur to pr	N SOURCE PRO oduce free flowin	DCESS (ATTACH F ng feedstock suitab	LOW DIAG	RAM): TAR® reacto	or.			
TYPE OF EMISSION SOU	IRCE (CHECK A	ND COMPLETE A	PPROPRIA	TE FORM B	1-B9 ON TH	IE FOLLOV	VING PAGI	ES):
Coal,wood,oil, gas, other burner (Form B1)	U Woodworking	g (Form B4)		🗆 Man	uf. of chemi	cals/coating	gs/inks (Form
 Int.combustion engine/generator (Liquid storage tanks (Form B3) 	Form B2)	Coating/finishStorage silos	hing/printing /bins (Form	(Form B5) B6)	☐ Incin ⊡ Othe	eration (For r (Form B9)	m B8)	
START CONSTRUCTION DATE: TBE)		DATE MA	NUFACTURI	ED: TBD			
MANUFACTURER / MODEL NO.: TB	D		EXPECTE	D OP. SCHE	EDULE: 260	0 hours/yea	r	
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	TS?):		NES	SHAP (SUBF	PARTS?):		
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 MA	R-MAY 2	5 JI	JN-AUG	25	SEP-NO	/ 25
CRITERIA A	AIR POLLUT	ANT EMISSIOI	NS INFO	RMATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECT	ED ACTUAL		POTENTIA	L EMISSIC	DNS
		EMISSION	(AFTER CON	TROLS / LIMITS)	BEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRON	S (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	IS (PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE A	PPENDIX B,	Table 14A			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD	()							
OTHER								
HAZARDOUS	AIR POLLU	TANT EMISSI	ONS INF	ORMATIO	N FOR T	HIS SOU	RCE	1
		SOURCE OF	EXPECT	ED ACTUAL		POTENTIA	L EMISSIC	DNS
		EMISSION	(AFTER CON	TROLS / LIMITS)	BEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE A	PPENDIX B,	Table 14A			
		l	İ		1			
			1	1	1			
TOXIC AI	R POLLUTAN	NT EMISSIONS	INFORI	ATION F	OR THIS	SOURC	E	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSIONS	AFTER CO	ONTROLS	
TOXIC AIR POLLUTANT	CAS NO			o/hr	lb/	dav		lb/vr
		THOTON .		5,111	10/	uuy		10/ yi
	1							
	1	1						
			SFF AP		Table 144			
		<u> </u>	1		I			

FORM B9 EMISSION SOURCE (OTHER)

EMISSION SOURCE DESCRIPTION: Screener EMISSION SOURCE ID NO. ES.39A OPERATING SCENARIO.	REVISED 09/22/16 NCDEQ/Division of Air Quality - A	pplication for	Air Permit to Construct/Operate		B9
CONTROL DEVICE ID NO(S): NA DERATING SCENARIO:	EMISSION SOURCE DESCRIPTION: Screener		EMISSION SOURCE ID NO: ES-39A	- -	
OPERATING SCENARIO:			CONTROL DEVICE ID NO(S): N/A		
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/AR) LIMITATION(UNIT/AR) Capacity ton 165 165 MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/AR) LIMITATION(UNIT/AR) Gapacity ton 165 165 MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): EACH EACH EACH MAXIMUM DESIGN (BATCHES / HOUR): (BATCHES / HOUR): (BATCHES / HOUR): EACUESTED CAPACITY ANNUAL FUEL USE: NA MAXIMUM DESIGN (BATCHES / HOUR): REQUESTED CAPACITY ANNUAL FUEL USE: NA COTAL MAXIMUM FIRING RATE (MILLION BTUHR): NA MAX. CAPACITY HOURLY FUEL USE: NA TOTAL MAXIMUM FIRING RATE (MILLION BTUHR): NA REQUESTED CAPACITY ANNUAL FUEL USE: NA	OPERATING SCENARIO:1 OF1		EMISSION POINT (STACK) ID NO(S	S): EP-39	
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/HR) LIMITATION(UNIT/HR) Capacity Ion 165 165 MAX. DESIGN Ion 165 165 MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Internation Ion Ion Ion Internation <td>DESCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIAGRAM): The scree</td> <td>ening process wi</td> <td>Il occur to produce free flowing feedsto</td> <td>ck suitable for the ST</td> <td>AR® reactor</td>	DESCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIAGRAM): The scree	ening process wi	Il occur to produce free flowing feedsto	ck suitable for the ST	AR® reactor
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/HR) LIMITATION(UNIT/HR) Capacity ton 165 165 Capacity 1 1 165 165 Capacity 1 1 165 165 Capacity 1 1 1 165 165 Capacity 1 1 1 165 165 Capacity 1 1 1 1 1 MATERIALS ENTERING PROCESS - BATCH OPERATION MAX: DESIGN REQUESTED CAPACITY 1 TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) 1 TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) 1 Capacity 1 1 1 1 1 Capacity 1 1 <t< td=""><td></td><td></td><td></td><td></td><td></td></t<>					
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/HR) LIMITATION(UNIT/HR) Capacity ton 165 165 Capacity ton 166 165 Capacity ion ion 165 Materials entering Process - Batch Operation Max. Design Requested Capacity MATERIals ENTERING PROCESS - Batch Operation Max. Design Requested Capacity TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Internation ion ion ion MAXERIALS ENTERING PROCESS - Batch Operation Max. Design Requested Capacity Maxerial Entering Process - Batch Operation Max. Design Iumitation (UNIT/BATCH) Internation Iumitation (UNIT/BATCH) Iumitation (UNIT/BATCH) Iumitation (UNIT/BATCH) Internation Iumitation (Iumitation (Iumitation (Iumitation (Iumitation (Iumitation (
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/HR) LIMITATION(UNIT/HR) Capacity ton 165 165 Capacity International Content of Capacity 165 165 MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) International Content of Capacity Internation (UNIT/BATCH) Internation (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): Internation (UNIT/BATCH) Internation (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): Internation (UNIT/BATCH) Internation (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): Internation (BATCHES / HOUR): Internation (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR):<					
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/HR) LIMITATION(UNIT/HR) Capacity Ion 165 165 MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Capacity Ion Ion Ion TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Capacity Ion Ion Ion Internation Ion Ion Ion MAXIMU					
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/HR) LIMITATION(UNIT/HR) Capacity ton 165 165 Capacity 165 165 165 MAX. DESIGN REQUESTED CAPACITY 165 MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Capacity (UNIT/BATCH) IMITATION (UNIT/BATCH) IMITATION (UNIT/BATCH) MAX. DESIGN (BATCHES / HOUR): Imitation (UNIT/BATCH) Imitation (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): Imitation (UNIT/BATCH) Imitation (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): Imitation (Imitation (Imitation (Imitation (Imitation (Imitation (Imitation (Imitation (Imitation (
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/HR) LIMITATION(UNIT/HR) Capacity ion 165 165 MAX. DESIGN REQUESTED CAPACITY 165 MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): Image: Capacity (UNIT/BATCH) Image: Capacity (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): (BATCHES/R): Image: Capacity HOURLY FUEL USE: N/A MAXIMUM DESIGN (BATCHES / HOUR): (BATCHES/R): FROUESTED LIMITATION (BATCHES / HOUR): FUEL USE: N/A TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A MAX. CAPACITY HOURLY FUEL U					
TYPE UNTS CAPACITY (UNIT/HR) LIMITATION(UNIT/HR) Capacity ton 165 165 Capacity ton 165 165 Capacity Capacity (UNIT/HR) 165 165 Capacity Capacity (UNIT/HR) 165 165 Capacity Capacity 165 165 Capacity Capacity 165 165 Capacity Capacity 165 165 MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Capacity Capacity (UNIT/BATCH) LIMITATION (UNIT/BATCH) Capacity Capacity (UNIT/BATCH) LIMITATION (UNIT/BATCH) Capacity Capacity (UNIT/BATCH) LIMITATION (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): Capacity (UNIT/BATCH) Capacity (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): (BATCHES/YR): Capacity ANNUAL FUEL USE: N/A MAXIMUM DESIGN (BATCHES / HOUR): (BATCHES/YR): FUEL USE: N/A MAXIMUM DESIGN (BATCHES / HOUR):	MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS	S	MAX. DESIGN	REQUESTED	CAPACITY
Capacity ton 165 165 Capacity I	TYPE	UNITS	CAPACITY (UNIT/HR)	LIMITATION	(UNIT/HR)
Image: Section of the synthesis of the synthesynthesis of the synthesis of the synthesis of	Capacity	ton	165		165
Image: Sector of the sector					
Image: Image:					
Image: state s					
MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): Interview Interview Interview MAXIMUM DESIGN (BATCHES / HOUR): (BATCHES/YR): Interview Interview FUEL USEID N/A TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A MAX. CAPACITY HOURLY FUEL USE: N/A REQUESTED CAPACITY ANNUAL FUEL USE: N/A COMMENTS: TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A REQUESTED CAPACITY ANNUAL FUEL USE: N/A					
MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) MAX. DESIGN CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) MAX. DESIGN (BATCHES / HOUR): Image: Capacity (UNIT/BATCH) Image: Capacity (UNIT/BATCH) MAXIMUM DESIGN (BATCHES / HOUR): (BATCHES/YR): Image: Capacity (UNIT/BATCH) FUEL USED: N/A TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A MAX. CAPACITY HOURLY FUEL USE: N/A COMMENTS: CAPACITY ANNUAL FUEL USE: N/A COMMENTS:					
MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Image: Comparison of the state					
MATERIALS ENTERING PROCESS - BATCH OPERATION MAX. DESIGN REQUESTED CAPACITY TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Image: Ima					
TYPE UNITS CAPACITY (UNIT/BATCH) LIMITATION (UNIT/BATCH) Image: Ima	MATERIALS ENTERING PROCESS - BATCH OPERATION		MAX. DESIGN	REQUESTED	CAPACITY
Image: Section of the section of t	ТҮРЕ	UNITS	CAPACITY (UNIT/BATCH)	LIMITATION (U	NIT/BATCH)
Image: Section of the section of t					
Image: Section of the section of t					
Image: Section of the section of th					
Image: Section of the section of t					
MAXIMUM DESIGN (BATCHES / HOUR): REQUESTED LIMITATION (BATCHES / HOUR): FUEL USED: N/A MAX. CAPACITY HOURLY FUEL USE: N/A COMMENTS:					
MAXIMUM DESIGN (BATCHES / HOUR): REQUESTED LIMITATION (BATCHES / HOUR): FUEL USED: N/A MAX. CAPACITY HOURLY FUEL USE: N/A COMMENTS:					
MAXIMUM DESIGN (BATCHES / HOUR): REQUESTED LIMITATION (BATCHES / HOUR): FUEL USED: N/A MAX. CAPACITY HOURLY FUEL USE: N/A COMMENTS:					
MAXIMUM DESIGN (BATCHES / HOUR): (BATCHES/YR): REQUESTED LIMITATION (BATCHES / HOUR): (BATCHES/YR): FUEL USED: N/A TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A MAX. CAPACITY HOURLY FUEL USE: N/A REQUESTED CAPACITY ANNUAL FUEL USE: N/A COMMENTS: COMMENTS:					
REQUESTED LIMITATION (BATCHES / HOUR): (BATCHES/YR): FUEL USED: N/A TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A MAX. CAPACITY HOURLY FUEL USE: N/A REQUESTED CAPACITY ANNUAL FUEL USE: N/A COMMENTS: COMMENTS:	MAXIMUM DESIGN (BATCHES / HOUR):				
FUEL USED: N/A TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A MAX. CAPACITY HOURLY FUEL USE: N/A REQUESTED CAPACITY ANNUAL FUEL USE: N/A COMMENTS: COMMENTS:	REQUESTED LIMITATION (BATCHES / HOUR):	(BATCHES/Y	′R):		
MAX. CAPACITY HOURLY FUEL USE: N/A REQUESTED CAPACITY ANNUAL FUEL USE: N/A COMMENTS:	FUEL USED: N/A	TOTAL MAX	IMUM FIRING RATE (MILLION BTU/H	R): N/A	
COMMENTS:	MAX. CAPACITY HOURLY FUEL USE: N/A	REQUESTE	D CAPACITY ANNUAL FUEL USE: N/A	4	
	COMMENTS:				

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

	EQ/DIVISION OF	Air Quality - Applicat	ion for Air	Permit to C	onstruct/O	perate		В
EMISSION SOURCE DESCRIPTION: S	Screener-Diese	l Engine		EMISSION	SOURCE I	D NO: ES-3	9B	
				CONTROL	DEVICE ID	NO(S): N/A	١	
OPERATING SCENARIO1_	OF	1	_	EMISSION	POINT (ST	ACK) ID NO)(S): EP-39	
DESCRIBE IN DETAILTHE EMISSION S Diesel Engine to run the Screener.	SOURCE PRO	CESS (ATTACH FLO)	W DIAGRAN	/):				
TYPE OF EMISSION SOU	RCE (CHECK	AND COMPLETE APP	ROPRIATE	FORM B1-	B9 ON THE	FOLLOWI	NG PAGES	5):
Coal,wood,oil, gas, other burner (Fc	orm B1)	Woodworking (Fo	orm B4)		🗌 Man	uf. of chemi	cals/coating	, gs/inks (Form I
Int.combustion engine/generator (Fc	orm B2)	Coating/finishing/	printing (Fo	rm B5)	🗌 Incin	eration (For	m B8)	
Liquid storage tanks (Form B3)	,	Storage silos/bins	(Form B6)	,	□ Othe	er (Form B9)	,	
START CONSTRUCTION DATE: TBD		_	DATE MAN	UFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBD			EXPECTE	OP. SCH	EDULE: 260	0 hours/vea	ar	
	SPS (SUBPAR	[S?)·			SHAP (SUB	PARTS?)		
		EB 25 MAR-M	 ∆V 25			5 SE		5
		TANT FMISSIONS				SOURC	F	.5
			EVDECTE					NS
		EMISSION						
			AFTER CONTI	tono/ur		ROLS / LIMITS	(AFTER COT	tene/ur
		FACTOR	ID/III	tons/yr	ID/III	tons/yr	ID/III	toris/yr
PARTICULATE MATTER OF MICRONS (РМ ₁₀)							
PARTICULATE MATTER<2.5 MICRONS ((PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE AP	PENDIX B,	Table 14B			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS (V	(OC)							
LEAD								
OTHER							_	
HAZARDOUS	AIR POLL	UTANT EMISSIO	IS INFOR	RMATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	NS
		EMISSION	AFTER CONT	ROLS / LIMITS	EFORE CONT	ROLS / LIMITS	(AFTER CON	ITROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CACNO				lh/hr	tons/yr	lb/hr	tons/yr
	CAS NO.	FACTOR	lb/hr	tons/yr				
	CAS NO.	FACTOR	lb/hr	tons/yr	10/11			
	CAS NO.	FACTOR	lb/hr	tons/yr	10/111			
		FACTOR	lb/hr	tons/yr				
		FACTOR	lb/hr	tons/yr				
		FACTOR	lb/hr	tons/yr				
		FACTOR	Ib/hr	tons/yr	Table 14B			
		FACTOR	Ib/hr	tons/yr PENDIX B,	Table 14B			
		FACTOR	Ib/hr	tons/yr PENDIX B,	Table 14B			
		FACTOR	Ib/hr	tons/yr	Table 14B			
		FACTOR	Ib/hr	PENDIX B,	Table 14B			
		FACTOR	Ib/hr	PENDIX B,	Table 14B			
		FACTOR	Ib/hr	PENDIX B,	Table 14B			
	R POLLUTA	FACTOR	Ib/hr SEE AP	TION FC	Table 14B	SOURCE		
	R POLLUTA	FACTOR	Ib/hr SEE AP	PENDIX B,	Table 14B	SOURCE		
TOXIC AIP	R POLLUTA	FACTOR	Ib/hr SEE AP	TION FC	Table 14B	SOURCE S AFTER CO	DNTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	Ib/hr SEE AP	tons/yr PENDIX B, TION FC	Table 14B	SOURCE S AFTER CC	DNTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	Ib/hr SEE AP	TION FC	Table 14B	SOURCE SAFTER CO	DNTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	Ib/hr SEE AP	tons/yr PENDIX B, TION FC D ACTUAL	Table 14B	SOURCE SAFTER CO	DNTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	Ib/hr SEE AP	tons/yr PENDIX B, TION FC D ACTUAL	Table 14B	SOURCE SAFTER CO	DNTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	Ib/hr SEE AP SEE CTE	tons/yr PENDIX B, TION FC D ACTUAL /hr APPENDI	Table 14B	SOURCE SAFTER CO day	DNTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	Ib/hr SEE AP SEE CTE EXPECTE	tons/yr PENDIX B, TION FC D ACTUAL /hr E APPENDI	Table 14B	SOURCE SAFTER CC day	DNTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	Ib/hr SEE AP	tons/yr PENDIX B, TION FC D ACTUAL /hr E APPENDI	Table 14B	SOURCE S AFTER CC day	DNTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	Ib/hr SEE AP SEE AP EXPECTE Ib SEI	tons/yr PENDIX B, TION FC D ACTUAL /hr E APPENDI	Table 14B	SOURCE S AFTER CC day	DNTROLS	/ LIMITATIONS

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source. **OMPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOUR**

EMISSION SOURCE (INTERNAL COMBUSTION ENGINES/TURBINES/GENERATORS)

REVISED 09/22/16	NCDEQ/Division of Air Quality	y - Application for Air Perm	it to Construct	/Operate	B2
EMISSION SOURCE DESCRIPTION: S	Screener-Diesel Engine		EMISSION SOL	URCE ID NO: ES-39B	_
			CONTROL DE	VICE ID NO(S): N/A	
OPERATING SCENARIO:	1 OF 1		EMISSION POI	NT (STACK) ID NO(S): EP-39	
	EMERGENCY	SPACE HEAT		RICAL GENERATION	
	PEAK SHAVER	OTHER (DESCRIBE): To o	perate the scree	ner.	
GENERATOR OUTPUT (KW)	ANTICIP		OPERATION (H	IRS/YR): 2600	
			01 210 11011 (11		
				ATER THAN 600 HP	AL FUEL ENGINE
	E):		(comple	te below)	
	N 🗌 LEAN BURN		(+++++++++++++++++++++++++++++++++		
EMISSION REDUCTION MODIFICATION		RETARD 🗌 PREIG	NITION CHAME		HER
OR 🗌 STATIONARY GAS TURB	INE (complete below)	NATURAL GAS PIPELINE	COMPRESSOR	OR TURBINE (complete below)	
		TYPE: 2-CYCLE LEAN	BURN	□ 4-CYCLE LEAN □ TU	RBINE
OTHER (DESCRIBE):		4-CYCLE RICH	IBURN	OTHER (DESCRIBE):	
		DLS: COMBUSTION	MODIFICATION	NS (DESCRIBE):	
		ISELECTIVE CATALYTIC RE	EDUCTION	SELECTIVE CATALYTIC R	EDUCTION
CONTROLS: UNATER-S		AN BURN AND PRECOMBL	ISTION CHAMB		
	LEAN-PREMIX				
OTHER (SPECIFY):					
	FUEL USAGE (II	NCLUDE STARTUP/BA	ACKUP FUE	L)	
		MAXIMUM DESIGN		REQUESTED CAPACI	TY
FUEL TYPE	UNITS	CAPACITY (UNIT/HR	R)	LIMITATION (UNIT/HF	र)
Diesel	gallons	3.75 @ 75 % load		2600 hr/vr	
	<u>y</u>				
	FUEL CHARACTERISTICS	G (COMPLETE ALL TH	AT ARE APP	PLICABLE)	
				SULFUR CONTEN	<u></u> Т
FUEL TYPE	BTU/UNIT	UNITS		(% BY WEIGHT)	
Diesel	6 40E±05	Hour			0.0015%
	0.402+00				0.001378
	MANUFACTURER'S SPE	L	TORS (IF AV	AILABLE)	
POLLUTANT	NOX	CO PM	P	M10 VOC	OTHER
EMISSION FACTOR LB/UNIT					_
DESCRIBE METHODS TO MINIMIZE	ISIBLE EMISSIONS DURING IDLI	NG, OR LOW LOAD OPERA	TIONS:		
COMMENTS:					

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCD	EQ/Division of A	Air Quality - Appli	cation for A	ir Permit to	Construct/	Operate		В
EMISSION SOURCE DESCRIPTION:	Crusher			EMISSION	SOURCE I	D NO: ES-4	0A	
				CONTROL	DEVICE ID	NO(S)· N/A	-	
OPERATING SCENARIO	OF.	1		EMISSION	POINT (ST		(S) EP-40	
							(O). EI 40	
Fly ash will be processed further by pa	ssing through a	crusher to remove	larger partie	cles and to p	roduce more	e fine and fr	ee flowing f	eedstock.
TYPE OF EMISSION SOU	RCE (CHECK A	ND COMPLETE A	PPROPRIA	TE FORM B	1-B9 ON TH	E FOLLOV	VING PAGE	S):
Coal,wood,oil, gas, other burner (F	Form B1)	U Woodworking	(Form B4)		🗆 Man	uf. of chemi	cals/coating	s/inks (Form
Int.combustion engine/generator (Form B2)	Coating/finish	ning/printing	(Form B5)	🗌 Incin	eration (For	m B8)	
Liquid storage tanks (Form B3)		Storage silos	/bins (Form	B6)	🗸 Othe	r (Form B9)		
START CONSTRUCTION DATE: TBD)		DATE MA	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBI	0		EXPECTE	D OP. SCHE	EDULE: 365	hours/year		
IS THIS SOURCE SUBJECT 🛛 I	NSPS (SUBPAR	TS?):		NES	HAP (SUBF	PARTS?):		
PERCENTAGE ANNUAL THROUGHF	PUT (%): DEC-F	EB 25 MA	R-MAY 2	5 Jl	JN-AUG	25	SEP-NO\	/ 25
CRITERIA A	IR POLLUT	ANT EMISSIOI	VS INFO	RMATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECT	ED ACTUAL		POTENTIA	L EMISSIC	NS
		EMISSION	(AFTER CON	FROLS / LIMITS)	BEFORE CONT	ROLS / LIMITS	(AFTER COM	ITROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	6 (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE A	PPENDIX B,	Table 15A			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD								
OTHER								
HAZARDOUS	AIR POLLU	TANT EMISSI	ONS INF	ORMATIO	N FOR T	HIS SOU	RCE	
		SOURCE OF	EXPECT	D ACTUAL		POTENTIA	L EMISSIC	NS
		EMISSION	(AFTER CON	FROLS / LIMITS)	BEFORE CONT	ROLS / LIMITS	(AFTER COM	ITROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE A	PPENDIX B,	Table 15A			
TOXIC AII	R POLLUTAI	NT EMISSIONS	S INFORI	/ATION F	OR THIS	SOURC	E	
		SOURCE OF	EXPECTE	D ACTUAL I	EMISSIONS	AFTER CO	ONTROLS /	LIMITATION
TOXIC AIR POLLUTANT	CAS NO.	FACTOR		o/hr	lb/o	day		lb/yr
		Ī						
		Ī						
		1	SEE AP	PENDIX B, T	Table 15A			
		1		,				
		1						
			1		1			
REVISED 09/22/16 NCDEQ/Division of Air Quality - Ap	plication for	Air Permit to Construct/Operate		B9				
--	---------------	-------------------------------------	---------------------------	---------------------				
EMISSION SOURCE DESCRIPTION: Crusher		EMISSION SOURCE ID NO: ES	-40A					
		CONTROL DEVICE ID NO(S): N	I/A					
OPERATING SCENARIO:1 OF1		EMISSION POINT (STACK) ID N	NO(S): EP-40					
DESCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIAGRAM): Fly ash will more fine and free flowing feedstock.	be processed	further by passing through a crushe	er to remove larger parti	cles and to produce				
MATERIALS ENTERING PROCESS - CONTINUOUS PROCESS		MAX. DESIGN	REQUEST	ED CAPACITY				
ТҮРЕ	UNITS	CAPACITY (UNIT/HR)	LIMITATIC	N(UNIT/HR)				
Capacity	ton	165 ton/day	165 ton/day					
MATERIALS ENTERING PROCESS - BATCH OPERATION	1	MAX. DESIGN	REQUEST	ED CAPACITY				
ТҮРЕ	UNITS	CAPACITY (UNIT/BATCH)	LIMITATION	(UNIT/BATCH)				
MAXIMUM DESIGN (BATCHES / HOUR):								
REQUESTED LIMITATION (BATCHES / HOUR):	(BATCHES/	r(R):						
FUEL USED: N/A	TOTAL MAX	IMUM FIRING RATE (MILLION BT	U/HR): N/A					
MAX. CAPACITY HOURLY FUEL USE: N/A	REQUESTE	D CAPACITY ANNUAL FUEL USE	: N/A					
COMMENTS:								

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCI	DEQ/Division of	Air Quality - Applica	ation for Air	Permit to (Construct/C)perate		В
EMISSION SOURCE DESCRIPTION	: Crusher-Diesel	Engine		EMISSION	SOURCE	ID NO: ES-4	40B	
				CONTROL	DEVICE ID) NO(S): N/	A	
OPERATING SCENARIO	1OF	1		EMISSION	I POINT (ST	ACK) ID N	O(S): EP-4	0
DESCRIBE IN DETAILTHE EMISSIO Diesel Engine to run the Crusher.	IN SOURCE PRO	DCESS (ATTACH FL	OW DIAGRA	AM):				
TYPE OF EMISSION SO	URCE (CHECK	AND COMPLETE AP	PROPRIATI	E FORM B1	-B9 ON TH	E FOLLOW	ING PAGE	S):
Coal,wood,oil, gas, other burner (Form B1)	□ Woodworking (F	orm B4)		🗆 Manu	uf. of chemi	cals/coating	gs/inks (Form
☑ Int.combustion engine/generator ((Form B2)	Coating/finishing	/printing (Fo	orm B5)	🗌 Incin	eration (For	m B8)	
Liquid storage tanks (Form B3)		Storage silos/bin	is (Form B6)		□ Othe	r (Form B9)	1	
START CONSTRUCTION DATE: TBI	D		DATE MA	NUFACTUF	RED: TBD			
MANUFACTURER / MODEL NO.: TB	D		EXPECTE	D OP. SCH	EDULE: 36	5 hours/yea	r	
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):		
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 MAR-	MAY 25	JUN	I-AUG	25	SEP-NOV	25
CRITERIA	AIR POLLUT	TANT EMISSION	S INFORM	MATION I	OR THIS	SOURC	E	-
		SOURCE OF	EXPECTE			POTENTIA		ONS
		FMISSION	AFTER CONT				(AFTER CO	
		FACTOR	/lh/hr	tons/vr	lh/hr	tons/vr	lh/hr	tons/vr
		TROTOR	10/111	torio/yi	10/11	tor10/ y1	10/11	torio/ yr
	S(DM)							
PARTICULATE MATTER-25 MICRON	IS (PM)							
	10 (1 M _{2.5})							
					Table 45D			
			SEE AP	PENDIX B,				
	(1)(2)(2)							
	(VOC)		-					
LEAD			_					
OTHER								
HAZARDOU	IS AIR POLL	UTANT EMISSIO	NS INFOI	RMATION	IFOR IH	IS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIO	ONS
		EMISSION	AFTER CONT	ROLS / LIMITS	BEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
								Ļ
			SEE AP	PENDIX B,	Table 15B			
TOXIC A	IR POLLUTA	NT EMISSIONS	INFORMA	ATION FO	OR THIS S	SOURCE		
			EXPECTE	D ACTUAL	EMISSIONS	S AFTER C	ONTROLS	/ LIMITATION
		SOURCE OF						
TOXIC AIR POLLUTANT	CAS NO.	EMISSION FACTOR	R Ib	o/hr	lb/o	day		lb/yr
			SE		I X B. Table	15B		
					,	-		
			1		1			
		1	1		I			

MPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOUR Attach Additional Sheets As Necessary

EMISSION SOURCE (INTERNAL COMBUSTION ENGINES/TURBINES/GENERATORS)

REVISED 09/22/16	NCDEQ/Division of Air Qua	ity - Application for Air Perm	it to Construct/Ope	erate	B2
EMISSION SOURCE DESCRIPTION: 0	Crusher-Diesel Engine		EMISSION SOURC	E ID NO: ES-40B	
			CONTROL DEVICE	ID NO(S): N/A	
OPERATING SCENARIO:	1 OF 1		EMISSION POINT (STACK) ID NO(S): EP-40	
	EMERGENCY	SPACE HEAT			
	PEAK SHAVER	OTHER (DESCRIBE). To o	perate the crusher		
		PATED ACTUAL HOURS OF		YR): 365	
	///////			11().000	
			I ENGINE GREATE		
	F).		(complete b	elow)	
	N 🗌 LEAN BURN				
		RETARD D PREIG	NITION CHAMBER		ξ
OR STATIONARY GAS TURB	INE (complete below)	NATURAL GAS PIPELINE	COMPRESSOR OR	TURBINE (complete below)	
					VE
				OTHER (DESCRIBE):	
			MODIFICATIONS (DESCRIBE):	
		NSELECTIVE CATALYTIC R		SELECTIVE CATALYTIC REDU	JCTION
		EAN BURN AND PRECOMBL	JSTION CHAMBER		
	LEAN-PREMIX				
	FUEL USAGE	INCLUDE STARTUP/B	ACKUP FUEL)		
		MAXIMUM DESIGN		REQUESTED CAPACITY	
FUEL TYPE	UNITS	CAPACITY (UNIT/HF	R)	LIMITATION (UNIT/HR)	
Diesel	aallons	11 71 @ 75% load		365 br/vr	
	ganono	11.71 @ 707010dd		000 11/91	
	FUEL CHARACTERISTIC	S (COMPLETE ALL TH		CABLE)	
				SULEUR CONTENT	
FUEL TYPE	BTU/UNIT	UNITS		(% BY WEIGHT)	
Disasl	2.405.0			· · · · ·	0.00159/
Diesei	2.10E+0				0.0015%
	MANUFACTURER'S SP	ECIFIC EMISSION FAC	TORS (IF AVAIL		
POLLUTANT	NOX		PM10	VOC	OTHER
			1 1110		
DESCRIBE METHODS TO MINIMIZE \	ISIBLE EMISSIONS DURING ID	LING, OR LOW LOAD OPERA	ATIONS:		
COMMENTS:					

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCDE	Q/Division of A	Air Quality - Applic	ation for A	r Permit to	Construct/	Operate		В
EMISSION SOURCE DESCRIPTION: V	Vet Ash Receiv	ing-Transfer to She	ed	EMISSION	SOURCE I	D NO: F-1		
				CONTROL	DEVICE ID	NO(S): N/	A	
OPERATING SCENARIO1_	OF	1		EMISSION	POINT (ST	ACK) ID N	O(S): FUGI	TIVE FEP-1
DESCRIBE IN DETAILTHE EMISSION Transfer of materials to storage shed.	SOURCE PRC	OCESS (ATTACH F	LOW DIAG	RAM):				
TYPE OF EMISSION SOUR	CE (CHECK A	ND COMPLETE A	PPROPRIA	TE FORM B	1-B9 ON TH	HE FOLLO	WING PAG	ES):
Coal,wood,oil, gas, other burner (Fo	orm B1)	Woodworking	(Form B4)		🗆 Manı	uf. of chemi	icals/coating	gs/inks (Form E
Int.combustion engine/generator (For a second se	orm B2)	Coating/finish	ning/printing	(Form B5)	🗌 Incin	eration (Fo	rm B8)	
Liquid storage tanks (Form B3)		Storage silos	/bins (Form	B6)	🚽 Othe	r (Form B9))	
START CONSTRUCTION DATE: TBD			DATE MAI	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBD			EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT 🛛 N	SPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGHPL	JT (%): DEC-F	EB 25 MA	R-MAY 2	5 J	UN-AUG	25	SEP-NO	V 25
CRITERIA AI	R POLLUTA	ANT EMISSION	IS INFOR	MATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	AL EMISSIC	DNS
		EMISSION	AFTER CONT	ROLS / LIMITS)	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	(PM ₁₀)							
PARTICULATE MATTER<2.5 MICRONS	(PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE A	PPENDIX E	3, Table 8A			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS (V	/OC)							
LEAD								
OTHER								
HAZARDOUS	AIR POLLU	TANT EMISSIO	ONS INFO	ORMATIO	N FOR T	'HIS SOL	IRCE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	AL EMISSIC	DNS
		EMISSION	AFTER CONT	ROLS / LIMITS)	EFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE A	PPENDIX E	3, Table 8A			
TOXIC AIR	POLLUTAN	IT EMISSIONS	INFORM	IATION F	OR THIS	SOURC	E	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSIONS	S AFTER C	ONTROLS	/ LIMITATIONS
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lb	/hr	lb/o	day		lb/yr
			1					
			SEE AP	PENDIX B,	Table 8A			
							İ	
			1				1	
Attachments: (1) emissions calculations and s	supporting docum	nentation: (2) indicate	all requested	state and fee	leral enforcea	able permit lir	mits (e.a. hou	urs of operation.

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

 IPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOU

 Attach Additional Sheets As Necessary

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate									
EMISSION SOURCE DESCRIPTION: Wet Ash Receiving-Tra	insfer to Shed	EMISSION SOURCE ID NO: F-1							
		CONTROL DEVICE ID NO(S): N/A	A						
OPERATING SCENARIO:1 OF1	l	EMISSION POINT (STACK) ID NO	D(S): FUGITIVE FEP-1						
DESCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIA		nais to storage sneu.							
MATERIALS ENTERING PROCESS - CONTINUC	DUS PROCESS	MAX. DESIGN	REQUESTED CAPACITY						
TYPE	UNITS	CAPACITY (UNIT/HR)	LIMITATION(UNIT/HR)						
Transfer	Tons	70	70						
MATERIALS ENTERING PROCESS - BATCH	OPERATION	MAX. DESIGN	REQUESTED CAPACITY						
ТҮРЕ	UNITS	CAPACITY (UNIT/BATCH)	LIMITATION (UNIT/BATCH)						
MAXIMUM DESIGN (BATCHES / HOUR):									
REQUESTED LIMITATION (BATCHES / HOUR):	(BATCHES/	YR):							
FUEL USED: N/A	TOTAL MAX	(IMUM FIRING RATE (MILLION BTU	/HR): N/A						
MAX. CAPACITY HOURLY FUEL USE: N/A	REQUESTE	D CAPACITY ANNUAL FUEL USE: N	N/A						
COMMENTS:									

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCD	EQ/Division of	Air Quality - Applic	ation for Ai	r Permit to	Construct/0	Operate		В		
EMISSION SOURCE DESCRIPTION:	Wet Ash Receiv	ing-Transfer to Hop	per	EMISSION	SOURCE I	D NO: F-2				
				CONTROL) NO(S): N/4	4			
OPERATING SCENARIO	1 OF	1		EMISSION						
		CESS (ATTACH EI				AOR) ID NO	00).1001			
Transfer of materials to feed hopper.				,.						
TYPE OF EMISSION SOU	IRCE (CHECK A	ND COMPLETE A	PROPRIAT	E FORM B	I-B9 ON TH	E FOLLOW	/ING PAGE	S):		
Coal,wood,oil, gas, other burner (F	Form B1)	Woodworking	(Form B4)		□ Man	uf. of chemi	cals/coating	gs/inks (Form B		
☐ Int.combustion engine/generator (Form B2)	Coating/finishi	na/printina (Form B5)		eration (For	m B8)			
☐ Liquid storage tanks (Form B3)	,	Storage silos/b	oins (Form B	6)	U Othe	r (Form B9)	- /			
START CONSTRUCTION DATE: TBD)		DATE MA	NUFACTUR	ED: TBD					
MANUFACTURER / MODEL NO.: TBE)		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR		
	NSPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):				
PERCENTAGE ANNUAL THROUGHE	PUT (%): DEC-F	EB 25 MAR	-MAY 25	JU	N-AUG	25	SEP-NOV	25		
CRITERIA A	AIR POLLUT	ANT EMISSION	IS INFOR	MATION	FOR THI	S SOUR	CE	-		
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	DNS		
		EMISSION	AFTER CONT	ROLS / LIMITS	EFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)		
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr		
PARTICULATE MATTER (PM)		Ī	1							
PARTICULATE MATTER<10 MICRONS	S (PM ₁₀)									
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})									
SULFUR DIOXIDE (SO2)										
NITROGEN OXIDES (NOx)			SEE A		, Table 8B					
CARBON MONOXIDE (CO)										
VOLATILE ORGANIC COMPOUNDS	(VOC)									
LEAD										
OTHER										
HAZARDOUS	S AIR POLLU	ITANT EMISSIC	DNS INFC	RMATIO	N FOR T	HIS SOU	RCE			
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	VISSIONS		
		EMISSION	AFTER CONT	ROLS / LIMITS	TS)EFORE CONTROLS / LIMITS (AFTER CONTRO			NTROLS / LIMITS)		
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr		
			SEE A	PPENDIX E	8, Table 8B					
TOXIC AII	R POLLUTAI	NT EMISSIONS	INFORM	ATION F	OR THIS	SOURCE	-			
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER CO	ONTROLS	/ LIMITATIONS		
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lb	/hr	lb/d	day		lb/yr		
			SEE AP	PENDIX B,	Table 8B					
			+							
			1							
Attachments: (1) emissions calculations and	supporting docur	entation: (2) indicate a		state and fede	ral enforceab	le nermit limi	ts (e.a. hour	s of operation		
emission rates) and describe how these are	monitored and wit	th what frequency; and	(3) describe a	any monitoring	g devices, ga	uges, or test p	ports for this	source.		

WPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOU

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate									
EMISSION SOURCE DESCRIP	PTION: Wet	Ash Receivin	g-Transfer to Hopper	EMISSION SOURCE ID	NO: F-2				
				CONTROL DEVICE ID N	NO(S): N/A				
OPERATING SCENARIO:	1	OF	1	EMISSION POINT (STA	CK) ID NO(S): FUGITIVE	FEP-2			
		TACH FLOW							
MATERIALS ENTE		CESS - CONT		MAX. DESIGN	REQUES	STED CAPACITY			
	TYPE		UNITS	CAPACITY (UNIT/H	HR) LIMITAT	ION(UNIT/HR)			
Transfer	ansfer		Tons		70	70			
MATERIALS ENT	ERING PRO	DCESS - BA	TCH OPERATION	MAX. DESIGN	REQUES	TED CAPACITY			
	TYPE		UNITS	CAPACITY (UNIT/BA	TCH) LIMITATIO	N (UNIT/BATCH)			
			(BATCHE)	S/VR):					
		561().							
MAX CAPACITY HOURLY FU		<u> </u>							
COMMENTS:									

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCD	EQ/Division of A	ir Quality - Applic	ation for A	ir Permit to	Construct	Operate		В
EMISSION SOURCE DESCRIPTION:	Wet Ash Receive	ing-Unloading Pile		EMISSION SOURCE ID NO: F-3				
				CONTROL	DEVICE ID) NO(S): N/	A	
OPERATING SCENARIO	1 OF	1		EMISSION	POINT (ST	ACK) ID N	O(S)· FUGI	TIVE FEP-3
DESCRIBE IN DETAILTHE EMISSIO Unloading Pile Windblown Fugitive Du	N SOURCE PRO Ist Emissions.	CESS (ATTACH F	ELOW DIAG	RAM):				
TYPE OF EMISSION SOU	RCE (CHECK A	ND COMPLETE A	PPROPRIA	TE FORM B	1-B9 ON T	HE FOLLO	WING PAG	ES):
Coal,wood,oil, gas, other burner (I	Form B1)	Woodworking	g (Form B4)		🗆 Man	uf. of chemi	icals/coating	gs/inks (Form E
Int.combustion engine/generator (Form B2)	Coating/finish	ning/printing	(Form B5)	🗌 Incin	eration (Fo	rm B8)	
Liquid storage tanks (Form B3)		Storage silos	/bins (Form	B6)	🔽 Othe	er (Form B9))	
START CONSTRUCTION DATE: TBE)		DATE MA	NUFACTUR	ED: TBD			
MANUFACTURER / MODEL NO.: TBI	D		EXPECTE	D OP. SCHI	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 MA	R-MAY 2	5 J	UN-AUG	25	SEP-NO	V 25
CRITERIA A	IR POLLUTA	NT EMISSION	IS INFOR	RMATION	FOR TH	IS SOUR	RCE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	AL EMISSIC	ONS
		EMISSION	AFTER CONT	ROLS / LIMITS)	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	S (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})							
SULFUR DIOXIDE (SO2)								L
NITROGEN OXIDES (NOx)			SEE A	PPENDIX E	3, Table 10			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD								
OTHER								
HAZARDOUS	AIR POLLU	ANT EMISSIO	ONS INFO	DRMATIO	N FOR T	HIS SOL	JRCE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	AL EMISSIC	ONS
HAZARDOUS AIR POLLUTANT	CAS NO.	EMISSION FACTOR	AFTER CONT lb/hr	ROLS / LIMITS) tons/yr	BEFORE CONT	TROLS / LIMITS	(AFTER CON Ib/hr	vTROLS / LIMITS)
			SEE A		3, Table 10			
								
TOXIC AIF	R POLLUTAN	IT EMISSIONS	INFORM	IATION F	OR THIS	SOURC	E	
		SOURCE OF EMISSION	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lt	/hr	lb/	day		lb/yr
			SEE AP	PENDIX B,	Table 10			
Attachments: (1) emissions calculations and	d supporting docum	entation; (2) indicate	all requested	state and fed	leral enforce	able permit li	mits (e.g. hou	urs of operation,

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source. IPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOU

REVISED 09/22/16	NCDEQ/Divi	sion of Air Quality - Applicati	on for Air Permit to Construct/O	perate	B9
EMISSION SOURCE DESCRIPTI	ON: Wet Ash Recei	ving-Unloading Pile	EMISSION SOURCE ID NO:	F-3	
			CONTROL DEVICE ID NO(S	8): N/A	
OPERATING SCENARIO:	1 OF	1	EMISSION POINT (STACK)	ID NO(S): FUGITIVE FEP	-3
DESCRIBE IN DETAIL THE PRO	LESS (ATTACH FL	Ow Diagram): Unloading Pi	e winabiown Fugitive Dust Emissi	UNS.	
MATERIALS ENTERI	NG PROCESS - CC		MAX DESIGN	REQUESTER	
	TYPE	UNITS	CAPACITY (UNIT/HR)		(UNIT/HR)
ITPE		Acres	0.33 Acres	N/A	
		/10/00			
MATERIALS ENTER	RING PROCESS -	BATCH OPERATION	MAX. DESIGN	REQUESTE	CAPACITY
	TYPE	UNITS	CAPACITY (UNIT/BATCH	H) LIMITATION (U	NIT/BATCH)
MAXIMUM DESIGN (BATCHES /	HOUR):				
REQUESTED LIMITATION (BATC	CHES / HOUR):	(BATCHE	ES/YR):		
FUEL USED: N/A		TOTAL N	IAXIMUM FIRING RATE (MILLION	I BTU/HR): N/A	
MAX. CAPACITY HOURLY FUEL	USE: N/A	REQUES	TED CAPACITY ANNUAL FUEL U	JSE: N/A	
COMMENTS:					

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCD	EQ/Division of A	Air Quality - Applic	ation for Ai	ir Permit to	Construct/0	Operate		В
EMISSION SOURCE DESCRIPTION:	Ash Basin			EMISSION	SOURCE I	D NO: F-4		•
				CONTROL	DEVICE ID	NO(S): N/	Ą	
OPERATING SCENARIO	_1OF _	1		EMISSION	I POINT (ST	ACK) ID N	D(S): FUGI	TIVE FEP-4
DESCRIBE IN DETAILTHE EMISSIO Dust may be generated by wind erosic	N SOURCE PRO on of exposed are	CESS (ATTACH FI a within an industria	-OW DIAGF al facility.	RAM):				
TYPE OF EMISSION SOL	JRCE (CHECK A	ND COMPLETE AF	PROPRIA	re form B'	1-B9 ON TH	IE FOLLOV	VING PAGE	ES):
Coal,wood,oil, gas, other burner (F	Form B1)	Woodworking	(Form B4)		🗆 Manı	uf. of chemi	cals/coatin	gs/inks (Form E
Int.combustion engine/generator (Form B2)	Coating/finishi	ng/printing (Form B5)	🗌 Incin	eration (Fo	rm B8)	
Liquid storage tanks (Form B3)		Storage silos/b	oins (Form E	36)	🚽 Othe	er (Form B9))	
START CONSTRUCTION DATE: N/A			DATE MA	NUFACTUR	ED: N/A			
MANUFACTURER / MODEL NO.: N/A	N N		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT	NSPS (SUBPAR	rs?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 MAR	R-MAY 25	i JU	IN-AUG	25	SEP-NOV	/ 25
CRITERIA A	AIR POLLUT	ANT EMISSION	IS INFOR	RMATION	FOR THI	S SOUR	CE	
		SOURCE OF	EXPECTE	ED ACTUAL		POTENTIA	AL EMISSIC	ONS
		EMISSION	AFTER CONT	ROLS / LIMITS	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS	S (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	S (PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE /	APPENDIX B	B, Table 11			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD								
OTHER								
HAZARDOUS	S AIR POLLU	TANT EMISSIC	ONS INFO	ORMATIO	N FOR T	HIS SOU	RCE	
		SOURCE OF	EXPECTE	ED ACTUAL		POTENTIA	L EMISSIC	ONS
		EMISSION	AFTER CONT	ROLS / LIMITS	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE /	APPENDIX B	B, Table 11			
TOXIC AI	R POLLUTAN	NT EMISSIONS	INFORM	IATION F	OR THIS	SOURCI	<u> </u>	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION:
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lk	o/hr	lb/d	day		lb/yr
			SEE AP	PENDIX B,	Table 11			
			1		1			

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

 WPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOU

 Attach Additional Sheets As Necessary

REVISED 09/22/16	NCDI	EQ/Division of Air Quali	ty - Application	for Air Permit to Construct/Ope	rate	B9
EMISSION SOURCE DESCRI	PTION: Ash Ba	sin		EMISSION SOURCE ID NO: F-	4	
				CONTROL DEVICE ID NO(S): I	N/A	
OPERATING SCENARIO:	1	OF1	_	EMISSION POINT (STACK) ID	NO(S): FUGITIVE FEP-	4
DESCRIBE IN DETAIL THE P	OCESS (ATTA	CH FLOW DIAGRAM):	Dust may be ger	terated by wind erosion of expose	d area within an industri	ai taciiity.
MATERIALS ENTE		SS - CONTINUOUS PRO	CESS	MAX DESIGN	REQUESTED	
MATERIALS ENTERING PROCESS - CONTINUOUS PI TYPE ctive Basin Area			UNITS	CAPACITY (UNIT/HR)		UNIT/HR)
ctive Basin Area			Acres	321 Acres	N/A	0
MATERIALS EN	FERING PROC	ESS - BATCH OPERAT	TION	MAX. DESIGN	REQUESTED	CAPACITY
	TYPE		UNITS	CAPACITY (UNIT/BATCH)	LIMITATION (U	NIT/BATCH)
MAXIMUM DESIGN (BATCHE	S / HOUR):					
REQUESTED LIMITATION (BA	ATCHES / HOU	R):	(BATCHES/	YR):		
FUEL USED: N/A			TOTAL MAX	IMUM FIRING RATE (MILLION B	TU/HR): N/A	
MAX. CAPACITY HOURLY FU	EL USE: N/A		REQUESTE	D CAPACITY ANNUAL FUEL USE	E: N/A	
COMMENTS: Maximum ash t	nroughput = 43	U,UUU ton/yr				

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCD	EQ/Division of A	ir Quality - Applic	ation for A	ir Permit to	Construct/	Operate		В
EMISSION SOURCE DESCRIPTION:	Ash Handling			EMISSION	SOURCE I	D NO: F-5		
				CONTROL	DEVICE ID	0 NO(S): N/	Ą	
OPERATING SCENARIO	_1OF _	1		EMISSION	POINT (ST	ACK) ID NO	D(S): FUGI	TIVE FEP-4
DESCRIBE IN DETAILTHE EMISSIO Emissions from the handling of materi	N SOURCE PRO al at an industrial	CESS (ATTACH F site.	LOW DIAG	RAM):				
TYPE OF EMISSION SOU	RCE (CHECK A	ND COMPLETE A	PPROPRIA	TE FORM B	1-B9 ON TI	HE FOLLO	WING PAG	ES):
Coal,wood,oil, gas, other burner (Form B1)	U Woodworking	(Form B4)		🗆 Man	uf. of chemi	cals/coating	gs/inks (Form I
Int.combustion engine/generator (Form B2)	Coating/finish	ning/printing	(Form B5)	🗌 Incin	eration (Fo	rm B8)	
Liquid storage tanks (Form B3)		Storage silos	/bins (Form	B6)	🗸 Othe	er (Form B9))	
START CONSTRUCTION DATE: N/A			DATE MA	NUFACTUR	ED: N/A			
MANUFACTURER / MODEL NO.: N/A	A		EXPECTE	D OP. SCH	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT \Box	NSPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGH	PUT (%): DEC-F	EB 25 MA	R-MAY 2	5 J	UN-AUG	25	SEP-NO	V 25
CRITERIA A	IR POLLUTA	NT EMISSION	NS INFOR	RMATION	FOR TH	IS SOUR	CE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	DNS
		EMISSION	AFTER CONT	ROLS / LIMITS	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRON	S (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRON	IS (PM _{2.5})							
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)			SEE /		3, Table 12			
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS	(VOC)							
LEAD	× ,							
OTHER								
HAZARDOUS	AIR POLLU	TANT EMISSIO	ONS INFO	ORMATIC	N FOR T	THIS SOL	IRCE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA		ONS
		EMISSION	AFTER CONT	ROLS / LIMITS	SEFORE CONT	ROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
			SEE A		B, Table 12			
			1					1
		1						
TOXIC AII	R POLLUTAN	IT EMISSIONS	INFORM	ATION F	OR THIS	SOURC	E	
		SOURCE OF	EXPECTE	D ACTUAL	EMISSION	S AFTER C	ONTROLS	/ LIMITATION
TOXIC AIR POLLUTANT	CAS NO.	FACTOR	lk	/hr	lb/o	dav		lb/vr
						,		
			SEE AP	PENDIX B,	Table 12			
		I	1		1			

emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

 IPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOU

 Attach Additional Sheets As Necessary

REVISED 09/22/16 NCDEQ/Division of Air Quality	- Application	for Air Permit to Construct/Opera	te	B9	
EMISSION SOURCE DESCRIPTION: Ash Handling		EMISSION SOURCE ID NO: F-5			
		CONTROL DEVICE ID NO(S): N/	٩		
OPERATING SCENARIO:1 OF1		EMISSION POINT (STACK) ID NO	D(S): FUGITIVE FEP-4	ļ	
DESCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIAGRAM): Er	missions from tl	he handling of material at an industr	ial site.		
	Eee		DEQUERTED		
	LINITS		LIMITATION		
	Tong				
	10113	49.03	N/A		
MATERIALS ENTERING PROCESS - BATCH OPERATIO	ON	MAX. DESIGN	REQUESTED	CAPACITY	
ТҮРЕ	UNITS	CAPACITY (UNIT/BATCH)	LIMITATION (UN	IIT/BATCH)	
MAXIMUM DESIGN (BATCHES / HOUR):		•			
REQUESTED LIMITATION (BATCHES / HOUR):	(BATCHES/Y	′R):			
FUEL USED: N/A	TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A				
MAX. CAPACITY HOURLY FUEL USE: N/A	REQUESTED	CAPACITY ANNUAL FUEL USE:	N/A		
COMMENTS: Maximum ash throughput = 430,000 ton/yr					

SPECIFIC EMISSION SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 09/22/1 NCDEQ/I	Division of Air	Quality - Appl	ication for	Air Permit	to Constru	ct/Operate		В
EMISSION SOURCE DESCRIPTION: H	laul Roads			EMISSION	SOURCE	D NO: F-6		
				CONTROL) NO(S) [.] N//	4	
OPERATING SCENARIO 1	OF	1		FMISSION	POINT (ST) (S)· FUGI	TIVE FEP-4
DESCRIBE IN DETAILTHE EMISSION A portion of the ash will be moved by tru wheels on the road surface. This force of wheels and the road surface is exposed	SOURCE PRO ick to an offsite causes pulveriz to strong air cu	CESS (ATTAC location. Parti zation of the sur urrents, which g	H FLOW D culate emis face materi enerate airt	AGRAM): sions are ge al. The part porne partice	enerated fro ticles are liff ulate emiss	m the haul i ted and drop ions.	roads from oped from t	the force of the he rolling
	E (CHECK ANI		APPROPRI	ATE FORM	B1-B9 ON	THE FOLLO	OWING PA	GES):
└ Coal,wood,oil, gas, other burner (Fo	rm B1)		ing (Form E	34)	🗆 Man	uf. of chemi	cals/coating	gs/inks (Form B
□ Int.combustion engine/generator (Fo	orm B2)	Coating/fin	ishing/print	ing (Form B	🗌 Incin	eration (For	m B8)	
Liquid storage tanks (Form B3)		Storage si	los/bins (Fo	rm B6)	🔽 Othe	r (Form B9)		
START CONSTRUCTION DATE: N/A			DATE MAN	NUFACTUR	ED: N/A			
MANUFACTURER / MODEL NO.: N/A			EXPECTE	D OP. SCHI	EDULE: 24	HR/DAY 7	DAY/WK 5	52 WK/YR
IS THIS SOURCE SUBJECT 🛛 N	SPS (SUBPAR	TS?):			SHAP (SUB	PARTS?):_		
PERCENTAGE ANNUAL THROUGHPU	IT (%): DEC-F	EB 25 I	MAR-MAY	25	JUN-AU	G 25	SEP	-NOV 25
CRITERIA AIR	POLLUTAI	NT EMISSIO	NS INFO	RMATIO	N FOR T	HIS SOU	RCE	
		SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMISSIC	ONS
		EMISSION	AFTER CONT	ROLS / LIMITS)	BEFORE CON	FROLS / LIMITS	(AFTER CO	NTROLS / LIMITS)
AIR POLLUTANT EMITTED		FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS (PM ₁₀)							
PARTICULATE MATTER<2.5 MICRONS	(PM _{2.5})							
SULFUR DIOXIDE (SO2)		SEI		X B, Table	13B & 13C			
NITROGEN OXIDES (NOx)								
CARBON MONOXIDE (CO)								
							-	
OTHER							-	
HAZARDOUS A	IR POLLUT	ANT EMISS	IONS INF	ORMATI	ON FOR	THIS SO	URCE	
	1	SOURCE OF	EXPECTE	Ο ΔΟΤΙΙΔΙ		POTENTIA		ONS
		FMISSION	AFTER CONT		REFORE CON		(AFTER CO	
HAZARDOUS AIR POLLUTANT	CAS NO.	FACTOR	lb/hr	tons/vr	lb/hr	tons/vr	lb/hr	tons/vr
			12711	torio, yr		tono, j.		tono, yi
N/A								
	+							
		FMISSION		MATION	FOR TH	S SOUR	CE	I
						0.000/10	-	
		SOURCE OF EMISSION	EXPECTE	D ACTUAL	EMISSION	S AFTER CO	ONTROLS	/ LIMITATIONS
	CAS NO.	FACTOR	lb	/hr	lb/	day		lb/yr
N/A								
								,
Attachments: (1) emissions calculations and s operation, emission rates) and describe how the	upporting docum	entation; (2) indicated ed and with what	ate all reques	ted state and	tederal enfor	ceable permit	t limits (e.g. h pauges, or te	ours of st ports for this
source.			,, ar	(-,	. ,	J . 1.1500, g	,	

PLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SO Attach Additional Sheets As Necessary

REVISED 09/22/16 NCDEQ/Division of Air Quality	- Application f	or Air Permit to Construct/Operat	te	B9
EMISSION SOURCE DESCRIPTION: Haul Roads	, approacion i	EMISSION SOURCE ID NO: E-6		
		CONTROL DEVICE ID NO(S): N/	Δ	
		EMISSION POINT (STACK) ID N		.4
DESCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIAGRAM): A generated from the haul roads from the force of the wheels on the road su and dropped from the rolling wheels and the road surface is exposed to s	portion of the as urface. This for trong air current	sh will be moved by truck to an offs ce causes pulverization of the surfa ts, which generate airborne particul	ite location. Particula ice material. The part ate emissions.	te emissions are licles are lifted
MATERIALS ENTERING PROCESS - CONTINUOUS PROC	FSS		REQUESTER	
		CAPACITY (UNIT/HR)		
	UNITO .		Liwithtion	
MATERIALS ENTERING PROCESS - BATCH OPERATIO	ON	MAX. DESIGN	REQUESTED	CAPACITY
TYPE	UNITS	CAPACITY (UNIT/BATCH)	LIMITATION (U	NIT/BATCH)
MAXIMUM DESIGN (BATCHES / HOUR):				
REQUESTED LIMITATION (BATCHES / HOUR):	(BATCHES/Y	R):		
FUEL USED: N/A	TOTAL MAXI	MUM FIRING RATE (MILLION BTU	J/HR): N/A	
MAX. CAPACITY HOURLY FUEL USE: N/A	REQUESTED	CAPACITY ANNUAL FUEL USE:	N/A	
COMMENTS: Loaded truck weight 50 tons and unloaded truck weight 25	tons.			

FORM D1 FACILITY-WIDE EMISSIONS SUMMARY

						D1	
	AR POLLUTAN	I ENISSIONS				[
		EXPECTE	SIONS	POTENTIAL	EMISSIONS	POTENTIAL	EMISSIONS
		(AFTER CO	ONTROLS /	(BEFORE C	ONTROLS /	(AFTER C	ONTROLS /
		LIMITA	TIONS)	LIMITA	TIONS)	LIMITA	TIONS)
AIR POLLUTANT EMITTED		tons/yr		ton	s/yr	tor	is/yr
PARTICULATE MATTER (PM)		330.27		N	/A	33	0.27
PARTICULATE MATTER < 10 MICRONS (PM ₁₀)		322.27		N	/A	32	2.27
PARTICULATE MATTER < 2.5 MICRONS ($PM_{2.5}$)		322.06		N/A		32	2.06
SULFUE DIOXIDE (SO ₂)		15 183 29		N/A		15.1	83 29
		5 259 AF		N//A		5.26	59.45
		1 196 54		N/A		3,20	00.40
		1,100.54		N/A		1,10	0.34
		120.34		N/A		120	5.34
		0.771		N	/A	0.	771
GREENHOUSE GASES (GHG) (SHORT TONS)		116,604.15		N	/A	116,6	04.15
OTHER							
HAZARDOUS	AIR POLLUTA			TION - FACILI		1	
		EXPECTE		POTENTIAL	EMISSIONS	POTENTIAL	EMISSIONS
				(BEFORE C		(AFTER C	
		tons/vr		LIMITATIONS)		LIMITA	
	CAS NO.	255.20			S/yi	101	5/yi
Benzene	71-43-2	255.30		N/A		25	3.30
Formaldenyde	50-00-0	7,780.20		N/A		7,780.20	
Hexane	110-54-3	25,303.13		N/A		25,303.13	
Naphthalene	91-20-3	5.69E-03		IN/A		5.69	/E-03
Toluene	108-88-3	4,211,520.32		N/A		4,211,520.32	
Arsenic	7440-38-2	1.94E-01		N/A		0.	19
Antimony	7440-36-0	1.41E-04		N/A		1.41E-04	
Beryllium	7440-41-7	1.06E-01		N/A		0.11	
Cadmium	7440-43-9	7.14		N/A		7.14	
Chromium	7440-47-3	4.84E-03		N/A		4.84	E-03
Chromium VI	18540-29-9	112.49		N/A		11:	2.49
Cobalt	7440-48-4	1.42E-03		N/A		1.42	2E-03
Manganese	7439-96-5	11,443.34		N	/A	11,443.34	
Mercury	7439-97-6	219.79		N	/A	21	9.79
Nickel	7440-02-0	42.37		N	/A	42	
Selenium	7782-49-2	4.82E-03		N	/A	4.82	2E-03
Xylene	1330-20-7	12.68		N	/A	12	2.68
1,3-Butadiene	106-99-0	0.61		N	/A	0.	.61
Acetaldehvde	75-07-0	3.49		N	/A	3.	49
Acrolein	107-02-8	2.84		N	/A	2	.84
Total PAH (including Naphthalene)	101 02 0	2 04E-04		N	/Α	2.04	<u></u> IF-04
		EMISSIONS I	NFORMATION	- FACILITY-	NIDE	2.0	
INDICATE REQUESTED ACTUAL EMISSIONS AFTE						SION RATE (TP	ER) IN 154
NCAC 2Q .0711 MAY REQUIRE AIR DISPERSION M	ODELING. USE N	NETTING FORM	1 D2 IF NECESS	SARY.			
					Modelina	Required ?	1
TOXIC AIR POLLUTANT EMITTED	CAS NO	lb/hr lb/day		lb/vear	Yes	No	
Sulfuric Acid Mist	7664-93-9	947 13	10.781 10		x		t
Benzene	71_42_2	0.1.10		510 598 49	x		t
Formaldehyde	50-00-0	1 776 30		010,000.49	x		<u> </u>
Hevene	110 54 2	1,110.30	138 647 29		v		<u> </u>
Tolvana	110-54-3	061 534 33	11 502 642 44		~		<u> </u>
rouene	108-88-3	901,334.32	11,090,042.41	207.55	~ ~		ł
Arsenic	7440-38-2			387.55	X		<u> </u>
Beryllium	/440-41-7			212.67	X		<u> </u>
Cadmium	7440-43-9			14,274.49	X		<u> </u>
Chromium VI	18540-29-9		616.41	1	Х		1

 Cadmium
 7440-43-9
 14,274.49
 X

 Chromium VI
 18540-29-9
 616.41
 X

 Manganese
 7439-96-5
 62,703.25
 X

 Mercury
 7439-97-6
 1,204.33
 X

 Nickel
 7440-02-0
 232.17
 X

COMMENTS:

For modeling purposes toxic air pollutant facility wide emissions include emissions from the STAR facility and the Steam Electric Plant. Proposed emission rates of HAPs and TAPs that are modeled are optimized rates, proposed emission rate for all other pollutants are potential emissions. Diesel engines (ES-39B and ES-40B) were not modeled in the TPER analysis per 15A NCAC 2Q.0702 (a)(27).

AIR POLLUTANT NETTING WORKSHEET AND FACILITY-WIDE EMISSION SUMMARY

REVISED 09/22/16	NCDEQ/Division of Air Quality - A	pplication for Air Permit to Construct	/Operate D2
PURPOSE OF NETTING: AIR TO	DXICS		
TOXIC AIR POLLUTANT:	Sulfuric Acid Mist	CAS NO.: 7664-93-9	
EMISSION SOURCE ID NOS .:	ES-31, ES-10, ES-11, ES-12, ES-13, F	ES-14, ES-1A, ES-1B and ES-1C	
SECTIO	ON A - EMISSION OFFSETTIN	G ANALYSIS FOR MODIFIED/	NEW SOURCES
Summarize in this section	EMI	ISSIONS - USE APPROPRIATE COLUM	VINS ONLY
using the B forms	LB/YEAR	LB/DAY	LB/HR
MODIFICATION	NI/Δ		
INCREASE			
- MINUS -	- MINUS -	- MINUS -	- MINUS -
MODIFICATION	N/Δ		
DECREASE	ГWА		
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =
NET CHANGE	NI/Δ		
FROM MODIFICATION			
	SECTION B - FACILITY-WI	DE EMISSION NETTING ANAL	YSIS
CREDITABLE			
INCREASE			
- MINUS -	- MINUS -	- MINUS -	- MINUS -
CREDITABLE			
DECREASE			
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =
NET CREDITABLE			
CHANGE			
	SECTION C - FA	CILITY-WIDE EMISSIONS	
TOTAL FACILITY	Ν/Δ	10 781	947 13
EMISSIONS			347.13
TPER LEVELS (2Q .0711)	N/A	0.25	0.25
Are the total facility-wide emissions	s less than the TPER levels?:	YES 7] NO
If YES, no further analysis is requir	red.		
Air dispersion modeling analysis is (TPER) and the source emitting the	required if the total facility-wide emission e toxic air pollutant is not exempted by '	on level is greater than the 2Q .0711 To 15A NCAC 2Q .0702(a)(27) "Exemptions	kic Air Pollutant Permitting Emissions Rate s".
CHECK HERE IF AN AIR DISPER	SION MODELING ANALYSIS IS REQU	JIRED 🔽	
If air dispersion modeling analysis	is required, complete the stack paramet	ters section of Form D3-1 for each emiss	sion source that emits this TAP. Review the
modeling plan requirements.			

AIR POLLUTANT NETTING WORKSHEET AND FACILITY-WIDE EMISSION SUMMARY

REVISED 09/22/16	NCDEQ/Division of Air Quality - A	pplication for Air Permit to Construct/O	perate D2
PURPOSE OF NETTING: AIR TOX	ICS		
TOXIC AIR POLLUTANT: E	enzene	CAS NO.: 71-43-2	
EMISSION SOURCE ID NOS.: E	S-31, ES-10, ES-11, ES-12, ES-13, I	ES-14, ES-1A, ES-1B, ES-1C and Existing	J Aux Equip
SECTION	A - EMISSION OFFSETTIN	G ANALYSIS FOR MODIFIED/NE	EW SOURCES
Summarize in this section	EMI	ISSIONS - USE APPROPRIATE COLUMN	IS ONLY
using the B forms	LB/YEAR	LB/DAY	LB/HR
MODIFICATION		N/A	NI/A
INCREASE		N/A	N/A
- MINUS -	- MINUS -	- MINUS -	- MINUS -
MODIFICATION		N/A	NI/A
DECREASE		N/A	IV/A
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =
NET CHANGE		N/A	NI/A
FROM MODIFICATION		N/A	IN/A
	SECTION B - FACILITY-WI	DE EMISSION NETTING ANALY	SIS
CREDITABLE			
INCREASE			
- MINUS -	- MINUS -	- MINUS -	- MINUS -
CREDITABLE			
DECREASE			
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =
NET CREDITABLE			
CHANGE			
	SECTION C - FA	CILITY-WIDE EMISSIONS	
TOTAL FACILITY	E10 E09	N//A	NI/A
EMISSIONS	510,596	N/A	N/A
TPER LEVELS (2Q .0711)	8.1	N/A	N/A
Are the total facility-wide emissions le	ess than the TPER levels?:	YES 🗸	NO
If YES, no further analysis is required	ł.		
Air dispersion modeling analysis is re (TPER) and the source emitting the t	equired if the total facility-wide emissic oxic air pollutant is not exempted by	on level is greater than the 2Q .0711 Toxic 15A NCAC 2Q .0702(a)(27) "Exemptions".	Air Pollutant Permitting Emissions Rate
CHECK HERE IF AN AIR DISPERSI	ON MODELING ANALYSIS IS REQU	JIRED 🗹	
If air dispersion modeling analysis is	required, complete the stack paramet	ters section of Form D3-1 for each emissio	n source that emits this TAP. Review the
modeling plan requirements.			
COMMENTS.			

AIR POLLUTANT NETTING WORKSHEET AND FACILITY-WIDE EMISSION SUMMARY

REVISED 09/22/16	NCDEQ/Division of Air Quality - Ap	oplication for Air Permit to Construct	t/Operate D2
PURPOSE OF NETTING: AIR TO	XICS		
TOXIC AIR POLLUTANT:	Formaldehyde	CAS NO.: 50-00-0	
EMISSION SOURCE ID NOS .:	ES-31, ES-10, ES-11, ES-12, ES-13, E	ES-14, ES-1A, ES-1B, ES-1C and Exist	ing Aux Equip
SECTIO	NA - EMISSION OFFSETTING	GANALYSIS FOR MODIFIED/I	NEW SOURCES
Summarize in this section	EMIS	SSIONS - USE APPROPRIATE COLUI	MNS ONLY
using the B forms	LB/YEAR	LB/DAY	LB/HR
MODIFICATION	N/A	N/A	
INCREASE			
- MINUS -	- MINUS -	- MINUS -	- MINUS -
MODIFICATION	 N/A	N/A	
DECREASE			
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =
NET CHANGE		Ν/Δ	
FROM MODIFICATION			
	SECTION B - FACILITY-WI	DE EMISSION NETTING ANAL	YSIS
CREDITABLE			
INCREASE			
- MINUS -	- MINUS -	- MINUS -	- MINUS -
CREDITABLE		1	
DECREASE			
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =
NET CREDITABLE			
CHANGE			
	SECTION C - FAC	CILITY-WIDE EMISSIONS	
TOTAL FACILITY	N/Δ	Ν/Δ	1776 30
EMISSIONS			1770.30
TPER LEVELS (2Q .0711)	N/A	N/A	0.04
Are the total facility-wide emissions	s less than the TPER levels?:	YES 2	/] NO
If YES, no further analysis is requir	red.		
Air dispersion modeling analysis is (TPER) and the source emitting the	required if the total facility-wide emission e toxic air pollutant is not exempted by 1	n level is greater than the 2Q .0711 To: 5A NCAC 2Q .0702(a)(27) "Exemption	xic Air Pollutant Permitting Emissions Rate s".
CHECK HERE IF AN AIR DISPER	SION MODELING ANALYSIS IS REQU	IRED 🗹	
If air dispersion modeling analysis i modeling plan requirements.	s required, complete the stack parameter	ers section of Form D3-1 for each emiss	sion source that emits this TAP. Review the
COMMENTS:			

AIR POLLUTANT NETTING WORKSHEET AND FACILITY-WIDE EMISSION SUMMARY

Summarize in this section LB/YEAR LB/DAY LB/HR MODIFICATION N/A N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - N/A N/A - MINUS - - MINUS - N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - N/A N/A - MINUS - - MODIFICATION N/A N/A - MINUS -				
TOXIC AIR POLLUTANT: Hexane CAS NO.: 110-54-3 EMISSION SOURCE ID NOS.: ES-31, ES-1A, ES-1B, ES-1C and Existing Aux Equip Section A - EMISSION OFFSETTING ANALYSIS FOR MODIFIED/NEW SOURCES Summarize in this section EMISSIONS - USE APPROPRIATE COLUMNS ONLY using the B forms LB/YEAR LB/DAY LB/HR MODIFICATION N/A N/A N/A INCREASE - MINUS - - MINUS - - MINUS - MODIFICATION N/A N/A - MINUS - MODIFICATION N/A N/A - MINUS - MODIFICATION N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - = EQUALS = = EQUALS = = EQUALS = = EQUALS =				
EMISSION SOURCE ID NOS.: ES-31, ES-1A, ES-1B, ES-1C and Existing Aux Equip SECTION A - EMISSION OFFSETTING ANALYSIS FOR MODIFIED/NEW SOURCES Summarize in this section EMISSIONS - USE APPROPRIATE COLUMNS ONLY using the B forms LB/YEAR LB/DAY LB/HR MODIFICATION N/A N/A N/A INCREASE - MINUS - - MINUS - - MINUS - MODIFICATION N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - MODIFICATION N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - - MODIFICATION N/A N/A N/A - MINUS - = EQUALS = = EQUALS = = EQUALS = = EQUALS = = EQUALS =				
SECTION A - EMISSION OFFSETTING ANALYSIS FOR MODIFIED/NEW SOURCES Summarize in this section EMISSIONS - USE APPROPRIATE COLUMNS ONLY using the B forms LB/YEAR LB/DAY LB/HR MODIFICATION N/A N/A N/A INCREASE - MINUS - - MINUS - - MINUS - MODIFICATION N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - MODIFICATION N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - - MODIFICATION N/A N/A N/A - MINUS -				
Summarize in this section using the B forms EMISSIONS - USE APPROPRIATE COLUMNS ONLY MODIFICATION INCREASE LB/YEAR LB/DAY LB/HR - MINUS - N/A N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - MODIFICATION INCREASE N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - MODIFICATION DECREASE N/A N/A N/A				
using the B forms LB/YEAR LB/DAY LB/HR MODIFICATION N/A N/A N/A INCREASE - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - MODIFICATION N/A N/A - MINUS - DECREASE = FQUALS = = FQUALS = - FQUALS =				
MODIFICATION INCREASE N/A N/A - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - - MINUS - MODIFICATION DECREASE N/A N/A				
INCREASE INCR - MINUS - - MINUS - MODIFICATION N/A DECREASE - FOULALS =				
- MINUS - - MINUS - - MINUS - MODIFICATION DECREASE N/A N/A				
MODIFICATION N/A DECREASE = FOUALS =				
DECREASE = FOULLIS = FOULLIS = FOULLIS = FOULLIS =				
NET CHANGE N/A N/A				
FROM MODIFICATION				
SECTION B - FACILITY-WIDE EMISSION NETTING ANALYSIS				
CREDITABLE				
INCREASE				
- MINUS MINUS MINUS MINUS -				
CREDITABLE				
DECREASE				
= EQUALS = = EQUALS = = EQUALS = = EQUALS =				
NET CREDITABLE				
CHANGE				
SECTION C - FACILITY-WIDE EMISSIONS				
TOTAL FACILITY N/A 138,647 N/A				
IPER LEVELS (2Q.0/11) N/A 23 N/A				
Are the total facility-wide emissions less than the TPER levels ?:				
If YES, no further analysis is required. Air dispersion modeling analysis is required if the total facility-wide emission level is greater than the 20, 0711 Toxic Air Pollutant Permitting Emissions Rate				
(TPER) and the source emitting the toxic air pollutant is not exempted by 15A NCAC 2Q .0702(a)(27) "Exemptions".				
CHECK HERE IF AN AIR DISPERSION MODELING ANALYSIS IS REQUIRED				
If air dispersion modeling analysis is required, complete the stack parameters section of Form D3-1 for each emission source that emits this TAP. Review the				
COMMENTS:				

AIR POLLUTANT NETTING WORKSHEET AND FACILITY-WIDE EMISSION SUMMARY

REVISED 09/22/16	NCDEQ/Division of Air Quality - A	pplication for Air Permit to Construct/C)perate D2
PURPOSE OF NETTING: AIR TO)XICS		
TOXIC AIR POLLUTANT:	Toluene	CAS NO.: 108-88-3	
EMISSION SOURCE ID NOS .:	ES-31, ES-10, ES-11, ES-12, ES-13, E	ES-14, ES-1A, ES-1B, ES-1C and Existing	g Aux Equip
SECTIO	ON A - EMISSION OFFSETTING	G ANALYSIS FOR MODIFIED/N	EW SOURCES
Summarize in this section	EMI	ISSIONS - USE APPROPRIATE COLUM	NS ONLY
using the B forms	LB/YEAR	LB/DAY	LB/HR
MODIFICATION	ΝI/Δ	N/A	
INCREASE			
- MINUS -	- MINUS -	- MINUS -	- MINUS -
MODIFICATION	N/A	N/A	
DECREASE	1973	19/7 \	
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =
NET CHANGE	N/A		
FROM MODIFICATION	1973		
	SECTION B - FACILITY-WI	DE EMISSION NETTING ANALY	'SIS
CREDITABLE			
INCREASE			
- MINUS -	- MINUS -	- MINUS -	- MINUS -
CREDITABLE		T	T
DECREASE			
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =
NET CREDITABLE		T	T
CHANGE			
	SECTION C - FA	CILITY-WIDE EMISSIONS	
TOTAL FACILITY	N/A	11.593.642	961.534
EMISSIONS		,	
TPER LEVELS (2Q .0711)	N/A	98	14.4
Are the total facility-wide emissions	s less than the TPER levels?:	YES 🗹	NO
If YES, no further analysis is requir	ed.		
Air dispersion modeling analysis is (TPER) and the source emitting the	required if the total facility-wide emissio e toxic air pollutant is not exempted by 1	on level is greater than the 2Q .0711 Toxic 15A NCAC 2Q .0702(a)(27) "Exemptions".	; Air Pollutant Permitting Emissions Rate
CHECK HERE IF AN AIR DISPER	SION MODELING ANALYSIS IS REQU	JIRED 🔽	
If air dispersion modeling analysis i	is required, complete the stack paramet	ters section of Form D3-1 for each emission	on source that emits this TAP. Review the
COMMENTS:			

REVISED 09/22/16	ED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate D2			D2
PURPOSE OF NETTING: AIR TO	XICS			
TOXIC AIR POLLUTANT:	Arsenic	CAS NO.: 7440-38-2		
EMISSION SOURCE ID NOS .:	ES-30A, ES-30B, ES-31, ES-34, ES-3 F-2, F-3, F-4, F-5, ES-10, ES-11, ES-	35, ES-36A, ES-36B, ES-37A, ES-37B, ES -12, ES-13, ES-14, ES-1A, ES-1B, ES-1C a	-38, ES-38A, ES-38B, ES-39A, ES and Existing Aux Equip	S-40A, F-1,
SECT	FION A - EMISSION OFFSETTI	NG ANALYSIS FOR MODIFIED/N	EW SOURCES	
Summarize in this section	E	MISSIONS - USE APPROPRIATE COLUM	INS ONLY	
using the B forms	LB/YEAR	LB/DAY	LB/HR	
MODIFICATION		NI/A	N//A	
INCREASE		IN/A	IN/A	
- MINUS -	- MINUS -	- MINUS -	- MINUS -	
MODIFICATION		NI/A	NI/A	
DECREASE		IN/A	IN/A	
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	
NET CHANGE		NI/A	NI/A	
FROM MODIFICATION		IN/A	IN/A	
	SECTION B - FACILITY-	WIDE EMISSION NETTING ANAL	YSIS	
CREDITABLE				
INCREASE				
- MINUS -	- MINUS -	- MINUS -	- MINUS -	
CREDITABLE				
DECREASE				
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	
NET CREDITABLE				
CHANGE				
	SECTION C - F	ACILITY-WIDE EMISSIONS		
TOTAL FACILITY	207 55	N1/A	N1/A	
EMISSIONS	387.55	N/A	N/A	
TPER LEVELS (2Q .0711)	0.053	N/A	N/A	
Are the total facility-wide emission	ns less than the TPER levels?:	YES 🗹	NO	
If YES, no further analysis is requ	ired.			
Air dispersion modeling analysis i (TPER) and the source emitting the	s required if the total facility-wide emiss ne toxic air pollutant is not exempted by	sion level is greater than the 2Q .0711 Toxi / 15A NCAC 2Q .0702(a)(27) "Exemptions'	c Air Pollutant Permitting Emissior	ns Rate
CHECK HERE IF AN AIR DISPER	RSION MODELING ANALYSIS IS REQ	UIRED 🗹		
If air dispersion modeling analysis	s is required, complete the stack param	eters section of Form D3-1 for each emiss	ion source that emits this TAP. Re	eview the
modeling plan requirements.				
COMMENTS.				

AIR POLLUTANT NETTING WORKSHEET AND FACILITY-WIDE EMISSION SUMMARY

REVISED 09/22/16	NCDEQ/Division of Air Quality -	Application for Air Permit to Construe	ct/Operate	D2	
PURPOSE OF NETTING: AIR TO	OXICS				
TOXIC AIR POLLUTANT:	Beryllium	CAS NO.: 7440-41-7			
EMISSION SOURCE ID NOS.:	ES-30A, ES-30B, ES-31, ES-34, ES- F-2, F-3, F-4, F-5, ES-10, ES-11, ES	-35, ES-36A, ES-36B, ES-37A, ES-37B, -12, ES-13, ES-14, ES-1A, ES-1B, ES-	, ES-38, ES-38A, ES-38B, ES-39A 1C and Existing Aux Equip	, ES-40A, F-1,	
SEC	TION A - EMISSION OFFSETT	ING ANALYSIS FOR MODIFIE	D/NEW SOURCES		
Summarize in this section		EMISSIONS - USE APPROPRIATE CO	LUMNS ONLY		
using the B forms	LB/YEAR	LB/DAY	LB/HR		
MODIFICATION		N//A	NI/A		
INCREASE		N/A	IN/A		
- MINUS -	- MINUS -	- MINUS -	- MINUS -		
MODIFICATION		N/A	N/A		
DECREASE		N/A	IN/A		
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	:	
NET CHANGE		N/A	NI/A		
FROM MODIFICATION		N/A	IN/A		
SECTION B - FACILITY-WIDE EMISSION NETTING ANALYSIS					
CREDITABLE					
INCREASE					
- MINUS -	- MINUS -	- MINUS -	- MINUS -		
CREDITABLE					
DECREASE					
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	:	
NET CREDITABLE					
CHANGE					
	SECTION C - I	FACILITY-WIDE EMISSIONS			
TOTAL FACILITY	212.67	N/A	N/A		
EMISSIONS	212.01	1077	14/74		
TPER LEVELS (2Q .0711)	0.28	N/A	N/A		
Are the total facility-wide emission	ns less than the TPER levels?:	YES [NO NO		
If YES, no further analysis is requ	ired.				
Air dispersion modeling analysis i (TPER) and the source emitting the	is required if the total facility-wide emis he toxic air pollutant is not exempted by	sion level is greater than the 2Q .0711 y 15A NCAC 2Q .0702(a)(27) "Exempti	Toxic Air Pollutant Permitting Emis ons".	sions Rate	
CHECK HERE IF AN AIR DISPER	RSION MODELING ANALYSIS IS REC	QUIRED 🗹			
If air dispersion modeling analysis modeling plan requirements.	s is required, complete the stack paran	neters section of Form D3-1 for each er	nission source that emits this TAP.	Review the	
COMMENTS:					

AIR POLLUTANT NETTING WORKSHEET AND FACILITY-WIDE EMISSION SUMMARY				
REVISED 09/22/16	NCDEQ/Division of Air Quality - App	blication for Air Permit to Construct/Op	Derate D2	
PURPOSE OF NETTING: AIR TO	DXICS			
TOXIC AIR POLLUTANT:	Cadmium	CAS NO.: 7440-43-9		
EMISSION SOURCE ID NOS.:	ES-30A, ES-30B, ES-31, ES-34, ES-35, F-2, F-3, F-4, F-5, ES-10, ES-11, ES-12	ES-36A, ES-36B, ES-37A, ES-37B, ES- , ES-13, ES-14, ES-1A, ES-1B, ES-1C a	38, ES-38A, ES-38B, ES-39A, ES-40A, F-1, nd Existing Aux Equip	
SECT	TION A - EMISSION OFFSETTING	G ANALYSIS FOR MODIFIED/N	EW SOURCES	
Summarize in this section	EMI	SSIONS - USE APPROPRIATE COLUM	NS ONLY	
using the B forms	LB/YEAR	LB/DAY	LB/HR	
MODIFICATION		N/A	N/A	
INCREASE		N/A	17/2	
- MINUS -	- MINUS -	- MINUS -	- MINUS -	
MODIFICATION		N/A	N/A	
DECREASE				
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	
NET CHANGE		N/A	N/A	
FROM MODIFICATION			1.971	
SECTION B - FACILITY-WIDE EMISSION NETTING ANALYSIS				
CREDITABLE				
INCREASE				
- MINUS -	- MINUS -	- MINUS -	- MINUS -	
CREDITABLE				
DECREASE				
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	
NET CREDITABLE				
CHANGE				
	SECTION C - FA	CILITY-WIDE EMISSIONS		
TOTAL FACILITY	14,274,49	N/A	N/A	
EMISSIONS				
TPER LEVELS (2Q .0711)	0.37	N/A	N/A	
Are the total facility-wide emission	ns less than the TPER levels?:	🗆 YES 🗹	NO	
If YES, no further analysis is requ	ired.			
Air dispersion modeling analysis i (TPER) and the source emitting the	s required if the total facility-wide emission ne toxic air pollutant is not exempted by 15	n level is greater than the 2Q .0711 Toxic 5A NCAC 2Q .0702(a)(27) "Exemptions".	c Air Pollutant Permitting Emissions Rate	
CHECK HERE IF AN AIR DISPERSION MODELING ANALYSIS IS REQUIRED				
If air dispersion modeling analysis modeling plan requirements.	s is required, complete the stack paramete	ers section of Form D3-1 for each emission	on source that emits this TAP. Review the	
ICOMMENTS:				

AIR POLLUTANT NETTING WORKSHEET AND FACILITY-WIDE EMISSION SUMMARY

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate											
PURPOSE OF NETTING: AIR TO	DXICS										
TOXIC AIR POLLUTANT:	Chromium VI	CAS NO.: 18540-29-9									
EMISSION SOURCE ID NOS.:	ES-30A, ES-30B, ES-31, ES-34, ES 2, F-3, F-4, F-5, ES-10, ES-11, ES-1	3-35, ES-36A, ES-36B, ES-37A, ES-37B, ES- 12, ES-13, ES-14, ES-1A, ES-1B, ES-1C and	38, ES-38A, ES-38B, ES-39A, Existing Aux Equip	ES-40A, F-1, F-							
SECT	TION A - EMISSION OFFSET	TING ANALYSIS FOR MODIFIED/N	EW SOURCES								
Summarize in this section		EMISSIONS - USE APPROPRIATE COLUM	NS ONLY								
using the B forms	LB/YEAR	LB/DAY	LB/HR								
MODIFICATION	N/A		N/A								
INCREASE											
- MINUS -	- MINUS -	- MINUS -	- MINUS -								
MODIFICATION	N/A		N/A								
DECREASE											
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =								
NET CHANGE	N/A		N/A								
FROM MODIFICATION											
	SECTION B - FACILITY	-WIDE EMISSION NETTING ANAL	(SIS								
CREDITABLE											
INCREASE											
- MINUS -	- MINUS -	- MINUS -	- MINUS -								
CREDITABLE											
DECREASE											
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =								
NET CREDITABLE											
CHANGE											
	SECTION C -	FACILITY-WIDE EMISSIONS	-								
TOTAL FACILITY EMISSIONS	N/A	616.410	N/A								
TPER LEVELS (2Q .0711)	N/A	0.013	N/A								
Are the total facility-wide emission	is less than the TPER levels?:	YES 🗹	NO								
If YES, no further analysis is requi	ired.										
Air dispersion modeling analysis is (TPER) and the source emitting the	s required if the total facility-wide emis	ssion level is greater than the 2Q .0711 Toxic by 15A NCAC 2Q .0702(a)(27) "Exemptions".	Air Pollutant Permitting Emiss	sions Rate							
CHECK HERE IF AN AIR DISPER	RSION MODELING ANALYSIS IS REC	QUIRED 🔽									
If air dispersion modeling analysis	s is required, complete the stack parar	meters section of Form D3-1 for each emission	on source that emits this TAP.	Review the							
COMMENTS:											

REVISED 09/22/16	NCDEQ/Division of Air Quality - A	opplication for Air Permit to Construct/	Operate	D2
PURPOSE OF NETTING: AIR TO	OXICS			
TOXIC AIR POLLUTANT:	Manganese	CAS NO.: 7439-96-5		
	ES-30A, ES-30B, ES-31, ES-34, ES-3 E 2 E 3 E 4 E 5 ES 10 ES 11 ES	35, ES-36A, ES-36B, ES-37A, ES-37B, E	S-38, ES-38A, ES-38B, ES-39A	, ES-40A, F-1,
EMISSION SOURCE ID NOS.:		NC ANALYSIS FOR MODIFIED/		
SEC		NG ANAL ISIS FOR MODIFIED	NEW SOURCES	
Summarize in this section	E LEN/EAD	MISSIONS - USE APPROPRIATE COLU	MNS ONLY	
	LB/YEAR	LB/DAY	LB/HR	
MODIFICATION	N/A		N/A	
INCREASE		MINUIC	MINULO	
- MINUS -	- MINUS -	- MINUS -	- MINUS -	
MODIFICATION	N/A		N/A	
DECREASE		50000		
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	
NET CHANGE	N/A		N/A	
FROM MODIFICATION			Vala	
	SECTION B - FACILITY-V	VIDE EMISSION NETTING ANAI	YSIS	
CREDITABLE				
INCREASE				
- MINUS -	- MINUS -	- MINUS -	- MINUS -	
CREDITABLE				
DECREASE				
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	-
NET CREDITABLE				
CHANGE				
	SECTION C - F	ACILITY-WIDE EMISSIONS		
TOTAL FACILITY	N/A	62 703 249	N/A	
EMISSIONS	10/1	02,100.210	10/7	
TPER LEVELS (2Q .0711)	N/A	0.63	N/A	
Are the total facility-wide emission	ns less than the TPER levels?:	Tes I	NO	
If YES, no further analysis is requ	iired.			
Air dispersion modeling analysis	is required if the total facility-wide emiss	sion level is greater than the 2Q .0711 To	xic Air Pollutant Permitting Emis	sions Rate
		TSA NCAC 2Q :0702(a)(27) Exemptions	ð.	
If air dispersion modeling analysis	s is required, complete the stack param	eters section of Form D3-1 for each emis	sion source that emits this TAP	Review the
modeling plan requirements.				
COMMENTS:				
L				

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate												
PURPOSE OF NETTING: AIR TO	DXICS											
TOXIC AIR POLLUTANT:	Mercury	CAS NO.: 7439-97-6										
EMISSION SOURCE ID NOS.:	ES-30A, ES-30B, ES-31, ES-34, ES-3 F-2, F-3, F-4, F-5, ES-10, ES-11, ES-	35, ES-36A, ES-36B, ES-37A, ES-37B, E 12, ES-13, ES-14, ES-1A, ES-1B, ES-1C	S-38, ES-38A, ES-38B, ES-39A and Existing Aux Equip	, ES-40A, F-1,								
SECT	ION A - EMISSION OFFSETTI	NG ANALYSIS FOR MODIFIED	NEW SOURCES									
Summarize in this section	E	MISSIONS - USE APPROPRIATE COLL	JMNS ONLY									
using the B forms	LB/YEAR	LB/DAY	LB/HR									
MODIFICATION	N/A		N/A									
INCREASE	11/2		10/74									
- MINUS -	- MINUS -	- MINUS -	- MINUS -									
MODIFICATION	N/A		N/A									
DECREASE	11/2		N/A									
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	=								
NET CHANGE	N/A		N/A									
FROM MODIFICATION	11/2		N/A									
	SECTION B - FACILITY-V	VIDE EMISSION NETTING ANA	LYSIS									
CREDITABLE												
INCREASE												
- MINUS -	- MINUS -	- MINUS -	- MINUS -									
CREDITABLE												
DECREASE												
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS =	=								
NET CREDITABLE												
CHANGE												
	SECTION C - F	ACILITY-WIDE EMISSIONS										
TOTAL FACILITY	N/A	1 204 327	N/A									
EMISSIONS		1,204.021	10/74									
TPER LEVELS (2Q .0711)	N/A	0.0013	N/A									
Are the total facility-wide emission	is less than the TPER levels?:	🗆 YES 🗹	NO									
If YES, no further analysis is requi	ired.											
Air dispersion modeling analysis is (TPER) and the source emitting the	s required if the total facility-wide emiss ne toxic air pollutant is not exempted by	sion level is greater than the 2Q .0711 To 15A NCAC 2Q .0702(a)(27) "Exemption	oxic Air Pollutant Permitting Emis s".	sions Rate								
CHECK HERE IF AN AIR DISPER	SION MODELING ANALYSIS IS REQ	UIRED 🔽										
If air dispersion modeling analysis	is required, complete the stack parameters	eters section of Form D3-1 for each emis	ssion source that emits this TAP	. Review the								
COMMENTS:												
L												

REVISED 09/22/16 NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate D2												
PURPOSE OF NETTING: AIR T	OXICS											
TOXIC AIR POLLUTANT:	Nickel	CAS NO.: 7440-02-0										
EMISSION SOURCE ID NOS.:	ES-30A, ES-30B, ES-31, ES-34, ES-3 2, F-3, F-4, F-5, ES-10, ES-11, ES-12	35, ES-36A, ES-36B, ES-37A, ES-37B, E 2, ES-13, ES-14, ES-1A, ES-1B, ES-1C a	S-38, ES-38A, ES-38B, ES-39A nd Existing Aux Equip	A, ES-40A, F-1, F								
SEC	TION A - EMISSION OFFSETTI	NG ANALYSIS FOR MODIFIED/	NEW SOURCES									
Summarize in this section	E	MISSIONS - USE APPROPRIATE COLL	IMNS ONLY									
using the B forms	LB/YEAR	LB/DAY	LB/HR									
MODIFICATION	N/A		N/A									
INCREASE												
- MINUS -	- MINUS -	- MINUS -	- MINUS -									
MODIFICATION	N/A		N/A									
DECREASE			N// X									
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS	=								
NET CHANGE	N/A		N/A									
FROM MODIFICATION	IN/A		N/A									
	SECTION B - FACILITY-V	VIDE EMISSION NETTING ANA	LYSIS									
CREDITABLE												
INCREASE												
- MINUS -	- MINUS -	- MINUS -	- MINUS -									
CREDITABLE												
DECREASE												
= EQUALS =	= EQUALS =	= EQUALS =	= EQUALS	=								
NET CREDITABLE												
CHANGE												
	SECTION C - F	ACILITY-WIDE EMISSIONS										
TOTAL FACILITY	N1/A	000.470	N1/A									
EMISSIONS	N/A	232.172	N/A									
TPER LEVELS (2Q .0711)	N/A	0.13	N/A									
Are the total facility-wide emission	ns less than the TPER levels?:	YES 🗹	NO									
If YES, no further analysis is requ	uired.											
Air dispersion modeling analysis (TPER) and the source emitting t	is required if the total facility-wide emiss he toxic air pollutant is not exempted by	sion level is greater than the 2Q .0711 To 15A NCAC 2Q .0702(a)(27) "Exemption:	xic Air Pollutant Permitting Emis s".	ssions Rate								
CHECK HERE IF AN AIR DISPE	RSION MODELING ANALYSIS IS REQ	UIRED 🗹										
If air dispersion modeling analysi	s is required, complete the stack parame	eters section of Form D3-1 for each emis	sion source that emits this TAP	. Review the								
modeling plan requirements.												
COMMENTS:												
	Attack Additio	nal Chasta As Nasaaani										

FORM D5 TECHNICAL ANALYSIS TO SUPPORT PERMIT APPLICATION

RE	VISED 09/22/16	NCDEQ/Division of Air Quality	- Application for Air Permit to Construct/Operate	D5
	PROV	IDE DETAILED TECHNICAL CALCUL	TIONS TO SUPPORT ALL EMISSION, CONTRO)L, AND REGULATORY
	DEMON	NECESSARY TO SUPPORT AND C	ARIEY CALCULATIONS AND ASSUMPTIONS	ADDRESS THE
		FOLLOWING	PECIFIC ISSUES ON SEPARATE PAGES:	
•				
A	SPECIFIC EMISSION FACTORS, MATERIA	S SOURCE (EMISSION INFORMATION) (L BALANCES, AND/OR OTHER METHOD	FROM WHICH THE POLLUTANT EMISSION RATES	S USED, INCLUDING EMISSION IN THIS APPLICATION WERE DERIVED.
	INCLUDE CALCULAT	ION OF POTENTIAL BEFORE AND, WHE	LE APPLICABLE, AFTER CONTROLS. CLEARLY STA	TE ANY ASSUMPTIONS MADE AND
	PROVIDE ANY REFE	RENCES AS NEEDED TO SUPPORT MA	-RIAL BALANCE CALCULATIONS.	
в	SPECIFIC EMISSION	SOURCE (REGULATORY INFORMATIO)(FORM E2 - TITLE V ONLY) - PROVIDE AN ANALYS	S OF ANY REGULATIONS APPLICABLE
	TO INDIVIDUAL SOU	RCES AND THE FACILITY AS A WHOLE.	INCLUDE A DISCUSSION OUTING METHODS (e.g. F	OR TESTING AND/OR MONITORING
	PROCESS RATES OF	R COMPLYING WITH APPLICABLE REG R OTHER OPERATIONAL PARAMETERS.	PROVIDE JUSTIFICATION FOR AVOIDANCE OF AN	FEDERAL REGULATIONS
	(PREVENTION OF SI	GNIFICANT DETERIORATION (PSD), NE	SOURCE PERFORMANCE STANDARDS (NSPS), N/	TIONAL EMISSION STANDARDS FOR
	APPLICABLE TO THI	S FACILITY, SUBMIT ANY REQUIRED IN	ORMATION TO DOCUMENT COMPLIANCE WITH AN	ONS WHICH WOULD OTHERWISE BE IY REGULATIONS. INCLUDE EMISSION
1	RATES CALCULATED	D IN ITEM "A" ABOVE, DATES OF MANUF	CTURE, CONTROL EQUIPMENT, ETC. TO SUPPOR	T THESE CALCULATIONS.
<u>_</u>		NALYON (FORM Cland of the such ON)		
	CONTROL DEVICE A	CIES LISTED ON SECTION C FORMS, OI	USED TO REDUCE EMISSION RATES IN CALCULAT	TIONS UNDER ITEM "A" ABOVE. INCLUDE
				, AND PARAMETERS AS APPLIED FOR IN
	POTENTIAL FOR THE	E PARTICULAR CONTROL DEVICES AS I	MPLOYED AT THIS FACILITY. DETAIL PROCEDURE	S FOR ASSURING PROPER OPERATION
	OF THE CONTROL D	EVICE INCLUDING MONITORING SYSTE	IS AND MAINTENANCE TO BE PERFORMED.	
_				
U	PROCESS AND OPE PROCESS, OPERATI	ONAL, OR OTHER DATA TO DEMONSTR	ATE COMPLIANCE. REFER TO COMPLIANCE REQUI	REMENTS IN THE REGULATORY
	ANALYSIS IN ITEM "	B" WHERE APPROPRIATE. LIST ANY CO	NDITIONS OR PARAMETERS THAT CAN BE MONITO	RED AND REPORTED TO
	DEMONSTRATE COM	IPLIANCE WITH THE APPLICABLE REGI	LATIONS.	
Е	PROFESSIONAL ENG	GINEERING SEAL - PURSUANT T	0 15A NCAC 2Q .0112 "APPLICATION REQUIRING A	PROFESSIONAL ENGINEERING SEAL,"
	A PROFESSIONAL E	NGINEER REGISTERED IN NORTH CAR	LINA SHALL BE REQUIRED TO SEAL TECHNICAL P	ORTIONS OF THIS APPLICATION FOR
	NEW SOURCES AND	MODIFICATIONS OF EXISTING SOURC	S. (SEE INSTRUCTIONS FOR FURTHER APPLICAB	ILIIY).
	<i>I</i> ,	Thomas O. Pritcher at	est that this application forDuke Energy Progress	, LLC - H.F. Lee Steam Electric Plant
		has been revi	wed by me and is accurate, complete and consistent wi	th the information supplied
	in the engineering pla proposed design con	ns , calculations, and all other supporting o cent has been prepared in accordance w	cumentation to the best of my knowledge. I further atte h the applicable regulations Although certain portions	st that to the best of my knowledge the of this submittal package may have been
	developed by other pr	ofessionals, inclusion of these materials ur	ler my seal signifies that I have reviewed this material a	nd have judged it to be consistent with the
	proposed design con	cept . Note: In accordance with NC Gene	al Statutes 143-215.6A and 143-215.6B, any person wi	no knowingly makes any false statement,
	up to \$25,000 per viol	ation.		exceed \$10,000 as well as civil periallies
	(PLEASE USE BLUE	INK TO COMPLETE THE FOLLOWING)	PLACE NORTH	I CAROLINA SEAL HERE
	NAME:			
	DATE:			
	COMPANY:	Environmental Consulting & Technology	⁵ North Ca	
	ADDRESS:	7208 Falls of Neuse Road, Suite 102, Ra	igh, NC	
	TELEPHONE:	919-861-8888		
	SIGNATURE:			
	PAGES CERTIFIED:	Appendix A & Appendix B		
	(10	ENTIFY ABOVE EACH PERMIT FORM A THAT IS BEING CERTIFIED BY TH	S SEAL)	

NORTH CAROLINA MODELING PROTOCOL CHECKLIST (2 Pages)

REVISED 09/22/16

NCDEQ/Division of Air Quality - Application for Air Permit to Construct/Operate

D6-1

The North Carolina Modeling Protocol Checklist may be used in lieu of developing the traditional written modeling plan for North Carolina toxics and criteria pollutant modeling. The protocol checklist is designed to provide the same level of information as requested in a modeling protocol as discussed in Chapter 2 of the *Guideline for Evaluating the Air Quality Impacts of Toxic Pollutants in North Carolina*. The modeling protocol checklist is submitted with the modeling analysis. The above referenced *Guideline* can be found at the following web link:

https://ncdenr.s3.amazonaws.com/s3fs-public/Air%20Quality/permits/mets/Guidance.pdf

Although most of the information requested in the modeling protocol checklist is self-explanatory, additional comments are provided, where applicable, and are discussed in greater detail in the toxics modeling *Guideline* referenced above. References to sections, tables, figures, appendices, etc., in the protocol checklist are found in the toxics modeling *Guideline*.

INSTRUCTIONS: The modeling report supporting the compliance demonstration should include most of the information listed below. As appropriate, answer the following questions or indicate by check mark the information provided or action taken is reflected in your report.

FACILITY INFORMATION												
Facility Name:	H.F. Lee Steam Electric Plant	Consultant (if app	plicable):									
		Environme	ntal Consulting & Technology of North Carolina, PLLC									
Facility ID:	9600017											
Address:	1199 Black Jack Church Road	7208 Falls	Of Neuse Road									
	Goldsboro, NC, 27530	Suite 102										
		Raleigh, N	C 27615									
Contact Name:	Erin Wallace	Contact Name:	Thomas Pritcher									
Phone Number:	919-546-5797	Phone Number:	919-861-8888									
Email Address:	erin.wallace@duke-energy.com	Email Address:	tpritcher@ectinc.com									

GENERAL INFORMATION		
Description of New Source or Source/Process Modification: P rovide a short description of the new or modified source(s) and a brief discussion of how this change affects facility production or process operation.	7	Included N/A
Source/Pollutant Identification: Provide a table of the affected pollutants, by source, which identifies the source type (point, area, or volume), maximum pollutant emission rates over the applicable averaging period(s), and, for point sources, indicate if the stack is capped or non-vertical (C/N).	7	Included
Pollutant Emission Rate Calculations: Indicate how the pollutant emission rates were derived (e.g. AP-42 emission factors, mass balance, etc.) and where applicable, provide the calculations	I	Included N/A
Site/Facility Diagram: Provide a diagram or drawing showing the location of all existing and proposed emission sources, buildings or structures, public right-of-ways, and the facility property (toxics)/fence line (criteria pollutants) boundaries. The diagram should also include a scale, true north indicator, and the UTM or latitude/longitude of at least one point.	7	Included
Certified Plat or Signed Survey: a certified plat (map) from the County Register of Deeds or a signed survey must be submitted to validate property boundaries modeled.	7	Included
Topographic Map: a topographic map covering approximately 5 km around the facility must be submitted. The facility boundaries should be annotated on the map as accurately as possible.		Included N/A
Cavity Impact Analysis: no cavity analysis is required if using AERMOD. See Section 4.2		Included N/A
Background Concentrations (criteria Pollutant analyses only): Background concentrations must be determined for each pollutant for each averaging period evaluated. The averaged background value used (e.g. high, high-second-high, high-third-high, etc.) is based on the		Included
pollutant and averaging period evaluated. The background concentrations are added to the modeled concentrations, which are then compared to the applicable air quality standard to determine compliance.	7	N/A
Offsite Source Inventories (criteria pollutant analyses only): Offsite source inventories must be developed and modeled for all pollutants for which onsite source emissions are modeled in excess of the specific pollutant significant impact levels (SILs) as defined in the PSD New Source Review Workshop Manual. The DAO AOAB must approve the inventories. An initial working inventory can be requested from the		Included
AQAB.	~	N/A
Attach Additional Sheets as Necessary	Pac	ae 1 of 2

SCREEN LEVEL MODELING		D6-2
Model: The latest version of the AERSCREEN model must be used. The use of other screening models should be approved by NCDAQ prior to submitting the modeling report.	AERSCF	REEN Version
Source/Source Emission Parameters: Provide a table listing the sources modeled and the applicable source emission parameters. See NC Form 3 - Appendix A.		NA
Merged Sources: Identify merged sources and show all appropriate calculations. See Section 3.3		NA
GEP Analysis: See Section 3.2 and NC Form 1 - Appendix A		NA
Terrain: Indicate the terrain modeled: simple (Section 4.4), and complex (Section 4.5 and NC Form 4 Appendix A). If complex terrain is within 5 kilometers of the facility, complex terrain must be evaluated. Simple terrain must include terrain elevations if any terrain is greater than the stack base of any source modeled. Mark the appropriate terrain type		Simple
Meteorology: Refer to Section 4.1 for AERSCREEN inputs.		••••
Receptors: AERSCREEN - use shortest distance to property boundary for each source modeled and use sufficient range to find maximum [See Section 4.1(i) and (j)]. Terrain above stack base must be evaluated.		NA
Modeling Results: For each affected pollutant, modeling results should be summarized, converted to the applicable averaging period (See		NA
Table 3), and presented in tabular format indicating compliance status with the applicable AAL, SIL, or NAAQS. See NC Form S5 - Appendix A.		NA
		Electronic
Modeling Files: Either electronic or hard copies of AERSCREEN output must be submitted.		Hard Copy

REFINED LEVEL MODELING												
Model: The latest version of AERMOD should be used. The use of other refined models must be approved by NCDAQ prior to submitting the modeling report.	AERMOD Version											
The latest version of AERMOD may be found at the following web address: <u>http://www.epa.gov/scram001/dispersion_prefrec.htm</u>	16216r											
Source/Source Emission Parameters: Provide a table listing the sources modeled and the applicable source emission parameters. See NC Form 3 - Appendix A.	Y											
GEP Analysis: Use BPIP-Prime with AERMOD.												
Cavity Impact Analysis: No separate cavity analysis is required when using AERMOD as long as receptors are placed in cavity susceptible areas. See Section 4.2 and 5.2.	NA											
Terrain: Use digital elevation data from the USGS NED database. Use of other sources of terrain elevations or the non-regulatory Flat Terrain option will require prior approval from DAQ AQAB.	USGS NED											
The USGS NED database can be found at the following web address: <u>http://viewer.nationalmap.gov/launch/</u>												
Coordinate System: Specify the coordinate system used (e.g. NAD27, NAD83, etc.) to identify the source, building, and receptor locations. Note: Be sure to specify in the AERMAP input file the correct base datum (NADA) to be used for identifying source input data locations. Clearly note in both the protocol checklist and the modeling report which datum was used.	Coordinate System: NAD83											
Receptors: The receptor grid should be of sufficient size and resolution to identify the maximum pollutant impact. See Section 5.3.	Y											
Meteorology: Indicate the AQAB, pre-processed, 5-year data set used in the modeling demonstration: See Section 5.5 and Appendix B)	Data Set Used: Rocky Mount-Wilson (surface) / Newport											
AERMOD Version:	NA											
If processing your own raw meteorology, then pre-approval from AQAB is required. Additional documentation files (e.g. AERMET state processing files) will also be necessary. For NC toxics, the modeling demonstration requires only the last year of the standard 5-year data set (e.g. 2005) provided the maximum impacts are less than 50% of the applicable AAL(s).	NA											
Modeling Results: For each affected pollutant and averaging period, modeling results should be summarized and presented in tabular format indicating compliance status with the applicable AAL, SIL, or NAAQS. See NC Form R5 - Appendix A.	Y											
Modeling Files: Submit input and output files for AERMOD. Also include BPIP-Prime files, AERMAP files, DEM files, and any AERMET input and output files, including raw meteorological data.	Y											

Attach Additional Sheets as Necessary

Page 2 of 2

APPENDIX B

SUPPORTING EMISSION CALCULATIONS



Table 1A - Toxic Permitting Emission Rate (TPER) Analysis based on Potential Emissions from the Existing and Proposed Sources

	Existi	ng Turbines	s 10-13	Exis	ting Turbir	ne 14	Existing	Turbines 1	A, 1B, 1C	Existing	Auxiliary E	quipment	S	TAR Facili	ty		Total			TPER		Mode	ling Requir	red?
Pollutants	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr
Sulfuric Acid Mist	3.24E+01	7.78E+02		8.01E+00	1.92E+02		2.30E+02	5.52E+03		0.00E+00	0.00E+00		1.00E-01	2.40E+00		270.61	6494.64		0.025	0.25		YES	YES	
Benzene			8.23E+02			2.23E+02			7.33E+02			4.16E+00			3.34E+00			1787.54			8.1			YES
Formaldehyde	5.32E+00			1.38E+00			4.89E+00			1.22E-02			7.64E-03			11.61			0.04			YES		
Hexane							2.40E+00	5.75E+01		1.71E-01	4.11E+00			2.54E+00			64.18			23.0			YES	1
Toluene	2.78E+00	6.68E+01		7.54E-01	1.81E+01		8.82E-01	2.12E+01		1.95E-03	4.69E-02		1.32E-03	3.17E-02		4.42	106.11		14.4	98.0		NO	YES	l.
Arsenic			1.65E+02			4.47E+01			7.10E+01			2.08E-01			8.60E+00			289.30			0.053			YES
Beryllium			4.64E+00			1.26E+00			2.00E+00			1.25E-02			9.42E-01			8.86			0.28			YES
Cadmium			7.18E+01			1.95E+01			3.10E+01			1.14E+00			6.07E-01			124.13			0.37			YES
Chromium VI	1.34E-02	3.21E-01		3.63E-03	8.71E-02		7.11E-02	1.71E+00		1.33E-04	3.20E-03			4.05E-04			2.12			0.013			YES	
Manganese	5.92E+00	1.42E+02		1.60E+00	3.84E+01		5.10E+00	1.22E+02		3.62E-05	8.68E-04			3.34E-02			302.91			0.630			YES	
Mercury	8.98E-03	2.16E-01		2.44E-03	5.86E-02		7.74E-03	1.86E-01		2.48E-05	5.94E-04			4.64E-04			0.46			0.013			YES	. <u></u>
Nickel	3.45E-02	8.27E-01		9.34E-03	2.24E-01		2.97E-02	7.13E-01		2.00E-04	4.79E-03			1.71E-02			1.79			0.013			YES	. <u></u>

Existing Equipment: Emissions from Tables 3-2 through 3-4 (November 2010) and Tables 4-7 through 4-9 and 4-13 (April 2011). Tables provided in Appendix C.

Table 1B - Toxic Permitting Emission Rate (TPER) Analysis based on Optimized Emissions from the Existing and Proposed Sources

	Existi	ng Turbines	10-13	Exis	sting Turbin	e 14	Existing	isting Turbines 1A, 1B, 1C Existin				quipment	ST	AR Facility	/		Total			TPER		Mode	ling Requir	red?
Pollutants	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr	lb/hr	lb/day	lb/yr
Sulfuric Acid Mist	1.13E+02	1.29E+03		2.80E+01	3.19E+02		8.05E+02	9.17E+03		0.00E+00	0.00E+00		3.50E-01	3.98E+00		947.13	10,781.10		0.025	0.25		YES	YES	
Benzene			2.47E+05			6.70E+04			1.94E+05			1.25E+03			1.00E+03			510,598.49			8.1			YES
Formaldehyde	8.14E+02			2.11E+02			7.48E+02			1.86E+00			1.17E+00			1,776.30			0.04			YES		
Hexane							5.42E+03	1.30E+05		1.71E-01				8.58E+03			138,647.28			23.0			YES	
Toluene	6.05E+05	7.30E+06		1.64E+05	1.98E+06		1.92E+05	2.31E+06		4.25E+02	5.13E+03		2.87E+02	3.46E+03		961,534.32	11,593,642.41		14.4	98.0		YES	YES	
Arsenic			2.23E+02			6.03E+01			9.58E+01			2.81E-01			8.60E+00			387.55			0.053			YES
Beryllium			1.11E+02			3.03E+01			4.81E+01			2.99E-01			2.26E+01			212.67			0.28			YES
Cadmium			8.26E+03			2.25E+03			3.57E+03			1.31E+02			6.97E+01			14,274.49			0.37			YES
Chromium VI	3.89E+00	9.34E+01		1.06E+00	2.54E+01		2.07E+01	4.97E+02		3.88E-02	9.32E-01			1.18E-01			616.41			0.013			YES	
Manganese	1.23E+03	2.94E+04		3.31E+02	7.95E+03		1.06E+03	2.53E+04		7.49E-03	1.80E-01			6.91E+00			62,703.25			0.630			YES	
Mercury	2.35E+01	5.63E+02		6.38E+00	1.53E+02		2.02E+01	4.85E+02		6.47E-02	1.55E+00			1.21E+00			1,204.33			0.013			YES	
Nickel	4.48E+00	1.08E+02		1.21E+00	2.91E+01		3.86E+00	9.27E+01		2.60E-02	6.23E-01			2.23E+00			232.17			0.013			YES	

Duke Energy H.F. Lee Plant Table 2A - Facility-wide Emissions Summary - Shortterm

	STAR [®] F Worst-C	Fly Ash + ase Fuel	EUE Em	issions	Pre STAF	R Unit Silo	Post ST	AR Unit	Pollution C	ontrol Silo	Wet Ash R	eceiving	Storago Bil	Emissions	Ash E	Pacin	Ash H	andling	Hauli	Poade	Scro	opor	Cru	shor	Screener/	/Crusher	Facilit Contr Emis	y Total rolled	Facility Perm	/ Total litted
Pollutant	lb/hr	ton/vr	lb/br	ton/vr	lb/hr	ton/vr	lb/hr	ton/vr	lb/hr	ton/vr	lb/hr	ton/vr	Ib/br	ton/vr	lb/hr	ton/vr	Asir ha	ton/vr	lb/hr	ton/vr	lb/br	ton/vr	lh/hr	ton/vr	lb/hr	ton/vr	lb/hr	ton/vr	lb/br	ton/vr
PM	16.61		6.86		0.02		0.04		0.11		4 50E-03		3 14F-03		1.61E+00		3 22E-02		3 49E-01		0.02		0.01		0.86		26.52		26.52	
PM	15.28		6.31		0.02		0.04		0.10		2.13E-03		1.57E-03		8.05E-01		1 52E-02		9.02E-02		0.02		0.004		0.86		23.50		23.50	
	9.90		3.63		0.01		0.02		0.10		2.10E 00		2.25E.04		1.21E.01		2 20E 02		0.02E 02		0.0003		0.004		0.00		12.50		12.52	
°O	0.00		5.05		0.01		0.02		0.00		5.222-04		2.332-04		1.212-01		2.302-03		9.032-03		0.0003		0.001		0.80		13.32		24.04	
	24.14																								0.80		24.94		24.94	
NO _X	47.60									- ·· ·															12.12		59.72		59.72	
	22.40																								2.61		25.01		25.01	
VUC	2.24																								0.97		3.21		3.21	
$GHG(CO_2e \text{ Basis})$	0.40																										0.40		0.40	
	0.10		1.005.04		0.075.07		0.005.07				0.005.00		0.005.00		0.005.05		0.005.07				0.005.07		1.045.07				0.10		0.10	
Lead	3.59E-04		1.36E-04		3.87E-07		8.22E-07				8.93E-08		6.22E-08		3.20E-05		6.38E-07				3.00E-07		1.64E-07		0.555.00		5.30E-04		5.30E-04	
Benzene	1.24E-04																								2.55E-03		2.68E-03		2.68E-03	
Hovano	4.41E-03																								3.23E-03		1.04E-03		1.04E-03	
Toluene	2.00E-04																								1 12E-03		1.00E-01		1.00E-01	
Arsenic	6.53E-04		2.64E-04		7.51E-07		1.60E-06				1.73E-07		1.21E-07		6.21E-05		1.24E-06				5.83E-07		3.18E-07		1.122 00		9.84E-04		9.84E-04	
Antimony	2.13E-05		8.78E-06		2.49E-08		5.31E-08				5.76E-09		4.01E-09		2.06E-06		4.12E-08				1.94E-08		1.06E-08				3.23E-05		3.23E-05	
Beryllium	7.13E-05		2.91E-05		8.28E-08		1.76E-07				1.91E-08		1.33E-08		6.84E-06		1.37E-07				6.43E-08		3.51E-08				1.08E-04		1.08E-04	
Cadmium	6.77E-05		1.23E-06		3.51E-09		7.47E-09				8.10E-10		5.64E-10		2.90E-07		5.79E-09				2.72E-09		1.49E-09				6.92E-05		6.92E-05	
Chromium	5.01E-04		1.73E-04		4.91E-07		1.04E-06				1.13E-07		7.90E-08		4.06E-05		8.10E-07				3.81E-07		2.08E-07				7.17E-04		7.17E-04	
Chromium VI	1.11E-05		4.59E-06		1.31E-08		2.77E-08				3.01E-09		2.10E-09		1.08E-06		2.15E-08				1.01E-08		5.53E-09				1.69E-05		1.69E-05	
Cobalt	2.16E-04		8.69E-05		2.47E-07		5.25E-07				5.71E-08		3.98E-08		2.04E-05		4.08E-07				1.92E-07		1.05E-07				3.24E-04		3.24E-04	
Manganese	9.24E-04		3.72E-04		1.06E-06		2.25E-06				2.44E-07		1.70E-07		8.74E-05		1.75E-06				8.21E-07		4.48E-07				1.39E-03		1.39E-03	
Mercury	1.80E-05		1.10E-06		3.12E-09		6.62E-09				7.20E-10		5.02E-10		2.58E-07		5.15E-09				2.42E-09		1.32E-09				1.93E-05		1.93E-05	
Nickel	5.11E-04		1.60E-04		4.54E-07		9.66E-07				1.05E-07		7.32E-08		3.76E-05		7.50E-07		_		3.53E-07		1.92E-07				7.12E-04		7.12E-04	
Selenium	1.41E-04		5.71E-05		1.62E-07		3.49E-07				3.74E-08		2.61E-08		1.34E-05		2.68E-07				1.26E-07		6.86E-08		7.005.04		2.13E-04		2.13E-04	
Xylenes																									7.80E-04		7.80E-04		7.80E-04	
																									1.07E-04		1.07E-04		1.07E-04	
Acrolein																									2.10E-03		2.10E-03		2.10E-03	
Total PAH																									4 60F-04		4 60F-04		2.55E-04	
Naphthalene	3.59E-05																								2.32E-04		2.68E-04		2.68E-04	
Acenaphthalene	0.001 00																								1.38E-05		1.38E-05		1.38E-05	
Acenaphthene															1										3.89E-06		3.89E-06		3.89E-06	
Fluorene																									7.99E-05		7.99E-05		7.99E-05	
Phenanthrene																									8.05E-05		8.05E-05		8.05E-05	
Anthracene																									5.12E-06		5.12E-06		5.12E-06	
Fluoranthene																									2.08E-05		2.08E-05		2.08E-05	
Pyrene																									1.31E-05		1.31E-05		1.31E-05	
Benzo(a)anthracene																									4.60E-06		4.60E-06		4.60E-06	
Chrysene																									9.66E-07		9.66E-07		9.66E-07	
Benzo(b)fluoranthene																									2./1E-07		2.71E-07		2./1E-07	
Benzo(k)filloranthene															┤───┤										4.24E-07		4.24E-07		4.24E-07	
benzo(a)pyrene															+		+								5.15E-07		5.15E-07		5.15E-07	
Dibenz(a b)enthrocone	┼───┤						+								┨────┤		+								1.030-00				1.032-00	
Benzo(a h l)pervlene																	+								1.34F-06		1.34F-06		1.34E-06	
Maximum HAP			1			1	1	I	1	1	1		1	1	1 1		1	1	1		1	1		1	1.072 00		1.06E-01		1.06E-01	
Total HAP	1																										1.26E-01		1.26E-01	

Note: Duke Energy expects 6%-15% LOI. LOI will affect throughput. Duke Energy wont go above 400,000 tpy.

[§] Based on SEFA stack test performed September 2016. Sulfuric Acid Mist was 0.05 lb/hr for contingency ECT doubled the number to 0.1 lb/hr.

NC15A NCAC 02Q .0711 EMISSION RATES REQUIRING A PERMIT

Pollutant	Facility Total Controlled Emissions							
	lb/hr	lb/day						
Sulfuric Acid Mist	0.10	2.40						
Benzene								
Formaldehyde	7.64E-03							
Hexane		2.54						
Toluene	1.32E-03	3.17E-02						
Arsenic								
Beryllium								
Cadmium								
Chromium VI	1.69E-05	4.05E-04						
Manganese		3.34E-02						
Mercury		4.64E-04						
Nickel		1.71E-02						

Duke Energy H.F. Lee Plant Table 2B - Facility-wide Emissions Summary - Annual

	STAR [®] F Worst-C Controlled	Fly Ash + case Fuel Emissions	EHE Er	missions	Pre STAI Emis	R Unit Silo ssions	Post S Silo/Dome	TAR Unit Emissions	Pollution C Emiss	ontrol Silo	Wet Ash Emis	Receiving	Storage P	ile Emissions	Ash	Basin	Ash H	landling	Haul	Roads	Scr	eener	Cru	isher	Screene End	er/Crusher gines	Facili Cont Emis	:y Total rolled ssions	Facility Perm Emis	/ Total litted sions
Pollutant	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr
PM		72.74		30.03		0.04		0.04		0.49		1.29E-02		1.37E-02		7.05E+00		1.41E-01		1.53E+00		1.97E-02		1.51E-03		3.81E-01		112.49	(<u> </u>	112.49
PM ₁₀		66.92		27.63		0.02		0.02		0.45		6.08E-03		6.87E-03		3.53E+00		6.66E-02		3.95E-01		6.61E-03		6.78E-04		3.81E-01		99.43	(99.43
PM _{2.5}		38.55		15.92		0.02		0.02		0.26		9.21E-04		1.03E-03		5.29E-01		1.01E-02		3.95E-02		4.47E-04		1.25E-04		3.81E-01		55.73	· +	55.73
SO ₂		98.18																								0.35		98.53	· +	98.53
NOv		193.60																								5.36		198,96	+	198.96
<u> </u>		91.10																								1 16		92.26	·	92.26
VOC		9.11																								0.43		9.54	· +	9.54
GHG (Mass Basis)*		116,401																								198.14		116598.85	· +	116,599
GHG (CO ₂ e Basis)*		116,406																								198.14		116604.15	· +	116,604
Sulfuric Acid Mist [§]		0.44																										0.44	· +	0.44
Lead		1.57E-03		5.96E-04		7.73E-07		7.73E-07				2.55E-07		2.73E-07		1.40E-04		2.80E-06				3.90E-07		2.99E-08				2.31E-03	· +	2.31E-03
Benzene		5.41E-04																								1.13E-03		1.67E-03	ر +	1.67E-03
Formaldehyde		1.93E-02																				1				1.43E-03		2.08E-02	· •	2.08E-02
Hexane		4.64E-01																										4.64E-01		4.64E-01
Toluene		8.76E-04																								4.95E-04		1.37E-03	/	1.37E-03
Arsenic		2.86E-03		1.16E-03		1.50E-06		1.50E-06				4.96E-07		5.29E-07		2.72E-04		5.43E-06				7.58E-07		5.80E-08				4.30E-03		4.30E-03
Antimony		9.34E-05		3.84E-05		4.99E-08		5.00E-08				1.65E-08		1.76E-08		9.03E-06		1.80E-07				2.52E-08		1.93E-09				1.41E-04		1.41E-04
Beryllium		3.12E-04		1.28E-04		1.66E-07		1.66E-07				5.46E-08		5.84E-08		3.00E-05		5.99E-07				8.36E-08		6.40E-09				4.71E-04		4.71E-04
Cadmium		2.97E-04		5.41E-06		7.01E-09		7.03E-09				2.31E-09		2.47E-09		1.27E-06		2.54E-08		_		3.54E-09		2.71E-10				3.03E-04		3.03E-04
Chromium		2.19E-03		7.57E-04		9.82E-07		9.82E-07				3.24E-07		3.46E-07		1.78E-04		3.55E-06		_		4.95E-07		3.79E-08				3.14E-03	ل	3.14E-03
		4.87E-05		2.01E-05		2.61E-08		2.61E-08				8.61E-09		9.20E-09		4.73E-06		9.44E-08				1.32E-08		1.01E-09				7.38E-05		7.38E-05
Cobait		9.44E-04		3.01E-04		4.94E-07		4.94E-07				1.03E-07		1.74E-07		0.94E-05		1.79E-06				2.49E-07		1.91E-08				1.42E-03	,	1.42E-03
Mercury		7.86E-05		4.81E-06		6.23E-09		6.23E-00				2.06E-09		2 20E-09		1 13E-06		2 25E-08				3.15E-09		2.41E-10				8.46E-05		8.46E-05
Nickel		2.24E-03		7.01E-04		9.09E-07		9.09E-07				3.00E-07		3.20E-07		1.65E-04		3.29E-06				4.59E-07		3.51E-08		1		3.11E-03		3.11E-03
Selenium		6.19E-04		2.50E-04		3.24E-07		3.28E-07				1.07E-07		1.14E-07		5.87E-05		1.17E-06				1.64E-07		1.25E-08				9.30E-04	· +	9.30E-04
Xylenes																										3.45E-04		3.45E-04	· +	3.45E-04
1,3-Butadiene																										4.74E-05		4.74E-05	,	4.74E-05
Acetaldehyde																										9.29E-04		9.29E-04		9.29E-04
Acrolein																										1.12E-04		1.12E-04		1.12E-04
Total PAH																										2.04E-04		2.04E-04		2.04E-04
Naphthalene		1.57E-04																								1.03E-04		2.60E-04		2.60E-04
Acenaphthalene																										6.13E-06		6.13E-06		6.13E-06
Acenaphthene																				_						1.72E-06		1.72E-06		1.72E-06
Fluorene																										3.54E-05		3.54E-05		3.54E-05
Anthracono		+ +								+		_				+						+ +				3.30E-05		3.30E-05	,	3.30E-03
Fluoranthene																										9.227E-06		9.227E-00	,	9.22F-06
Pyrene																										5 79E-06		5.79E-06		5.79E-06
Benzo(a)anthracene																						1				2.04E-06		2.04E-06	+ +	2.04E-06
Chrvsene																										4.28E-07		4.28E-07	(4.28E-07
Benzo(b)fluoranthene																										1.20E-07		1.20E-07	· +	1.20E-07
Benzo(k)fluoranthene																										1.88E-07		1.88E-07		1.88E-07
Benzo(a)pyrene																										2.28E-07		2.28E-07		2.28E-07
Indeno(1,2,3-cd)pyrene																										4.54E-07		4.54E-07		4.54E-07
Dibenz(a,h)anthracene																										7.06E-07		7.06E-07	Ţ	7.06E-07
Benzo(g,h,l)perylene																										5.92E-07		5.92E-07		5.92E-07
Maximum HAP																												4.64E-01		4.64E-01
I otal HAP																												5.10E-01	, I	5.10E-01

Note: Duke Energy expects 6%-15% LOI. LOI will affect throughput. Duke Energy wont go above 400,000 tpy.

[§] Based on SEFA stack test performed September 2016. Sulfuric Acid Mist was 0.05 lb/hr for contingency ECT doubled the number to 0.1 lb/hr.

NC15A NCAC 02Q .0711 EMISSION RATES REQUIRING A PERMIT

Pollutant	Facility Total Controlled Emissions
Sulfuric Acid Mist	1.8.91
Benzene	3.34
Formaldehyde	
Hexane	
Toluene	
Arsenic	8.60
Beryllium	0.94
Cadmium	0.61
Chromium VI	
Manganese	
Mercury	
Nickel	
Natural Gas Emissions

	Emission				Emis	sions	
Pollutant	Factor	Units	Throughput	Units	lb/hr	ton/yr	Reference
PM/PM ₁₀ /PM _{2.5}	7.6	lb/MMscf	58,824	scf/hr	0.45	1.96	EPA AP-42, Table 1.4-2 (07/98)
SO ₂	0.6	lb/MMscf	58,824	scf/hr	0.04	0.15	EPA AP-42, Table 1.4-2 (07/98)
NO _X	140	lb/MMscf	58,824	scf/hr	8.24	36.07	EPA AP-42, Table 1.4-1 (07/98)
СО	84	lb/MMscf	58,824	scf/hr	4.94	21.64	EPA AP-42, Table 1.4-1 (07/98)
VOC	5.5	lb/MMscf	58,824	scf/hr	0.32	1.42	EPA AP-42, Table 1.4-2 (07/98)
Lead	0.0005	lb/MMscf	58,824	scf/hr	2.94E-05	1.29E-04	EPA AP-42, Table 1.4-2 (07/98)
Benzene	0.0021	lb/MMscf	58,824	scf/hr	1.24E-04	5.41E-04	EPA AP-42, Table 1.4-3 (07/98)
Formaldehyde	0.075	lb/MMscf	58,824	scf/hr	4.41E-03	1.93E-02	EPA AP-42, Table 1.4-3 (07/98)
Hexane	1.8	lb/MMscf	58,824	scf/hr	1.06E-01	4.64E-01	EPA AP-42, Table 1.4-3 (07/98)
Naphthalene	0.00061	lb/MMscf	58,824	scf/hr	3.59E-05	1.57E-04	EPA AP-42, Table 1.4-3 (07/98)
Toluene	0.0034	lb/MMscf	58,824	scf/hr	2.00E-04	8.76E-04	EPA AP-42, Table 1.4-3 (07/98)
Arsenic	0.0002	lb/MMscf	58,824	scf/hr	1.18E-05	5.15E-05	EPA AP-42, Table 1.4-4 (07/98)
Beryllium	0.000012	lb/MMscf	58,824	scf/hr	7.06E-07	3.09E-06	EPA AP-42, Table 1.4-4 (07/98)
Cadmium	0.0011	lb/MMscf	58,824	scf/hr	6.47E-05	2.83E-04	EPA AP-42, Table 1.4-4 (07/98)
Chromium	0.0014	lb/MMscf	58,824	scf/hr	8.24E-05	3.61E-04	EPA AP-42, Table 1.4-4 (07/98)
Cobalt	0.000084	lb/MMscf	58,824	scf/hr	4.94E-06	2.16E-05	EPA AP-42, Table 1.4-4 (07/98)
Manganese	0.00038	lb/MMscf	58,824	scf/hr	2.24E-05	9.79E-05	EPA AP-42, Table 1.4-4 (07/98)
Mercury	0.00026	lb/MMscf	58,824	scf/hr	1.53E-05	6.70E-05	EPA AP-42, Table 1.4-4 (07/98)
Nickel	0.0021	lb/MMscf	58,824	scf/hr	1.24E-04	5.41E-04	EPA AP-42, Table 1.4-4 (07/98)
Selenium	0.000024	lb/MMscf	58,824	scf/hr	1.41E-06	6.18E-06	EPA AP-42, Table 1.4-4 (07/98)

Sample Calculations

Natural Gas Flow =	60 MMBtu	10 ⁶ Btu	scf Nat. Gas	=	58,824	scf/hr Natural Gas
	hr	MMBtu	1020 Btu			
NO_x Emissions =	58824 scf	MMscf	140 lb NOx	=	8.24	lb/hr NO _x
	hr	10 ⁶ scf	MMscf			
	8.24 lb NO _x	8760 hr	ton	=	36.07	tpy NO _x
	hr	yr	2000 lb			
	50004 (ll. //
CO Emissions =	58824 scf	MIMSCT	84 ID CO	=	4.94	Ib/hr CO
	hr	10 [°] scf	MMscf			
			I .			
	4.94 lb CO	8760 hr	ton	=	21.64	tpy CO
	hr	yr	2000 lb			

Annual Natural Gas usage provided by SEFA

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Propane Emissions

	Emission				Emissions			
Pollutant	Factor	Units	Throughput	Units	lb/hr	ton/yr	Reference	
PM/PM ₁₀ /PM _{2.5}	0.7	lb/10 ³ gal	663	gal/hr	0.46	2.03	EPA AP-42, Table 1.5-1 (07/08)	
SO ₂	0.018	lb/10 ³ gal	663	gal/hr	0.01	0.05	EPA AP-42, Table 1.5-1 (07/08)	Propane sulfur content 0.18 gr/100 ft3
NO _X	13	lb/10 ³ gal	663	gal/hr	8.62	37.75	EPA AP-42, Table 1.5-1 (07/08)	
СО	7.5	lb/10 ³ gal	663	gal/hr	4.97	21.78	EPA AP-42, Table 1.5-1 (07/08)	
VOC	1	lb/10 ³ gal	663	gal/hr	0.66	2.90	EPA AP-42, Table 1.5-1 (07/08)	

Sample Calculations

Propane Flow =	60 MMBtu	10 ⁶ Btu	gal Propane	=	663 gal/hr Propane
	hr	MMBtu	90,500 Btu		
NO_x Emissions =	663 gal	10 ³ gal	13 lb NOx	=	8.62 lb/hr NO _x
	hr	1000 gal	10 ³ gal		
	8.62 lb NO_{x}	8760 hr	ton	=	37.75 tpy NO _x
	hr	yr	2000 lb		
CO Emissions =	663 gal	10 ³ gal	7.5 lb CO	=	4.97 lb/hr CO
	hr	1000 gal	10 ³ gal		
	4.97 lb CO	8760 hr	ton	=	21.78 tpy CO
	hr	yr	2000 lb		

Annual Propane usage provided by SEFA

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Flyash Emissions

	Emission				Uncontrolle	d Emissions	Controlled	Emissions	
Pollutant	Factor	Units	Throughput	Units	lb/hr	ton/yr	lb/hr	ton/yr	Reference
NO _X	0.34	lb/MMBtu	140	MMBtu/hr	47.60	208.49	47.60	208.49	Based on SEFA operation experience
со	0.16	lb/MMBtu	140	MMBtu/hr	22.40	98.11	22.40	98.11	Based on SEFA operation experience
VOC	0.016	lb/MMBtu	140	MMBtu/hr	2.24	9.81	2.24	9.81	Based on stack test performed at a different STAR facility, CO emissions are expected to be 10% (or less) of VOC emissions.
Lead	19.85	ppmw			3.30E-04	1.44E-03	3.30E-04	1.44E-03	Duke Energy Average Ash Analysis and Water Injection
Arsenic	38.58	ppmw			6.41E-04	2.81E-03	6.41E-04	2.81E-03	Duke Energy Average Ash Analysis and Water Injection
Antimony	1.28	ppmw			2.13E-05	9.34E-05	2.13E-05	9.34E-05	Duke Energy Average Ash Analysis and Water Injection
Beryllium	4.25	ppmw			7.06E-05	3.09E-04	7.06E-05	3.09E-04	Duke Energy Average Ash Analysis and Water Injection
Cadmium	0.18	ppmw			3.00E-06	1.31E-05	3.00E-06	1.31E-05	Duke Energy Average Ash Analysis and Water Injection
Chromium	25.20	ppmw			4.19E-04	1.83E-03	4.19E-04	1.83E-03	Duke Energy Average Ash Analysis and Water Injection
Chromium VI	0.67	ppmw			1.11E-05	4.87E-05	1.11E-05	4.87E-05	Duke Energy Average Ash Analysis and Water Injection
Cobalt	12.68	ppmw			2.11E-04	9.22E-04	2.11E-04	9.22E-04	Duke Energy Average Ash Analysis and Water Injection
Manganese	54.31	ppmw			9.02E-04	3.95E-03	9.02E-04	3.95E-03	Duke Energy Average Ash Analysis and Water Injection
Mercury	0.16	ppmw			2.66E-06	1.16E-05	2.66E-06	1.16E-05	Duke Energy Average Ash Analysis and Water Injection
Nickel	23.34	ppmw			3.88E-04	1.70E-03	3.88E-04	1.70E-03	Duke Energy Average Ash Analysis and Water Injection
Selenium	8.43	ppmw			1.40E-04	6.13E-04	1.40E-04	6.13E-04	Duke Energy Average Ash Analysis and Water Injection

HAP/TAP emission factors from the STAR unit are based on site-specific ash analysis with the addition of metals in the water used for water injection

Sample Calculations

NO_x Emissions =	0.34 lb NO_{x}	140 MMBtu		=	47.60 lb/hr NO _x
	MMBtu	hour			
Arsenic Emissions =	38.58 lb As	17.79 lb PM	=	6.86E-04 lk	o/hr Arsenic
(Uncontrolled)	10 ⁶ lb	hr			

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Worst-Case STAR® Reactor Unit Emissions

							STAR® Rea Worst-C	ctor Fly Ash + ase Fuel	STAR® Reactor Fly Ash + Worst-Case Fuel	
	Natural Gas	s Emissions	Propane E	missions	Fly Ash E	missions	Controlled	Emissions	Permitted Emissions	
Pollutant	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr
PM							16.61		16.61	
PM ₁₀							15.28		15.28	-
PM _{2.5}							8.80		8.80	
SO ₂							24.14		24.14	
NO _X	8.24	36.07	8.62	37.75	47.60	208.49	35.82		47.60	-
со	4.94	21.64	4.97	21.78	22.40	98.11	17.77		22.40	-
VOC	0.32	1.42	0.66	2.90	2.24	9.81	1.94		2.24	-
Lead	2.94E-05	1.29E-04			3.30E-04	1.44E-03	3.59E-04		3.59E-04	
Benzene	1.24E-04	5.41E-04					1.24E-04		1.24E-04	
Formaldehyde	4.41E-03	1.93E-02					4.41E-03		4.41E-03	
Hexane	1.06E-01	4.64E-01					1.06E-01		1.06E-01	-
Naphthalene	3.59E-05	1.57E-04					3.59E-05		3.59E-05	
Toluene	2.00E-04	8.76E-04					2.00E-04		2.00E-04	
Arsenic	1.18E-05	5.15E-05			6.41E-04	2.81E-03	6.53E-04		6.53E-04	
Antimony					2.13E-05	9.34E-05	2.13E-05		2.13E-05	
Beryllium	7.06E-07				7.06E-05	3.09E-04	7.13E-05		7.13E-05	
Cadmium	6.47E-05	2.83E-04			3.00E-06	1.31E-05	6.77E-05		6.77E-05	
Chromium	8.24E-05	3.61E-04			4.19E-04	1.83E-03	5.01E-04		5.01E-04	
Chromium VI					1.11E-05	4.87E-05	1.11E-05		1.11E-05	
Cobalt	4.94E-06	2.16E-05			2.11E-04	9.22E-04	2.16E-04		2.16E-04	
Manganese	2.24E-05	9.79E-05			9.02E-04	3.95E-03	9.24E-04		9.24E-04	
Mercury	1.53E-05	6.70E-05			2.66E-06	1.16E-05	1.80E-05		1.80E-05	
Nickel	1.24E-04	5.41E-04			3.88E-04	1.70E-03	5.11E-04		5.11E-04	
Selenium	1.41E-06	6.18E-06			1.40E-04	6.13E-04	1.41E-04		1.41E-04	

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Natural Gas Emissions

	Emission				Emis	sions	
Pollutant	Factor	Units	Throughput	Units	lb/hr	ton/yr	Reference
PM/PM ₁₀ /PM _{2.5}	7.6	lb/MMscf	58,824	scf/hr	0.45	1.96	EPA AP-42, Table 1.4-2 (07/98)
SO ₂	0.6	lb/MMscf	58,824	scf/hr	0.04	0.15	EPA AP-42, Table 1.4-2 (07/98)
NO _X	140	lb/MMscf	58,824	scf/hr	8.24	36.07	EPA AP-42, Table 1.4-1 (07/98)
СО	84	lb/MMscf	58,824	scf/hr	4.94	21.64	EPA AP-42, Table 1.4-1 (07/98)
VOC	5.5	lb/MMscf	58,824	scf/hr	0.32	1.42	EPA AP-42, Table 1.4-2 (07/98)
Lead	0.0005	lb/MMscf	58,824	scf/hr	2.94E-05	1.29E-04	EPA AP-42, Table 1.4-2 (07/98)
Benzene	0.0021	lb/MMscf	58,824	scf/hr	1.24E-04	5.41E-04	EPA AP-42, Table 1.4-3 (07/98)
Formaldehyde	0.075	lb/MMscf	58,824	scf/hr	4.41E-03	1.93E-02	EPA AP-42, Table 1.4-3 (07/98)
Hexane	1.8	lb/MMscf	58,824	scf/hr	1.06E-01	4.64E-01	EPA AP-42, Table 1.4-3 (07/98)
Naphthalene	0.00061	lb/MMscf	58,824	scf/hr	3.59E-05	1.57E-04	EPA AP-42, Table 1.4-3 (07/98)
Toluene	0.0034	lb/MMscf	58,824	scf/hr	2.00E-04	8.76E-04	EPA AP-42, Table 1.4-3 (07/98)
Arsenic	0.0002	lb/MMscf	58,824	scf/hr	1.18E-05	5.15E-05	EPA AP-42, Table 1.4-4 (07/98)
Beryllium	0.000012	lb/MMscf	58,824	scf/hr	7.06E-07	3.09E-06	EPA AP-42, Table 1.4-4 (07/98)
Cadmium	0.0011	lb/MMscf	58,824	scf/hr	6.47E-05	2.83E-04	EPA AP-42, Table 1.4-4 (07/98)
Chromium	0.0014	lb/MMscf	58,824	scf/hr	8.24E-05	3.61E-04	EPA AP-42, Table 1.4-4 (07/98)
Cobalt	0.000084	lb/MMscf	58,824	scf/hr	4.94E-06	2.16E-05	EPA AP-42, Table 1.4-4 (07/98)
Manganese	0.00038	lb/MMscf	58,824	scf/hr	2.24E-05	9.79E-05	EPA AP-42, Table 1.4-4 (07/98)
Mercury	0.00026	lb/MMscf	58,824	scf/hr	1.53E-05	6.70E-05	EPA AP-42, Table 1.4-4 (07/98)
Nickel	0.0021	lb/MMscf	58,824	scf/hr	1.24E-04	5.41E-04	EPA AP-42, Table 1.4-4 (07/98)
Selenium	0.000024	lb/MMscf	58,824	scf/hr	1.41E-06	6.18E-06	EPA AP-42, Table 1.4-4 (07/98)

Sample Calculations

Natural Gas Flow =	60 MMBtu	10 ⁶ Btu	scf Nat. Gas	=	58,824	scf/hr Natural Gas
	hr	MMBtu	1020 Btu			
NO_x Emissions =	58824 scf	MMscf	140 lb NOx	=	8.24	lb/hr NO _x
	hr	10 ⁶ scf	MMscf			
	8.24 lb NO_{x}	8760 hr	ton	=	36.07	tpy NO _x
	hr	yr	2000 lb			
CO Emissions =	58824 scf	MMscf	84 lb CO	=	4.94	lb/hr CO
	hr	10 ⁶ scf	MMscf			
	4.94 lb CO	8760 hr	ton	=	21.64	tpy CO
	hr	yr	2000 lb			

Anuual Natural Gas usage provided by SEFA

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Propane Emissions

	Emission				Emissions			
Pollutant	Factor	Units	Throughput	Units	lb/hr	ton/yr	Reference	
PM/PM ₁₀ /PM _{2.5}	0.7	lb/10 ³ gal	663	gal/hr	0.46	2.03	EPA AP-42, Table 1.5-1 (07/08)	
SO ₂	0.018	lb/10 ³ gal	663	gal/hr	0.01	0.05	EPA AP-42, Table 1.5-1 (07/08)	Propane sulfur content 0.18 gr/100 ft3
NO _X	13	lb/10 ³ gal	663	gal/hr	8.62	37.75	EPA AP-42, Table 1.5-1 (07/08)	
со	7.5	lb/10 ³ gal	663	gal/hr	4.97	21.78	EPA AP-42, Table 1.5-1 (07/08)	
VOC	1	lb/10 ³ gal	663	gal/hr	0.66	2.90	EPA AP-42, Table 1.5-1 (07/08)	

Sample Calculations

Propane Flow =	60 MMBtu	10 ⁶ Btu	gal Propane	=	663 gal/hr Propane
	hr	MMBtu	90,500 Btu		
NO _x Emissions =	663 gal	10 ³ gal	13 lb NOx	=	8.62 lb/hr NO _x
	hr	1000 gal	10 ³ gal		
	8.62 lb NO _x	8760 hr	ton	=	37.75 tpy NO _x
	hr	yr	2000 lb		
		2	1		
CO Emissions =	663 gal	10° gal	7.5 lb CO	=	4.97 lb/hr CO
	hr	1000 gal	10 ³ gal		
		0700 h -	l tau		04 70 tou 00
	4.97 16 CO	8760 nr	ton	=	21.78 tpy CO
	nr	yr	2000 lb		

Anuual Propane usage provided by SEFA

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Flyash Emissions

	Emission				Uncontrolle	d Emissions	Controlled	Emissions	
Pollutant	Factor	Units	Throughput	Units	lb/hr	ton/yr	lb/hr	ton/yr	Reference
NO _X	0.34	lb/MMBtu	130	MMBtu/hr	44.20	193.60	44.20	193.60	Based on SEFA operation experience
со	0.16	lb/MMBtu	130	MMBtu/hr	20.80	91.10	20.80	91.10	Based on SEFA operation experience
VOC	0.016	lb/MMBtu	130	MMBtu/hr	2.08	9.11	2.08	9.11	Based on stack test performed at a different STAR facility, CO emissions are expected to be 10% (or less) of VOC emissions.
Lead	19.85	ppmw			3.30E-04	1.44E-03	3.30E-04	1.44E-03	Duke Energy Average Ash Analysis and Water Injection
Arsenic	38.58	ppmw			6.41E-04	2.81E-03	6.41E-04	2.81E-03	Duke Energy Average Ash Analysis and Water Injection
Antimony	1.28	ppmw			2.13E-05	9.34E-05	2.13E-05	9.34E-05	Duke Energy Average Ash Analysis and Water Injection
Beryllium	4.25	ppmw			7.06E-05	3.09E-04	7.06E-05	3.09E-04	Duke Energy Average Ash Analysis and Water Injection
Cadmium	0.18	ppmw			3.00E-06	1.31E-05	3.00E-06	1.31E-05	Duke Energy Average Ash Analysis and Water Injection
Chromium	25.20	ppmw			4.19E-04	1.83E-03	4.19E-04	1.83E-03	Duke Energy Average Ash Analysis and Water Injection
Chromium VI	0.67	ppmw			1.11E-05	4.87E-05	1.11E-05	4.87E-05	Duke Energy Average Ash Analysis and Water Injection
Cobalt	12.68	ppmw			2.11E-04	9.22E-04	2.11E-04	9.22E-04	Duke Energy Average Ash Analysis and Water Injection
Manganese	54.31	ppmw			9.02E-04	3.95E-03	9.02E-04	3.95E-03	Duke Energy Average Ash Analysis and Water Injection
Mercury	0.16	ppmw			2.66E-06	1.16E-05	2.66E-06	1.16E-05	Duke Energy Average Ash Analysis and Water Injection
Nickel	23.34	ppmw			3.88E-04	1.70E-03	3.88E-04	1.70E-03	Duke Energy Average Ash Analysis and Water Injection
Selenium	8.43	ppmw			1.40E-04	6.13E-04	1.40E-04	6.13E-04	Duke Energy Average Ash Analysis and Water Injection

HAP/TAP emission factors from the STAR unit are based on site-specific ash analysis with the addition of metals in the water used for water injection

Sample Calculations

NO_x Emissions =	0.34 lb NO _x	130 N	IMBtu	=	44.20 lb/hr NO _x
	MMBtu	ho	ur		
Arsenic Emissions = (Uncontrolled)	38.58 lb As 10 ⁶ lb	17.79 lb PM hr	=	6.86E-04 lb	/hr Arsenic

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Worst-Case STAR® Reactor Unit Emissions

			_				STAR® Rea Worst-C	ctor Fly Ash + case Fuel	STAR® Reactor Fly Ash + Worst-Case Fuel	
Pollutant	Natural Gas	s Emissions	Propane E Ib/hr	missions	Fly Ash E lb/hr	ton/vr	Controlled	Emissions	Permitted	Emissions
		toninyi		tonii yi		ton#yr	10/111	72.74		72 74
PM ₁₀								66.92		66.92
PM ₂ c								38.55		38.55
SO ₂								98.18		98.18
NO _x	8.24	36.07	8.62	37.75	44.20	193.60		141.99		193.60
CO	4.94	21.64	4.97	21.78	20.80	91.10		70.84		91.10
VOC	0.32	1.42	0.66	2.90	2.08	9.11		7.81		9.11
Lead	2.94E-05	1.29E-04			3.30E-04	1.44E-03		1.57E-03		1.57E-03
Benzene	1.24E-04	5.41E-04						5.41E-04		5.41E-04
Formaldehyde	4.41E-03	1.93E-02						1.93E-02		1.93E-02
Hexane	1.06E-01	4.64E-01						4.64E-01		4.64E-01
Naphthalene	3.59E-05	1.57E-04						1.57E-04		1.57E-04
Toluene	2.00E-04	8.76E-04						8.76E-04		8.76E-04
Arsenic	1.18E-05	5.15E-05			6.41E-04	2.81E-03		2.86E-03		2.86E-03
Antimony					2.13E-05	9.34E-05		9.34E-05		9.34E-05
Beryllium	7.06E-07	3.09E-06			7.06E-05	3.09E-04		3.12E-04		3.12E-04
Cadmium	6.47E-05	2.83E-04			3.00E-06	1.31E-05		2.97E-04		2.97E-04
Chromium	8.24E-05	3.61E-04			4.19E-04	1.83E-03		2.19E-03		2.19E-03
Chromium VI					1.11E-05	4.87E-05		4.87E-05		4.87E-05
Cobalt	4.94E-06	2.16E-05			2.11E-04	9.22E-04		9.44E-04		9.44E-04
Manganese	2.24E-05	9.79E-05			9.02E-04	3.95E-03		4.05E-03		4.05E-03
Mercury	1.53E-05	6.70E-05			2.66E-06	1.16E-05		7.86E-05		7.86E-05
Nickel	1.24E-04	5.41E-04			3.88E-04	1.70E-03		2.24E-03		2.24E-03
Selenium	1.41E-06	6.18E-06			1.40E-04	6.13E-04		6.19E-04		6.19E-04

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Est. Gas Flow, acfm		77,500			
PM Emission Rate, gr/acf		0.025			
Estimated Emissions					
PM (lb/hr)		16.61			
		12.14			
		lb/hr			
	PM	16.61			
	PM ₁₀ (Note 2)	15.28			
	PM _{2.5} (Note 3)	8.80			

Notes:

- 1. PM Emission Factor (grains/acf)
- 2. PM₁₀ = 3. PM_{2.5} =
 - 92% 53%

of Total PM (From AP-42 Table 1.1-6 (09/98)) of Total PM (From AP-42 Table 1.1-6 (09/98))

4. TPY = Tons per Year

Duke Energy H.F. Lee Plant Table 3D - STAR[®] Emissions - SO₂ - Shortterm (ES-31)

Process Throughput							
Raw Feed LOI (%)	6.0%	7.0%	8.0%	9.0%	10.0%	11.0%	
Max Heat Input (MMBtu/hr)	140	140	140	140	140	140	
Carbon (Btu/lb)	14,500	14,500	14,500	14,500	14,500	14,500	
Carbon (lb/hr)	9,655	9,655	9,655	9,655	9,655	9,655	
Raw Feed Rate (TPH)	80.46	68.97	60.34	53.64	48.28	43.89	
Feed Ash Sulfur %	0.15%	0.15%	0.15%	0.15%	0.15%	0.15%	
Estimated Emissions							
SO ₂ (lb/hr) - Uncontrolled - Ash	482.76	413.79	362.07	321.84	289.66	263.32	
SO ₂ (lb/hr) - Uncontrolled - NG/Propane	0.04	0.04	0.04	0.04	0.04	0.04	
SO ₂ (lb/hr) - Uncontrolled - Total	482.79	413.83	362.10	321.87	289.69	263.36	
SO ₂ (lb/hr) - Controlled							
95.00%	24.14	20.69	18.11	16.09	14.48	13.17	

12.0%	13.0%	14.0%	15.0%
140	140	140	140
14,500	14,500	14,500	14,500
9,655	9,655	9,655	9,655
40.23	37.14	34.48	32.18
0.15%	0.15%	0.15%	0.15%
241.38	222.81	206.90	193.10
0.04	0.04	0.04	0.04
241.41	222.85	206.93	193.14
12 07	11 14	10.35	9.66
12.07	11.14	10.00	0.00

Duke Energy H.F. Lee Plant

Table 3E - STAR[®] Emissions - SO₂ - Annual (ES-31)

Process Throughput							
Raw Feed LOI (%)	6.0%	7.0%	8.0%	9.0%	10.0%	11.0%	
Max Heat Input (MMBtu/hr)	130	130	130	130	130	130	
Carbon (Btu/lb)	14,500	14,500	14,500	14,500	14,500	14,500	
Carbon (lb/hr)	8,966	8,966	8,966	8,966	8,966	8,966	
Raw Feed Rate (TPH)	74.71	64.04	56.03	49.81	44.83	40.75	
Feed Ash Sulfur %	0.15%	0.15%	0.15%	0.15%	0.15%	0.15%	
Estimated Emissions							
SO ₂ (lb/hr) - Uncontrolled - Ash	448.28	384.24	336.21	298.85	268.97	244.51	
SO ₂ (lb/hr) - Uncontrolled - NG/Propane	0.04	0.04	0.04	0.04	0.04	0.04	
SO ₂ (lb/hr) - Uncontrolled - Total	448.31	384.27	336.24	298.89	269.00	244.55	
SO ₂ (lb/hr) - Controlled							
95.00%	22.42	19.21	16.81	14.94	13.45	12.23	

12.0%	13.0%	14.0%	15.0%
130	130	130	130
14,500	14,500	14,500	14,500
8,966	8,966	8,966	8,966
37.36	34.48	32.02	29.89
0.15%	0.15%	0.15%	0.15%
224.14	206.90	192.12	179.31
0.04	0.04	0.04	0.04
0.04	0.04	0.04	170.05
224.17	206.93	192.15	179.35
11.21	10.35	9.61	8.97

Duke Energy H.F. Lee Plant Table 4 - EHE Emissions Unit 1 and Unit 2 (ES-34 and ES-35)

Maximum annual emissions are based on the lb/hr of a single unit * 8760 hours per year.

	Est. En	nissions		
	lb/hr	TPY (Total for		
	(per unit)	both units)		
PM (Note 2)	6.86	30.03		
PM ₁₀ ^(Note 3)	6.31	27.63		
PM _{2.5} (Note 4)	3.63	15.92		

		ļ	Emissions		
Pollutant	Emission Factor	Units	lb/hr (per unit)	ton/yr (Total for both units)	Reference
Lead	19.85	ppmw	1.36E-04	5.96E-04	Duke Energy Average Ash Analysis
Arsenic	38.55	ppmw	2.64E-04	1.16E-03	Duke Energy Average Ash Analysis
Antimony	1.28	ppmw	8.78E-06	3.84E-05	Duke Energy Average Ash Analysis
Beryllium	4.25	ppmw	2.91E-05	1.28E-04	Duke Energy Average Ash Analysis
Cadmium	0.18	ppmw	1.23E-06	5.41E-06	Duke Energy Average Ash Analysis
Chromium	25.20	ppmw	1.73E-04	7.57E-04	Duke Energy Average Ash Analysis
Chromium VI	0.67	ppmw	4.59E-06	2.01E-05	Duke Energy Average Ash Analysis
Cobalt	12.68	ppmw	8.69E-05	3.81E-04	Duke Energy Average Ash Analysis
Manganese	54.29	ppmw	3.72E-04	1.63E-03	Duke Energy Average Ash Analysis
Mercury	0.16	ppmw	1.10E-06	4.81E-06	Duke Energy Average Ash Analysis
Nickel	23.33	ppmw	1.60E-04	7.01E-04	Duke Energy Average Ash Analysis
Selenium	8.32	ppmw	5.71E-05	2.50E-04	Duke Energy Average Ash Analysis

Notes:

1. Exhaust Flow (dSCFM):

32,000 2. PM Emission Factor (grains/dSCF) 0.025

 3. PM₁₀ =
 92%
 of Total PM (From AP-42 Table 1.1-6 (09/98))

 4. PM_{2.5} =
 53%
 of Total PM (From AP-42 Table 1.1-6 (09/98))

5. TPY = Tons per Year

Vendor Guarantee

Duke Energy H.F. Lee Plant Table 5 - Pre STAR Unit Silo Emissions

Potential Emissions

	Emission		ES-30A Feed Silo Filling (125 tph, 400,000 tpy)		ES-30B Feed Silo Unloading (75 tph, 400,000 tpy)		ES-36A Transfer Silo Filling (125 tph, 400,000 tpy)		ES-36B Transfer Silo Unloading (75 tph, 400,000 tpy)		Total Silo Emissions		
Pollutant	Factor	Units	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	Reference
PM	0.0000487	lb/ton	6.09E-03	9.74E-03	3.65E-03	9.74E-03	6.09E-03	9.74E-03	3.65E-03	9.74E-03	1.95E-02	3.90E-02	SEFA Winyah Generating Station Permit Application
PM ₁₀	0.000023	lb/ton	2.88E-03	4.60E-03	1.73E-03	4.60E-03	2.88E-03	4.60E-03	1.73E-03	4.60E-03	9.20E-03	1.84E-02	SEFA Winyah Generating Station Permit Application
PM _{2.5}	0.000023	lb/ton	2.88E-03	4.60E-03	1.73E-03	4.60E-03	2.88E-03	4.60E-03	1.73E-03	4.60E-03	9.20E-03	1.84E-02	SEFA Winyah Generating Station Permit Application
Lead	19.85	ppmw	1.21E-07	1.93E-07	7.25E-08	1.93E-07	1.21E-07	1.93E-07	7.25E-08	1.93E-07	3.87E-07	7.73E-07	Duke Energy Average Ash Analysis
Arsenic	38.55	ppmw	2.35E-07	3.75E-07	1.41E-07	3.75E-07	2.35E-07	3.75E-07	1.41E-07	3.75E-07	7.51E-07	1.50E-06	Duke Energy Average Ash Analysis
Antimony	1.28	ppmw	7.79E-09	1.25E-08	4.68E-09	1.25E-08	7.79E-09	1.25E-08	4.68E-09	1.25E-08	2.49E-08	4.99E-08	Duke Energy Average Ash Analysis
Beryllium	4.25	ppmw	2.59E-08	4.14E-08	1.55E-08	4.14E-08	2.59E-08	4.14E-08	1.55E-08	4.14E-08	8.28E-08	1.66E-07	Duke Energy Average Ash Analysis
Cadmium	0.18	ppmw	1.10E-09	1.75E-09	6.57E-10	1.75E-09	1.10E-09	1.75E-09	6.57E-10	1.75E-09	3.51E-09	7.01E-09	Duke Energy Average Ash Analysis
Chromium	25.20	ppmw	1.53E-07	2.45E-07	9.20E-08	2.45E-07	1.53E-07	2.45E-07	9.20E-08	2.45E-07	4.91E-07	9.82E-07	Duke Energy Average Ash Analysis
Chromium VI	0.67	ppmw	4.08E-09	6.53E-09	2.45E-09	6.53E-09	4.08E-09	6.53E-09	2.45E-09	6.53E-09	1.31E-08	2.61E-08	Duke Energy Average Ash Analysis
Cobalt	12.68	ppmw	7.72E-08	1.24E-07	4.63E-08	1.24E-07	7.72E-08	1.24E-07	4.63E-08	1.24E-07	2.47E-07	4.94E-07	Duke Energy Average Ash Analysis
Manganese	54.29	ppmw	3.30E-07	5.29E-07	1.98E-07	5.29E-07	3.30E-07	5.29E-07	1.98E-07	5.29E-07	1.06E-06	2.12E-06	Duke Energy Average Ash Analysis
Mercury	0.16	ppmw	9.74E-10	1.56E-09	5.84E-10	1.56E-09	9.74E-10	1.56E-09	5.84E-10	1.56E-09	3.12E-09	6.23E-09	Duke Energy Average Ash Analysis
Nickel	23.33	ppmw	1.42E-07	2.27E-07	8.52E-08	2.27E-07	1.42E-07	2.27E-07	8.52E-08	2.27E-07	4.54E-07	9.09E-07	Duke Energy Average Ash Analysis
Selenium	8.32	ppmw	5.06E-08	8.10E-08	3.04E-08	8.10E-08	5.06E-08	8.10E-08	3.04E-08	8.10E-08	1.62E-07	3.24E-07	Duke Energy Average Ash Analysis

Note: HAP/TAP emission factors for the fly ash is based on site-specific ash analysis without the addition of metals in the water used for water injection.

Sample Calculations

PM ₁₀ Emissions =	0.000023 lb PM ₁₀ ton ash	125 ton ash hour	=	2.88E-03	lb/hr PM ₁₀		
PM ₁₀ Emissions =	0.000023 lb PM ₁₀ ton ash	400,000 tons year	ash	ton 2000 lb	_ =	4.60E-03	tpy PM ₁₀
Arsenic Emissions =	38.55 lb As 10 ⁶ lb	0.00609 lb PM hr	=	2.35E-07	lb/hr Arsenic		

Duke Energy H.F. Lee Plant Table 6 - Post STAR Unit Silos and Dome Emissions

Potential Emissions

	Emission		ES-38 Lo (300 tph,	oadout Silo 400,000 tpy)	ES-38A Loa (100 tp	dout Silo Chute 1A h, 200,000 tpy)	ES-38B Load (100 tph	lout Silo Chute 1B , 200,000 tpy)	ES-37A Sto (75 tph	rage Dome Filling , 400,000 tpy)	ES-37B S Uni (275 tph,	itorage Dome loading _400,000 tpy)	Total Silo	Emissions	
Pollutant	Factor	Units	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	lb/hr	ton/yr	Reference
PM	0.0000487	lb/ton	1.46E-02	9.74E-03	4.87E-03	4.87E-03	4.87E-03	4.87E-03	3.65E-03	9.74E-03	1.34E-02	9.74E-03	4.14E-02	3.90E-02	SEFA Winyah Generating Station Permit Application
PM ₁₀	0.000023	lb/ton	6.90E-03	4.60E-03	2.30E-03	2.30E-03	2.30E-03	2.30E-03	1.73E-03	4.60E-03	6.33E-03	4.60E-03	1.96E-02	1.84E-02	SEFA Winyah Generating Station Permit Application
PM _{2.5}	0.000023	lb/ton	6.90E-03	4.60E-03	2.30E-03	2.30E-03	2.30E-03	2.30E-03	1.73E-03	4.60E-03	6.33E-03	4.60E-03	1.96E-02	1.84E-02	SEFA Winyah Generating Station Permit Application
Lead	19.85	ppmw	2.90E-07	1.93E-07	9.67E-08	9.67E-08	9.67E-08	9.67E-08	7.25E-08	1.93E-07	2.66E-07	1.93E-07	8.22E-07	7.73E-07	Duke Energy Average Ash Analysis and Water Injection
Arsenic	38.58	ppmw	5.64E-07	3.76E-07	1.88E-07	1.88E-07	1.88E-07	1.88E-07	1.41E-07	3.76E-07	5.17E-07	3.76E-07	1.60E-06	1.50E-06	Duke Energy Average Ash Analysis and Water Injection
Antimony	1.28	ppmw	1.88E-08	1.25E-08	6.25E-09	6.25E-09	6.25E-09	6.25E-09	4.69E-09	1.25E-08	1.72E-08	1.25E-08	5.31E-08	5.00E-08	Duke Energy Average Ash Analysis and Water Injection
Beryllium	4.25	ppmw	6.21E-08	4.14E-08	2.07E-08	2.07E-08	2.07E-08	2.07E-08	1.55E-08	4.14E-08	5.69E-08	4.14E-08	1.76E-07	1.66E-07	Duke Energy Average Ash Analysis and Water Injection
Cadmium	0.18	ppmw	2.64E-09	1.76E-09	8.79E-10	8.79E-10	8.79E-10	8.79E-10	6.59E-10	1.76E-09	2.42E-09	1.76E-09	7.47E-09	7.03E-09	Duke Energy Average Ash Analysis and Water Injection
Chromium	25.20	ppmw	3.68E-07	2.45E-07	1.23E-07	1.23E-07	1.23E-07	1.23E-07	9.21E-08	2.45E-07	3.38E-07	2.45E-07	1.04E-06	9.82E-07	Duke Energy Average Ash Analysis and Water Injection
Chromium VI	0.67	ppmw	9.79E-09	6.53E-09	3.26E-09	3.26E-09	3.26E-09	3.26E-09	2.45E-09	6.53E-09	8.97E-09	6.53E-09	2.77E-08	2.61E-08	Duke Energy Average Ash Analysis and Water Injection
Cobalt	12.68	ppmw	1.85E-07	1.24E-07	6.18E-08	6.18E-08	6.18E-08	6.18E-08	4.63E-08	1.24E-07	1.70E-07	1.24E-07	5.25E-07	4.94E-07	Duke Energy Average Ash Analysis and Water Injection
Manganese	54.31	ppmw	7.93E-07	5.29E-07	2.64E-07	2.64E-07	2.64E-07	2.64E-07	1.98E-07	5.29E-07	7.27E-07	5.29E-07	2.25E-06	2.12E-06	Duke Energy Average Ash Analysis and Water Injection
Mercury	0.16	ppmw	2.34E-09	1.56E-09	7.79E-10	7.79E-10	7.79E-10	7.79E-10	5.84E-10	1.56E-09	2.14E-09	1.56E-09	6.62E-09	6.23E-09	Duke Energy Average Ash Analysis and Water Injection
Nickel	23.34	ppmw	3.41E-07	2.27E-07	1.14E-07	1.14E-07	1.14E-07	1.14E-07	8.52E-08	2.27E-07	3.13E-07	2.27E-07	9.66E-07	9.09E-07	Duke Energy Average Ash Analysis and Water Injection
Selenium	8.43	ppmw	1.23E-07	8.21E-08	4.10E-08	4.10E-08	4.10E-08	4.10E-08	3.08E-08	8.21E-08	1.13E-07	8.21E-08	3.49E-07	3.28E-07	Duke Energy Average Ash Analysis and Water Injection

Note: HAP/TAP emission factors for the fly ash is based on site-specific ash analysis with the addition of metals in the water used for water injection.

Sample Calculations

PM ₁₀ Emissions =	0.000023 lb PM ₁₀ ton ash	300 ton ash hour	=	6.90E-03	lb/hr PM ₁₀		
PM ₁₀ Emissions =	0.000023 lb PM ₁ ton ash	400,000 ye	tons ash ear	ton 2000 lb	_ =	4.60E-03	tpy PM ₁₀
Arsenic Emissions =	38.58 lb As 10 ⁶ lb	0.0146 lb PM hr	=	5.64E-07	/ Ib/hr Arsenic		

Duke Energy H.F. Lee Plant Table 7 - Pollution Control Silos

	Est. Gas Flow,	PM loading Rate,	ES-32 FGD B	yproduct Silo	ES-33 FGD A	bsorbent Silo	То	tal
Pollutant	acfm	gr/acf	lb/hr	tpy	lb/hr	tpy	lb/hr	tpy
PM	1300	0.005	0.06	0.24	0.06	0.24	0.11	0.49
PM ₁₀ (Note 2)	1300	0.005	0.05	0.22	0.05	0.22	0.10	0.45
PM _{2.5} (Note 3)	1300	0.005	0.03	0.13	0.03	0.13	0.06	0.26

Notes:

1. PM Emission Factor (grains/acf)

 2. PM₁₀ =
 92%
 of Total PM (From AP-42 Table 1.1-6 (09/98))

 3. PM_{2.5} =
 53%
 of Total PM (From AP-42 Table 1.1-6 (09/98))

4. lb/hr = pounds per hour; tpy = Tons per Year

Duke Energy H.F. Lee Plant Wet Ash Receiving Emissions (F-1 and F-2)

Table 8A - Transfer of material to storage shed (F-1)

Section 13.2-4 Aggregate Handling and Storage Piles, Ap-42 Fifth Edition November 2006

E= k*	0.0032 * (((U/5)^1.3)	/((M/2)^1.4))	
E =	lb/ton		
k =	particle s	ize multiplier (dimensionless)	
	PM	0.74	
	PM ₁₀	0.35	
	PM _{2.5}	0.053	
U =	mean wir	nd speed, miles per hour (mph) 2	Average wind speed for 2016 Rosewood Weather Station approximately 1 mile from the site. Source: weatherunderground.com
M =	material	moisture content	15% moisture content is an conservatively low estimate typical moisture is 20%
		15	
	70 tph 400,000 tpy	Based on Air Data Tracking S	heet, Item 13

	lb/hr	tpy
PM	1.50E-03	4.29E-03
PM ₁₀	7.09E-04	2.03E-03
PM _{2.5}	1.07E-04	3.07E-04

Note: assumed 50% control as a result of the shed having three side to enclose pile

			Emis	sions	
Pollutant	Emission Factor	Units	lb/hr	ton/yr	Reference
Lead	19.85	ppmw	2.98E-08	8.51E-08	Duke Energy Average Ash Analysis
Arsenic	38.55	ppmw	5.78E-08	1.65E-07	Duke Energy Average Ash Analysis
Antimony	1.28	ppmw	1.92E-09	5.49E-09	Duke Energy Average Ash Analysis
Beryllium	4.25	ppmw	6.37E-09	1.82E-08	Duke Energy Average Ash Analysis
Cadmium	0.18	ppmw	2.70E-10	7.71E-10	Duke Energy Average Ash Analysis
Chromium	25.20	ppmw	3.78E-08	1.08E-07	Duke Energy Average Ash Analysis
Chromium VI	0.67	ppmw	1.00E-09	2.87E-09	Duke Energy Average Ash Analysis
Cobalt	12.68	ppmw	1.90E-08	5.43E-08	Duke Energy Average Ash Analysis
Manganese	54.29	ppmw	8.14E-08	2.33E-07	Duke Energy Average Ash Analysis
Mercury	0.16	ppmw	2.40E-10	6.86E-10	Duke Energy Average Ash Analysis
Nickel	23.33	ppmw	3.50E-08	1.00E-07	Duke Energy Average Ash Analysis
Selenium	8.32	ppmw	1.25E-08	3.57E-08	Duke Energy Average Ash Analysis

Note: HAP/TAP emission factors for the fly ash is based on site-specific ash analysis without the addition of metals in the water used for water injection.

Duke Energy H.F. Lee Plant Wet Ash Receiving Emissions (F-1 and F-2)

Table 8B - Transfer of material to hopper (F-2)

Section 13.2-4 Aggregate Handling and Storage Piles, Ap-42 Fifth Edition November 2006

E= k*0.0032 * (((U/5)^1.3)/((M/2)^1.4))

E = k =	lb/ton particle size	multiplier (dimensionless)	
	PM PM	0.74	
	PM ₁₀ PM _{2.5}	0.053	
U =	mean wind s	peed, miles per hour (mph) 2	Average wind speed for 2016 Rosewood Weather Station approximately 1 mile from the site. Source: weatherunderground.com
M =	material moi	sture content 5	15% moisture content is an conservatively low estimate typical moisture is 20%
	70 tph	-	

400,000 tpy

Based on Air Data Tracking Sheet, Item 13

	lb/hr	tpy
PM	3.00E-03	8.57E-03
PM ₁₀	1.42E-03	4.05E-03
PM _{2.5}	2.15E-04	6.14E-04

			Emis	sions	
Pollutant	Emission Factor	Units	lb/hr	ton/yr	Reference
Lead	19.85	ppmw	5.95E-08	1.70E-07	Duke Energy Average Ash Analysis
Arsenic	38.55	ppmw	1.16E-07	3.30E-07	Duke Energy Average Ash Analysis
Antimony	1.28	ppmw	3.84E-09	1.10E-08	Duke Energy Average Ash Analysis
Beryllium	4.25	ppmw	1.27E-08	3.64E-08	Duke Energy Average Ash Analysis
Cadmium	0.18	ppmw	5.40E-10	1.54E-09	Duke Energy Average Ash Analysis
Chromium	25.20	ppmw	7.56E-08	2.16E-07	Duke Energy Average Ash Analysis
Chromium VI	0.67	ppmw	2.01E-09	5.74E-09	Duke Energy Average Ash Analysis
Cobalt	12.68	ppmw	3.80E-08	1.09E-07	Duke Energy Average Ash Analysis
Manganese	54.29	ppmw	1.63E-07	4.65E-07	Duke Energy Average Ash Analysis
Mercury	0.16	ppmw	4.80E-10	1.37E-09	Duke Energy Average Ash Analysis
Nickel	23.33	ppmw	7.00E-08	2.00E-07	Duke Energy Average Ash Analysis
Selenium	8.32	ppmw	2.50E-08	7.13E-08	Duke Energy Average Ash Analysis

Note: HAP/TAP emission factors for the fly ash is based on site-specific ash analysis without the addition of metals in the water used for water injection.

Duke Energy H.F. Lee Plant Wet Ash Receiving Emissions (F-1 and F-2)

Total Emissions

Pollutant	lb/hr	tpy
PM	4.50E-03	1.29E-02
PM ₁₀	2.13E-03	6.08E-03
PM _{2.5}	3.22E-04	9.21E-04
Lead	8.93E-08	2.55E-07
Arsenic	1.73E-07	4.96E-07
Antimony	5.76E-09	1.65E-08
Beryllium	1.91E-08	5.46E-08
Cadmium	8.10E-10	2.31E-09
Chromium	1.13E-07	3.24E-07
Chromium VI	3.01E-09	8.61E-09
Cobalt	5.71E-08	1.63E-07
Manganese	2.44E-07	6.98E-07
Mercury	7.20E-10	2.06E-09
Nickel	1.05E-07	3.00E-07
Selenium	3.74E-08	1.07E-07

Duke Energy H.F. Lee Plant Table 9 - GHG Emissions

1,028	btu/scf	Table C-1 to subpart C of 40 CFR Part 98 (natural gas)
15,840	MMBtu/yr	Total Supplemental / Auxiliary Fuel = 12 months x 3 cold starts x 400 MM Btu = 14,400 MM Btu's + 10% = 15,840 MM Btu's per year.
24 8,760	hrs/day hrs/year	
53.06	kg CO ₂ /MMBtu	Table C-1 to subpart C of 40 CFR Part 98 (natural gas)
1.00E-03	kg CH₄/MMBtu	Table C-2 to subpart C of 40 CFR Part 98 (natural gas)
1.00E-04	kg N ₂ O/MMBtu	Table C-2 to subpart C of 40 CFR Part 98 (natural gas)
2.20462	lb/kg	Table A-2 to subpart A of 40 CFR Part 98
116.98	lb/MMBtu	
2.20E-03	lb/MMBtu	
2.20E-04	lb/MMBtu	
	1,028 15,840 24 8,760 53.06 1.00E-03 1.00E-04 2.20462 116.98 2.20E-03 2.20E-03 2.20E-04	1,028 btu/scf 15,840 MMBtu/yr 24 hrs/day 8,760 hrs/year 53.06 kg CO2/MMBtu 1.00E-03 kg CH4/MMBtu 1.00E-04 lb/kg 2.20462 lb/kg 116.98 lb/MMBtu 2.20E-03 lb/MMBtu b/MMBtu lb/MMBtu

Global Warming Potential		
CO ₂	1	Table A-1 to subpart A of 40 CFR Part 98
CH ₄	25	Table A-1 to subpart A of 40 CFR Part 98
N ₂ O	298	Table A-1 to subpart A of 40 CFR Part 98

Emission Rates - GHG (CO2e)

CO ₂	lb/yr 1.852.917.85	tpy 926,46
CH_4 (CO ₂ e)	873.03	0.44
N ₂ O (CO2e)	1,040.65	0.52
GHG (CO ₂ e)		927.42
	lb/yr	tpy
CO ₂	lb/yr 1,852,917.85	tpy 926.46
CO ₂ CH ₄	lb/yr 1,852,917.85 34.92	tpy 926.46 0.02
CO ₂ CH ₄ N ₂ O	lb/yr 1,852,917.85 34.92 3.49	tpy 926.46 0.02 0.00

Duke Energy H.F. Lee Plant Table 9 - GHG Emissions

Heating Value of Propane	0.091	MMBtu/gal	Table C-1 to subpart C of 40 CFR Part 98 (petroleum products)
Heat Input	15,840	MMBtu/yr	
Emission Factors			
CO ₂	61.46	kg CO ₂ /MMBtu	Table C-1 to subpart C of 40 CFR Part 98 (propane - petroleum products)
CH ₄	3.00E-03	kg CH₄/MMBtu	Table C-2 to subpart C of 40 CFR Part 98 (petroleum)
N ₂ O	6.00E-04	kg N ₂ O/MMBtu	Table C-2 to subpart C of 40 CFR Part 98 (petroleum)
	2.20462	lb/kg	Table A-2 to subpart A of 40 CFR Part 98
CO ₂	135.50	lb/MMBtu	
CH ₄	6.61E-03	lb/MMBtu	
N ₂ O	1.32E-03	lb/MMBtu	

Global Warming Potential		
CO ₂	1	Table A-1 to subpart A of 40 CFR Part 98
CH ₄	25	Table A-1 to subpart A of 40 CFR Part 98
N ₂ O	298	Table A-1 to subpart A of 40 CFR Part 98

Emission Rates - GHG (CO2e)

	lb/yr	tpy
CO ₂	2,146,255.77	1,073.13
$CH_4(CO_2e)$	2,619.09	1.31
N ₂ O (CO2e)	6,243.91	3.12
GHG (CO ₂ e)		1,077.56
	lb/yr	tpy
CO ₂	2,146,255.77	1,073.13
CH ₄	104.76	0.05
CH ₄ N ₂ O	104.76 20.95	0.05 0.01

STAR CO₂ Production

Yearly Feed Rate (TPY) Average Feed LOI Availability	400,000 7.80% 80.00%	
Avg. Feed Rate (TPH)	57.08	400,000/ (8760*80%)
Avg. Fuel Input (MMBtu/hr)	129.11	57.08*2000*7.80%*14500/1000000
Max. CO ₂ Production (TPY)	114,401	57.08*2000*7.80%*3.6667*8760*80%/2000

Expected GHG Emission Range				
_	Natural Gas	Propane	Fly Ash	Total
CO ₂	926.46	1,073.13	114,401	116,400.63
$CH_4(CO_2e)$	0.44	1.31		1.75
N ₂ O (CO2e)	0.52	3.12		3.64
GHG (CO ₂ e)				116,406.02
CO ₂	926.46	1,073.13	114,401	116,400.63
CH ₄	0.02	0.05		0.07
N ₂ O	0.00	0.01		0.01
GHG (Mass Basis)				116,400.71

Duke Energy H.F. Lee Plant Table 10 - Unloading Pile Windblown Fugitive Dust Emissions (F-3)

Section 13.2.5 of the U.S. EPA's AP-42 document was used to estimate emissions.

The first step is to calculate a height-to-base ratio to determine if Equation (4) can be used to determine the friction velocity (u*):

0.33	acres, Acreage of Fly Ash Pile
4,046.9	m ² /acre, Conversion Factor
1,335.5	m ² , Typical Active Area

Assuming a square area, this active area yields an approximate length as follows:

36.5	m, Linear Dimension of Active Area
3.3	ft/m, Conversion Factor
119.9	ft, Linear Dimension of Active Area

4 ft, Approximate Mean Elevation of the Active Area (Above Grade)

Per page 13.2.5-5 of AP-42, if the height to base ratio is less than 0.2 then Equation (4) can be used to calculate the friction velocity (u*).

0.033 Calculated Height to Base Ratio

Therefore equation (4) from AP-42 13.2.5 can be used for calculation of the friction velocity.

Per the following website: http://www.nc-climate.ncsu.edu/dynamic_scripts/cronos/query.php (maintained by the North Carolina State Climate Office), the anemometer height for the fastest mile data is:

10 m, Anemometer Height

Since the reported fastest wind speeds are from an anemometer of height 10 m, using equation (5) on page 13.2.5-6 is not necessary:

When the calculated friction velocity (u^*) exceeds the threshold friction velocity (u_t^*), emissions from wind erosion occur. As shown in Equation 3 of AP-42, if $u^* \le u_t^*$, emissions are zero.

From Table 13.2.5-1 threshold friction velocity (ut*) is as follows. The most conservative value presented in AP-42 has been used.

0.43 m/s, ut* Threshold Friction Velocity

Therefore, in order to generate emissions, the following wind speed must be exceeded.

3,600 sec/hr, Conversion Factor 1,609.3 m/mile, Conversion Factor

18.15 mph, u₁₀⁺ 8.11 m/s, u₁₀⁺ 0.43 m/s, u*

Duke Energy H.F. Lee Plant Table 10 - Unloading Pile Windblown Fugitive Dust Emissions (F-3)

AERMOD allows users to account for the variability of wind speed when determining offsite impacts. The scalars below are used based on the respective wind speed range. (AERMOD User Guide 3.3.4. Using Variable Emission Rates). There are zero wind based emissions in classes 1 thru 4 because the threshold friction velocity is not exceeded (ut*). The scalar for Class 5 is determined as the ratio of emission factors for Class 5 and Class 6. Emission factor derivation follows.

Wind Speed Range Class	1	2	3	4	5	6
Scalar	0	0	0	0	0.77	1.00
where:						
Class 1 =	0 - 3.4 mph					
Class 2 =	3.4 - 6.8 mph					
Class 3 =	6.8 - 11.3 mph					
Class 4 =	11.3 - 18.1 mph					
Class 5 =	18.1 - 23.8 mph					
Class 6 =	greater than 23.8 n	nph				

The emissions rate (which is dependent on the friction velocity (u^{*})) varies linearly with wind speed. For Class 5, emissions will increase linearly as wind speed increases. AERMOD does not facilitate the variable emission rates based on wind speed. Therefore, the friction velocity for Class 5 is determined using the upper end wind speed of 23.8 mph. Using Equation (4) on page 13.2.5-5, the equivalent friction velocity (u^{*}) may be calculated.

 $u^* = 0.053u_{10}^+$ 23.8 mph, u_{10}^+ 23.8 m/s, u_{10}^+ Class 5 0.56 m/s, u*, Class 5 Wind Speed Range

The friction velocity for Class 6 is determined using the average of the maximum daily wind gusts for each month.



Emission factors for Class 5 and Class 6 are determined using AP-42 Section 13.2.5 Equation (3) which is shown below:

$$PM\left(\frac{g}{m^2}\right) = 58(u^* - u^*)^2 + 25(u^* - u^*)$$

Equation (3) from AP-42 13.2.5

Where:

 u^* is the friction velocity (m/s) u^*_t is the threshold friction velocity (m/s)

Class 54.39g/m² (of Disturbed Area), Class 5 Wind Speed RangeClass 65.67g/m² (of Disturbed Area), Class 6 Wind Speed Range

Duke Energy H.F. Lee Plant

Table 10 - Unloading Pile Windblown Fugitive Dust Emissions (F-3)

As stated in AP-42, on page 13.2.5-2, emissions generated by wind erosion are also dependent on the frequency of disturbance of the erodible surface because each time that a surface is disturbed, its erosion potential is restored. A disturbance is defined as an action that results in the exposure of fresh surface material. Only a fraction of the active area is disturbed each day. This disturbed area is used to calculate the potential daily emission rate.

	0.33 acres, Working Area 100% Fraction of Active Area Disturbed Daily 1,335.47 m ² , Average Area Disturbed Daily	0% 0.00	Fraction of Inactive Area m ² , Average Inactive Area
	453.6 g/lb, Conversion Factor	453.6	g/lb, Conversion Factor
Class 5 Class 6	12.9 lb/day 16.7 lb/day	Class 5 0.0 Class 6 0.0	lb/day lb/day

The facility will implement mitigation to suppress dust emissions. Control efficiencies are based on engineering judgment and supported by *WRAP Fugitive Dust Handbook, September 7, 2006.* The controlled emission rates for Class 5 and Class 6 emissions are as follows:

	61% Apply Water every 3.2 ho	ours to disturbed areas	80%	Inherent Moisture and Watering
Class 5**	5.0 lb/day	Class 5	0.0	lb/day
Class 6**	6.5 lb/day	Class 6	0.0	lb/day

For the purposes of determining potential emissions for permitting, wind data has been applied as shown below.

Total Class 5 Emissions	5.0	lb/day
Total Class 6 Emissions	6.5	lb/day

Fraction of time in Class 50.0120 (approximately 105 hours in Class 5)Fraction of time in Class 60.0023 (approximately 20 hours in Class 6)

Time fraction spent in Class 5 and Class 6 determined by analyzing hourly wind speeds for the 5 year period required to be modeled 2012-2016 from DAQ Approved Met Data. The worst case year (year with the most hours) was used to determine the time fraction. For Class 5 it was 2016 and for Class 6 it was 2015.

Total emissions per day 0.08 lb/day

Emissions from the unloading pile will only occur when Class 5 and Class 6 wind speed conditions are met. AERMOD will utilize meteorological data to determine when these conditions occur. For the purposes of the PSD analysis, permitting, and TPER evaluation, it is conservatively assumed that Class 6 condition occur year round.

Compound	Avg Ash Analysis (ppm)	Emissions (lb/hr)	Emissions (lb/day)	Emissions (lb/yr)	Emissions (ton/yr)
PM	1.00 **	0.003	0.08	27.47	0.01
PM ₁₀	0.50 **	0.002	0.04	13.73	0.007
PM _{2.5}	0.08 **	0.0002	0.006	2.06	0.001
Lead	19.85	6.22E-08	1.49E-06	5.45E-04	2.73E-07
Arsenic	38.55	1.21E-07	2.90E-06	1.06E-03	5.29E-07
Antimony	1.28	4.01E-09	9.63E-08	3.52E-05	1.76E-08
Beryllium	4.25	1.33E-08	3.20E-07	1.17E-04	5.84E-08
Cadmium	0.18	5.64E-10	1.35E-08	4.94E-06	2.47E-09
Chromium	25.20	7.90E-08	1.90E-06	6.92E-04	3.46E-07
Chromium VI	0.67	2.10E-09	5.04E-08	1.84E-05	9.20E-09
Cobalt	12.68	3.98E-08	9.54E-07	3.48E-04	1.74E-07
Manganese	54.29	1.70E-07	4.09E-06	1.49E-03	7.46E-07
Mercury	0.16	5.02E-10	1.20E-08	4.39E-06	2.20E-09
Nickel	23.33	7.32E-08	1.76E-06	6.41E-04	3.20E-07
Selenium	8.32	2.61E-08	6.26E-07	2.29E-04	1.14E-07

HAP/TAP emission factors for the fly ash is based on site-specific ash analysis without the addition of metals in the water used for water injection.

** PM distribution factors (k value) taken from AP-42 Page 13.2.5-3 All other values in ppm.

Duke Energy H.F. Lee Plant Table 11 - Emissions Estimate: Wind Erosion at the Ash Basin (F-4)

Dust may be generated by wind erosion of exposed area within an industrial facility. Section 13.2.5 of the U.S. EPA's AP-42 document was used to estimate emissions.

The first step is to calculate a height-to-base ratio to determine if Equation (4) can be used to determine the friction velocity (u*):

321	acres, Typical Active Area of Ash Pond
4,046.9	m ² /acre, Conversion Factor
1,299,045.3	m ² , Typical Active Area

Assuming a square area, this active area yields an approximate length as follows:

1139.8 i	m, Linear Dimension of Active Area
3.3 f	it/m, Conversion Factor
3739.4 f	it, Linear Dimension of Active Area
15]f	it, Approximate Mean Elevation of the Active Area (Above Grade)

Per page 13.2.5-5 of AP-42, if the height to base ratio is less than 0.2 then Equation (4) can be used to calculate the friction velocity (u*).

0.004 Calculated Height to Base Ratio

Therefore equation (4) from AP-42 13.2.5 can be used for calculation of the friction velocity.

Per the following website: http://www.nc-climate.ncsu.edu/dynamic_scripts/cronos/query.php (maintained by the North Carolina State Climate Office), the anemometer height for the fastest mile data is:

10 m, Anemometer Height

Since the reported fastest wind speeds are from an anemometer of height 10 m, using equation (5) on page 13.2.5-6 is not necessary:

When the calculated friction velocity (u^*) exceeds the threshold friction velocity (u_t^*), emissions from wind erosion occur. As shown in Equation 3 of AP-42, if $u^* \le u_t^*$, emissions are zero.

From Table 13.2.5-1 threshold friction velocity (ut*) is as follows. The most conservative value presented in AP-42 has been used.

0.43 m/s, ut* Threshold Friction Velocity

Therefore, in order to generate emissions, the following wind speed must be exceeded.

3,600 sec/hr, Conversion Factor 1,609.3 m/mile, Conversion Factor



Duke Energy H.F. Lee Plant Table 11 - Emissions Estimate: Wind Erosion at the Ash Basin (F-4)

AERMOD allows users to account for the variability of wind speed when determining offsite impacts. The scalars below are used based on the respective wind speed range. (AERMOD User Guide 3.3.4. Using Variable Emission Rates). There are zero wind based emissions in classes 1 thru 4 because the threshold friction velocity is not exceeded (ut*). The scalar for Class 5 is determined as the ratio of emission factors for Class 5 and Class 6. Emission factor derivation follows.

Wind Speed Range Class	1	2	3	4	5	6
Scalar	0	0	0	0	0.77	1.00
where:						
Class 1 =	0 - 3.4 mph					
Class 2 =	3.4 - 6.8 mph					
Class 3 =	6.8 - 11.3 mpl	h				
Class 4 =	11.3 - 18.1 m	ph				
Class 5 =	18.1 - 23.8 m	ph				
Class 6 =	greater than	23.8 mph				
	-					

The emissions rate (which is dependent on the friction velocity (u*)) varies linearly with wind speed. For Class 5, emissions will increase linearly as wind speed increases. AERMOD does not facilitate the variable emission rates based on wind speed. Therefore, the friction velocity for Class 5 is determined using the upper end wind speed of 23.8 mph. Using Equation (4) on page 13.2.5-5, the equivalent friction velocity (u*) may be calculated.

 $u^* = 0.053u_{10}^+$ 23.8 mph, u_{10}^+ 23.8 m/s, u_{10}^+ Class 5 0.56 m/s, u*, Class 5 Wind Speed Range

The friction velocity for Class 6 is determined using the average of the maximum daily wind gusts for each month.



Emission factors for Class 5 and Class 6 are determined using AP-42 Section 13.2.5 Equation (3) which is shown below:

$$PM\left(\frac{g}{m^2}\right) = 58(u^* - u^*)^2 + 25(u^* - u^*)$$

Equation (3) from AP-42 13.2.5

Where:

 u^* is the friction velocity (m/s) u^*_t is the threshold friction velocity (m/s)

Class 54.39 g/m² (of Disturbed Area), Class 5 Wind Speed RangeClass 65.67 g/m² (of Disturbed Area), Class 6 Wind Speed Range

Duke Energy H.F. Lee Plant

Table 11 - Emissions Estimate: Wind Erosion at the Ash Basin (F-4)

As stated in AP-42, on page 13.2.5-2, emissions generated by wind erosion are also dependent on the frequency of disturbance of the erodible surface because each time that a surface is disturbed, its erosion potential is restored. A disturbance is defined as an action that results in the exposure of fresh surface material. Only a fraction of the active area is disturbed each day. This disturbed area is used to calculate the potential daily emission rate.

	10 acres, Working Area 3% Fraction of Active Area Disturbed Daily 40,468.70 m ² , Average Area Disturbed Daily	97% Fraction of Inactive Area 1,258,576.57 m ² , Average Inactive Area
	453.6 g/lb, Conversion Factor	453.6 g/lb, Conversion Factor
Class 5 Class 6	391.4 lb/day 506.2 lb/day	Class 5 12173.0 lb/day Class 6 15741.3 lb/day

The facility will implement mitigation to suppress dust emissions. Control efficiencies are based on engineering judgment and supported by *WRAP Fugitive Dust Handbook, September 7, 2006.* The controlled emission rates for Class 5 and Class 6 emissions are as follows:

	61% Apply Water every 3.2 ho	urs to disturbed areas	80%	Inherent Moisture and Watering
Class 5**	152.7 lb/day	Class 5	2434.6	lb/day
Class 6**	197.4 lb/day	Class 6	3148.3	lb/day

For the purposes of determining potential emissions for permitting, wind data has been applied as shown below.

Total Class 5 Emissions	2587.3	lb/day
Total Class 6 Emissions	3345.7	lb/day

Fraction of time in Class 50.0120 (approximately 105 hours in Class 5)Fraction of time in Class 60.0023 (approximately 20 hours in Class 6)

Time fraction spent in Class 5 and Class 6 determined by analyzing hourly wind speeds for the 5 year period required to be modeled 2012-2016 from DAQ Approved Met Data. The worst case year (year with the most hours) was used to determine the time fraction. For Class 5 it was 2016 and for Class 6 it was 2015.

Total emissions per day 38.65 lb/day

Emissions from the ash pond will only occur when Class 5 and Class 6 wind speed conditions are met. AERMOD will utilize meteorological data to determine when these conditions occur. For the purposes of the PSD analysis, permitting, and TPER evaluation, it is conservatively assumed that Class 6 condition occur year round.

Compound	Avg Ash Analysis (ppm)	Emissions (Ib/hr)	Emissions (Ib/day)	Emissions (lb/yr)	Emissions (ton/yr)
PM	1.00 **	1.61	38.65	14,107.30	7.05
PM ₁₀	0.50 **	0.81	19.33	7,053.65	3.53
PM _{2.5}	0.08 **	0.12	2.90	1,058.05	0.53
Lead	19.85	3.20E-05	7.67E-04	2.80E-01	1.40E-04
Arsenic	38.55	6.21E-05	1.49E-03	5.44E-01	2.72E-04
Antimony	1.28	2.06E-06	4.95E-05	1.81E-02	9.03E-06
Beryllium	4.25	6.84E-06	1.64E-04	6.00E-02	3.00E-05
Cadmium	0.18	2.90E-07	6.96E-06	2.54E-03	1.27E-06
Chromium	25.20	4.06E-05	9.74E-04	3.56E-01	1.78E-04
Chromium VI	0.67	1.08E-06	2.59E-05	9.45E-03	4.73E-06
Cobalt	12.68	2.04E-05	4.90E-04	1.79E-01	8.94E-05
Manganese	54.29	8.74E-05	2.10E-03	7.66E-01	3.83E-04
Mercury	0.16	2.58E-07	6.18E-06	2.26E-03	1.13E-06
Nickel	23.33	3.76E-05	9.02E-04	3.29E-01	1.65E-04
Selenium	8.32	1.34E-05	3.22E-04	1.17E-01	5.87E-05

HAP/TAP emission factors for the fly ash is based on site-specific ash analysis without the addition of metals in the water used for water injection.

** PM distribution factors (k value) taken from AP-42 Page 13.2.5-3 All other values in ppm.

Duke Energy H.F. Lee Plant Table 12 - Emissions Estimate: Ash Handling Operations (F-5)

Where:

Section 13.2.4 (Aggregate Handling and Storage Piles) of U.S. EPA's AP-42 document is used to estimate emissions from the handling of material at an industrial site. The "Drop Equation" is shown below:



E is the emission factor in [lb/ton]

K is the particle size multiplier [dimensionless] U is the average wind speed [mph]

M is the average moisture content [%]



 Constant
 PM_{2.5}
 PM₁₀
 PM

 k
 0.053
 0.35
 0.74

 Wind data from Rocky Mount - Wilson Airport 2012-2016

The HAP and TAP emissions are derived from the PM estimate based on the average trace element analysis: Emissions are calculated assuming a maximum throughput of ash:



					Total
Ash Trace Element	Average	Emission	Annual	Annual	Annual
Analysis	Concentration	Factor	PTE	PTE	PTE
_	(ppm)	(lb/ton)	(lb/yr)	(lb/hr)	(ton/yr)
PM		2.18E-04	281.74	0.03	0.14
PM ₁₀		1.03E-04	133.26	0.02	0.07
PM _{2.5}		1.56E-05	20.18	0.002	0.01
Lead	19.85	4.34E-09	5.59E-03	6.38E-07	2.80E-06
Arsenic	38.55	8.42E-09	1.09E-02	1.24E-06	5.43E-06
Antimony	1.28	2.80E-10	3.61E-04	4.12E-08	1.80E-07
Beryllium	4.25	9.28E-10	1.20E-03	1.37E-07	5.99E-07
Cadmium	0.18	3.93E-11	5.07E-05	5.79E-09	2.54E-08
Chromium	25.20	5.50E-09	7.10E-03	8.10E-07	3.55E-06
Chromium VI	0.67	1.46E-10	1.89E-04	2.15E-08	9.44E-08
Cobalt	12.68	2.77E-09	3.57E-03	4.08E-07	1.79E-06
Manganese	54.29	1.19E-08	1.53E-02	1.75E-06	7.65E-06
Mercury	0.16	3.49E-11	4.51E-05	5.15E-09	2.25E-08
Nickel	23.33	5.10E-09	6.57E-03	7.50E-07	3.29E-06
Selenium	8.32	1.82E-09	2.34E-03	2.68E-07	1.17E-06

Note: HAP/TAP emission factors for the fly ash is based on site-specific ash analysis without the addition of metals in the water used for water injection.

Duke Energy H.F. Lee Plant Table 13A - Truck Traffic VMT Estimates

	Ash Trucked Offsite (ton/yr)	Truck Capacity (ton/truck)	Truck Loads/Year	Route Distance (miles)	Total Miles Traveled VMT/yr	Total VMT/yr
Empty Trucks to Loading Area	430.000	25.00	17 200	2.33	40,076.00	80 152 00
Loaded Trucks to Offsite	430,000	23.00	17,200	2.33	40,076.00	00,152.00

H. F. Lee Approximate Haul Routes



• Override 1	Lay of Land Area
CCP Site Contacts	Unknown, Eng. Wetlands, Landfill, Other
<all other="" values=""></all>	<all other="" values=""></all>
Active Basin	Active Basin
Currently Being Excavated	Currently Being Excavated
Inactive	Inactive

Lay of Land Area
Unknown, Eng. Wetlands, Landfill, Other
Duke Energy
Piedmont Natural Gas
Counties

0 0.175 0.35 0.7 km

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Duke Energy H.F. Lee Plant Table 13B - Additional Haul Roads Supporting the Movement of Ash Offsite - Loaded Trucks (F-6)

A portion of the ash will be moved by truck to an offsite location. Particulate emissions are generated from the haul roads from the force of the wheels on the road surface. This force causes pulverization of the surface material. The particles are lifted and dropped from the rolling wheels and the road surface is exposed to strong air currents, which generate airborne particulate emissions.

The methodology presented below is taken from Section 13.2.2 (Unpaved Roads) of the U.S. EPA's AP-42 document and is based on the vehicle miles traveled (VMT) at the site.



Where: E is the size-specific emission factor (lb/VMT) s is the surface material silt content (%) W is the mean vehicle weight (tons) k, a, and b are empirical constants

Equation 1a of AP-42 Section 13.2.2 for vehicles traveling on unpaved surfaces at industrial sites

Constant	Ind	ads				
Constant	PM _{2.5} PM ₁₀ PM					
k	0.15	1.5	4.9			
а	0.9	0.9	0.7			
b	0.45	0.45	0.45			

5.1 %, Average Silt Content of Plant Roads at a Coal Mining Site (Table 13.2.2-1) 50 tons, Mean Vehicle Loaded Weight (Fleet Average)

0.25	Ib/VMT, Calculated PM _{2.5} Emission Factor (Road Silt Portion)
2.46	Ib/VMT, Calculated PM_{10} Emission Factor (Road Silt Portion)
9.55	Ib/VMT, Calculated PM Emission Factor (Road Silt Portion)

Emissions associated with the exhaust, brake wear, and tire wear must be added to the values calculated above. The values shown below were taken from Table 13.2.2-4.

Particle Size	PM _{2.5}	PM ₁₀	РМ	
lb/VMT "adder"	0.00036	0.00047	0.00047	
	_			
0.25	lb/VMT, Ca	alculated PI	M _{2.5} Emissio	on Factor (Total, No natural mitigation
2.46	lb/VMT, Ca	alculated PI	M ₁₀ Emissio	on Factor (Total, No natural mitigation
0.55		laulated D		Easter (Total No natural mitigation)

9.55 Ib/VMT, Calculated PM Emission Factor (Total, No natural mitigation)

All roads are subject to natural mitigation because of rainfall and other precipitation. The following equation accounts for reductions in the emission factor due to natural mitigation.

$E_{EXT} = E\left[\frac{(365 - P)}{365}\right]$	Where:	E_{EXT} is the adjusted emission factor accounting for natural mitigation E is emission factor from Equation 1a P is the number of days per year with at least 0.01 inches of precipitation
120 days, Pr	ecipitation G	reater than 0.01 inches at Plant Location (Figure 13.2.2-1)

0.17	Ib/VMT, Calculated PM _{2.5} Emission Factor (Total, With natural mitigation)
1.65	Ib/VMT, Calculated PM ₁₀ Emission Factor (Total, With natural mitigation)
6.41	Ib/VMT, Calculated PM Emission Factor (Total, With natural mitigation)

In addition to natural mitigation, the following mitigation will be implemented at the site. Control efficiencies taken from the WRAP Fugitive Dust Handbook, September 7, 2006.

57%	Limit on-site vehicle speeds (on unpaved roads) to 15 mph.
84%	Application of Gravel on Dirt Surfaces
90%	Implement watering for industrial unpaved road.
0.04	Ib/VMT, Calculated PM Emission Factor (Total, With natural mitigation, and water sprays)
0.01	lb/VMT, Calculated PM ₁₀ Emission Factor (Total, With natural mitigation, and water sprays)
0.001	lb/VMT, Calculated PM _{2.5} Emission Factor (Total, With natural mitigation, and water sprays)
40,076	miles/year, "Loaded Truck VMT"
2000	lb/ton, Conversion Factor
8.84E-01	tpy, PM Emissions
2.28E-01	tpy, PM ₁₀ Emissions
2.28E-02	tpy, PM _{2.5} Emissions
2.02E-01	Ib/hr, PM Emissions
5.20E-02	Ib/hr, PM ₁₀ Emissions
5.21E-03	lb/hr, PM _{2.5} Emissions

Duke Energy H.F. Lee Plant Table 13C - Additional Haul Roads Supporting the Movement of Ash Offsite - Unloaded Trucks (F-6)

A portion of the ash will be trucked to an offsite location. Particulate emissions are generated from the haul roads from the force of the wheels on the road surface. This force causes pulverization of the surface material. The particles are lifted and dropped from the rolling wheels and the road surface is exposed to strong air currents, which generate airborne particulate emissions.

The methodology presented below is taken from Section 13.2.2 (Unpaved Roads) of the U.S. EPA's AP-42 document and is based on the vehicle miles traveled (VMT) at the site.

$$E = k \left(\frac{s}{12}\right)^a \left(\frac{W}{3}\right)^b$$
 Where:

E is the size-specific emission factor (lb/VMT) s is the surface material silt content (%) W is the mean vehicle weight (tons) k, a, and b are empirical constants

Equation 1a of AP-42 Section 13.2.2 for vehicles traveling on unpaved surfaces at industrial sites

Constant	Industrial Roads			
Constant	PM _{2.5} PM ₁₀		PM	
k	0.15	1.5	4.9	
а	0.9	0.9	0.7	
b	0.45	0.45	0.45	

5.1 %, Average Silt Content of Plant Roads at a Coal Mining Site (Table 13.2.2-1) 25 tons, Mean Vehicle Empty Weight (Fleet Average)

0.18 lb/VMT, Calculated PM_{2.5} Emission Factor (Road Silt Portion) 1.80 lb/VMT, Calculated PM₁₀ Emission Factor (Road Silt Portion) 6.99 lb/VMT, Calculated PM Emission Factor (Road Silt Portion)

Emissions associated with the exhaust, brake wear, and tire wear must be added to the values calculated above. The values shown below were taken from Table 13.2.2-4.

Particle Size	PM _{2.5}	PM ₁₀	РМ
lb/VMT "adder"	0.00036	0.00047	0.00047

Where:

0.18 lb/VMT, Calculated PM_{2.5} Emission Factor (Total, No natural mitigation) 1.80 lb/VMT, Calculated PM₁₀ Emission Factor (Total, No natural mitigation) 6.99 lb/VMT, Calculated PM Emission Factor (Total, No natural mitigation)

All roads are subject to natural mitigation because of rainfall and other precipitation. The following equation accounts for reductions in the emission factor due to natural mitigation.

F - F	$\left[(365 - P) \right]$
$L_{EXT} - L$	365

 E_{EXT} is the adjusted emission factor accounting for natural mitigation E is emission factor from Equation 1a P is the number of days per year with at least 0.01 inches of precipitation

120 days, Precipitation Greater than 0.1 inches at Plant Location (Figure 13.2.2-1)

0.12 lb/VMT, Calculated PM_{2.5} Emission Factor (Total, With natural mitigation) 1.21 lb/VMT, Calculated PM₁₀ Emission Factor (Total, With natural mitigation) 4.69 lb/VMT, Calculated PM Emission Factor (Total, With natural mitigation)

In addition to natural mitigation, the following mitigation will be implemented at the site. Control efficiencies taken from the WRAP Fugitive Dust Handbook, September 7, 2006.

57% Limit on-site vehicle speeds (on unpaved roads) to 15 mph. 84% Application of Gravel on Dirt Surfaces 90% Implement watering for industrial unpaved road.

0.03 lb/VMT, Calculated PM Emission Factor (Total, With natural mitigation, and water sprays) 0.008 lb/VMT, Calculated PM₁₀ Emission Factor (Total, With natural mitigation, and water sprays) 0.0008 lb/VMT, Calculated PM_{2.5} Emission Factor (Total, With natural mitigation, and water sprays)

40,076 miles/day, One-way Vehicle Distance from Source to Offsite 2000 lb/ton, Conversion Factor

6.47E-01	tpy, PM Emissions
1.67E-01	tpy, PM ₁₀ Emissions
1.67E-02	tpy, PM _{2.5} Emissions

1.48E-01 lb/hr, PM Emissions 3.81E-02 lb/hr, PM₁₀ Emissions 3.82E-03 lb/hr, PM_{2.5} Emissions

Duke Energy H.F. Lee Plant Table 14A - Screener Emissions (ES-39A) Spyder 514TS Double Deck

Capacity, ton/yr	430,000	Duke Energy
Hours of operation, hr/yr	2600	Based on 50/wk M-F
Capacity, ton/hr	165	Duke Energy

Pollutant	Emission Factor ¹	Potential Emission Rates	
1 onutant	lb/ton	(lb/hr)	(tpy)
PM	0.0022	0.015	0.020
PM ₁₀	0.00074	0.005	0.007
PM _{2.5}	0.00005	0.0003	0.0004

Lead	19.85	3.00E-07	3.90E-07	Duke Energy Average Ash Analysis
Arsenic	38.55	5.83E-07	7.58E-07	Duke Energy Average Ash Analysis
Antimony	1.28	1.94E-08	2.52E-08	Duke Energy Average Ash Analysis
Beryllium	4.25	6.43E-08	8.36E-08	Duke Energy Average Ash Analysis
Cadmium	0.18	2.72E-09	3.54E-09	Duke Energy Average Ash Analysis
Chromium	25.20	3.81E-07	4.95E-07	Duke Energy Average Ash Analysis
Chromium VI	0.67	1.01E-08	1.32E-08	Duke Energy Average Ash Analysis
Cobalt	12.68	1.92E-07	2.49E-07	Duke Energy Average Ash Analysis
Manganese	54.29	8.21E-07	1.07E-06	Duke Energy Average Ash Analysis
Mercury	0.16	2.42E-09	3.15E-09	Duke Energy Average Ash Analysis
Nickel	23.33	3.53E-07	4.59E-07	Duke Energy Average Ash Analysis
Selenium	8.32	1.26E-07	1.64E-07	Duke Energy Average Ash Analysis

Notes:

1. Emission Factor for Screening operation from AP-42, Table 11.19.2-2

2. HAP/TAP emission factors for the fly ash is based on site-specific ash analysis without the addition of metals in the water used for water injection.

uke Energy l able 14B - Scre	H.F. Lee Plant ener Engine Emi	ssions (ES	-39B)				
Engine rating Permitted Hours: No. of Engines: Heat Input:	91 2,600 1 0.64	hp hrs/yr MMBtu/hr (H	IHV)		Diesel Sulfur Content: Diesel Heat Content:	0.001 7,000	5 weight % Btu/hp-hr
Pollutant	Emission Factor	Potential Emission Rates		HAP Pollutant ¹	Emission Factor	Potential Emission Rates	
	lb/hp-hr	(lb/hr)	(tpy)		(Ib/MMBtu)	(lb/hr)	(tpy)
NO _x	0.031	2.82	3.667	Benzene	9.33E-04	5.94E-04	7.73E-04
СО	6.68E-03	0.61	0.790	Toluene	4.09E-04	2.61E-04	3.39E-04
VOC	2.47E-03	0.22	0.292	Xylenes	2.85E-04	1.82E-04	2.36E-04
SO ₂	2.05E-03	0.19	0.243	1,3-Butadiene	3.91E-05	2.49E-05	3.24E-05
PM	2.20E-03	0.20	0.260	Formaldehyde	1.18E-03	7.52E-04	9.77E-04
PM ₁₀	2.20E-03	0.20	0.260	Acetaldehyde	7.67E-04	4.89E-04	6.35E-04
PM _{2.5}	2.20E-03	0.20	0.260	Acrolein	9.25E-05	5.89E-05	7.66E-05
				Total PAH	1.68E-04	1.07E-04	1.39E-04
				Naphthalene	8.48E-05	5.40E-05	7.02E-05
				Acenaphthalene	5.06E-06	3.22E-06	4.19E-06
				Acenaphthene	1.42E-06	9.05E-07	1.18E-06
				Fluorene	2.92E-05	1.86E-05	2.42E-05
				Phenanthrene	2.94E-05	1.87E-05	2.43E-05
				Anthracene	1.87E-06	1.19E-06	1.55E-06
				Fluoranthene	7.61E-06	4.85E-06	6.30E-06
				Pyrene	4.78E-06	3.04E-06	3.96E-06
				Benzo(a)anthracene	1.68E-06	1.07E-06	1.39E-06
				Chrysene	3.53E-07	2.25E-07	2.92E-07
				Benzo(b)fluoranthene	9.91E-08	6.31E-08	8.21E-08
				Benzo(k)fluoranthene	1.55E-07	9.87E-08	1.28E-07
				Benzo(a)pyrene	1.88E-07	1.20E-07	1.56E-07
				Indeno(1,2,3-cd)pyrene	3.75E-07	2.39E-07	3.11E-07
				Dibenz(a,h)anthracene	5.83E-07	3.71E-07	4.83E-07
				Benzo(g,h,l)perylene	4.89E-07	3.11E-07	4.05E-07

Summary of GHG Emissions:

	Emission Factor	Emissions (metric	Emissions (US
Pollutant	(kg/MMBtu) ²	tons/yr) ³	tons/yr)⁴
CO ₂	73.96	122.5	134.99
CH₄	3.0E-03	0.005	0.005
N ₂ O	6.0E-04	0.001	0.001
CO₂e⁵		122.91	135.45

-

Notes

Assume PM = PM10 = PM2.5

Emission Factor based on Table 3.3 1, EPA AP 42, Chapter 3.3 Gasoline & Diesel Industrial Engines

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1. HAPs Emission Factor based on Table 3.3 2, Chapter 3.3 Gasoline & Diesel Industrial Engines. Per 15A NCAC 2Q.0702 (a)(27) these emissions were not included in the TPER analysis. 2. Based on EPA default factors in Subpart C Tables C-1 and C-2 for Distillate Fuel Oil No. 2.

3. Calculated based on the heat input, emission factors, and equations C-1b and C-8b of Subpart C. CO₂ e based on Subpart A Table A-1 factors.

 CO_2 , CH_4 , or N_2O (metric tpy) = 1E-03 * Gas (MMBtu/yr) * Emission Factor (kg/MMBtu)

4. 1 metric ton = 1.102 US ton

5. $CO_2 e = CO_2$, CH_4 , or $N_2 O$ (tpy) * Global Warming Potential factor (GWP)

CO₂ GWP	1
CH₄ GWP	25
$N_2 O GWP$	298

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Duke Energy H.F. Lee Plant Table 15A - Crusher Emissions (ES-40A) 4043T Impact Crusher

Capacity, ton/yr	43,000	Duke Energy
Max Hours of operation, hr/day	1	Duke Energy
Hours of operation, hr/yr	365	Based on 1 hr/day 365 days/year
Capacity, ton/day	165	Duke Energy

Pollutant	Emission Factor ¹	Potential Em	ission Rates
rondtant	lb/ton	(lb/hr)	(tpy)
PM	0.0012	0.008	0.002
PM ₁₀	0.00054	0.004	0.001
PM _{2.5}	0.0001	0.001	0.0001

Lead	19.85	1.64E-07	2.99E-08	Duke Energy Average Ash Analysis
Arsenic	38.55	3.18E-07	5.80E-08	Duke Energy Average Ash Analysis
Antimony	1.28	1.06E-08	1.93E-09	Duke Energy Average Ash Analysis
Beryllium	4.25	3.51E-08	6.40E-09	Duke Energy Average Ash Analysis
Cadmium	0.18	1.49E-09	2.71E-10	Duke Energy Average Ash Analysis
Chromium	25.20	2.08E-07	3.79E-08	Duke Energy Average Ash Analysis
Chromium VI	0.67	5.53E-09	1.01E-09	Duke Energy Average Ash Analysis
Cobalt	12.68	1.05E-07	1.91E-08	Duke Energy Average Ash Analysis
Manganese	54.29	4.48E-07	8.17E-08	Duke Energy Average Ash Analysis
Mercury	0.16	1.32E-09	2.41E-10	Duke Energy Average Ash Analysis
Nickel	23.33	1.92E-07	3.51E-08	Duke Energy Average Ash Analysis
Selenium	8.32	6.86E-08	1.25E-08	Duke Energy Average Ash Analysis

Notes:

1. Emission Factor for Crushing operation from AP-42, Table 11.19.2-2

2. HAP/TAP emission factors for the fly ash is based on site-specific ash analysis without the addition of metals in the water used for water injection.

uke Energy	H.F. Lee Plant	sions (ES /	108)				
Engine rating			+0B)				
Permitted Hours	365	bre/vr					
No of Engines:	1	111 3/ yi			Diesel Sulfur Content:	0.001	5 weight %
Heat Input:	2 10	MMBtu/hr (F	IHV)		Diesel Heat Content:	7 000	Btu/hp-hr
nout input.	2.10				Dieser reat Content.	7,000	Btd/np m
Pollutant	Emission Factor	Potential Em	nission Rates	HAP Pollutant ¹	Emission Factor	Potential Emis	ssion Rates
i onatant	lb/hp-hr	(lb/hr)	(tpy)		(Ib/MMBtu)	(lb/hr)	(tpy)
NO _x	0.031	9.30	1.697	Benzene	9.33E-04	1.96E-03	3.58E-04
CO	6.68E-03	2.00	0.366	Toluene	4.09E-04	8.59E-04	1.57E-04
VOC	2.47E-03	0.74	0.135	Xylenes	2.85E-04	5.99E-04	1.09E-04
SO ₂	2.05E-03	0.62	0.112	1,3-Butadiene	3.91E-05	8.21E-05	1.50E-05
PM	2.20E-03	0.66	0.120	Formaldehyde	1.18E-03	2.48E-03	4.52E-04
PM ₁₀	2.20E-03	0.66	0.120	Acetaldehyde	7.67E-04	1.61E-03	2.94E-04
PM _{2.5}	2.20E-03	0.66	0.120	Acrolein	9.25E-05	1.94E-04	3.55E-05
				Total PAH	1.68E-04	3.53E-04	6.44E-05
				Naphthalene	8.48E-05	1.78E-04	3.25E-05
				Acenaphthalene	5.06E-06	1.06E-05	1.94E-06
				Acenaphthene	1.42E-06	2.98E-06	5.44E-07
				Fluorene	2.92E-05	6.13E-05	1.12E-05
				Phenanthrene	2.94E-05	6.17E-05	1.13E-05
				Anthracene	1.87E-06	3.93E-06	7.17E-07
				Fluoranthene	7.61E-06	1.60E-05	2.92E-06
				Pyrene	4.78E-06	1.00E-05	1.83E-06
				Benzo(a)anthracene	1.68E-06	3.53E-06	6.44E-07
				Chrysene	3.53E-07	7.41E-07	1.35E-07
				Benzo(b)fluoranthene	9.91E-08	2.08E-07	3.80E-08
				Benzo(k)fluoranthene	1.55E-07	3.26E-07	5.94E-08
				Benzo(a)pyrene	1.88E-07	3.95E-07	7.21E-08
				Indeno(1,2,3-cd)pyrene	3.75E-07	7.88E-07	1.44E-07
				Dibenz(a,h)anthracene	5.83E-07	1.22E-06	2.23E-07
				Benzo(g,h,l)perylene	4.89E-07	1.03E-06	1.87E-07

Summary of GHG Emissions:

		Emissions	Emissions
	Emission Factor	(metric	(US
Pollutant	(kg/MMBtu) ²	tons/yr) ³	tons/yr) ⁴
CO ₂	73.96	56.7	62.47
CH ₄	3.0E-03	0.002	0.003
N ₂ O	6.0E-04	0.0005	0.0005
CO₂e ⁵		56.88	62.69

-

Notes

Assume PM = PM10 = PM2.5

Emission Factor based on Table 3.3 1, EPA AP 42, Chapter 3.3 Gasoline & Diesel Industrial Engines

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1. HAPs Emission Factor based on Table 3.3 2, Chapter 3.3 Gasoline & Diesel Industrial Engines. Per 15A NCAC 2Q.0702 (a)(27) these emissions were not included in the TPER analysis. 2. Based on EPA default factors in Subpart C Tables C-1 and C-2 for Distillate Fuel Oil No. 2.

3. Calculated based on the heat input, emission factors, and equations C-1b and C-8b of Subpart C. CO₂e based on Subpart A Table A-1 factors.

 CO_2 , CH_4 , or N_2O (metric tpy) = 1E-03 * Gas (MMBtu/yr) * Emission Factor (kg/MMBtu)

-

4. 1 metric ton = 1.102 US ton

5. $CO_2e = CO_2$, CH_4 , or N_2O (tpy) * Global Warming Potential factor (GWP)

$CO_2 GWP$	1
CH_4 GWP	25
N ₂ O GWP	298

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Duke Energy H.F. Lee PlantGoldsboro, North CarolinaWayne CountyTable 16 - Fly Ash and water sprayReactor water spray flow rate

GPM

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Parameter	Compound Category	Injection Concentration (mg/L) ¹	Injection Concentration (PPM) ²	Injection Concentration (lb/hr)	Fly Ash Speciation (PPM)	Fly Ash Speciation ³ (lb/hr)	Injection Concentration + Fly ash (lb/hr)	Injection Concentration + Fly ash concentration (PPM)
Aluminum		3.2	3.2	0.208	NA	NA	NA	NA
Antimony	HAP	0.0079	0.0079	0.001	1.28	0.19	0.193	1.283
Arsenic	HAP, TAP	0.08	0.08	0.005	38.55	5.78	5.788	38.585
Barium		0.17	0.17	0.011	548.00	82.20	82.211	548.074
Beryllium	HAP, TAP	ND	ND	ND	4.25	0.64	0.638	4.250
Cadmium	HAP, TAP	0.0009	0.0009	0.000	0.18	0.03	0.027	0.180
Calcium		440.0	440.0	28.638	NA	NA	NA	NA
Chromium	HAP, TAP	0.0064	0.0064	0.000	25.20	3.78	3.780	25.203
Chromium VI	HAP, TAP	ND	ND	ND	0.67	0.10	0.101	0.670
Cobalt	HAP	0.0035	0.0035	0.000	12.68	1.90	1.902	12.682
Copper		ND	ND	ND	46.18	6.93	6.927	46.180
Iron		1.5	1.5	0.098	NA	NA	NA	NA
Lead	HAP	0.0048	0.0048	0.000	19.85	2.98	2.978	19.852
Magnesium		60.0	60.0	3.905	NA	NA	NA	NA
Manganese	HAP, TAP	0.047	0.047	0.003	54.29	8.14	8.147	54.310
Mercury	HAP, TAP	0.000047	0.000047	0.000	0.16	0.02	0.024	0.160
Molybdenum		ND	ND	ND	2.58	0.39	0.387	2.580
Nickel	HAP, TAP	0.012	0.012	0.001	23.33	3.50	3.500	23.335
Potassium		17.0	17.0	1.106	NA	NA	NA	NA
Selenium	HAP	0.25	0.25	0.016	8.32	1.25	1.264	8.428
Silver		ND	ND	ND	0.72	0.11	0.108	0.720
Sodium		120.0	120.0	7.810	NA	NA	NA	NA
Thallium		ND	ND	ND	1.30	0.20	0.195	1.300
Vanadium		0.056	0.056	0.004	65.12	9.77	9.772	65.144
Zinc		0.036	0.036	0.002	23.41	3.51	3.514	23.426

Winyah wash water sample analysis
 mg/L = PPM
 STAR Reactor hourly throughput = 75 tph

ND - Not Determined in sample analysis NA - Not in the Fly Ash speciation

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APPENDIX C

EMISSION CALCULATIONS SUPPORT DOCUMENATION



	HF Lee Average	EPRI Basis
Compound	Lab Ash	Average Ash
	Analysis (ppm)	Analysis (ppm)
Antimony	1.28	19.47
Arsenic	38.55	118.52
Barium	548.00	1007.45
Beryllium	4.25	24.55
Cadmium	0.18	21.16
Chromium	25.20	143.92
Chromium VI	0.67	15.83
Cobalt	12.68	57.57
Copper	46.18	160.85
Lead	19.85	126.99
Manganese	54.29	253.98
Mercury	0.16	0.76
Molybdenum	2.58	55.03
Nickel	23.33	143.92
Selenium	8.32	38.94
Silver	0.72	2.46
Thallium	1.30	14.39
Vanadium	65.12	279.38
Zinc	23.41	296.31

Compound	HF Lee Average	HF Lee Range
Sulfur	0.03%	0.013 to 0.065%
LOI	9.65%	1.71 to 21.9%

(ID Nos. Lee IC Unit 1A, Lee IC Unit 1B and Lee IC Unit 1C) shall not exceed the following limits.

Regulated Pollutant	Limits/Standards (tons per year)	Applicable Regulation
nitrogen oxides	3,414.6	15A NCAC 02Q.0317(a)(1) (PSD avoidance)
sulfur dioxide	14,663.1	
particulate matter/ PM-10/ PM-2.5	218.2	
carbon monoxide	829.3	
VOCs	65.1	
sulfuric acid	64.3	
lead	0.77	

Monitoring/Recordkeeping [15A NCAC 02Q .0508(f)]

b. The Permittee shall keep records of the monthly emissions from each source (ID Nos. Lee IC Unit 1A, Lee IC Unit 1B and Lee IC Unit 1C), in a logbook (written or in electronic format). The Permittee shall be deemed in noncompliance with 15A NCAC 02D .0530(g) if these records are not kept or if any of the above limits are exceeded. Emissions shall be determined as follows:

$$Total \ Emissions \ = \sum \ Lee \ IC \ Unit \ 1A + Lee \ IC \ Unit \ 1B + Lee \ IC \ Unit \ 1C$$

Nitrogen Oxides

Emissions of nitrogen oxides shall be determined using a continuous emissions monitoring (CEM) system meeting the requirements of 15A NCAC 02D .0613 - 40 CFR Part 60 Appendix B "Performance Specifications" and Appendix F "Quality Assurance Procedures." If the owner or operator has installed a nitrogen oxides CEMS to meet the requirements of 40 CFR Part 75 and is continuing to meet the ongoing requirements of 40 CFR Part 75, that CEMS may be used to meet the requirements of this section, and used to calculate total nitrogen oxide emissions in accordance with the following equation. Data reported to meet the requirements of this section shall include data substituted using the missing data procedures in subpart D of 40 CFR Part 75 and may be bias adjusted according to the procedures of 40 CFR Part 75.

 $Total \ Emissions \ (NOx) = Lee \ IC \ Unit \ IA \ CEMS + Lee \ IC \ Unit \ IB \ CEMS + Lee \ IC \ Unit \ IC \ CEMS \ \leq \ 3414.6 \frac{tons}{12 \ months}$

Source	Emission Rates	Acrolein (lb/hr)	Ammonia (lb/hr)	Formaldehyde (lb/hr)	Sulfuric Acid (lb/hr)
Coal-fired Boiler 1 and 2*	Potential Optimized	3.73E-03 3.73E-03	_	3.53E-02† 3.53E-02†	2.48E+01 2.48E+01
Coal-fired Boiler 3*	Potential Optimized	4.88E-03 4.88E-03	2.50E+00 2.50E+00	4.62E-02† 4.62E-02†	1.35E+00 1.35E+00
Lee IC Turbine 4	Potential Optimized	1.70E-02 1.55E+01		7.50E-02 1.16E+01	3.49E+00 2.09E+01
Lee IC Turbine 5	Potential Optimized	2.89E-02 2.63E+01		1.27E-01 1.97E+01	5.92E+00 3.55E+01
Lee IC Turbine 6	Potential Optimized	2.89E-02 2.63E+01		1.27E-01 1.97E+01	5.92E+00 3.55E+01
Lee IC Turbine 7	Potential Optimized	2.89E-02 2.63E+01		1.27E-01 1.97E+01	5.92E+00 3.55E+01
Lee IC Turbine 10 and 11 (fuel oil)	Potential Optimized	1.22E-01 1.11E+02		5.39E-01 8.35E+01	3.71/3.77 1.86E+01/2.26E+01
Lee IC Turbine 10 and 11(natural gas)	Potential Optimized	1.23E-02 1.12E+01		1.37E+00 2.12E+02	
Lee IC Turbine 12 and 13 (fuel oil)	Potential Optimized	1.16E-01 1.06E+02		5.09E-01 7.89E+01	3.54/3.59 2.12E+01/2.15E+01
Lee IC Turbine 12 and 13 (natural gas)	Potential Optimized	1.16E-02 1.06E+01		1.29E+00 2.00E+02	
Lee IC Turbine 14 (fuel oil)	Potential Optimized	1.29E-01 1.17E+02		5.69E-01 8.82E+01	3.96E+00 2.38E+01
Lee IC Turbine 14 (natural gas)	Potential Optimized	1.24E-02 1.13E+01	—	1.38E+00 2.14E+02	
Fuel gas heater	Potential Optimized	_	1.08E-06 1.46E-04	4.04E-04 6.26E-02	
Black start engine generator	Potential Optimized	1.52E-04 1.38E-01		1.94E-04 3.01E-02	
Fire water pump	Potential Optimized	1.86E-04 1.69E-01		2.73E-03 4.23E-01	
Coal handling activities*	Potential Optimized				

Table 3-2. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for 1-Hour TAPs

Source	Emission Rates	Acrolein (lb/hr)	Ammonia (lb/hr)	Formaldehyde (lb/hr)	Sulfuric Acid (lb/hr)
Gasoline Storage Tank	Potential Optimized			_	_
Proposed combined-cycle firing natural gas	Potential Optimized	1.44E-02 1.31E+01	3.62E+01 4.89E+03	1.63E+00 2.53E+02	1.03E+00 6.18E+00
Proposed combined-cycle firing fuel oil	Potential Optimized	0.00E+00 0.00E+00	2.93E+01 3.96E+03	6.03E-01 9.35E+01	2.30E+00 1.38E+01
Proposed simple-cycle firing natural gas	Potential Optimized	1.42E-02 1.29E+01		1.58E+00 2.45E+02	1.90E-01 1.14E+00
Proposed simple-cycle firing fuel oil	Potential Optimized			6.03E-01 9.35E+01	5.00E-01 3.00E+00
Proposed auxiliary boiler	Potential Optimized			3.86E-03 5.98E-01	
Proposed fuel gas heater	Potential Optimized			3.31E-04 5.13E-02	
Proposed dew point heater	Potential Optimized			5.74E-04 8.90E-02	
Proposed firewater pump	Potential Optimized	1.72E-04 1.57E-01		2.19E-03 3.39E-01	

Table 3-2. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for 1-Hour TAPs (Continued, Page 2 of 2)

*Emissions for existing coal-fired boilers and associated coal handling activities were not optimized. †Emissions represent the fuel oil combustion

Source: ECT Calculations – Appendix A

Table 3-3. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Daily TAPs

Source	Emission Rates	Chromic Acid (lb/hr)	Hexane (lb/hr)	Manganese (lb/hr)	Mercury (lb/hr)	Nickel (lb/hr)	Sulfuric Acid (lb/hr)	Toluene (lb/hr)	Xylene (lb/hr)
Coal-fired Boiler 1 and 2*	Potential	2.98E-03	9.62E-04	3.85E-02	1.04E-02	8.48E-01†	2.48E+01	2.36E-02†	3.04E-03†
Cool fired Pailer 2*	Detential	2.98E-03	9.02E-04	<u>3.85E-02</u>	1.04E-02	$\frac{8.48E-011}{1.11E+0.04}$	2.48E+01 1 25E+00	2.30E-021 2.08E-02*	3.04E-031
Coal-filed Boller 5	Ontimized	3.49E-03	1.20E-03	4.40E-02 4.40E-02	1.14E-02	1.11E+0.0	1.35E+00 1.35E+00	3.08E-02†	3.98E-03†
Lee IC Turbine 4	Potential	4 79E-04		2 12E-01	3 22E-04	1 23E-03	3 49E+00	9.95E-02	6.93E-02
Lee le Turbine 4	Ontimized	1.65E-01	_	3 88E+01	7 37E-01	7 13E-01	2.09E+01	4 34E+03	2 53E+03
Lee IC Turbine 5	Potential	8 13E-04		3 59E-01	5 46E-04	2 09E-03	5 92E+00	1 69E-01	1 18E-01
	Optimized	2.80E-01	_	6.57E+01	1.25E+00	1.21E+00	3.55E+01	7.38E+03	4.30E+03
Lee IC Turbine 6	Potential	8.13E-04		3.59E-01	5.46E-04	2.09E-03	5.92E+00	1.69E-01	1.18E-01
	Optimized	2.80E-01		6.57E+01	1.25E+00	1.21E+00	3.55E+01	7.38E+03	4.30E+03
Lee IC Turbine 7	Potential	8.13E-04		3.59E-01	5.46E-04	2.09E-03	5.92E+00	1.69E-01	1.18E-01
	Optimized	2.80E-01		6.57E+01	1.25E+00	1.21E+00	3.55E+01	7.38E+03	4.30E+03
Lee IC Turbine 10 and 11 (fuel oil)	Potential	3.44E-03		1.52E+00	2.31E-03	8.86E-03	3.71/3.77	7.15E-01	4.98E-01
	Optimized	1.19E+00	_	2.78E+02	5.29E+00	5.14E+00	1.86E+01/	3.12E+04	1.81E+04
							2.26E+01		
Lee IC Turbine 10 and 11(natural gas)	Potential	—	—	—	—	—	6.55E+00	2.50E-01	1.23E-01
	Optimized						3.93E+01	1.09E+04	4.48E+03
Lee IC Turbine 12 and 13 (fuel oil)	Potential	3.25E-03	—	1.44E+00	2.18E-03	8.37E-03	3.54/3.59	6.76E-01	4.70E-01
	Optimized	1.12E+00	_	2.64E+02	4.99E+00	4.85E+00	2.12E+01/	2.95E+04	1.71E+04
							2.15E+01		
Lee IC Turbine 12 and 13 (natural gas)	Potential		—	—	—	—	6.19E+00	2.36E-01	1.16E-01
	Optimized						3.71E+01	1.03E+04	4.23E+03
Lee IC Turbine 14 (fuel oil)	Potential	3.63E-03	—	1.60E+00	2.44E-03	9.34E-03	3.96E+00	7.54E-01	5.25E-01
	Optimized	1.25E+00		2.93E+02	5.58E+00	5.42E+00	2.38E+01	3.29E+04	1.91E+04
Lee IC Turbine 14 (natural gas)	Potential		—	—	—	—	6.60E+00	2.52E-01	1.24E-01
	Optimized						3.96E+01	1.10E+04	4.52E+03
Fuel gas heater	Potential	7.55E-06	9.71E-03	2.05E-06	1.40E-06	1.13E-05	—	1.83E-05	—
	Optimized	2.60E-03	4.11E+01	3.75E-04	3.20E-03	6.55E-03		7.99E-01	
Black start engine generator	Potential		—	—	—	—	—	6.72E-04	4.68E-04
	Optimized							2.93E+01	1.71E+01
Firewater pump	Potential			—	—	_		8.22E-04	5.73E-04
	Optimized							3.59E+01	2.09E+01
Coal handling activities*	Potential	1.08E-05		1.90E-05	6.96E-08	1.08E-05		—	—
	Optimized	5./3E-03		3.48E-03	1.59E-04	6.26E-03			
Gasoline Storage Tank	Potential	—	1.01E-03		_	—		4.77E-03	1.64E-03
	Optimized	—	4.28E+00			—		2.08E+02	5.98E+01

Table 3-3. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Daily TAPs (Continued, Page 2 of 2)

Source	Emission Rates	Chromic Acid (lb/hr)	Hexane (lb/hr)	Manganese (lb/hr)	Mercury (lb/hr)	Nickel (lb/hr)	Sulfuric Acid (lb/hr)	Toluene (lb/hr)	Xylene (lb/hr)
Proposed combined-cycle firing natural gas	Potential Optimized	6.22E-04 2.15E-01	7.99E-01 3.38E+03	1.69E-04 3.09E-02	1.15E-04 2.63E-01	9.33E-04 5.41E-01	1.03E+00 6.18E+00	2.94E-01 1.28E+04	1.44E-01 5.25E+03
Proposed combined-cycle firing fuel oil	Potential Optimized	2.37E-02 8.18E+00		1.70E+00 3.11E+02	2.58E-03 5.90E+00	9.90E-03 5.74E+00	2.30E+00 1.38E+01		
Proposed simple-cycle firing natural gas	Potential Optimized	_					1.90E-01 1.14E+00	2.89E-01 1.26E+04	1.42E-01 5.18E+03
Proposed simple-cycle firing fuel oil	Potential Optimized	2.37E-02 8.18E+00		1.70E+00 3.11E+02	2.58E-03 5.90E+00	9.90E-03 5.74E+00	5.00E-01 3.00E+00		
Proposed auxiliary boiler	Potential Optimized	7.20E-05 2.48E-02	9.26E-02 3.92E+02	1.95E-05 3.57E-03	1.34E-05 3.07E-02	1.08E-04 6.26E-02		1.75E-04 7.64E+00	
Proposed fuel gas heater	Potential Optimized	6.18E-06 2.13E-03	7.94E-03 3.36E+01	1.68E-06 3.07E-04	1.15E-06 2.63E-03	9.26E-06 5.37E-03		1.50E-05 6.55E-01	
Proposed dew point heater	Potential Optimized	1.07E-05 3.69E-03	1.38E-02 5.84E+01	2.91E-06 5.33E-04	1.99E-06 4.55E-03	1.61E-05 9.34E-03		2.60E-05 1.14E+00	
Proposed firewater pump	Potential Optimized					_		7.59E-04 3.31E+01	5.29E-04 1.93E+01

*Emissions for existing coal-fired boilers and associated coal handling activities were not optimized. †Emissions represent the fuel oil combustion.

Source: ECT Calculations – Appendix A

Source	Emission Rates	1,3-Butadiene (lb/hr)	Arsenic (lb/hr)	Benzene (lb/hr)	Beryllium (lb/hr)	Cadmium (lb/hr)
Coal-fired Boiler 1 and 2*	Actual	1.01E-07	2.61E-06	5.45E-07	3.04E-07	5.59E-07
	Potential	2.08E-01*	3.25E-02	7.66E-03	3.65E-03	7.34E-03
	Optimized	2.08E-01†	3.25E-02	7.66E-03	3.65E-03	7.34E-03
Coal-fired Boiler 3*	Actual	7.49E-08	3.22E-06	7.35E-07	3.67E-07	7.14E-07
	Potential	2.71E-01†	3.52E-02	1.00E-02	3.72E-03	8.57E-03
	Optimized	2.71E-01†	3.52E-02	1.00E-02	3.72E-03	8.57E-03
Lee IC Turbine 4	Actual	3.60E-07	2.02E-07	1.10E-06	6.35E-09	9.83E-08
	Potential	9.79E-04	6.73E-04	3.37E-03	1.90E-05	2.94E-04
	Optimized	2.56E+00	1.08E-03	1.31E-01	6.34E-02	5.88E-02
Lee IC Turbine 5	Actual	3.92E-07	2.66E-07	1.40E-06	7.81E-09	1.26E-07
	Potential	1.66E-03	1.14E-03	5.71E-03	3.22E-05	4.99E-04
	Optimized	4.34E+00	1.82E-03	2.23E-01	1.08E-01	9.98E-02
Lee IC Turbine 6	Actual	3.92E-07	2.66E-07	1.33E-06	7.64E-09	1.26E-07
	Potential	1.66E-03	1.14E-03	5.71E-03	3.22E-05	4.99E-04
	Optimized	4.34E+00	1.82E-03	2.23E-01	1.08E-01	9.98E-02
Lee IC Turbine 7	Actual	3.43E-07	2.96E-07	1.48E-06	8.43E-09	1.31E-07
	Potential	1.66E-03	1.14E-03	5.71E-03	3.22E-05	4.99E-04
	Optimized	4.34E+00	1.82E-03	2.23E-01	1.08E-01	9.98E-02
Lee IC Turbine 10 and 11 (fuel oil)	Actual	1.49E-06/	1.04E-06/	5.15E-06/	2.77E-08/	4.51E-07/
		7.17E-07	5.00E-07	2.49E-06	1.32E-08	2.17E-07
	Potential	7.03E-03	4.84E-03	2.42E-02	1.36E-04	2.11E-03
	Optimized	1.84E+01	7.74E-03	9.44E-01	4.54E-01	4.22E-01
Lee IC Turbine 10 and 11(natural gas)	Actual	7.94E-08/		2.06E-06/		
		3.15E-08		8.78E-07	—	
	Potential	1.89E-04		5.27E-03	—	
	Optimized	4.95E-01		2.06E-01		
Lee IC Turbine 12 and 13 (fuel oil)	Actual	7.55E-07/	5.19E-07/	2.59E-06/	1.87E-08/	2.27E-07/
		8.92E-07	6.13E-07	3.07E-06	2.20E-08	2.68E-07
	Potential	6.65E-03	4.57E-03	2.28E-02	1.29E-04	1.99E-03
	Optimized	1.74E+01	7.31E-03	8.89E-01	4.31E-01	3.98E-01
	optimized	1.7 12 01	7.51E 05	0.072 01	I.DIE 01	5.501 01

Table 3-4. Worst-Case Emission Rates (Actual, Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Annual TAPs

Source	Emission Rates	1,3-Butadiene (lb/hr)	Arsenic (lb/hr)	Benzene (lb/hr)	Beryllium (lb/hr)	Cadmium (lb/hr)
Lee IC Turbine 12 and 13 (natural gas)	Actual	5.47E-08/		1.53E-06/		
		5.90E-08	—	1.64E-06	—	
	Potential	1.79E-04	—	4.98E-03	—	
	Optimized	4.68E-01		1.94E-01		
Lee IC Turbine 14 (fuel oil)	Actual	7.42E-03	5.10E-03	2.55E-02	1.44E-04	2.23E-03
	Potential	7.42E-03	5.10E-03	2.55E-02	1.44E-04	2.23E-03
	Optimized	1.94E+01	8.16E-03	9.95E-01	4.81E-01	4.46E-01
Lee IC Turbine 14 (natural gas)	Actual	1.90E-04		5.32E-03	—	
	Potential	1.90E-04		5.32E-03	—	
	Optimized	4.97E-01		2.07E-01	—	
Fuel gas heater	Actual			3.60E-09	2.06E-11	1.89E-09
-	Potential	—	_	2.59E-06	1.48E-08	1.35E-06
	Optimized	—	_	1.01E-04	4.94E-05	2.70E-04
Black start engine generator	Actual	3.67E-06		8.75E-05		
	Potential	3.67E-06	_	8.75E-05	—	_
	Optimized	9.60E-03	—	3.41E-03	—	
Firewater pump	Actual	4.48E-06		1.07E-04		
	Potential	4.48E-06		1.07E-04	_	
	Optimized	1.17E-02		4.17E-03	_	
Coal handling activities*	Actual		8.86E-06		1.83E-06	1.58E-06
-	Potential		8.86E-06	_	1.83E-06	1.58E-06
	Optimized	_	8.86E-06	_	1.83E-06	1.58E-06
Gasoline Storage Tank	Actual			1.27E-03		
C C	Potential	_		1.27E-03	_	
	Optimized	_		4.96E-02	_	
Proposed combined-cycle firing natural gas	Actual	9.67E-04	8.88E-05	2.79E-02	5.33E-06	4.89E-04
. , , , ,	Potential	9.67E-04	8.88E-05	2.79E-02	5.33E-06	4.89E-04
	Optimized	2.53E+00	1.42E-04	1.09E+00	1.78E-02	9.78E-02
Proposed combined-cycle firing fuel oil	Actual	3.93E-03	2.70E-03	1.35E-02	7.62E-05	1.18E-03
	Potential	3.93E-03	2.70E-03	1.35E-02	7.62E-05	1.18E-03
	Optimized	1.03E+01	4.32E-03	5.27E-01	2.54E-01	2.36E-01

Table 3-4. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Annual TAPs (Continued, Page 2 of 3)

Source	Emission Rates	1,3-Butadiene (lb/hr)	Arsenic (lb/hr)	Benzene (lb/hr)	Beryllium (lb/hr)	Cadmium (lb/hr)
Proposed simple-cycle firing natural gas	Actual	2.18E-04	_	6.09E-03	_	_
	Potential	2.18E-04		6.09E-03		
	Optimized	5.71E-01		2.38E-01	_	_
Proposed simple-cycle firing fuel oil	Actual	3.93E-03	2.70E-03	1.35E-02	7.62E-05	1.18E-03
	Potential	3.93E-03	2.70E-03	1.35E-02	7.62E-05	1.18E-03
	Optimized	1.03E+01	4.32E-03	5.27E-01	2.54E-01	2.36E-01
Proposed auxiliary boiler	Actual		1.03E-05	1.08E-04	6.17E-07	5.66E-05
1 2	Potential	_	1.03E-05	1.08E-04	6.17E-07	5.66E-05
	Optimized		1.65E-05	4.21E-03	2.06E-03	1.13E-02
Proposed fuel gas heater	Actual		8.82E-07	9.26E-06	5.29E-08	4.85E-06
	Potential		8.82E-07	9.26E-06	5.29E-08	4.85E-06
	Optimized		1.41E-06	3.61E-04	1.77E-04	9.70E-04
Proposed dew point heater	Actual		1.53E-06	1.61E-05	9.18E-08	8.41E-06
	Potential		1.53E-06	1.61E-05	9.18E-08	8.41E-06
	Optimized	_	2.45E-06	6.28E-04	3.07E-04	1.68E-03
Proposed firewater pump	Actual	4.14E-06		9.88E-05		
· · · ·	Potential	4.14E-06		9.88E-05	_	_
	Optimized	1.08E-02	—	3.85E-03		

Table 3-4. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Annual TAPs (Continued, Page 3 of 3)

*Emissions for the existing coal-fired boilers and associated coal handling activities were not optimized. †Emissions represent the fuel oil combustion.

Source: ECT Calculations – Appendix A

Source	Emission Rates	Acrolein (lb/hr)	Ammonia (lb/hr)	Formaldehyde (lb/hr)	Sulfuric Acid (lb/hr)
Coal-fired Boiler 1 and 2*	Potential Optimized	3.73E-03	_	3.53E-02† 3.53E-02‡	2.48E+01 2.48E+01
Coal-fired Boiler 3*	Potential Optimized	4.88E-03 4.88E-03	2.50E+00 2.50E+00	4.62E-02† 4.62E-02†	1.35E+00 1.35E+00
Lee IC Turbine 4	Potential Optimized	1.70E-02 1.55E+01		7.50E-02 1.16E+01	3.49E+00 1.15E+01
Lee IC Turbine 5	Potential Optimized	2.89E-02 2.63E+01		1.27E-01 1.97E+01	5.92E+00 1.95E+01
Lee IC Turbine 6	Potential Optimized	2.89E-02 2.63E+01		1.27E-01 1.97E+01	5.92E+00 1.95E+01
Lee IC Turbine 7	Potential Optimized	2.89E-02 2.63E+01		1.27E-01 1.97E+01	5.92E+00 1.95E+01
Lee IC Turbine 10 and 11 (fuel oil)	Potential Optimized	1.22E-01 1.11E+02		5.39E-01 8.36E+01	8.11E+00 2.68E+01
Lee IC Turbine 10 and 11(natural gas)	Potential Optimized	1.23E-02 1.12E+01		1.37E+00 2.12E+02	9.10E-01 3.00E+00
Lee IC Turbine 12 and 13 (fuel oil)	Potential Optimized	1.16E-01 1.05E+02		5.09E-01 7.89E+01	8.09E+00 2.67E+01
Lee IC Turbine 12 and 13 (natural gas)	Potential Optimized	1.16E-02 1.06E+01		1.29E+00 2.00E+02	8.30E-01 2.74E+00
Lee IC Turbine 14 (fuel oil)	Potential Optimized	1.29E-01 1.17E+02		5.69E-01 8.81E+01	8.01E+00 2.64E+01
Lee IC Turbine 14 (natural gas)	Potential Optimized	1.24E-02 1.13E+01		1.38E+00 2.14E+02	8.30E-01 2.74E+00
Black start engine generator	Potential Optimized	1.52E-04 1.38E-01		1.94E-03 3.01E-01	
Fire water pump	Potential Optimized	1.86E-04 1.69E-01	_	2.37E-03 3.67E-01	_

Table 4-7. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for 1-Hour TAPs

Table 4-7. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for 1-Hour TAPs (Continued, Page 2 of 2)

Source	Emission Rates	Acrolein (lb/hr)	Ammonia (lb/hr)	Formaldehyde (lb/hr)	Sulfuric Acid (lb/hr)
Coal handling activities*	Potential Optimized	_			_
Gasoline storage tank	Potential Optimized				
Proposed combined-cycle firing natural gas	Potential Optimized	1.44E-02 1.31E+01	3.62E+01 4.89E+03	1.63E+00 2.53E+02	1.03E+00 3.40E+00
Proposed combined-cycle firing fuel oil	Potential Optimized		2.93E+01 3.96E+03	6.03E-01 9.34E+01	7.67E+01 2.53E+02
Proposed simple-cycle firing natural gas	Potential Optimized	1.42E-02 1.30E+01		1.58E+00 2.45E+02	1.90E-01 6.27E-01
Proposed simple-cycle firing fuel oil	Potential Optimized			6.03E-01 9.34E+01	1.67E-01 5.50E+01
Proposed auxiliary boiler	Potential Optimized			6.25E-03 9.69E-01	
Proposed dew point heater	Potential Optimized			8.82E-04 1.27E-01	
Proposed firewater pump	Potential Optimized	3.93E-04 3.58E-01		5.02E-03 7.78E-01	

*Emissions for existing coal-fired boilers and associated coal handling activities were not optimized. †Emissions represent the fuel oil combustion

Source: ECT, 2011.

Table 4-8. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Daily TAPs

Source	Emission Rates	Chromic Acid (lb/hr)	Hexane (lb/hr)	Manganese (lb/hr)	Mercury (lb/hr)	Nickel (lb/hr)	Sulfuric Acid (lb/hr)	Toluene (lb/hr)	Xylene (lb/hr)
Coal-fired Boiler 1 and 2*	Potential Optimized	2.98E-03 2.98E-03	9.62E-04 9.62E-04	3.85E-02 3.85E-02	1.04E-02 1.04E-02	8.48E-01† 8.48E-01†	2.48E+01 2.48E+01	2.36E-02† 2.36E-02†	3.04E-03† 3.04E-03†
Coal-fired Boiler 3*	Potential Optimized	3.49E-03 3.49E-03	1.26E-03 1.26E-03	4.40E-02 4.40E-02	1.14E-02 1.14E-02	1.11E+00† 1.11E+00†	1.35E+00 1.35E+00	3.08E-02† 3.08E-02†	3.98E-03† 3.98E-03†
Lee IC Turbine 4	Potential Optimized	4.79E-04 1.48E-01		2.12E-01 3.79E+01	3.22E-04 7.24E-01	1.23E-03 7.25E-01	3.49E+00 6.98E+00	9.95E-02 1.98E+03	6.93E-02 2.07E+03
Lee IC Turbine 5	Potential Optimized	8.13E-04 2.52E-01		3.59E-01 6.43E+01	5.46E-04 1.23E+00	2.09E-03 1.23E+00	5.92E+00 1.18E+01	1.69E-01 3.36E+03	1.18E-01 3.51E+03
Lee IC Turbine 6	Potential Optimized	8.13E-04 2.52E-01		3.59E-01 6.43E+01	5.46E-04 1.23E+00	2.09E-03 1.23E+00	5.92E+00 1.18E+01	1.69E-01 3.36E+03	1.18E-01 3.51E+03
Lee IC Turbine 7	Potential Optimized	8.13E-04 2.52E-01		3.59E-01 6.43E+01	5.46E-04 1.23E+00	2.09E-03 1.23E+00	5.92E+00 1.18E+01	1.69E-01 3.36E+03	1.18E-01 3.51E+03
Lee IC Turbine 10 and 11 (fuel oil)	Potential Optimized	3.44E-03 1.07E+00		1.52E+00 2.72E+02	2.31E-03 5.20E+00	8.86E-03 5.21E+00	8.11E+00 1.62E+01	7.15E-01 1.42E+04	4.98E-01 1.49E+04
Lee IC Turbine 10 and 11(natural gas)	Potential Optimized						9.10E-01 1.82E+00	2.50E-01 4.98E+03	1.23E-01 3.68E+03
Lee IC Turbine 12 and 13 (fuel oil)	Potential Optimized	3.25E-03 1.01E+00		1.44E+00 2.57E+02	2.18E-03 4.91E+00	8.37E-03 4.92E+00	8.09E+00 1.62E+01	6.76E-01 1.34E+04	4.70E-01 1.41E+04
Lee IC Turbine 12 and 13 (natural gas)	Potential Optimized						8.30E-01 1.66E+00	2.36E-01 4.70E+03	1.16E-01 3.48E+03
Lee IC Turbine 14 (fuel oil)	Potential Optimized	3.63E-03 1.12E+00		1.60E+00 2.87E+02	2.44E-03 5.48E+00	9.34E-03 5.49E+00	8.01E+00 1.60E+01	7.54E-01 1.50E+04	5.25E-01 1.57E+04
Lee IC Turbine 14 (natural gas)	Potential Optimized						8.30E-01 1.66E+00	2.52E-01 5.01E+03	1.24E-01 3.71E+03
Black start engine generator	Potential Optimized							6.72E-04 1.34E+01	4.68E-04 1.40E+01
Firewater pump	Potential Optimized							8.22E-04 1.63E+01	5.73E-04 1.71E+01
Coal handling activities*	Potential Optimized	1.08E-05 1.08E-05		1.90E-05 1.90E-05	6.96E-08 6.96E-08	1.08E-05 1.08E-05			
Gasoline storage tank	Potential Optimized		1.01E-03 5.96E+00	_	_	_	_	4.77E-03 9.48E+01	1.64E-03 4.90E+01

Table 4-8. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Daily TAPs (Continued, Page 2 of 2)

Source	Emission Rates	Chromic Acid (lb/hr)	Hexane (lb/hr)	Manganese (lb/hr)	Mercury (lb/hr)	Nickel (lb/hr)	Sulfuric Acid (lb/hr)	Toluene (lb/hr)	Xylene (lb/hr)
Proposed combined-cycle firing natural gas	Potential Optimized	6.22E-04 1.93E-01	7.99E-01 4.72E+03	1.69E-04 3.02E-02	1.15E-04 2.60E-01	9.33E-04 5.48E-01	1.03E+00 2.06E+00	2.94E-01 5.84E+03	1.44E-01 5.25E+03
Proposed combined-cycle firing fuel oil	Potential Optimized	2.37E-02 7.34E+00	_	1.70E+00 3.04E+02	2.58E-03 5.81E+00	9.90E-03 5.82E+00	7.67E+01 1.53E+02	_	_
Proposed simple-cycle firing natural gas	Potential Optimized		_	_	_	_	1.90E-01 3.80E+00	2.89E-01 5.75E+03	1.42E-01 5.18E+03
Proposed simple-cycle firing fuel oil	Potential Optimized	2.37E-02 7.34E+00	_	1.70E+00 3.04E+02	2.58E-03 5.80E+00	9.90E-03 5.82E+00	1.67E+01 3.33E+01	_	_
Proposed auxiliary boiler	Potential Optimized	7.20E-05 2.23E-02	9.26E-02 5.46E+02	1.95E-05 3.50E-03	1.34E-05 3.01E-02	1.08E-04 6.35E-02		1.75E-04 3.48E+00	
Proposed dew point heater	Potential Optimized	5.49E-06 1.70E-03	7.06E-03 4.17E+01	1.49E-06 2.67E-04	1.02E-06 2.30E-03	8.24E-06 4.83E-03		1.33E-05 2.64E-01	_
Proposed firewater pump	Potential Optimized		_	_	_	_	—	1.74E-03 3.46E+01	1.21E-03 1.93E+01

*Emissions for existing coal-fired boilers and associated coal handling activities were not optimized. †Emissions represent the fuel oil combustion.

Source: ECT, 2011.

Source	Emission	1,3-Butadiene	Benzene	Beryllium	Cadmium
	Rates	(lb/hr)	(lb/hr)	(lb/hr)	(lb/hr)
Coal-fired Boiler 1 and 2*	Actual	1.01E-07	5.45E-07	3.04E-07	5.59E-07
	Potential	2.08E-01†	7.66E-03	3.65E-03	7.34E-03
	Optimized	2.08E-01†	7.66E-03	3.65E-03	7.34E-03
Coal-fired Boiler 3*	Actual	7.49E-08	7.35E-07	3.67E-07	7.14E-07
	Potential	2.71E-01†	1.00E-02	3.72E-03	8.57E-03
	Optimized	2.71E-01†	1.00E-02	3.72E-03	8.57E-03
Lee IC Turbine 4	Actual	3.60E-07	1.10E-06	6.35E-09	9.83E-08
	Potential	4.29E-03	1.47E-02	8.31E-05	1.29E-03
	Optimized	5.28E+00	2.75E-01	5.32E-02	6.71E-02
Lee IC Turbine 5	Actual	3.92E-07	1.40E-06	7.81E-09	1.26E-07
	Potential	7.28E-03	2.50E-02	1.41E-04	2.18E-03
	Optimized	8.95E+00	4.68E-01	9.02E-02	1.13E-02
Lee IC Turbine 6	Actual	3.92E-07	1.40E-06	7.81E-09	1.26E-07
	Potential	7.28E-03	2.50E-02	1.41E-04	2.18E-03
	Optimized	8.95E+00	4.68E-01	9.02E-02	1.13E-02
Lee IC Turbine 7	Actual	3.92E-07	1.40E-06	7.81E-09	1.26E-07
	Potential	7.28E-03	2.50E-02	1.41E-04	2.18E-03
	Optimized	8.95+00	4.68E-01	9.02E-02	1.13E-02
Lee IC Turbine 10 and 11 (fuel oil)	Actual	1.49E-06/ 7.17E-07 7.03E-03	5.15E-06/ 2.49E-06 2.42E-02	2.77E-08/ 1.32E-08 1.36E-04	4.51E-07/ 2.17E-07 2.11E-03
Lee IC Turbine 10 and 11(natural gas)	Optimized Actual	8.65E+00 7.94E-08/	4.53E-01 2.06E-06/	8.72E-02	1.10E-01
	Potential Optimized	1.89E-04 2.32E-01	5.27E-03 9.86E-02		_

Table 4-9. Worst-Case Emission Rates (Actual, Potential, and Optimized) for Existing and Proposed Equipment at the Lee Facility for Annual TAPs

Source	Emission Rates	1,3-Butadiene	Benzene	Beryllium	Cadmium
Lee IC Turbine 12 and 13 (fuel oil)	Actual	7.55E-07/ 8 92E-07	2.59E-06/ 3.07E-06	1.87E-08/ 2 20E-08	2.27E-07/ 2.68E-07
	Potential Optimized	6.65E-03 8.17E+00	2.28E-02 4.27E-01	1.29E-04 8.24E-02	1.99E-03 1.04E-01
Lee IC Turbine 12 and 13 (natural gas)	Actual	5.47E-08/ 5.90E-08	1.53E-06/ 1.64E-06	—	—
	Potential Optimized	1.79E-04 2.20E-01	4.98E-03 9.31E-02	—	—
Lee IC Turbine 14 (fuel oil)	Actual Potential	7.42E-03 7.42E-03	2.55E-02 2.55E-02	1.44E-04 1.44E-04	2.23E-03 2.23E-03
Lee IC Turbine 14 (natural gas)	Optimized Actual	9.13E+00 1.90E-04	4.78E-01 5.32E-03	9.21E-02 —	1.16E-01 —
Plack start anging generator	Optimized	2.34E-01	9.95E-02 8.75E-05		
Diack start engine generator	Potential	3.67E-06 4.51E-03	8.75E-05 8.75E-05 1.64E-03	_	
Firewater pump	Actual Potential	4.48E-06 4.48E-06	1.07E-04 1.07E-04		
Coal handling activities*	Optimized Actual	5.51E-03	2.00E-03	 1.83E-06	 1.58E-06
	Potential Optimized	_	_	1.83E-06 1.83E-06	1.58E-06 1.58E-06
Gasoline storage tank	Actual Potential		1.27E-03 1.27E-03		
	Optimized	_	2.37E-02	—	_

Table 4-9. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Annual TAPs (Continued, Page 2 of 3)

Table 4-9. Worst-Case Emission Rates (Potential	and Optimized) for Existing and Proposed Ec	juipment at the Lee Facility for Annual TAPs (Con-
tinued, Page 3 of 3)		

Source	Emission Rates	1,3-Butadiene	Benzene	Beryllium	Cadmium
Proposed combined-cycle firing natural gas	Actual Potential	9.67E-04 9.67E-04	2.79E-02 2.79E-02	5.33E-06 5.33E-06	4.89E-04 4.89E-04
Proposed combined-cycle firing fuel oil	Optimized Actual	1.19E+00 3.44E-02	5.22E-01 1.18E-01	3.41E-03 6.67E-04	2.54E-02 1.03E-02
	Potential Optimized	3.44E-02 4.23E+01	1.18E-01 2.21E+00	6.67E-04 4.27E-01	1.03E-02 5.36E-01
Proposed simple-cycle firing natural gas	Actual Potential	9.56E-04 9.56E-04	2.67E-02 2.67E-02	_	
Proposed simple-cycle firing fuel oil	Optimized Actual	1.18E+00 3.44E-02	4.99E-01 1.18E-01	 6.67E-04	1.03E-02
	Potential Optimized	3.44E-02 4.23E+01	1.18E-01 2.21E+00	6.67E-04 4.27E-01	1.03E-02 5.36E-01
Proposed auxiliary boiler	Actual Potential		1.75E-04 1.75E-04	1.00E-06 1.00E-06	9.17E-05 9.17E-05
Pronosed dev point heater	Optimized		3.27E-03	6.40E-04	4.77E-03
r toposed dew point neater	Potential	_	2.47E-05 2.47E-05	1.41E-07 1.41E-07	1.29E-05 1.29E-05
Proposed firewater pump	Actual	9.48E-06	4.62E-04 2.26E-04	9.02E-05	6./1E-04 —
	Potential Optimized	9.48E-06 1.17E-02	2.26E-04 4.23E-03		_

*Emissions for the existing coal-fired boilers and associated coal handling activities were not optimized. †Emissions represent the fuel oil combustion.

Source: ECT, 2011.

Source	Emission Rates	Scenario 1 (lb/hr)	Scenario 2 (lb/hr)
Coal-fired Boiler 1 and 2*	Actual	2.61E-06	
	Potential	3.25E-02	
	Optimized	3.25E-02	
Coal-fired Boiler 3*	Actual	3.22E-06	
	Potential	3.52E-02	
	Optimized	3.52E-02	
Lee IC Turbine 4	Actual	2.02E-07	2.02E-07
	Potential	2.95E-03	6.73E-04
	Optimized	2.95E-03	1.08E-03
Lee IC Turbine 5	Actual	2.66E-07	2.66E-07
	Potential	5.01E-03	1.14E-03
	Optimized	1.82E-03	1.82E-03
Lee IC Turbine 6	Actual	2.66E-07	2.66E-07
	Potential	5.01E-03	5.01E-03
	Optimized	1.82E-03	1.82E-03
Lee IC Turbine 7	Actual	2.96E-07	2.96E-07
	Potential	5.01E-03	5.01E-03
	Optimized	1.82E-03	1.82E-03
Lee IC Turbine 10 and 11 (fuel oil)	Actual	1.04E-06/	1.04E-06/
		5.00E-07	5.00E-07
	Potential	4.84E-03	4.84E-03
	Optimized	4.84E-03	4.84E-03
Lee IC Turbine 10 and 11(natural gas)	Actual	_	
	Potential		
	Optimized	_	

Table 4-13. Worst-Case Emission Rates (Actual, Potential, and Optimized) for Existing and Proposed Equipment at the Lee Facility for Arsenic

Source	Emission Rates	Scenario 1 (lb/hr)	Scenario 2 (lb/hr)
Lee IC Turbine 12 and 13 (fuel oil)	Actual	5.19E-07/ 6.13E-07	5.19E-07/ 6.13E-07
	Potential	4.57E-03	4.57E-03
	Optimized	4.57E-03	4.57E-03
Lee IC Turbine 12 and 13 (natural gas)	Actual	—	—
	Potential	—	—
	Optimized		
Lee IC Turbine 14 (fuel oil)	Actual	5.10E-03	5.10E-03
	Potential	5.10E-03	5.10E-03
	Optimized	5.10E-03	5.10E-03
Lee IC Turbine 14 (natural gas)	Actual	—	—
	Potential	—	—
	Optimized		<u> </u>
Black start engine generator	Actual	—	_
	Potential	—	—
	Optimized	—	—
Firewater pump	Actual	—	—
	Potential		—
	Optimized		<u> </u>
Coal handling activities*	Actual	8.86E-06	
-	Potential	8.86E-06	—
	Optimized	8.86E-06	<u> </u>
Gasoline storage tank	Actual		
-	Potential		—
	Optimized		_

Table 4-13. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Arsenic (Continued, Page 2 of 3)

Table 4-13. Worst-Case Emission Rates (Potential and Optimized) for Existing and Proposed Equipment at the Lee Facility for Arsenic (Continued, Page 3 of 3)

Source	Emission	Scenario 1	Scenario 2
	Rates	(lb/hr)	(lb/hr)
Proposed combined-cycle firing natural gas	Actual	8.88E-05	8.88E-05
	Potential	8.88E-05	8.88E-05
Proposed combined-cycle firing fuel oil	Actual Potential	1.42E-04 1.89E-02 1.89E-02 4.32E-03	1.42E-04 2.37E-02 2.37E-02 4.32E-03
Proposed simple-cycle firing natural gas	Actual Potential Optimized		
Proposed simple-cycle firing fuel oil	Actual	1.89E-02	2.37E-02
	Potential	1.89E-02	2.37E-02
	Optimized	4.32E-03	4.32E-03
Proposed auxiliary boiler	Actual	1.67E-05	1.67E-05
	Potential	1.67E-05	1.67E-05
	Optimized	1.65E-05	1.65E-05
Proposed dew point heater	Actual	2.35E-06	2.35E-06
	Potential	2.35E-06	2.35E-06
	Optimized	8.16E-07	8.16E-07
Proposed firewater pump	Actual Potential Optimized		

*Emissions for the existing coal-fired boilers and associated coal handling activities were not optimized. †Emissions represent the fuel oil combustion.

Source: ECT, 2011.

APPENDIX D

FACILITY DRAWINGS



	FUGITIVE E	EMISSIONS/EMISS	SIONS POINT L	OCATIONS	
LOCATION #	DESCRIPTION	APPROX. DIMENSIONS	BASE ELEVATION	HEIGHT	COORDINATES
FEP1	WET ASH RECEIVING - TRANSFER TO SHED	133'-0" X 121'-0"	100'-0"	5'-0"	763602.00 m E, 3918135.00 m N
FEP2	WET ASH RECEIVING - TRANSFER TO HOPPER	36'-0" X 70'-0"	100'-0"	10'-0"	763612.40m E, 3918127.49 m N
FEP3	UNLOADING PILE	13'-0" x 45'-0"	100'-0"	4'-0"	763614.14 m E, 3918149.15 m N
EP30	FEED SILO (1500 TON)	40'-0" Ø	96'-0"	111'-0"	763692.00 m E, 3918059.00 m N
EP31	STAR REACTOR (EXHAUST STACK)	10'-0" Ø	97'-0"	110"-0"	763708.58 m E, 3918096.09 m N
EP32	FGD BYPRODUCT SILO	N/A	97'-0"	65'-0"	763723.30 m E, 3918081.52 m N
EP33	FGD ABSORBENT SILO	37'-0" X 42'-0"	96'-0"	100'-0"	763734.05 m E, 3918073.42 m N
EP34	EHE 1 (DUST COLLECTOR)	17'-0" x 30'-0"	98'-0"	65'-0"	763670.00 m E, 3918093.00 m N
EP35	EHE 2 (DUST COLLECTOR)	17'-0" x 30'-0"	98'-0"	65'-0"	763662.00 m E, 3918083.00 m N
EP36	TRANSFER SILO (300 TON)	14'-0" Ø	97'-0"	100'-0"	763674.00 m E, 3918075.00 m N
EP37	STORAGE DOME (ASH)	120'-0" Ø	95'-0"	125'-0"	763774.00 m E, 3918011.00 m N
EP38	LOADOUT SILO (1500 TON)	40'-0" Ø	96'-0"	111'-0"	763792.00 m E, 3918037.00 m N
EP38A	LOAD OUT SILO CHUTE 1A	77'-0" X 84'-0" (COMBINED)	96'-0"	111'-0"	763789.00 m E, 3918033.00 m N
EP38B	LOADOUT SILO CHUTE 1B	77'-0" X 84'-0" (COMBINED)	96'-0"	111'-0"	763795.00 m E, 3918041.00 m N
	FIN FANS	75'-0" X 30'-0"	0'-0"	45'-0"	
	BAG HOUSE	15'-0" X 32'-0"	0'-0"	60'-0"	
	CONTROL	80'-0" X 100'-0"	0'-0"	20'-0"	
	PROPANE STATION	30'-0" X 30'-0"	0'-0"	N/A	



NOTES: - BASE ELEVATION IS TAKEN FROM SEA LEVEL AND TO BE CONSIDERED PRELIMINARY. - HEIGHTS ARE FROM BASE ELEVATION AND CONSIDERED APPROXIMATE. - COORDINATES ARE TO BE CONSIDERED APPROXIMATE.

60 0 25 50

REV.	DESCRIPTION	CHK.	DATE	APF





APPENDIX E

AIR DISPERSION MODELING







APPENDIX F

NHSM DETERMINATION



North Carolina Department of Environment and Natural Resources

Pat McCrory Governor Donald R. van der Vaart Secretary

June 10, 2015

Mr. Jim Clayton The SEFA Group 217 Cedar Road Lexington, SC 29073

SUBJECT: Applicability Determination No. 2501 The SEFA Group Lexington, SC

Dear Mr. Clayton:

The North Carolina Division of Air Quality (DAQ) received your letter dated September 5, 2014, requesting the DAQ's concurrence with its determination of regulatory status of certain coal combustion residues, when used in its Staged Turbulent Air Reactor (STAR Reactor), in accordance with 40 CFR 241 "Solid Wastes Used As Fuels or Ingredients in Combustion Units" ("Solid Waste Definition Rule" or "Rule" hereinafter).

Specifically, SEFA Group (SEFA) requests the confirmation that coal ash obtained from the following specific sources meets the requirements in §241: flyash received directly from coal-fired power plant's particulate collection infrastructure (i.e., electrostatic precipitator or baghouse), and processed flyash received from landfills and ash ponds.

Unless exempt, combustion of "non-hazardous secondary material (NHSM), as defined in §241.2 would subject the emissions unit (such as STAR reactor) to requirements in 40 CFR 60 Subpart CCCC "Standards of Performance for Commercial and Industrial Solid Waste Incineration Units" or, Subpart DDDD "Emissions Guidelines and Compliance Times for Commercial and Industrial Solid Waste Incineration Units". These regulations are commonly known as CISWI ("Commercial and Industrial Solid Waste Incineration").

The DAQ has determined that the coal ash received directly from the coal-fired power plant's particulate collection infrastructure (i.e., electrostatic precipitator or baghouse) is a NHSM and an "ingredient", as defined in §241.2. DAQ has further determined that this flyash meets the legitimacy criteria included in §241.3(d)(2) and thus, concludes that it is not a solid waste. Therefore, the STAR Reactor is not subject to the requirements in CISWI.

Moreover, the processed flyash received from landfills or ash ponds is a NHSM and an ingredient, and DAQ has determined that this flyash also meets the legitimacy criteria included in 241.3(d)(2), and thus, concludes that it is not a solid waste. Therefore, the STAR Reactor is not subject to the requirements in CISWI.

1641 Mail Service Center, Raleigh, North Carolina 27699-1641 Phone: 919-707-8400 / Internet: www.ncdenr.gov

The following includes discussion on STAR Reactor, and technical and regulatory analysis supporting these conclusions for each of the above types of flyash:

STAR Reactor

The STAR Reactor is a patented technology developed by SEFA for thermal beneficiation / processing of either a low or high-Btu value fine particulate matter, such as the above described flyash [hereinafter "feedstock"], along with other ingredient materials (gas, solids, and liquids) into a variety of commercial products. These products are used not only for application as a partial cement replacement but for many other commercial and industrial applications. There are several products which SEFA is currently capable of producing because of the flexibility embodied in this reactor. For example, STAR[®] RP, Ultrix[®], Spherix[®], Fortimix[®], and PermanixTM.

The STAR Reactor process is inherently flexible in that operating parameters can be varied and different ingredients can be added to produce a desired product. The primary component of the STAR Reactor is a cylindrical refractory-lined vessel in which the majority of the process reactions take place. These reactions can include a range of both chemical and physical reactions. Air is required for pneumatic uplift of the solids and for the process reactions enters through the floor of the STAR Reactor as well as through the walls at multiple locations. The raw feedstock and any other ingredients are introduced through the walls of the STAR Reactor. All of the solids and gases exit together at the top of the reactor. The gas/solids mixture enters a hot cyclone where the majority of solids are separated from the gas and recycled back to the STAR Reactor. The very high rate of hot recycle solids increases the operating flexibility of the process. The process reactions can occur through this reactor/hot cyclone loop. Due to the high gas velocity, the multiple injection points, and the recycle solids, there is a significant amount of turbulence created which enhances the mixing of the ingredients and optimizes the reactions. The gas and remaining solids not collected by the hot cyclone are passed over a heat exchanger which can be designed to preheat the process air, used in heat recovery, or to simply cool the gas/solids mixture. Once cooled, the solids are separated from the gas in a fabric filter recovery device. Solids can also exit the STAR Reactor at the bottom or from the recycle loop. These solids can be combined with the solids/gas stream before the heat recovery equipment or, since they have different characteristics as compared to the solids exiting the hot cyclone, they can be processed separately for a particular application. By design the STAR Reactor operates under a wide range of process parameters.

Technical and Regulatory Analysis

Flyash Received Directly from Coal-fired Power Plant's Particulate Collection Infrastructure (i.e., Electrostatic precipitator or Baghouse)

As described above, the STAR Reactor is capable of utilizing flyash, received directly from coal-fired power plant's particulate emissions controls, as its primary ingredient along with other select ingredients in order to produce a variety of products for markets.

§241.2(b)(3) of the rule defines NHSM as "a secondary material that, when discarded, would not be identified as a hazardous waste under Part 261 of this chapter". Further the same section defines secondary material as "any material that is not the primary product of a manufacturing or commercial process, and can include post-consumer material, off-specification commercial chemical products or manufacturing chemical intermediates, post-industrial material, and scrap."

It is indisputable that flyash generated from combustion of coal is not a "primary product of a manufacturing" facility (such as electric generating facility) and this product can be deemed as "post-industrial material". Moreover, coal flyash is not regulated as a hazardous waste as per Part 261 of 40 CFR "Identification and Listing of Hazardous Waste". In fact, EPA has promulgated a rule on April 17, 2015 (80 FR 21302) to regulate disposal of coal combustion residues (fly ash, bottom ash, boiler slag, and flue gas desulfurization materials generated from burning coal for the purpose of generating electricity by electric utilities and independent power producers) [CCR] as solid waste under Subtitle D "State or Regional Solid Waste Plans" of the Resource Conservation Act (RCRA) [administrative regulations included in 40 CFR 257) and not under the Subtitle C of the RCRA "Hazardous Waste Management" [administrative regulations included in 40 CFR 261]. In addition, the beneficial uses (e.g., use of flyash in concrete manufacturing replacing traditional product cement) of CCR is exempt from this regulation.

Based, on the above discussion, it is concluded that the flyash generated from the coal combustion and received directly from coal-fired power plant's particulate emissions control devices, is a NHSM.

§241.3(b)(3) of the Solid Waste Definition Rule provides that NHSMs are not solid waste when "used as an ingredient in a combustion unit that meet the legitimacy criteria specified in paragraph (d)(2) of this section." §241.2 of the Solid Waste Definition Rule defines "ingredient" as "a non-hazardous secondary material that is a component in a compound, process or product." The feedstock is merely one component among a number of variables which are introduced to the STAR Reactor to produce many different products. Therefore, feedstock processed in the STAR Reactor is an ingredient under the Solid Waste Definition Rule.

Legitimacy Criteria

For a non-hazardous secondary material used as an ingredient to be excluded from the definition of solid waste under 241.3 of the Solid Waste Definition Rule, the material must satisfy the following legitimacy criteria under Subsection (d)(2):

- (i) The non-hazardous secondary material must be managed as a valuable commodity;
- (ii) The non-hazardous secondary material must provide a useful contribution to the production or manufacturing process.
- (iii) The non-hazardous secondary material must be used to produce a valuable product or intermediate.

(iv) The non-hazardous secondary material must result in products that contain contaminants at levels that are comparable in concentration to or lower than those found in traditional products that are manufactured without the non-hazardous secondary material.

Managed as a Valuable Commodity - §241.3(d)(2)(i)

SEFA stores its feedstock in silos and or covered shelters prior to using it as an ingredient in the STAR Reactor and conveys the material to the process equipment pneumatically. As per 241.3(d)(2)(i), the Solid Waste Definition Rule identifies the following three factors to be considered in determining whether a material is managed as a valuable commodity:

- (A) The storage of the non-hazardous secondary material prior to use must not exceed reasonable time frames;
- (B) Where there is an analogous ingredient, the non-hazardous secondary material must be managed in a manner consistent with the analogous ingredient or otherwise be adequately contained to prevent releases to the environment;
- (C) If there is no analogous ingredient, the non-hazardous secondary material must be adequately contained to prevent releases to the environment;

As per SEFA, in a previously permitted design, the storage capacity of the silos and partially enclosed storage bins for incoming feedstock ranges from 800-2000 tons and could accommodate approximately three to ten days of production when the STAR Reactor is operating on SEFA's normal production schedule. As such, under normal operations, the incoming feedstock is typically stored no more than three days prior to introduction into the STAR Reactor process. However, during shutdown of the STAR Reactor or when off-specification feedstock is received from a supplier, the feedstock may be stored for longer periods of time, but usually no more than sixty days. In the past, as per SEFA, shutdown of the STAR Reactor has generally not exceeded twenty days. With respect to the management of off-specification feedstock, SEFA has indicated that if this off-specification material can be blended with other feedstock at ratios which ensure that processing in the STAR Reactor produces an end product which meets SEFA's quality control standards, it will attempt to do so. Depending on the nature and amount of the material's deviation from SEFA's feedstock specifications, if it cannot be blended, the offspecification feedstock will have to be rejected and returned to the supplier. If it is capable of being blended, the blending process may require storage of the off-specification feedstock for as long as 60 days depending upon the quantity involved. Accordingly, even outside of the normal three-day processing scheduling for incoming feedstock, SEFA's storage of incoming feedstock does not exceed a reasonable time frame.

Additionally, SEFA manages the incoming feedstock as a valuable commodity and takes measures to prevent loss of material during off-loading and storage. In the preamble to the rule, EPA explains that "If on the other hand, a company does not manage the non-hazardous secondary material as it would traditional ingredients, that behavior may indicate that the non-

hazardous secondary material is being discarded." Refer to 76 FR 15543. The material must be "stored in a manner that both adequately prevents releases or other hazards to human health and the environment, considering the nature and toxicity of the non-hazardous secondary material." *Id.* In most cases, this requirement is satisfied if the material is in some manner "contained." *Id.* As noted, SEFA stores its feedstock in enclosed silos or covered and partially enclosed storage bins and therefore meets this criterion. Additionally, at all times prior to processing, SEFA handles the material in a manner consistent with this criterion. Feedstock is transferred from its suppliers (typically, coal-fired power plants) to SEFA either (i) directly by pneumatic conveyor into the silos or (ii) by truck to the SEFA facility. All bin vents within the pneumatic conveyer system are equipped with fabric filter recovery devices to minimize loss of this valuable material. Thus, SEFA believes that it unquestionably manages its feedstock as a valuable commodity.

Useful Contribution to the Production or Manufacturing Process - §241.3(d)(2)(ii)

SEFA believes that there is no question that the feedstock processed in the STAR Reactor provides a useful contribution to its production of the various end products marketed by SEFA. In the preamble to the Solid Waste Definition Rule, at 76 FR 15543, EPA explains the rationale behind this criterion for legitimacy:

A non-hazardous secondary material used as an ingredient in combustion systems provides a useful contribution if it contributes valuable ingredients to the production/manufacturing process or to the product or intermediate of the production/manufacturing process. This criterion is an essential component in the determination of legitimacy because legitimate use is not occurring if the nonhazardous secondary material doesn't add anything to the process, such that the non-hazardous secondary material is basically being disposed of or discarded. This criterion is intended to prevent the practice of "sham" recycling by adding non-hazardous secondary materials to a manufacturing operation simply as a means of disposing of them.

SEFA states that the feedstock processed in the STAR Reactor is clearly not added to dispose of that material and the processing of the feedstock in the STAR Reactor can in no manner be characterized as "sham" recycling. Additionally, the fact that some of the constituents of the feedstock are not needed or desirable for the STAR Process does not affect the status of the "useful contribution" of the feedstock:

For purposes of satisfying this criterion, not every constituent or component of the non-hazardous secondary material has to make a contribution to the production/manufacturing activity. For example, non-hazardous secondary materials used as ingredients may contain some constituents that are needed in the manufacturing process, such as, for example, zinc in non-hazardous secondary materials that are used to produce zinc-containing micronutrient fertilizers, while other constituents in the non-hazardous secondary material, such as lead, do not provide a useful contribution. Provided the zinc is at levels that provides a useful contribution, we believe the non-hazardous

secondary material would satisfy this criterion, although we would note that the constituents not directly contributing to the manufacturing process could still result in the non-hazardous secondary material not meeting the contaminant part of the legitimacy criteria. The Agency is not quantitatively defining how much of the non-hazardous secondary material needs to provide a useful contribution for this criterion to be met, since we believe that defining such a level would be difficult and is likely to be different, depending on the non-hazardous secondary material. The Agency recognizes that this could be an issue if persons argue that a non-hazardous secondary material is being legitimately used as an ingredient, but in fact, only a small amount or percentage of the non-hazardous secondary material is used.

76 FR 15543-44 (emphasis added).

The fact that reactions in the STAR Reactor eliminate certain undesirable constituents of the feedstock material does not preclude a determination that the feedstock meets the legitimacy criteria as an ingredient. As described above, the STAR Reactor has the capability to control the chemical and physical reactions in the process to produce marketable materials with a broad range of characteristics. The constituents and characteristics of each STAR Reactor product are tailored to the intended market and vary depending on the needs of that market. The elimination of certain constituents does not affect the determination that the feedstock is an ingredient which makes a useful contribution to the products produced in the STAR Reactor.

Produces a Valuable Product or Intermediate - §241.3(d)(2)(iii)

As per SEFA, it is undisputed that feedstock material is used in the STAR Reactor to make valuable products. "The product or intermediate is valuable if it is (i) sold to a third party or (ii) used as an effective substitute for a commercial product or as an ingredient or intermediate in an industrial process." Refer to 76 FR 15544. Also, as discussed above, the STAR Reactor has the capability to process its fly ash and other materials to produce a broad range of products. All of the products currently produced in the STAR Reactor are sold to third parties. Additionally, the various products produced in the STAR Reactor have application as both substitutes for commercial products and as ingredients in an industrial process. Ultrix[®] and STAR RP[®] are sold for use as partial replacement for Portland cement. Fortimix[®] is sold for use as an additive for rubber compounds. PermanixTM is designed for use as a broad-spectrum UV blocker. Accordingly, in all respects, SEFA's feedstock processed in the STAR Reactor satisfies this criterion for legitimacy as an ingredient.

Comparable Contaminants Concentration of End Product - § 241.3(d)(2)(iv)

Again, as discussed above, the STAR Reactor has the capability to process its feedstock to reduce or eliminate some undesirable constituents and to alter the chemical and physical characteristics of others in its various end products. The Solid Waste Definition Rules provides as follows:

> The non-hazardous secondary material must result in products that contain contaminants at levels that are comparable in concentration to or lower than those found in traditional products that are manufactured without the non-hazardous secondary material.

Refer to §241.3(d)(2)(iv).

The preamble to the Rule includes the following:

The assessment of whether the products produced from the use of nonhazardous secondary materials that have contaminants that are comparable to (or lower) in concentration can be made by a comparison of contaminant levels in the ingredients themselves to the traditional ingredients they are replacing, or by comparing the contaminant levels in the product itself with and without the use of the nonhazardous secondary material.

Refer to 76 FR 15544.

As applied to the use of the feedstock as an ingredient in the STAR Reactor, the relevant comparison is a comparison of the various STAR Reactor end products to comparable products in the industries in which each is used. For example, Ultrix[®] and STAR RP[®] are both used as supplementary cementitious materials in concrete, but, due to the unique processing regime of the STAR Reactor, neither has varying quantities of adsorptive unburned carbon, which characterize by-product fly ashes typically used in the marketplace. In fact, the air-entraining characteristics of Ultrix[®] and STAR RP[®] are tailored by STAR Reactor to exactly match the air-entraining characteristics of plain cement concrete.

The preamble to the proposed rule for the Solid Waste Definition Rule explains the rationale for and purpose of the comparison of contaminants in the legitimacy criteria for use of a non-hazardous secondary material as an ingredient:

The Agency recognizes that there may be instances where the contaminant levels in the products manufactured from non-hazardous secondary material ingredients may be somewhat higher than found in the traditional products that are manufactured without the non-hazardous secondary material, but the resulting concentrations would not be an indication of discard and would not pose a risk to human health and the environment.

Refer to 75 FR 31844, 31885 (Jun. 4, 2010).

In addition, EPA has recognized that contaminant levels in the products made from NHSM can have contaminant levels within a "small acceptable range" at 76 FR 15523 (March 21, 2011).

The above discussion clearly provides that it may be allowable under §241.3(d)(2)(iv) for certain contaminants in the end product made with non-hazardous secondary materials ingredients to be "somewhat higher" or within a "small acceptable range" than those in traditional products. Thus, SEFA's fly ash feedstock satisfies the legitimacy criterion in §241.3(d)(2)(iv) despite the slightly higher concentrations of arsenic and beryllium in the STAR RP[®] as compared to Portland Cement, as included in Attachment A to the SEFA's September 2014 letter. Also, using additional analytical data received from SEFA¹, it can be said that the contaminant levels in the SEFA product are within the range of contaminants levels or within a "small acceptable range" for Portland Cement (traditional product).

Additionally, as stated in the preamble to the proposed rule above, the purpose of the contaminant comparison criterion is to demonstrate that the use of the non-hazardous secondary material ingredient is not indicative of discard and does not pose a risk to human health and the environment. Expanding of the "indication of discard" aspect of this component of the legitimacy criteria, EPA further explains:

Based on our assessment of all of the comments, we believe it appropriate to include contaminant levels as a legitimacy criterion. Thus, we do not agree with those commenters that assert that contaminant comparisons are not appropriate to require as part of the legitimacy criteria. The Agency believes the criterion is necessary because non-hazardous secondary materials that contain contaminants that are not comparable in concentration to those contained in traditional fuel products or ingredients would suggest that these contaminants are being combusted as a means of discarding them, and thus the non-hazardous secondary material should be classified as a solid waste. In some cases, this can also be an indicator of sham recycling.

Refer to 75 FR 31871-72 (emphasis added).

As such, the primary purpose of the comparison on contaminants in an end product using the non-hazardous secondary material ingredient to that of traditional products made without the non-hazardous secondary material ingredient is to demonstrate that such use is not a means of discarding the non-hazardous secondary material or indicative of sham recycling.

With respect to the additional industrial uses for products produced by using fly ash feedstock as an ingredient in the STAR Reactor, a direct comparison of SEFA's end product to a traditional product which is manufactured without fly ash feedstock is not feasible for many of the end products produced in the STAR Reactor. However, based on the detailed comparison of the STAR[®] RP to Portland Cement and the various markets for SEFA's other STAR Reactor products as included in the above referenced submittal, it is clear that SEFA is not processing the fly ash feedstock as a means of discarding the fly ash or any of its constituents.

¹ Email dated 5/12/2015 from Thomas Pritcher, Environmental Consulting & Technology, Inc., to Rahul Thaker, NCDAQ.

To the extent that the purpose of the contaminant comparison is to demonstrate that these products do not pose a risk to human health and the environment, SEFA has provided additional information as well as copies of the material safety data sheets for these products to demonstrate that no such risk is posed in the various industrial uses of STAR Reactor end products. For example, the material safety data sheets for Spherix[®] and Fortimix[®] included in Attachment B to the SEFA's September 2014 letter. As per SEFA, in many cases, the STAR[®] Reactor end products provide a safe alternative to traditional products which may pose a potential risk to human health and the environment.

Flyash Received from Landfill or Ash Pond

\$241.3(b)(4) of the rule provides that NHSMs are not solid waste when "fuel or ingredient products that are used in a combustion unit, and that are produced from the processing of discarded non-hazardous secondary materials and that meet the legitimacy criteria specified in paragraph (d)(1) of this section, with respect to fuels, and paragraph (d)(2) of this section, with respect to ingredients."

As discussed above, the coal flyash disposed off in a landfill or an ash pond can be deemed as a NHSM. Prior to being used as an acceptable ingredient (feedstock) in the STAR Reactor, any flyash received from landfills or ash ponds must be "processed," as that term is defined in the rule. As discussed below, any commercial agreement between a supplier and SEFA will specify the acceptable criteria (i.e., specifications) for a feedstock that can be used in the STAR Reactor as a condition for supplying processed flyash to SEFA.

Pursuant to §241.2, "processing" means any operations that transform discarded nonhazardous secondary material into a non-waste fuel or non-waste ingredient product. Processing includes, but is not limited to, operations necessary to: remove or destroy contaminants; significantly improve fuel characteristics of the material, *e.g.* sizing or drying the material in combination with other operations; or chemically improve the as-fired energy content. Minimal operations that result only in modifying the size of the material by shredding do not constitute processing for purposes of this definition. Under the same section of the Rule, "Secondary material" is defined as any material that is not the primary product of a manufacturing or commercial process, and can include post-consumer material, off-specification commercial chemical products or manufacturing chemical intermediates, post-industrial material, and scrap.

While it is recognized that coal flyash which was initially placed into a landfill may be considered to have been "previously discarded" by custom and practice, coal-fired utilities also collect this coal ash in permitted wastewater treatment ponds. This coal ash has not historically been considered "discarded" as it was merely solids settling within a permitted wastewater unit. SEFA believes that the processing of these materials as required to satisfy SEFA's specifications for its feedstock would meet the requirements for processing of "previously discarded" materials under the Solid Waste Definition Rule as applied to CISWI. As such, the requisite processing of materials to be used as feedstock in the STAR Reactor would be sufficient to transform them to an ingredient.

The Solid Waste Definition Rule provides that a previously discarded material may be processed to transform the waste to a non-waste ingredient. Specifically, §241.3(b)(4) of the Solid Waste Definition Rule provides as follows:

Fuel or ingredient products that are used in a combustion unit, and are produced from the processing of discarded non-hazardous secondary materials and that meet the legitimacy criteria specified in paragraph (d)(1) of this section, with respect to fuels, and paragraph (d)(2) of this section, with respect to ingredients. The legitimacy criteria apply after the non-hazardous secondary material is processed to produce a fuel or ingredient product. Until the discarded nonhazardous secondary material is processed to produce a non-waste fuel or ingredient, the discarded non-hazardous secondary material is considered a solid waste and would be subject to all appropriate federal, state, and local requirements.

As per SEFA, any processing of materials from landfills or from ash ponds to meet SEFA's feedstock specifications will be undertaken under the control of the supplier prior to being received by SEFA for use an ingredient in its STAR Reactor. Accordingly, this feedstock when received by SEFA or used in the STAR Reactor would meet the legitimacy criteria for direct use as an ingredient and therefore would not be a solid waste under the Solid Waste Definition Rule. All feedstock shipped to SEFA for use as an ingredient in the STAR Reactor will first be required to undergo processing by the supplier to be:

- A. Free of all, but minimal contaminants (e.g., organic debris, slag);
- B. Finely-divided and free-flowing,
- C. Have consistent moisture content of $\leq 25\%$; and
- D. Have a consistent chemical composition, including organic content as measured by loss on ignition.

The above are SEFA specifications for acceptance of any coal flyash (discarded in landfills or ash ponds).

As per SEFA, the specific processing steps that may be needed to meet the SEFA specifications (as described above) and produce a suitable feedstock for the STAR Reactor will vary depend upon the specific characteristics of each source of coal flyash. Generally speaking, one or more of the following four processing steps will be necessary to produce a suitable feedstock for the STAR Reactor:

- 1) Dewatering,
- 2) Screening/Separation,
- 3) Milling, and
- 4) Blending.

For use as a feedstock in the STAR Reactor, coal ash from an ash pond having higher moisture content will likely need to be processed using most, if not all, of these steps. Coal ash
Mr. Jim Clayton June 10, 2015 Page 11

from a landfill may not require every step. For example, it may be unnecessary to dewater coal ash from landfills if the material has consistent and acceptable moisture content.

Depending on the source of the ash, the general steps described above can require sub processes. For example, feedstock appropriate for the STAR Reactor, it may be necessary to remove larger particles or other materials found with the ash. In addition, to meet SEFA's specifications, some coal ash may require further processing through a separate loop that includes equipment (e.g., roll crusher) needed to produce a more finely-divided, free-flowing feedstock. For others, it may be necessary to utilize a magnetic separator to remove metal constituents. Also, materials such as coal, pyrites, or other more coarse materials may need to be screened. The Screening/Separation step will occur routinely to produce a free-flowing, finely-divided feedstock suitable for the STAR Reactor. Depending on the source of coal ash, milling may not be necessary to achieve a finely-divided and free-flowing material.

As emphasized by SEFA, the specific processing steps and the specific processing equipment cited above are typical examples for how these materials might be processed to produce a suitable feedstock. Those performing the actual work (i.e., suppliers) will elect to use different techniques and/or equipment. SEFA states that as long as the processed coal ash conforms to SEFA's general specifications outlined above, the coal flyash received from landfills or ash ponds will have been sufficiently "processed" and will be a suitable feedstock as an ingredient in the STAR Reactor.

It needs to be noted here that the EPA has recognized similar processing steps (similar to SEFA suggested processing steps as above to meet the SEFA specifications) are "likely to meet our definition of processing, as it appears that these processes in fact remove contaminants and improve the ingredient characteristics of these recovered CCRs (i.e., ash from ponds and landfills)". Refer to 76 FR 15518, March 21, 2011 (emphasis added).

With respect to the requirement for meeting the legitimacy criteria in §241.3(d)(2), pursuant to §241.3(b)(4), for flyash received from landfill or ash pond, SEFA emphasizes that after completion of "processing", it will become similar to the flyash received directly from coal-fired plant's particulate collection infrastructure (i.e., Electrostatic precipitator or Baghouse), and thus, will meet all legitimacy criteria as discussed above for it.

Finally, with respect to the particular criterion for comparable contaminants concentration of end product (traditional products) in 241.3(d)(2)(iv), SEFA analyzed each of these materials for semi-volatile organic compounds, organo-chlorine pesticides, PCBs, chlorides, metals and sulfur content, during engineering studies to assess the suitability of coal ash previously placed in water treatment ponds (pond ash) or previously placed in landfills (landfill ash). A comparison of the constituents in dry source feedstock, pond ash and landfill ash from SCE&G's² Wateree facility is provided in Attachment C to the SEFA's September 2014 submittal. In comparison to the dry collection feedstock, the landfill ash is comparable with slightly higher results for a few constituents. The sampling results on pond ash indicate that all constituents detected were lower

² www.sceg.com

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than those for the dry collection feedstock and the landfill ash. Despite certain variables in the manner in which coal ash were previously placed in ponds or landfills, as per SEFA, these sampling results are sufficient to demonstrate that contaminants in coal flyash previously placed in ponds and landfills are comparable to or lower than those in dry collection coal flyash processed as feedstock (that is, flyash received directly from the coal-fired power plant's particulate emissions control) for the STAR Reactor. Furthermore, the metals and sulfur levels of the landfill ash are comparable to those of the dry collection feedstock, and the metals and sulfur levels of the pond ash are significantly lower than those of the dry collection feedstock. Finally, more recent sampling data (March-April 2015) for dry ash and pond ash, provided by SEFA, indicates that the contaminants in pond ash as are lower than the dry ash received directly from electric utility plant.³ Therefore, SEFA concludes that there will be no increase in emissions as a result of the use of pond ash and landfill ash as a feedstock for the STAR Reactor.

Conclusions

In summary, the DAQ has determined that the fly ash received directly from the coalfired power plant's particulate collection infrastructure (i.e., electrostatic precipitator or baghouse) is a NHSM and an "ingredient", as defined in §241.2. DAQ has further determined that this flyash meets the legitimacy criteria included in §241.3(d)(2). Thus, it concludes that it is not a solid waste and therefore, STAR Reactor is not subject to the requirements in CISWI.

Moreover, the processed flyash received from ash landfills or ash ponds meets the definition of "processing" in §241.2, and is also a NHSM and an ingredient. DAQ has further determined that this flyash also meets the legitimacy criteria included in §241.3(d)(2). Thus, it concludes that it is not a solid waste and therefore, STAR Reactor is not subject to the requirements in CISWI.

It needs to be emphasized here that this letter includes only the "non-waste" determination, which is specific to the materials discussed herein. Further, the determination does not give any permission to SEFA to burn or process flyash in the STAR Reactor. SEFA will need to evaluate and submit a permit application for an air permit, as needed, for burning / processing flyash, as discussed herein, in the STAR Reactor at any location in NC.

If you have any questions regarding this determination, please contact Rahul P. Thaker, P.E., QEP, at (919) 707-8470.

³ Email dated 5/12/2015 from Thomas Pritcher, Environmental Consulting & Technology, Inc., to Rahul Thaker, NCDAQ.

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Sincerely,

With With _

William D. Willets, P.E., Chief, Permitting Section Division of Air Quality, NCDENR

c: Central Files

APPENDIX G

CAM PLAN



COMPLIANCE ASSURANCE MONITORING PLAN

for

Sulfur Dioxide (SO₂) Emissions from STAR® Unit Duke Energy Progress, LLC – H. F. Lee Steam Electric Plant Goldsboro, Wayne County, North Carolina

I. Background

 SO_2 :

A.	Emissions Unit and Control Device	
	EU ID:	ES-31
	Description:	STAR® (Staged Turbulent Air Reactor) system with a 140 million Btu/hour total heat rate input that processes feed-stock (fly ash and other ingredient materials) into a variety of commercial products
	Control Device	Dry Flue Gas Desulfurization (FGD) scrubber and bagfilter for SO ₂ emissions control
B.	. Applicable Emissions Limits and Monitoring Practices	
	Emissions Limits:	

2.3 pounds of sulfur dioxide per million BTU input per 15A NCAC 02D .0516 Sulfur Dioxide Emission From Combustion

	Compliance Demonstration Requirements:			
•	SO ₂	Initial performance tests will be conducted.		
	Lime-to-Sulfur Ratio	XXX establish compliance demonstration procedures parametric monitoring systems.	for	
	Baghouse ΔP	XXX establish compliance demonstration procedures parametric monitoring systems.	for	
	Periodic Monitoring Requirements:			
	SO_2	TBD		
	Lime-to-Sulfur Ratio	TBD		

Baghouse ΔP TBD

C. Control Technology

Dry FGD scrubber and bagfilter for SO₂ emissions control

D. Potential Emission Rates

Pre-control SO₂: XXX tons/year Post-control SO₂: XXX tons/year (assumes 95% control)

II. Monitoring Approach

A. <u>Background</u>

For emissions of sulfur dioxide (SO₂) from the STAR® system, Duke Energy is subject to Compliance Assurance Monitoring (CAM) requirements for the state SO₂ standard, i.e., 2.3 lb/MMBtu per 15A NCAC 02D .0516.

Duke Energy selected Lime-to-Sulfur Ratio and Pressure drop across the baghouse (Baghouse ΔP) as indicators for the CAM Plan for SO₂ emissions from the STAR® system. Duke Energy conducted testing for SO₂ emissions to derive a relationship between the Lime-to-Sulfur Ratio and SO₂ emissions of the STAR® system. This relationship was then used to determine a Lime-to-Sulfur Ratio value for the applicable SO₂ limit, such that as long as the Lime-to-Sulfur Ratio is at or above the value during normal operation, there is a reasonable assurance that the STAR® system will also comply with the respective applicable SO₂ emission limit. This relationship was used to determine appropriate Lime-to-Sulfur Ratio value for the state standard of 2.3 lb/mmBtu. In addition, Duke Energy established an appropriate Baghouse ΔP range based on manufacturer's specifications and recommendations. It is assumed as long as the Baghouse ΔP is within the established range during normal operation, there is a reasonable assurance that the dry FGD baghouse is operating as designed and the STAR® system will also comply with the respective applicable SO₂ emission limit.

B. <u>CAM SO₂ Testing</u>

SO₂ testing was conducted to derive a relationship between the Lime-to-Sulfur Ratio and SO₂ emissions of the STAR® system. The SO₂ testing was conducted for operating conditions of the dry FGD system resulting in High-Ash Sulfur Content, Mid- Ash Sulfur Content and Low- Ash Sulfur Content.

The table below provides a summary of the test results for CAM testing completed on XXXX. Each test consisted of at least three runs using USEPA Test Method XXX for XXX. For the operating conditions tested, all SO₂ emission test results were less than XX percent of the applicable state SO₂ emission limitation (2.3 lb/mmBtu).

Insert Table of Results

Baghouse ΔP was monitored and recorded during the testing to verify that the operating range of is appropriate for the baghouse

C. <u>CAM Averaging Period</u>

The CAM Rule does not provide specific averaging periods to be used in the development of monitoring approaches. However, 40 CFR 64.3(d)(3)(i) implies that the appropriate averaging period is the averaging period of the underlying emissions standard. Since emissions testing for SO₂ includes at least three test runs, each nominally one-hour in duration, this indicates that a three-hour averaging period is an appropriate averaging time for purposes of CAM for the state rule.

D. <u>CAM Excursion</u>

During "normal operation", (i.e., periods other than startup, shutdown or malfunction), an excursion is a rolling three-hour period Lime-to-Sulfur Ratio is less than the establish value during testing. Each excursion must be investigated by the source to determine the monitoring status and operating conditions responsible for the excursion.

E. <u>CAM Excursion Corrective Action</u>

Upon detecting an excursion, Duke Energy will implement corrective action to restore the indicator to the appropriate indicator range. Corrective action should begin with an evaluation of the monitoring system to determine if the excursion is related to the monitoring system or the control device. Individual unit process and control device operating parameters will be reviewed to determine the cause of the excursion. To the extent possible, any corrective action should reduce the potential of similar excursions from recurring.

F. <u>CAM Reporting Requirements</u>

All excursions must be reported in the facility's semi-annual report. As required by the CAM Rule, the Permittee shall include summary information on the number, duration and cause of excursions and the corrective actions taken. It is not necessary to report SO₂ control equipment malfunctions that do not cause an excursion. Duke Energy will also include summary information on the number, duration, and cause of monitor downtime incidents.

G. <u>Summary of Proposed CAM for SO₂</u>

Continuous monitoring of Lime-to-Sulfur Ratio is required. If the Lime-to-Sulfur Ratio does not fall below the level established during initial compliance testing and the Baghouse ΔP is within the established range provided by manufacturer's specifications and recommendations, then compliance will be reasonably assured. The minimum Lime-to-Sulfur Ratio will not apply during periods of startup, shutdown, or malfunction. A summary of the CAM plan is provided in Table 1.

Table 1 SO₂ CAM Plan Summary – H. F. Lee Steam Electric Plant

STAR® Unit (ES-31)

A. Indicator	Lime-to-Sulfur Ratio and Baghouse ΔP
Measurement Approach	XXXX
B. Indicator Range	An excursion is defined as
	The Lime-to-Sulfur Ratio to be determined during the initial performance testing will provide reasonable assurance of compliance with limits to be contained in the Title V air permit. Excursions will trigger an inspection of the Lime injection system to determine the cause and necessary corrective action. If the Lime-to-Sulfur Ratio falls below acceptable levels (e.g. an excursion) for more than XX consecutive unit operating hours, a test will be performed to re-establish the SO ₂ emission rate and lime injection correlation for the ash sulfur content range.
	Baghouse $\Delta P \dots$
C. Performance Criteria	
1. Data Representativeness	TBD
2. Verification of Operational Status	TBD
3. QA/QC Practices and Criteria	TBD
4. Monitoring Frequency	TBD
5. Data Averaging Period	TBD
6. Data Collection	Automated data acquisition system (DAHS)

III. Monitoring Approach Justification

A. <u>Explanation of Applicability</u>Justification will be added based on final vendor design data

B. <u>Rationale for Selection of Indicator Ranges</u> To be determined...

NC DEQ will be provided copies of test results from all required tests.

C. Rationale for Selection of Corrective Actions

To be determined...

APPENDIX H

ZONING COMMISSION DOCUMENTATION





October 27, 2017

SENT VIA EMAIL

Mr. Chip Crumpler Director of Planning Wayne County 224 E. Walnut Street Goldsboro, NC 27530

Dear Mr. Crumpler,

On behalf of Duke Energy, I am writing to inform you that we intend to construct and an ash beneficiation plant at 1199 Black Jack Church Road in Goldsboro and Wayne County. I hereby certify that to the best of my knowledge, Wayne County is the only local government having jurisdiction over any part of the land on which the facility and its appurtenances are to be located.

In accordance with § 143-215.108(f) of the North Carolina General Statutes, we hereby request that you issue a determination as to whether your municipality has in effect a zoning or subdivision ordinance that is applicable to the proposed facility. Additionally, please issue a determination as to whether the proposed use would be consistent with applicable zoning or subdivision ordinances. For your convenience, I have included a form with which you may remit your determination and a copy of the draft air permit application. As a means of demonstrating proof of transmittal, please sign, title, stamp, and date the enclosed form and mail to the facility mailing address, my address, listed on the form, and the checked air quality office at your earliest convenience.

Thank you for your prompt attention to this matter. If you have any questions regarding this request, please contact me at 919-546-5797

Sincerely,

In Juda

Erin E. Wallace Duke Energy Environmental Services

Attachments: Zoning Consistency Determination Form Draft Air Permit Application

Zoning Consistency Determination

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Facility Name	Duke Energy Progress, LLC – HF Lee Steam Electric Plant			
Facility Street Address	1199 Black Jack Church Road			
Facility City	Goldsboro			
Description of Process	Generation of electricity for sale			
SIC/NAICS Code	4911			
Facility Contact	Erin Wallace			
Phone Number	919-546-5797			
Mailing Address	410 S. Wilmington Street			
Mailing City, State Zip	Raleigh, NC 27601			
Based on the information given above:				
✓ I have received a copy of the air permit application (draft or final) AND				
 There are no applicable zonin The proposed operation IS co The proposed operation IS No (please include a copy of t The determination is pending Other: 	ng ordinances for this facility at this time nsistent with applicable zoning ordinances OT consistent with applicable zoning ordinances he rules in the package sent to the air quality office) further information and can not be made at this time			
Agency	WAYNE COUNTY PLANNING			
Name of Designated Official	CHIP CRUMPLER			
Title of Designated Official	PLANNING DIRECTOR			
Signature	Ch X			
Date	10/30/2017			
Please forward to the facility mailing address listed above and the air quality office at the appropriate address as checked on the back of this form.				

Courtesy of the Small Business Environmental Assistance Program sb.ncdenr.gov 877-623-6748

All PSD and Title V Applications

Attn: William Willets, PE
 DAQ – Permitting Section
 1641 Mail Service Center
 Raleigh, NC 27699-1641

Local Programs

- Attn: David Brigman
 Western NC Regional Air Quality Agency
 49 Mount Carmel Road
 Asheville, NC 28806
 (828) 250-6777
- Attn: Leslie Rhodes
 Mecklenburg County Air Quality
 700 N. Tryon Street, Suite 205
 Charlotte, NC 28202-2236
 (704) 336-5430

Division of Air Quality Regional Offices

- Attn: Paul Muller
 Asheville Regional Office
 2090 U.S. Highway 70
 Swannanoa, NC 28778
 (828) 296-4500
- Attn: Steven Vozzo
 Fayetteville Regional Office
 225 Green Street, Suite 714
 Fayetteville, NC 28301
 (910) 433-3300
- Attn: Ron Slack
 Mooresville Regional Office
 610 East Center Avenue, Suite 301
 Mooresville, NC 28115
 (704) 663-1699
- Attn: Patrick Butler, PE Raleigh Regional Office 1628 Mail Service Center Raleigh, NC 27699-1628 (919) 791-4200

 Attn: William Minor Barnette
 Forsyth County Office of Environmental Assistance and Protection
 201 N. Chestnut Street
 Winston-Salem, NC 27101-4120
 (336) 703-2440

- Attn: Robert Fisher
 Washington Regional Office
 943 Washington Square Mall
 Washington, NC 27889
 (252) 946-6481
- Attn: Brad Newland
 Wilmington Regional Office
 127 Cardinal Drive Extension
 Wilmington, NC 28405
 (910) 796-7215
- Attn: Lisa Edwards, PE
 Winston-Salem Regional Office
 450 West Hanes Mill Road, Suite 300
 Winston-Salem, NC 27105
 (336) 776-9800